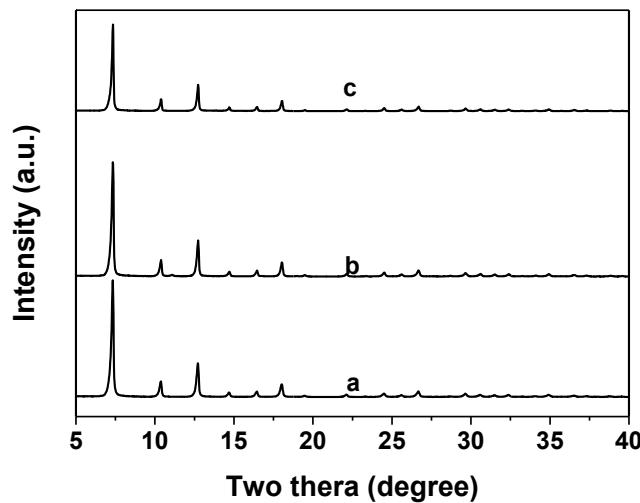
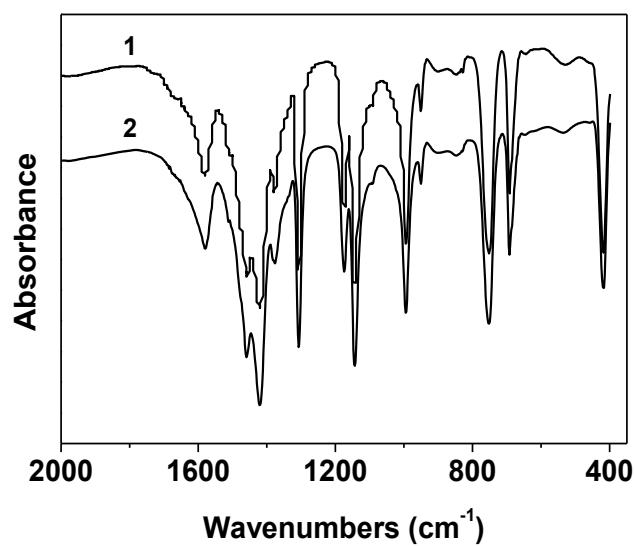


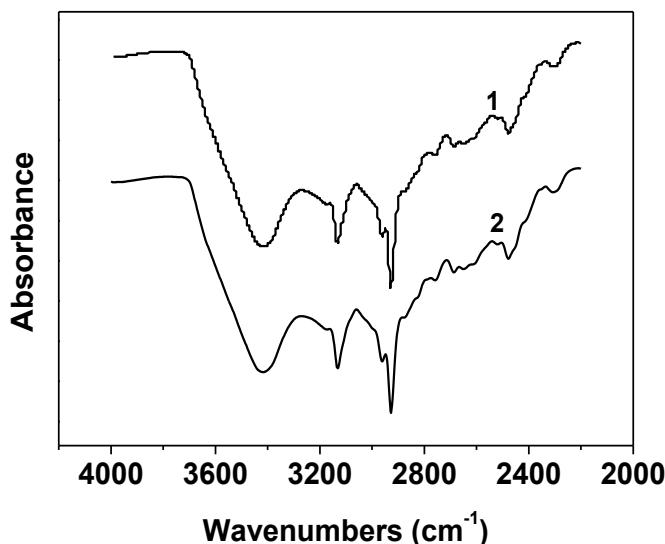
**Supplementary Figure 1. Scanning electron microscopy (SEM) images**  
 Comparison of the SEM images of solid zeolitic imidazolate framework-8 (ZIF-8) between (a) fresh, recovered from ZIF-8/glycol slurry after being used for (b) one, (c) two, and (d) three times in separating CO<sub>2</sub>/N<sub>2</sub> gas mixture ( $\chi_1=0.2231$ ) at 293.15 K, (e) recovered from ZIF-8/glycol-mIm slurry that has been used for 33 cycles of sorption/desorption at 303.15 K within 25 days. The morphology of recovered ZIF-8 is as the same as that of fresh sample.



**Supplementary Figure 2. Powder X-ray diffraction (PXRD) data** Comparison of the experimental XRD patterns of solid ZIF-8 between (a) fresh ZIF-8, (b) recovered from ZIF-8/glycol slurry after being used for separating CO<sub>2</sub>/N<sub>2</sub> gas mixture ( $z_1=0.2231$ ), and (c) recovered from ZIF-8/glycol-mIm that has been used for 33 cycles of sorption/desorption at 303.15 K within 25 days. Y-axis of the graph shows the relative intensity. The comparison shows that the framework structure of recovered ZIF-8 is as the same as that of fresh sample.

