# The effects of transit time heterogeneity on brain oxygenation during rest and functional activation

## Supplementary material

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#### Parallel changes in transit time and capillary transit time heterogeneity

There is relatively sparse literature on the extent to which the mean transit time  $\bar{\tau}_c$  and the capillary transit time heterogeneity (CTH), as quantified by the standard deviation of the transit time distribution  $\sigma_c$ , covary. The estimates presented in Jespersen & Øestergaard [1] suggest that  $\bar{\tau}_c$  and  $\sigma_c$  may covary in the sense, that decreased heterogeneity is observed for decreased transit times. This relationship was observed in data from a series of studies, where flow was manipulated by electrical stimulation [2, 3] by lowering blood oxygen content (hypoxemia) [4, 5] and by elevating blood carbon dioxide content (hypercapnia) [5, 6].

To further explore the covariation between  $\bar{\tau}_c$  and  $\sigma_c$  we conducted a simple simulation experiment based on a vascular anatomical network (VAN) model [7]. The VAN model provides a simplified representation of the vascular topology; the microcirculation is modelled as a branching network starting at a single feeding arteriole that, through a series of arterioles, branches into 64 capillaries and finally converges through venoules into a single draining venule. The model is based on physically measurable parameters, e.g. the resistance of individual vessel segments is modelled in terms of diameter, length, and apparent viscosity with numerical values corresponding to reports found in the literature. The VAN model accurately predicted blood pressure and hemoglobin oxygen saturation at different branch levels throughout the network despite the simplicity of the model [7]. Identical transit times are observed across all vessel segments at a specific branch order in the VAN model, e.g. all 64 capillary segments have same transit time. This lack of heterogeneity is partially due to the symmetrical topology of the network and partially due to all vessel segments at a specific branch order have identical resistance. To introduce CTH into the VAN model we follow a simple approach. In this approach we do not attempt accurately to model the *mechanism* underlying CTH. Rather a simple modification is introduced of which the *effect* is that CTH occurs in the network. Specifically, CTH was introduced as follows. In the basic form all capillary segments of the VAN model have a resistance of  $r_c = 3.9 \cdot 10^{10}$  mmHg·s/l. Instead of identical resistances we now let the individual capillary resistances be distributed uniformly centred at  $r_c$ . This modification results in presence of flow heterogeneity throughout the entire network. The study of Jespersen & Øestergaard [1] compiled a table with estimates of  $\sigma_c$  based on experimental data (Table 1 in their paper). For the two data set using electrical stimulation we computed the coefficient of variation  $(\sigma_c/\bar{\tau}_c)$  corresponding to baseline conditions. This coefficient was then averaged across the two data sets giving  $\sigma_c/\bar{\tau}_c = 0.78$ . The width of the resistance distribution, centred at  $r_c$ , was then adjusted such that the transit time coefficient of variation  $\sigma_c/\bar{\tau}_c$  observed in the modified VAN model approximated 0.78.

Following this modification of capillary resistances the vessel segments in the arteriolar part of the network were dilated in order to increase flow through the network. The arteriolar vessel volumes were increased from baseline values up to values that result in a relative flow increase of around 50%, similar to flow increases observed in functional activation [3, 8].

The total flow increased from a flow of ~ 10 nl/s to ~ 15 nl/s. Figure 1 shows traces of individual capillaries (thin gray curves) while thick dashed curves show the means across the 64 capillaries over the range of changes in total flow. Figure 2 shows traces of averages and standard deviations (both flow weighted) of capillary transit times and capillary velocities over the range of changes in total flow. Flow weighted quantities were computed as follows. We let  $f_i$  denote the flow through the *i*'th capillary and let the weight  $w_i = f_i / \sum_{i'} f_{i'}$ ,  $i' \in \{1, 2, ..., 64\}$  quantify the fractional flow through the *i*'th capillary. Let

 $\tau_i$  denote the transit time of the *i*'th capillary. The average of transit time and the standard deviation of transit times are computed as flow weighted quantities, with the average defined by

$$\bar{\tau}_{\rm c} = \sum_{i} w_i \tau_i,\tag{1}$$

and the standard deviation defined by

$$\sigma_c = \sqrt{\frac{N}{N-1} \sum_i w_i \left(\tau_i - \bar{\tau}_c\right)^2},\tag{2}$$

with N being the number of non-zero weights  $w_i$ .



