Supporting Information

Scheeler et al. 10.1073/pnas.1407232111

SI Text

Definition of the Center-Line Helicity

In defining the "center-line helicity," we are forced to adopt a convention for the implied contribution of the twist component of the total helicity. Physically, this corresponds to making a choice for how the vortex bundle should be wrapped around the center-line when twist cannot be directly resolved (Fig. S1). Our definition corresponds to the total helicity of a bundle with particularly simple internal structure, so that the total twist component is zero, $Tw_i = 0$, resulting in the following:

$$\mathcal{H}_{c} \equiv \mathcal{H}_{c, \text{ p.t.}} = \Gamma^{2} \left(\sum_{i \neq j} \mathcal{L}_{ij} + \sum_{i} W r_{i} \right).$$
 [S1]

Such a result can be obtained by constructing a bundle using the "parallel transport" framing, defined as one for which the twist rate of the normal vector, \hat{n} , is everywhere zero: $(\hat{n} \times \partial_s \hat{n}) \cdot d\ell = 0$.

To illustrate the consequences of our convention, consider a helix defined by the following:

$$x = a \cos kz$$
 [S2]

$$y = a \sin kz.$$
 [S3]

For a section spanning z = 0 to z = L, the number of helical turns is $N = \frac{kL}{2\pi}$ and the writhe is as follows:

$$Wr = N(1 - \cos\theta), \qquad [S4]$$

where the winding angle is $\theta = \tan^{-1}ka$. In the limit of small winding angle $(\theta \rightarrow 0)$, the resulting helicity is then given by the following:

$$\mathcal{H}_{c, p.t.} = \Gamma^2 Wr$$
 [S5]

$$\sim \Gamma^2 \, \frac{N\theta^2}{2}.$$
 [S6]

This has the important property that helicity goes smoothly to zero as the helix is flattened into a straight line. One apparent disadvantage of the parallel transport framing is that, in general, it does not close, meaning that an individual vortex filament does not reconnect with itself in a single trip around the bundle. We note, however, that this is expected for continuum fields; so long as a local twist rate can be defined, a noninteger total twist can be computed and corresponds to the mean linking of vortex filaments in the bundle (1).

One way to resolve the nonclosure of the bundle is to use a Frenet-Serret basis (in other words, \hat{n} is the Frenet-Serret normal vector). In this case, the twist and helicity are given by the following:

$$Tw_{\text{f.s.}} = \frac{1}{2\pi} \int ds \ \tau = N \cos \theta \qquad [S7]$$

$$\mathcal{H}_{c, f.s.} = \Gamma^2 \left(Wr + Tw_{f.s.} \right) = \Gamma^2 N.$$
[S8]

Note that this result always gives an integer $(n\Gamma^2)$ helicity, which is independent of the winding angle. Plotting the bundle resulting

from such a framing reveals the source of this extra helicity: the vortex filaments become significantly twisted as the winding angle is reduced (Fig. S1, left side). In fact, integer helicity always result for framings in which all filaments close with themselves, as they produce a uniform, integer filament linking. Furthermore, it follows that the helicity computed for such a bundle will change discontinuously under smooth deformations, as it is confined to integer values. This is especially problematic when computing the helicity for experimental data: even infinitesimal spirals will appear to have high helicity content, and so this convention produces wildly fluctuating center-line helicity. [In the context of the Frenet–Serret framing, this can also be viewed as due to the creation of inflection points, which cause the torsion to be undefined (2).]

In addition to its ease of computation, the center-line helicity for a parallel transport bundle has one other important property: it corresponds to the configuration that naturally results from viscous dissipation of the vortex core (as derived in the next section for a straight center-line). Moreover, our experimental results indicate that it is continuous through a vortex reconnection, suggesting it is the natural and relevant definition for helicity conservation.