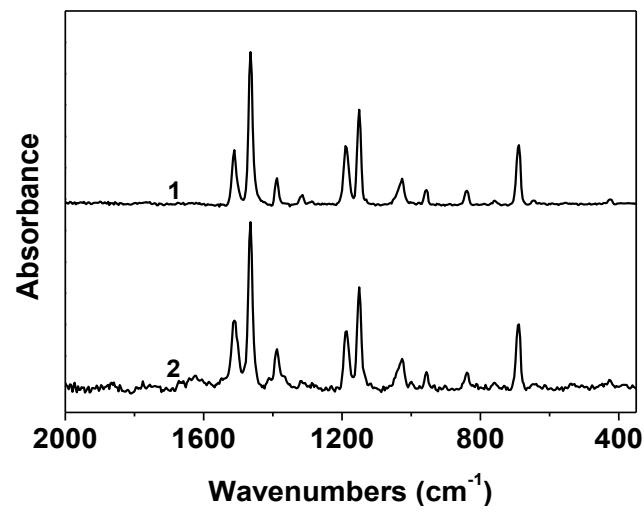


IR wavenumbers from 400 to 2000  $\text{cm}^{-1}$

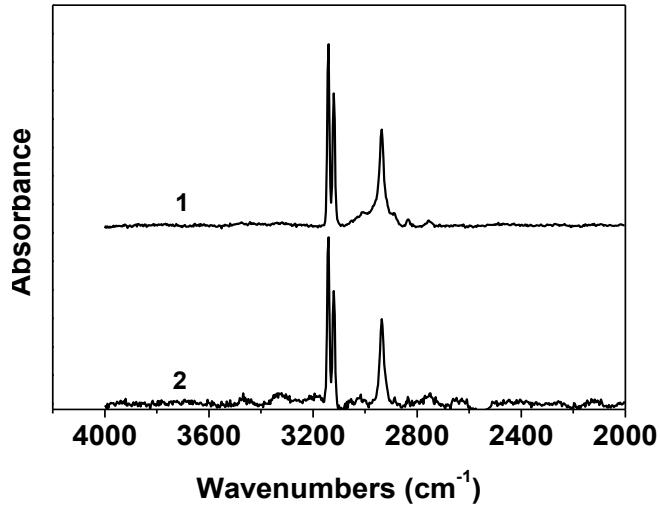


IR wavenumbers from 2000 to 4000  $\text{cm}^{-1}$

**Supplementary Figure 3. Fourier transform Infrared (FT-IR) measurements**  
 Comparison of the FT-IR spectra of solid ZIF-8 between (1) fresh and (2) recovered from ZIF-8/glycol slurry after being used for separating  $\text{CO}_2/\text{N}_2$  gas mixture ( $z_1=0.2231$ ) at 293.15 K. The result shows that the framework structure of recovered ZIF-8 is as the same as that of fresh sample.



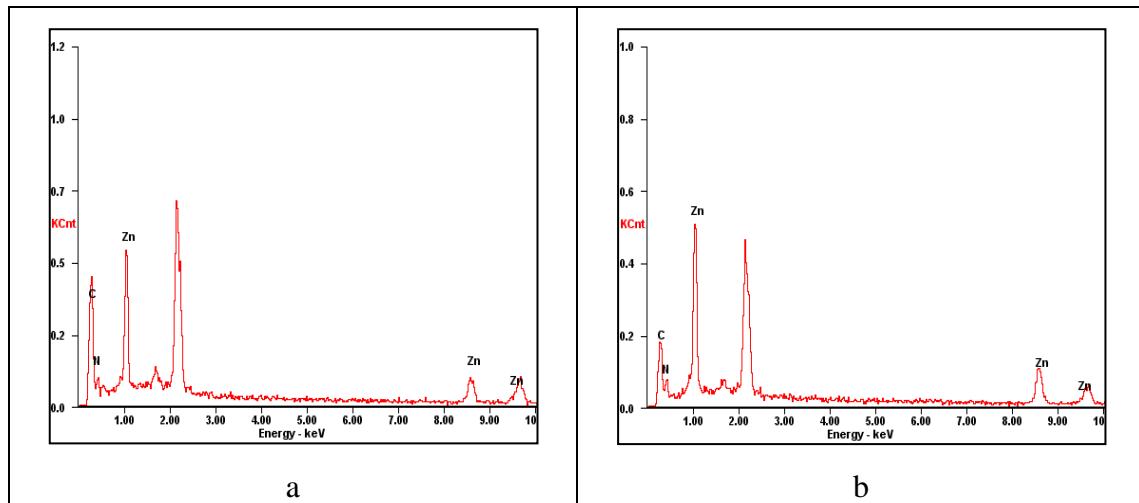
Raman wavenumbers from 400 to 2000  $\text{cm}^{-1}$



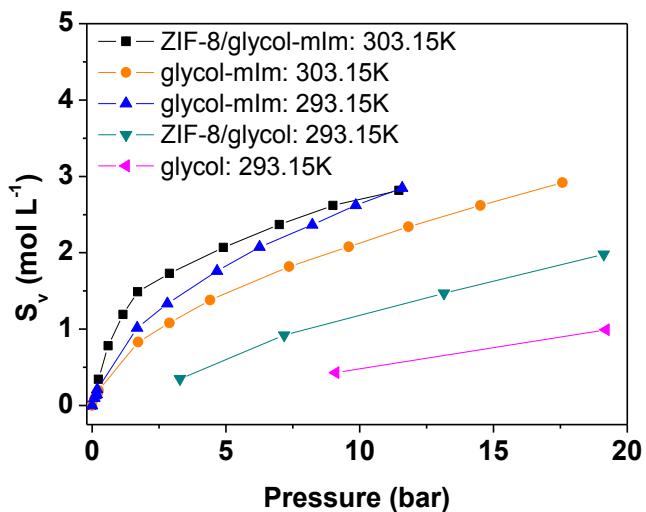
Raman wavenumbers from 2000 to 4000  $\text{cm}^{-1}$

