Supplementary Figures



Supplementary Figure 1: SEM image of a spherically shaped closed cell encapsulated by CMG flakes. CMG segregates to the oil/water interface during emulsification, stabilizing spherically shaped emulsion oil droplets that after freeze drying will lead to cell covered by CMG flakes in the CMG-CNs.



Supplementary Figure 2: Contact angle of water on GO films without (a) and with the addition of PVA (b). PVA molecules adsorbed on GO flakes reduce the contact angle of water by 15 ° indicating a change of wettability for GO.



Supplementary Figure 3: Processing and structural characterization of GO- and rGO-CNs as a function of additives. a. Maximum amount of oil emulsified in the GO-sus in order to get GO-em; b. mass loss and shrinkage of GO-CNs upon thermal annealing at 1000 °C in Ar/H₂ atmosphere; c. Density and d. Average cell size (d_{50}) of the resulted GO and rGO-CNs. The organic additives (PVA: sucrose in 1:1 wt%) are added to the GO-sus with 0.65wt% GO.



Supplementary Figure 4: Effect of organic additives sucrose and PVA on the CMG-CN cell wall topography. GO-CNs produced from suspensions containing 0.65 wt% GO and 1.2 wt% organics, with different proportions of PVA:sucrose: 3:1 (a), 1:1 (b) and 1:3 (c) or with 5 wt% organics (sucrose) (d). Scale bar for all figures in **a**.



Supplementary Figure 5: Mass loss during reduction at 1000 °C in Ar/H_2 atmosphere versus proportion of GO in the GO-CNs. GO content with regards to total amount of solids, i.e. GO and organic additives. The linear fit indicates that 0.91% of the binder is eliminated during the thermal treatment.



Supplementary Figure 6: Proportion of mass loss during thermal treatment at different temperatures for CMG-CNs produced with 0.3 and 1.2 wt% binders.



Supplementary Figure 7: Differential pore volume distribution on rGO-CNs obtained by Barret-Joyner-Halenda (BJH) method applied to desorption isotherms. a. Additive-free rGO-CNs. The peak at 4 nm results from nitrogen cavitation during the desorption; b. rGO-CNs produced with 1.2 wt% additives.



Supplementary Figure 8: Maximum stress at 50% compression at cycle one and five

(when there is recoverable deformation) for rGO-CNs and Nickel microlattice²⁶ as a function of material's density. rGO-CNs of different densities produced with 0 to 5 wt% additives and thermal annealed at 300 and 1000 $^{\circ}$ C.



recoverable deformation. a. History of maximum stress, work done by compression, energy loss coefficient and compressive modulus E for ten compression cycles at 50% strain. b-c. SEM images of recovered cellular network after it underwent ten compressive cycles. A microstructural overview showing the recovered cells and intact struts (indicated with the arrow) efficiently supporting the adjacent cells is shown in b. In c. rupture paths within the cell walls can be identified (arrows). They tend to be oriented towards the roughness (wrinkles) present on the cell wall. rGO-CN produced with 1.2 wt% additives and thermal annealed at 300 °C.



Supplementary Figure 10: Multicycle compression stress-strain curves of rGO-CN presenting recoverable deformation of 99 and 97 % after the first and tenth compression cycles. Loading-unloading curves of cycles 1, 2, 5 and 10 for an rGO-CN with 4.3 mg cm⁻³. rGO-CN produced by the addition of 1.2 wt% additives in the GO-sus and annealed at 950 °C.