Helicity Dissipation for a Twisted Core

Consider a straight center-line, uniformly twisted core vortex with profile:

$$\boldsymbol{\omega} = \Omega(r) \left(\hat{\boldsymbol{z}} + r\tau \hat{\boldsymbol{\phi}} \right), \qquad [S9]$$

where $\Omega(r)$ is the scalar core profile and τ is the twist rate. The helicity dissipation rate is given by the following (3):

$$\partial_t \mathcal{H} = -2\nu \int \boldsymbol{\omega} \cdot (\nabla \times \boldsymbol{\omega}) \, dV = -4\nu\tau \int \Omega^2(r) dA \, dz, \qquad [S10]$$

which can be rewritten as a relative decay rate:

$$\partial_t \mathcal{H} = -\mathcal{H} \frac{8\pi\nu}{A_{eff}},$$
 [S11]

where A_{eff} is an effective core area given by the following:

$$A_{eff} = \frac{\left(\int \Omega(r) dA\right)^2}{\int \Omega^2(r) dA}.$$
 [S12]

Equivalently, we note that this is equivalent to a dissipation of the total twist: $\partial_t Tw = -Tw\frac{8\pi\nu}{A_{eff}}$, where the total twist is given by $Tw = \int \tau ds$. For experimental vortices in a viscous fluid, the core size is expected to grow like $r \sim \sqrt{4\nu t}$, or ~2 mm for our experiments (for water, $\nu = 1.0 \text{ mm}^2 \cdot \text{s}^{-1}$ and the typical experimental timescale is $t \sim 1$ s, which is roughly the time at which the reconnection start). The resulting dissipation rate is as follows: $\partial_t Tw/Tw \sim 5 \text{ s}^{-1}$.

Experimental Vortex Generation

The experiments were carried out using the vortex generation and imaging techniques described in ref. 4. Vortices are generated using shaped hydrofoils generated by a 3D printer. These hydrofoils are attached to a frame, which is then rapidly accelerated using a short, open pneumatic cylinder driven by a quick-release valve, where typical accelerations are on the order of $a = 285 \text{ m/s}^2$, reaching speeds of $U \sim 2 \text{ m/s}$. The hydrofoils used for the data shown in the main text have a chord of Ch = 22.5 mm, a leading edge thickness of $t_1 = 3.75 \text{ mm}$, a trailing edge thickness of $t_2 = 0.225 \text{ mm}$, and a bend of $\theta = 15^\circ$. Images of the 3D models used to print each hydrofoil are reproduced in Fig. S2.

The trailing edge path (which is traced by the resulting vortices) had an r.m.s. radius of $\bar{r} = 69.3$ mm in the case of the trefoil knot and an r.m.s. radius of $\bar{r} = 75.5$ mm in the case of the linked rings. Hydrofoils (and vortices) have also been generated at smaller scales and are observed to have qualitatively similar dynamics. A volumetric image of the vortex core is obtained with a laser-scanning tomography apparatus (the obtained volumes have a size of 384^3 voxels with an adjustable resolution of 0.6 mm/voxel). The effects of perspective in the imaging apparatus are corrected for in the resulting data. The circulation of the vortices is estimated using the formula for the circulation around a thin flat plate in inviscid flow (5):

$$\Gamma = \pi \ U \ Ch \ \sin \alpha, \qquad [S13]$$

where $\alpha \approx \theta/2$ is the effective angle of attack. The speed of the hydrofoil is directly measured using an encoder attached to the hydrofoil acceleration frame. The circulation obtained from this estimate is consistent with the forward speed of simple vortex rings and the stretching rate observed for knotted vortices.

Experimental Vortex Shape Reconstruction

To reconstruct the shape of the vortices from experimental volumetric data, we have adapted methods from biomedical image analysis. Due to the nature of the raw data, some apparent gaps along the vortex path may arise from nonuniform bubble density. Previously, manual identification of vortices was used, along with automated line tracing (4). As an improvement, we have developed a two-step process for numerically identifying vortices before joining them together into a complete path.