#### **Supplementary Figure 4. Fourier transform Raman (FT-Raman) measurements**

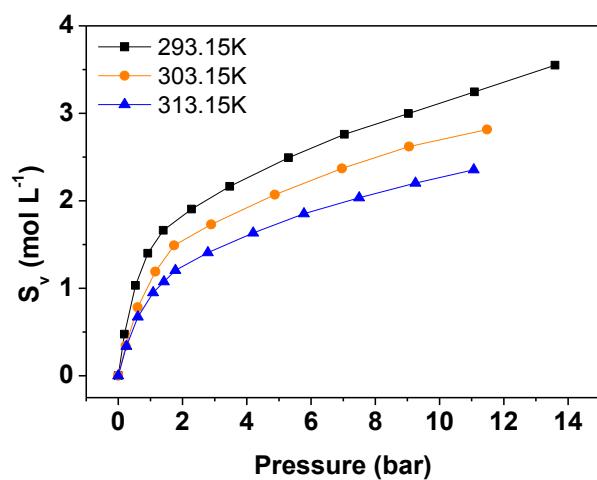
Comparison of the FT-Raman spectra of solid ZIF-8 between (1) fresh and (2) recovered from ZIF-8/glycol slurry after being used for separating  $\text{CO}_2/\text{N}_2$  gas mixture ( $z_1=0.2231$ ). The result shows that the framework structure of recovered ZIF-8 is as the same as that of fresh sample.



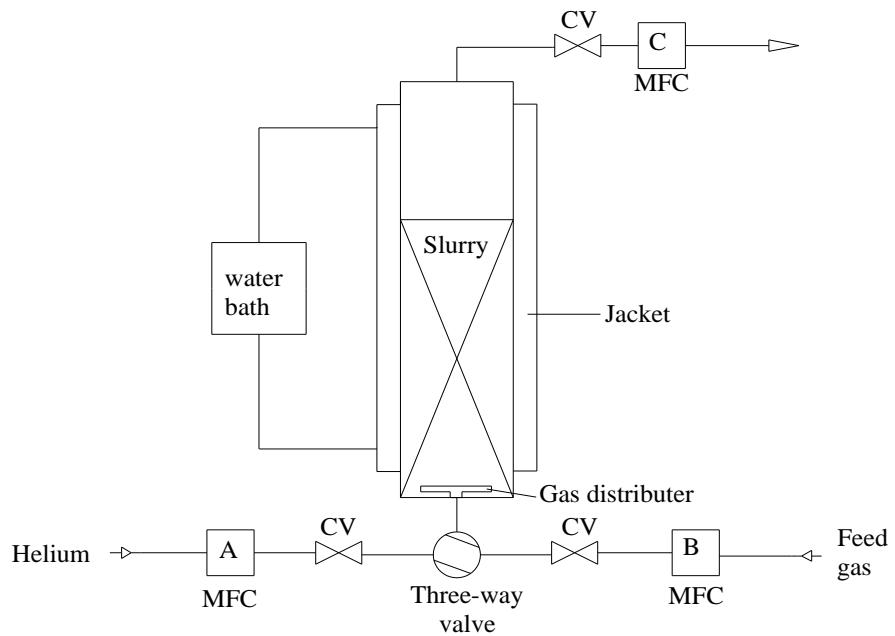
**Supplementary Figure 5. Energy dispersive X-ray (EDX) measurements** EDX spectra of solid ZIF-8 between (a) fresh and (b) recovered from ZIF-8/glycol slurry after being used for one time. The elementary composition of recovered ZIF-8 from ZIF-8/glycol slurry is as the same as that of fresh sample.



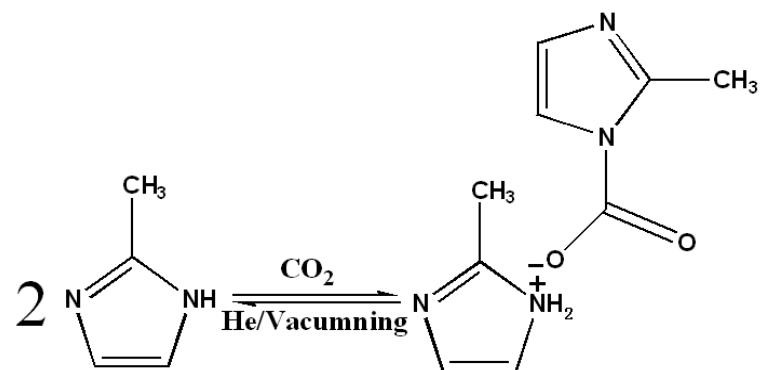
**Supplementary Figure 6.  $\text{CO}_2$  absorption isotherms** The apparent volumetric solubility ( $S_v$ ) of  $\text{CO}_2$  in pure glycol, glycol-mIm (3:2) mixture, ZIF-8 (15.2 wt%)/glycol slurry, and ZIF-8 (15 wt%)/glycol-mIm (3:2) slurry at different temperatures. As can be seen, the order of  $S_v$  is ZIF-8/glycol-mIm > glycol-mIm > ZIF-8/glycol > glycol, demonstrating the superiority of absorption-adsorption hybrid method for  $\text{CO}_2$  capture.



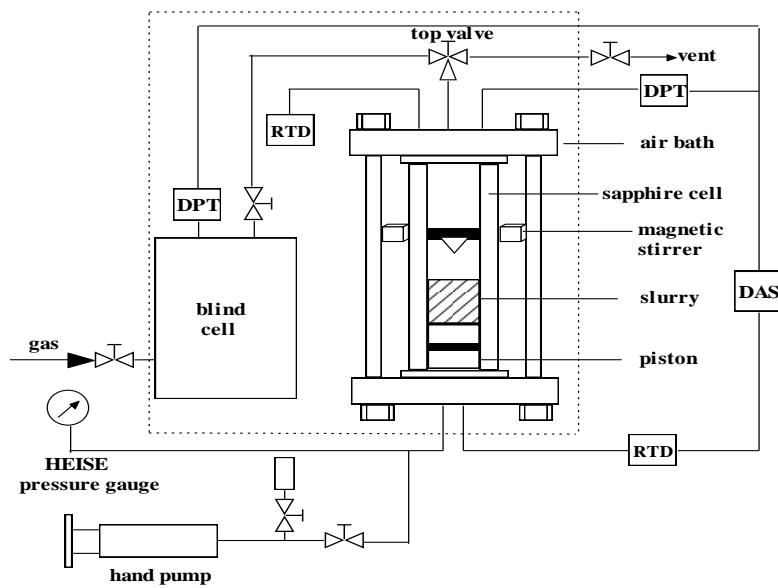
**Supplementary Figure 7. Variable temperature isotherms** The apparent volumetric solubility of CO<sub>2</sub> ( $S_v$ ) in ZIF-8/glycol-mIm slurry at three different temperatures.



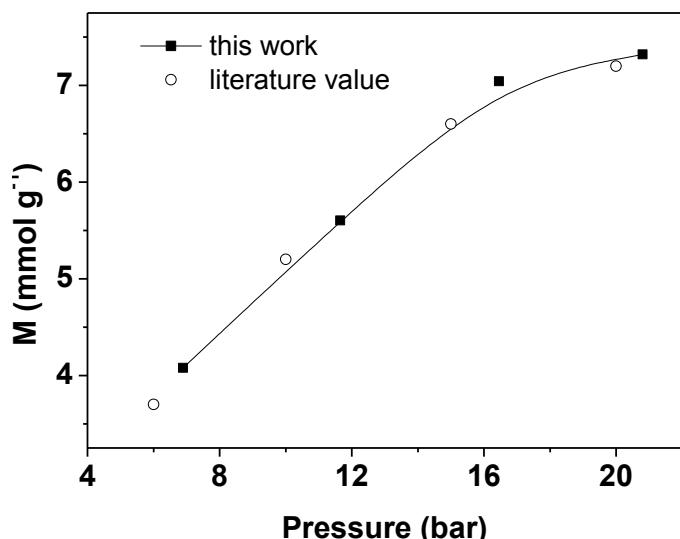
**Supplementary Figure 8. Column breakthrough experiment.** MFC stands for the mass flow controller.



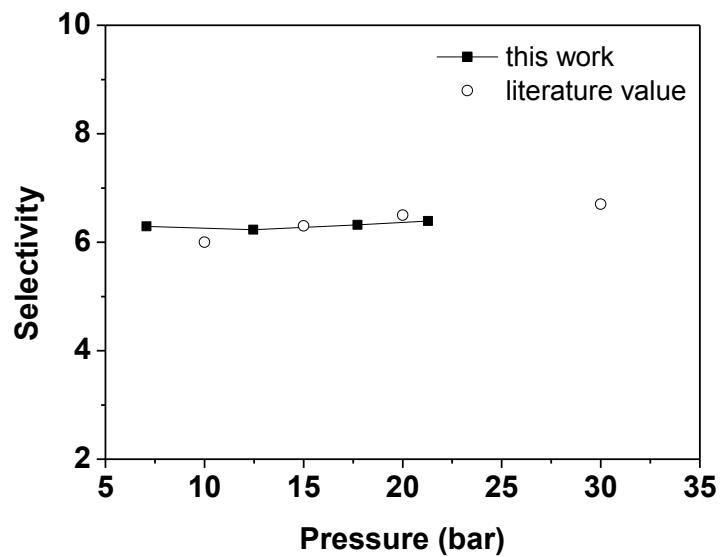
**Supplementary Figure 9.** Schematic for the absorption mechanism of  $\text{CO}_2$  in glycol-mIm solution.



**Supplementary Figure 10. Schematic diagram of the experimental apparatus.**  
 RTD, resistance thermocouple detector; DPT, differential pressure transducer; and  
 DAS, data acquisition system.



**Supplementary Figure 11.  $\text{CO}_2$  adsorption isotherms** Comparison of the pure  $\text{CO}_2$  adsorption isotherm in solid ZIF-8 at 303.15 K measured in this work and the one reported in literature<sup>1</sup>.



**Supplementary Figure 12.  $\text{CO}_2/\text{N}_2$  mixture on ZIF-8** Comparison of gas selectivities obtained for  $\text{CO}_2/\text{N}_2$  ( $z_1=0.2286$ ) mixture in solid ZIF-8 at 303.15 K measured in this work and the ones reported in literature<sup>2</sup>.