Vortices appear as one-dimensional ridge lines in the 3D image: the locus of points for which image intensity is maximized relative to motion along the minor and medium eigenvectors of the image Hessian (6). For the detection and spatial localization of vortices, we adapt a method of particle-based ridge sampling (7). Image identification "particles" move within the image domain, subject to forces from other particles, while constrained to stay within ridge lines. These particles are subject to a synthetic radial potential function that monotonically decreases away from r = 0 but with a slight attractive potential well at tunable position, producing approximately equidistant spacing. The point locations are iteratively updated to minimize the total energy of the system. Points are periodically added to ensure complete coverage of detected ridge features and deleted where the feature fades to noise. For each energy-minimizing iteration, the points are constrained to ridges with Newton optimization using the gradient and Hessian of the continuous image, as reconstructed by convolution with the C^2 cubic B-spline.

Once particles have converged, the recovered vortex segments are joined via fast marching (8).

Calculation of Linking and Writhe

Linking and writhe are computed by projecting the 3D paths into a plane and counting signed crossings between line segments. To protect against numerical errors, which may be especially problematic with the noisy experimental data, three random orientations are checked for consistency, and more orientations are computed if the results do not agree. To compute the noninteger portion of the writhe, an additional term is added to account for the twist of the implied framing (9). A black-board framing (i.e., a framing chosen to always be exactly perpendicular to the projection direction) is used instead of the traditional Frenet–Serret framing; this was found to produce more accurate results in the presence of noise, as confirmed by comparing the results to the average summed crossing number over random projections.

Theory of Helicity Conservation Through a Reconnection

As described in the main text, the conservation of helicity in reconnecting vortices is due to the reconnection events happening across regions where the vortex path is antiparallel. Typically, linking is described in terms of planar knot diagrams; however, in this case, it does not produce an intuitive description of the observed mechanism. For example, vortex reconnections are conventionally depicted as taking place at crossings in a planar diagram (Fig. S3A), leading one to the incorrect conclusion that helicity must change by $|\Delta \mathcal{H}_c| = 1\Gamma^2$. (We note that, in all cases, the center-line helicity is given by the following: $\mathcal{H}_c/\Gamma^2 =$ $\sum \mathcal{L}_{ij} + \sum Wr_i = N_+ - N_-$, where N_{\pm} are the number of signed crossings, averaged over all projections. For nearly planar shapes, all projections have the same number of crossings.) We can modify our diagram to add two-antiparallel extensions and place the reconnection in this region; in this case, we conclude the helicity is conserved (Fig. S3B). Although this geometry seems unintuitive in a plane, it forms naturally for fully 3D paths. This is particularly true for reconnecting vortices driven by stretching, which are expected to adopt an antiparallel configuration to conserve energy (4). In the event that the reconnection is not perfectly antiparallel, as is apparently the case for small GPE vortices, this conservation may be imperfect.

Helistogram Analysis

Helistograms for a given curve are constructed by smoothing the original path with a Blackmann windowed sinc kernel of increasingly larger cutoff wavelengths incremented by a small $d\lambda$. By taking the difference between the helicity $\mathcal{H}(\lambda)$ calculated for a path smoothed by λ and the helicity $\mathcal{H}(\lambda + d\lambda)$ of the slightly more smoothed path, we can compute the helicity stored on the scale of λ . This progressive smoothing process can be seen in Movie S1, which shows the path corresponding to each cutoff wavelength.

For a helically wound ring, the locations of the peaks on a helistogram correspond to the helical wavelength L/n of the path, where L is the total length of the path and n is the winding number. A collection of helically wound rings with different values of L/n along with their corresponding helistograms are shown in Movie S2. Note that, as the helical wavelength of the structures increases, the helicity should decrease in magnitude and shift to larger length scales, both of which are captured by the shrinking and translation of the single peak in the helistogram. Helistograms can also be constructed for GPE data, as shown in Fig. S4; the results are qualitatively similar to experimental data for the same initial shape, although all three reconnections happen simultaneously.