**Supplementary Table 1:** CO<sub>2</sub>/N<sub>2</sub> gas mixture ( $z_1=0.2231$ ) separation results by using ZIF-8/glycol slurry with a ZIF-8 mass fraction of 0.152 at 293.15 K and different initial gas-slurry volume ratios  $\Phi$  and initial pressures  $P_0$ .

$P_0$ (bar)	$P_E$ (bar)	$\Phi$	$P_{E-CO_2}$ (bar)	$y_1$ (%)	$x_1$ (%)	$\beta$	$S_c$ (mol L <sup>-1</sup> bar <sup>-1</sup> )
7.14	6.25	18	0.58	9.22	96.68	286	0.21
12.41	10.56	31	1.05	9.89	93.69	135	0.18
17.58	15.00	45	1.52	10.10	89.54	76	0.18
23.25	20.17	59	2.34	11.58	86.81	50	0.14
28.71	25.79	75	3.06	11.85	86.87	49	0.13

**Supplementary Table 2:** CO<sub>2</sub>/N<sub>2</sub> gas mixture ( $z_1=0.2231$ ) separation results by using recycled ZIF-8/glycol slurries with a ZIF-8 mass fraction of 0.152 and nearly the same initial pressure of around 17.58 bar.

Reused times	$P_0$ (bar)	$P_E$ (bar)	$P_{E-CO_2}$ (bar)	$y_1$ (%)	$x_1$ (%)	$\beta$	$S_c$ (mol L <sup>-1</sup> bar <sup>-1</sup> )
0 <sup>a</sup>	17.58	15.00	1.52	10.10	89.54	76	0.18
1	17.82	15.33	1.79	11.67	91.16	78	0.14
2	17.75	14.96	1.37	9.18	89.84	88	0.21
3	18.00	15.16	1.43	9.41	88.99	78	0.21
4	17.64	15.14	1.64	10.86	90.13	75	0.16

<sup>a</sup>0 represents using fresh slurry.

**Supplementary Table 3:** CO<sub>2</sub>/N<sub>2</sub> gas mixture ( $z_1=0.2231$ ) separation results by using ZIF-8/glycol slurry with a ZIF-8 mass fraction of 0.152 at nearly the same initial pressure of around 17.58 bar and different experimental temperatures.

$T$ (K)	$P_E$ (bar)	$\Phi$	$P_{E-CO_2}$ (bar)	$y_1$ (%)	$x_1$ (%)	$\beta$	$S_c$ (mol L <sup>-1</sup> bar <sup>-1</sup> )
274.15	15.10	50	1.24	8.20	92.92	147	0.27
283.15	14.98	46	1.33	8.89	95.38	212	0.22
293.15	15.00	45	1.52	10.10	89.54	76	0.18
303.15	15.65	44	1.98	12.67	81.06	29	0.12

**Supplementary Table 4:** CO<sub>2</sub>/H<sub>2</sub> gas mixture ( $z_1=0.2386$ ) separation results by using ZIF-8/glycol slurry with a ZIF-8 mass fraction of 0.152 at 293.15 K and different pressures.

$P_0$ (bar)	$P_E$ (bar)	$\Phi$	$P_{E-CO_2}$ (bar)	$y_1$ (%)	$x_1$ (%)	$\beta$	$S_c$ (mol L <sup>-1</sup> bar <sup>-1</sup> )
7.33	6.18	18	0.72	11.62	98.99	745	0.15
9.28	8.12	23	1.03	12.71	98.14	362	0.16
12.43	10.52	31	1.02	9.68	95.47	197	0.22
17.25	14.36	43	1.24	8.66	95.46	133	0.26
27.62	23.82	70	2.59	10.87	92.34	99	0.18
36.85	32.38	94	3.94	12.17	88.54	56	0.14

**Supplementary Table 5:** CO<sub>2</sub>/CH<sub>4</sub> gas mixture ( $z_1=0.2268$ ) separation results by using ZIF-8/glycol slurry; ZIF-8 mass fraction in slurry and experimental temperature are respectively specified to 0.152 and 293.15 K except for the two labeled experimental runs.

$P_0$ (bar)	$P_E$ (bar)	$\Phi$	$P_{E-CO_2}$ (bar)	$y_1$ (%)	$x_1$ (%)	$\beta$	$S_c$ (mol L <sup>-1</sup> bar <sup>-1</sup> )
7.32	6.19	18	0.79	12.83	82.14	31	0.13
7.89	6.48	20	0.71	11.01	79.83	32	0.17
10.22	8.57	26	1.01	11.82	83.19	37	0.14
13.66	11.06	34	1.21	10.96	74.19	23	0.17
18.33	15.30	48	1.95	12.74	70.51	17	0.13
25.26	21.28	67	2.84	13.35	69.94	15	0.12
27.52	23.29	73	3.17	13.60	70.90	15	0.11
10.19 <sup>a</sup>	8.68	24	1.14	13.08	82.45	31	0.11
10.38 <sup>b</sup>	8.76	24	1.00	11.43	82.56	37	0.14

<sup>a</sup> The experimental temperature and ZIF-8 mass fraction in the slurry were specified to 303.15 K and 0.152, respectively.

<sup>b</sup> The experimental temperature and ZIF-8 mass fraction in the slurry were specified to 303.15 K and 0.173, respectively.

**Supplementary Table 6:** CO<sub>2</sub>/N<sub>2</sub> gas mixture ( $z_1=0.2231$ ) separation results by using slurries formed by ZIF-8 with different liquids at 293.15 K.

Slurry	$m_F$	$P_0$ (bar)	$P_E$ (bar)	$\Phi$	$P_{E-CO_2}$ (bar)	$y_1$ (%)	$x_1$ (%)	$\beta$ (mol L <sup>-1</sup> bar <sup>-1</sup> )	$S_c$
ZIF-8 + ethanol	0.275	18.01	15.57	66	2.24	14.41	64.62	11	0.14
ZIF-8 + cyclohexane	0.278	17.92	14.24	53	1.78	12.50	60.53	11	0.22
ZIF-8 + n-hexane	0.302	19.13	16.02	53	2.30	14.37	63.86	11	0.10
ZIF-8 + methylbenzene	0.257	22.88	20.64	89	3.46	16.76	75.98	16	0.08
ZIF-8 + tetrachloromethane	0.111	17.61	13.21	44	1.29	9.77	58.94	13	0.23
ZIF-8 + triethylene glycol	0.151	17.79	15.65	45	1.98	12.65	88.89	55	0.12

**Supplementary Table 7:** Experimental results in absorption separation of CO<sub>2</sub> containing gas mixtures using glycol or water at 293.15 K.

$P_0$ (bar)	$P_E$ (bar)	$\Phi$	$P_{E-CO_2}$ (bar)	$y_1$ (%)	$x_1$ (%)	$\beta$	$S_c$ (mol L <sup>-1</sup> bar <sup>-1</sup> )
Feed gas: 22.3% CO <sub>2</sub> + 77.7% N <sub>2</sub> ;						Solvent: glycol	
18.00	16.39	54	2.79	17.03	72.12	13	0.057
Feed gas: 22.7% CO <sub>2</sub> + 77.3% CH <sub>4</sub> ;						Solvent: water	
12.59	11.85	39	2.32	19.61	50.05	4.1	0.037

**Supplementary Table 8:** CO<sub>2</sub>/N<sub>2</sub> gas mixture ( $z_1=0.2286$ ) separation results in solid ZIF-8 at 293.15 K with different initial gas-solid volume ratio ( $\Phi'$ ) and initial pressure ( $P_0$ ).

$\Phi'$	$P_0$ (bar)	$P_E$ (bar)	$P_{E-CO_2}$ (bar)	$y_1$ (%)	$x_1$ (%)	$\beta'$
137	8.03	6.81	1.03	15.18	66.21	11
206	12.02	9.78	1.43	14.67	58.52	8.2
272	15.41	12.49	1.90	15.22	58.52	7.9
361	20.87	17.11	2.61	15.27	56.63	7.2
423	24.48	20.13	3.10	15.40	57.18	7.3
542	31.09	25.87	4.04	15.60	58.06	7.5

**Supplementary Table 9:** CO<sub>2</sub>/H<sub>2</sub> gas mixture ( $z_1=0.2386$ ) separation results in solid ZIF-8 at 293.15 K with different initial gas-solid volume ratio ( $\Phi'$ ) and initial pressure ( $P_0$ ).

$\Phi'$	$P_0$ (bar)	$P_E$ (bar)	$P_{E-CO_2}$ (bar)	$y_1$ (%)	$x_1$ (%)	$\beta'$
123	7.28	6.28	0.90	14.39	86.43	37
190	11.24	9.62	1.38	14.36	81.55	26
297	18.09	14.81	2.15	14.50	75.08	18
352	21.24	17.64	2.55	14.45	76.77	19
435	26.01	21.97	3.21	14.60	77.81	20
525	31.72	26.53	3.91	14.72	76.64	19

**Supplementary Table 10:** CO<sub>2</sub>/CH<sub>4</sub> gas mixture ( $z_1=0.2342$ ) separation results in solid ZIF-8 at 293.15 K with different initial gas-solid volume ratio ( $\Phi'$ ) and initial pressure ( $P_0$ ).

$\Phi'$	$P_0$ (bar)	$P_E$ (bar)	$P_{E-CO_2}$ (bar)	$y_1$ (%)	$x_1$ (%)	$\beta'$
157	9.16	6.23	1.09	17.42	36.58	2.7
230	13.44	9.48	1.64	17.29	38.80	3.0
323	18.41	13.52	2.38	17.60	39.49	3.0
419	23.48	17.77	3.13	17.62	40.98	3.2
520	28.72	22.20	4.00	18.02	41.11	3.2
588	32.08	25.40	4.60	18.12	42.33	3.3

**Supplementary Table 11:** CO<sub>2</sub>/N<sub>2</sub> gas mixture ( $z_1=0.2065$ ) separation results by using glycol-mIm liquid mixture where mass ratio between glycol and mIm in liquid and experimental temperature are specified to 3:2 and 303.15 K, respectively.