Gross–Pitaevskii Equation

Simulations of the Gross–Pitaevskii equation (GPE) were carried out using the same parameters as in ref. 10, where the GPE is considered in a dedimensionalized form:

$$2i\partial_t \Psi + \nabla^2 \Psi - |\Psi|^2 \Psi = 0, \qquad [S14]$$

where the circulation in these units is $\Gamma = 2\pi$, the healing length is $\xi = 1$, and we set a far-field density of $\rho_{\infty} = |\Psi_{\infty}|^2 = 1$. The simulations used a grid size of $\Delta x = \xi/2$ and time step $\Delta t = 0.02$, using periodic boundary conditions. The initial phase field was constructed by brute-force integration of the velocity field generated by the vortices (obtained from the Biot–Savart law), making use of the following relation:

$$\phi_{x_1} - \phi_{x_0} = \int_{x_0}^{x_1} \mathbf{v} \cdot d\boldsymbol{\ell},$$
 [S15]

where the periodicity is ensured by calculating the flow field for periodically copied versions of the desired vortex. (In practice, we use a $5 \times 5 \times 5$ cube of vortex copies, where the flow field is calculated in the central volume; this number was chosen empirically to produce smooth boundaries that do not generate sound waves when the simulation begins.) A similar integration method has recently been used for GPE simulations in other contexts (11). To create a phase volume, an arbitrary phase is assigned to one corner, which is then extended to a plane on one edge of the volume. Integrating from this plane then produces a phase volume. To ensure that the phase matches across periodic boundaries, a constant gradient is added. (This is equivalent to removing the uniform background flow produced by a periodic collection of vortex loops.)

The initial density field was calculated using a Padé approximant (12):

$$\rho(r) = \frac{\frac{11}{32}r^2 + \frac{11}{384}r^4}{1 + \frac{1}{3}r^2 + \frac{11}{384}r^4},$$
[S16]

- 1. Arnold VI (1986) The asymptotic Hopf invariant and its applications. *Selecta Math Sov* 5(4):327–375.
- Moffatt H, Ricca R (1992) Helicity and the Calugareanu invariant. Proc R Soc Math Phys Eng Sci 439(1906):411–429.
- 3. Moffatt HK (1969) Degree of knottedness of tangled vortex lines. J Fluid Mech 35(Pt 1):117–129.
- Kleckner D, Irvine WTM (2013) Creation and dynamics of knotted vortices. Nat Phys 9(4):253–258.
- 5. Acheson DJ (1990) Elementary Fluid Dynamics (Clarendon, Oxford).
- Eberly D (1996) Ridges in Image and Data Analysis (Kluwer Academic, Dordrecht, The Netherlands).
- Kindlmann GL, San José Estépar R, Smith SM, Westin C-F (2009) Sampling and visualizing creases with scale-space particles. *IEEE Trans Vis Comput Graph* 15(6):1415–1424.

where *r* was taken to be the distance to the closest vortex line. The vortex knot with r.m.s. radius $\bar{r} = 24\xi$ was simulated in a periodic cube with edge $a = 128\xi$ (256 grid points), and the simulation volume was scaled in proportion to the knots for other sizes. Weak density waves are observed to radiate from the vortex at the beginning of the simulation (due to the fact that the vortex curvature relaxes the core profile to a slightly different form than that given by the Padé approximant), resulting in a small reduction of the vortex length and energy from the initial condition. Vortex paths were obtained by tracing the phase defects in the simulated wave function. Time steps when the vortices begin to overlap, defined as when the vortex separation is less than $r_{min} < 2\xi$, are omitted from Fig. 4.

Biot-Savart Evolution of Thin Core Vortices

The Biot–Savart velocity of the vortex is calculated using an exact expression for the flow generated by nonadjacent segments (modeled as a polygonal path), and an explicit expression for the flow generated by the neighboring segments (treated as a circular arc going through the 3-point neighborhood). Time integration is performed using a fifth order Runge–Kutta scheme [Dormand–Prince (13)] with an adaptive time step so that the velocity error is kept below $\delta v < \sim 10^{-10} \Gamma/r_0$ (with segment length $\Delta \ell \sim 0.05$).