$\Phi$	$P_0$ (bar)	$P_E$ (bar)	$P_{E-CO_2}$ (bar)	$y_1$ (mol%)	$x_1$ (mol%)	$\beta$	$S_c$ (mol L <sup>-1</sup> bar <sup>-1</sup> )
11	5.65	4.55	0.10	2.26	82.65	206	0.94
15	7.68	6.20	0.15	2.40	86.90	270	0.86
20	9.82	8.00	0.22	2.70	87.70	257	0.75
24	11.63	9.45	0.24	2.53	83.81	199	0.82

**Supplementary Table 12:** CO<sub>2</sub>/N<sub>2</sub> gas mixture ( $z_1=0.2065$ ) separation results by using ZIF-8/glycol-mIm slurry; ZIF-8 mass fraction in slurry, mass ratio between glycol and mIm, and experimental temperature are respectively specified to 0.15, 3:2 and 303.15 K expect for the labeled experimental run.

$\Phi$	$P_0$ (bar)	$P_E$ (bar)	$P_{E-CO_2}$ (bar)	$y_1$ (mol%)	$x_1$ (mol%)	$\beta$	$S_c$ (mol L <sup>-1</sup> bar <sup>-1</sup> )
9	4.43	3.51	0.08	2.40	74.41	118	0.92
14	6.60	5.22	0.07	1.38	83.74	367	1.63
17	8.28	6.62	0.10	1.59	84.77	345	1.43
24	11.35	9.17	0.15	1.62	85.45	357	1.40
35	16.51	1.33	0.23	1.73	87.43	394	1.29
14 <sup>a</sup>	6.70	5.40	0.12	2.25	81.23	188	0.92

<sup>a</sup> The temperature of this experimental run was specified to 313.15 K.

**Supplementary Table 13:** CO<sub>2</sub>/N<sub>2</sub> gas mixture ( $z_1=0.2065$ ) separation results by using ZIF-8/glycol-mIm slurry with three different ZIF-8 mass fractions ( $m_F$ ) in slurry where mass ratio between glycol and mIm and experimental temperature are specified to 3:2 and 303.15 K, respectively.

$m_F$ (%)	$P_0$ (bar)	$P_E$ (bar)	$P_{E-CO_2}$ (bar)	$y_1$ (mol%)	$x_1$ (mol%)	$\beta$	$S_c$ (mol L <sup>-1</sup> bar <sup>-1</sup> )
5	6.30	5.13	0.11	2.18	85.08	256	1.00
10	6.46	5.12	0.08	1.53	82.99	313	1.48
15	6.60	5.22	0.07	1.38	83.74	367	1.63

**Supplementary Table 14:** CO<sub>2</sub>/CH<sub>4</sub> gas mixture ( $z_1=0.2193$ ) separation results by using ZIF-8/glycol-mIm slurry where ZIF-8 mass fraction in slurry, temperature, mass ratio between glycol, and mIm are specified to 0.15, 3:2, and 303.15 K, respectively.

$\Phi$	$P_0$ (bar)	$P_E$ (bar)	$P_{E-CO_2}$ (bar)	$y_1$ (mol%)	$x_1$ (mol%)	$\beta$	$S_c$ (mol L <sup>-1</sup> bar <sup>-1</sup> )
11	5.39	4.03	0.10	2.76	69.81	81	0.89
14	6.48	4.91	0.12	2.05	74.24	138	1.21
16	7.56	5.78	0.14	2.21	73.86	125	1.12
20	9.29	7.18	0.18	2.18	75.86	141	1.13
32	14.66	11.48	0.28	2.13	76.89	144	1.14
96	41.38	32.79	0.87	2.65	78.45	134	1.00
161	66.41	53.46	1.32	3.13	73.90	87	0.76

**Supplementary Table 15:** CO<sub>2</sub>/H<sub>2</sub> gas mixture ( $z_1=0.2360$ ) separation results by using ZIF-8/glycol-mIm slurry where ZIF-8 mass fraction in slurry, mass ratio between glycol and mIm, and temperature are specified to 0.15, 3:2, and 303.15 K, respectively.

$\Phi$	$P_0$ (bar)	$P_E$ (bar)	$P_{E-CO_2}$ (bar)	$y_1$ (mol%)	$x_1$ (mol%)	$\beta$	$S_c$ (mol L <sup>-1</sup> bar <sup>-1</sup> )
13	6.40	4.95	0.10	2.09	86.04	288	1.23
23	11.33	8.91	0.17	1.88	88.08	386	1.37
44	21.51	16.99	0.32	1.88	92.23	618	1.33
65	31.60	25.38	0.47	1.85	94.25	871	1.35
85	41.33	33.41	0.68	2.02	95.16	951	1.21

**Supplementary Table 16:** Results of the breakthrough experiment for CO<sub>2</sub>/N<sub>2</sub> mixture ( $z_1=0.2065$ ) with inlet gas flow rate,  $V_{in}$ , of 23 (mL min<sup>-1</sup>) in ZIF-8/glycol-mIm slurry.

Time (h)	N <sub>2</sub> in outlet gas (mol%)	outlet gas flow $V_{out}$ (mL min <sup>-1</sup> )	<sup>a</sup> $R_{N2}$ (%)	<sup>b</sup> $R_{CO2}$ (%)
0	0	0.0	-	
0.008	100	6.0	32.88	100
0.10	100	10.0	54.79	100
0.28	99.56	14.0	76.37	98.70
1.38	98.24	16.0	86.13	94.07
1.90	97.68	16.5	88.31	91.94
2.11	97.36	17.0	90.69	90.55
2.26	97.07	18.0	95.74	88.90
2.48	96.73	18.2	96.46	87.47
2.74	96.38	18.5	97.70	85.90
2.92	95.89	19.0	99.83	83.56
3.14	95.65	19.5	102.20	82.14
3.31	95.28	19.7	102.85	80.42
3.55	94.94	20.0	104.04	78.69
3.80	94.66	20.2	104.77	77.29
4.06	94.13	20.5	105.73	74.66
4.33	93.86	20.7	106.46	73.24
4.60	93.19	20.9	106.72	70.03
4.86	92.79	21.0	106.77	68.12
5.15	92.32	21.1	106.73	65.88
5.41	92.00	21.3	107.37	64.12
6.06	91.63	21.4	107.44	62.29
6.70	90.65	21.7	107.78	57.28

$$^a R_{N2} = \frac{V_{in} \times y_{in-N2}}{V_{out} \times y_{out-N2}} \times 100, R_{N2} \text{ is the transient recovery ratio of N}_2 \text{ in the outlet gas}$$

phase, where  $y_{in-N2}$  and  $y_{out-N2}$  are the mole fraction of N<sub>2</sub> in the feed gas and outlet gas, respectively;  $R_{N2}$  with a value higher than 100% indicates that N<sub>2</sub> is desorbed from the system.

$$^b R_{CO2} = 1 - \frac{V_{in} \times y_{in-CO2}}{V_{out} \times y_{out-CO2}} \times 100, R_{CO2} \text{ is the transient recovery ratio of CO}_2 \text{ in the slurry},$$

where  $y_{in-CO2}$  and  $y_{out-CO2}$  are the mole fraction of CO<sub>2</sub> in the feed gas and outlet gas, respectively.

**Supplementary Table 17:** Results of breakthrough experiment for CO<sub>2</sub>/CH<sub>4</sub> mixture ( $z_1=0.276$ ) with inlet gas flow rate,  $V_{\text{in}}$ , of 24 (mL min<sup>-1</sup>) in ZIF-8/glycol-mIm slurry.

Time (h)	CH <sub>4</sub> in outlet gas (mol%)	outlet gas flow $V_{\text{out}}$ (mL min <sup>-1</sup> )	$R_{\text{CH}4}$ (%)	$R_{\text{CO}2}$ (%)
0.00	0.00	0.0	-	-
0.01	100.00	6.0	35.51	100
0.10	100.00	9.0	53.27	100
0.17	99.79	10.0	59.06	99.70
0.50	98.48	11.0	64.11	97.65
0.88	97.48	12.0	69.23	95.74
1.37	96.96	12.5	71.73	94.65
1.75	96.10	13.0	73.94	92.86
2.70	95.49	13.5	76.30	91.43
3.38	94.44	14.0	78.25	89.04
4.23	93.44	14.5	80.19	86.61
4.87	92.41	15.5	84.77	83.44
6.03	90.92	17.0	91.48	78.27
6.95	89.86	18.5	98.39	73.59
7.70	88.98	19.0	100.06	70.53
9.07	87.84	20.0	103.98	65.77
9.38	87.27	20.5	105.89	63.27

**Supplementary Table 18:** Results of the breakthrough experiment for CO<sub>2</sub>/CH<sub>4</sub> mixture ( $z_1=0.276$ ) with inlet gas flow rate,  $V_{\text{in}}$ , of 24 (mL min<sup>-1</sup>) in pure water.

Time (h)	CH <sub>4</sub> in outlet gas (mol%)	outlet gas flow $V_{\text{out}}$ (mL min <sup>-1</sup> )	$R_{\text{CH}4}$ (%)	$R_{\text{CO}2}$ (%)
0.00	0.00	0.0	-	-
0.001	100	6.0	34.09	100
0.005	99.79	10.0	56.70	99.68
0.13	99.15	13.0	73.23	98.33
0.23	97.50	13.5	74.79	94.90
0.32	94.81	14.5	78.11	88.64
0.43	89.33	16.0	81.21	74.23
0.56	81.48	18.5	85.64	48.28
0.73	76.33	20.5	88.91	26.75
1.02	74.48	21.5	90.98	17.17
1.22	74.33	22.0	92.91	14.74
1.43	74.18	22.5	94.83	12.30

**Supplementary Table 19:** Henry constant ( $H$ ) of gas components in liquid glycol at 293.15 K.

Gas components	$H$ (MPa g mmol <sup>-1</sup> )
CO <sub>2</sub>	2.15
CH <sub>4</sub>	14.7
N <sub>2</sub>	48.2
H <sub>2</sub>	37.6

## **Supplementary references:**

1. Pérez-Pellitero, J. *et al.* Adsorption of CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub> on zeolitic imidazolate frameworks: experiments and simulations. *Chem. Eur. J.* **16**, 1560-1571 (2010).
2. Amrouche, H. *et al.* Experimental and computational study of functionality impact on sodalite-zeolitic imidazolate frameworks for CO<sub>2</sub> separation. *J. Phys. Chem. C* **115**, 16425-16432 (2011).