- Sethian JA (1996) A fast marching level set method for monotonically advancing fronts. Proc Natl Acad Sci USA 93(4):1591–1595.
- Klenin K, Langowski J (2000) Computation of writhe in modeling of supercoiled DNA. Biopolymers 54(5):307–317.
- Proment D, Onorato M, Barenghi CF (2012) Vortex knots in a Bose-Einstein condensate. Phys Rev E Stat Nonlin Soft Matter Phys 85(3 Pt 2):036306.
- Salman H (2013) Breathers on quantized superfluid vortices. Phys Rev Lett 111(16): 165301.
- Berloff NG (2004) Padé approximations of solitary wave solutions of the Gross-Pitaevskii equation. J Phys Math Gen 37(5):1617–1632.
- Dormand J, Prince P (1980) A family of embedded Runge-Kutta formulae. J Comput Appl Math 6(1):19–26.

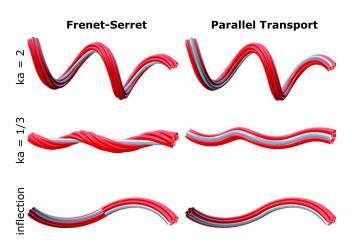


Fig. S1. An illustration of the vortex bundles produced for spiral-like center-lines using different framing methods. The left column shows bundles oriented with the Frenet–Serret normal vector, whereas the right uses a parallel transport (untwisted) framing. The first two rows are helices, whereas the third row shows an inflection point produced by merging two circular arcs.

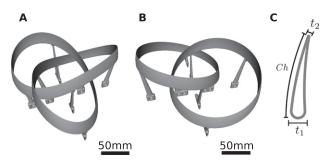


Fig. S2. (*A*) A 3D rendering of the trefoil knot hydrofoil used in experiment. (*B*) A 3D rendering of the link rings hydrofoil used in experiment. (*C*) The hydrofoil cross-section used in both the trefoil knot and linked rings with the following specifications: a chord of Ch = 22.5 mm, a leading edge thickness of $t_1 = 3.75$ mm, a trailing edge thickness of $t_2 = 0.225$ mm, and a bend of $\theta = 15^\circ$.

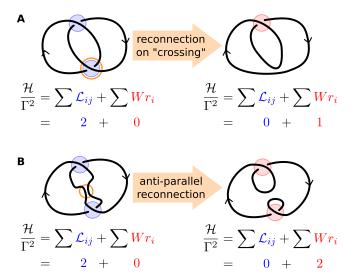


Fig. S3. (A) A diagram of a reconnection event occurring at a "crossing" for a nearly planar pair of linked rings. The helicity has an apparent change of $1\Gamma^2$ because an in-plane crossing is eliminated. (B) A reconnection event that occurs between antiparallel segments does not change the crossing number and so it conserves helicity.

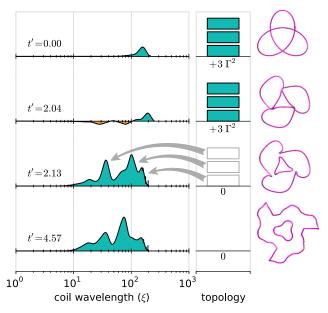
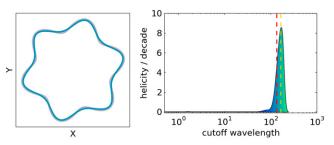
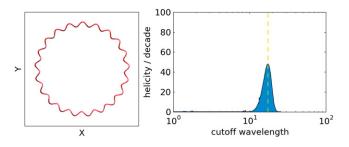


Fig. S4. A helistogram for a GPE trefoil knot with $\bar{r} = 36\xi$, shown along with renderings of the density iso-surfaces at the same simulation time. Unlike in the experiments, the perfect symmetry of the simulation causes all three reconnections to happen simultaneously, transferring nearly all of the helicity from knotting to coiling in a single event.



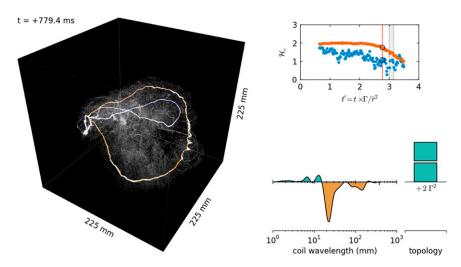
Movie S1. The construction of a helistogram for a helical ring with n = 6 windings. The smoothed path corresponding to each cutoff wavelength is shown (*Left*) along with the complete helistogram (*Right*). The cutoff of the current smoothing is indicated with the red dashed line; for cutoff values below the wavelength L/n (dashed gold line), the path is unaffected by the smoothing; however, once the cutoff value approaches L/n, the helix is rapidly smoothed down to a ring of zero helicity.

Movie S1



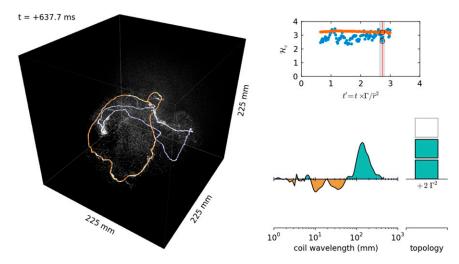
Movie S2. A video showing the helistograms (*Right*) for a collection of different helically wound rings (*Left*) with progressively smaller winding numbers, *n*, but with constant radii and helical amplitude. As the pitch of the helices increases, the helicity of the path becomes localized at progressively larger scales while diminishing in overall magnitude.

Movie S2



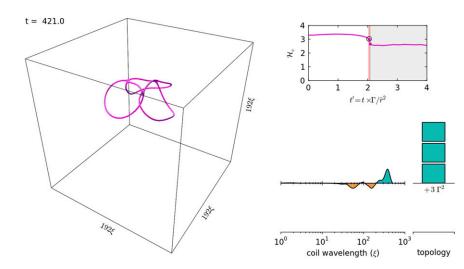
Movie S3. A volumetric image of a pair of linked vortices (*Left*), along with the total helicity (*Upper Right*) and helistogram (*Lower Right*) as a function of time. The initially linked vortices go through two reconnections to form a pair of unlinked rings, which results in the formation of large-scale helices with approximately the same amount of helicity as the initial linking. The volumetric data were recorded at 169.4 volumes per second, and is played back at 15 frames per second, except near the reconnection events where the playback is slowed to 3 frames per second. In frames for which the vortices could be successfully tracked, they are highlighted in blue and orange (corresponding to the first and second identified vortex loop).

Movie S3



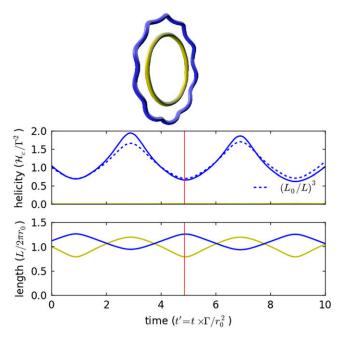
Movie S4. A volumetric image and helistogram for a vortex that is initially a trefoil knot, displayed as in Movie S3. The trefoil knot goes through three reconnections to become a pair of unlinked rings, although it is only possible to track it through the first two reconnections.

Movie S4



Movie S5. The density isosurface and helistogram for a Gross–Pitaevskii simulated trefoil vortex knot with mean radius $\bar{r} = 36\xi$. The final topology (two unlinked rings) is the same as the viscous fluid trefoil vortex knot, although all three reconnections happen simultaneously due to the perfect symmetry of the simulation.

Movie S5



Movie S6. A Biot–Savart simulation of a helical vortex ring leap-frogging a perfectly circular ring. A rendering of the 3D vortex paths is shown, along with the helicity and length as a function of time. The stretching and compressing experienced by the helical ring causes its helicity to vary dramatically.

Movie S6

DNAS

() <