Figure 1: Behaviour of absolute (A): capillary flow f, (B): velocity  $\gamma$ , (C): diameter d, and (D): transit time  $\tau$  of 64 individual capillaries (thin gray curves) against changes in total capillary flow  $f_{\text{total}}$ . Thick dashed curves are averages over all capillaries.



Figure 2: Traces of average capillary transit time ( $\bar{\tau}_c$ ) and transit time standard deviation ( $\sigma_c$ ). (A): Quantities on absolute scales, (B): relative changes in the quantities.

### **Model parameters**

Table 1 and 2 show model parameters. The models are completely parameterized by these parameters. Note that baseline flow, baseline metabolism, and the oxygen conductance (E) are not defined in the tables. These parameters are part of lumped model parameters that appear after mathematical manipulation of the models' equations. Lumped parameters were computed from parameters in Table 1 and 2. For example, the baseline metabolism is part of a lumped model parameter that is computed from  $K_m$ ,  $\lambda$ , and  $p_{i,0}$ .

Parameters values of the one-compartment model used in steady state simulations			
Parameter	Parameter value	Reference	
$\bar{\tau}_c$ [s]	1.2	[9, 10, 11, 12]	
$\lambda \text{ [ml O}_2/\text{mL blood]}$	0.206	[13]	
$p_{ac,0} \text{ [mmHg]}$	60	[14, 15]	
$p_{cv,0}$ [mmHg]	35	[14, 15]	
$p_{t,0} \text{ [mmHg]}$	25	[8, 15, 1]	
$p_{50} \text{ [mmHg]}$	36.0	[13]	
h	2.60	[13]	
$K_m$	0.001 \$	-	
$\sigma_{c,0}$ [s]	0.94 ‡	[1]	

Table 1: Parameters values of the one-compartment model used for simulation of steady state properties of the oxygen transport model. ‡ Corresponding to  $\sigma_c/\bar{\tau}_c = 0.78$ . \$ With this value the factor  $p_t/(K_m + p_t)$  primarily prevents  $p_t$  from becoming negative while having a relatively small impact on the oxygen metabolism since the relative difference between m and  $m^{max}$  is less than 1% if  $p_t > 0.1$  mmHg so  $m \approx m^{max}$ .

effects of capillary transit time heterogeneity			
Parameter	Parameter value	Reference	
β	[1 4]	[16, 11]	
$\bar{\tau}$ [s]	[0.5 4]	[9, 11, 12]	
$c_a$	[0.5 0.9] *	[16, 11]	
$w_c$	[0.4 0.5] †	[10]	
$w_t$	[32 49] <sup>‡</sup>	[10, 17]	
$\lambda \text{ [ml O}_2/\text{mL blood]}$	0.206 *	[13]	
$p_{in,0}$ [mmHg]	77.9 *	[18]	
$p_{ac,0} \text{ [mmHg]}$	[55 70]	[14, 15]	
$p_{cv,0}$ [mmHg]	33.5 *	[18]	
$p_{out,0}$ [mmHg]	33.5 *◊	[18]	
$p_{t,0}$ [mmHg]	[20 30]	[8, 15, 1]	
$p_{50} \text{ [mmHg]}$	36.0 *	[13]	
h	2.60 *	[13]	
$K_m$	0.001 *\$	-	
$\sigma_{c,0}$ [s]	[0.1 2]	[1]	

Parameters values of the multi-compartment model used in modeling dynamical effects of capillary transit time heterogeneity

Table 2: Parameters values of the multi-compartment model used in simulations of dynamics and for modeling the data set of Vazquez et al. [18]. Values marked with \* were fixed, whereas intervals define the range of the prior distributions used in the analysis of the data set of [18]. The center values of the intervals were used in the simulations of dynamics.  $\diamond$  Fractional contribution of the arteriolar compartment to the total resistance, the remaining resistance was equally distributed between the capillary and the venous compartment.  $\dagger w_c$  Fractional capillary contribution to the total vascular volume, the remaining vascular volume was equally distributed between the arterial and the venous compartment.  $\ddagger w_t$  Fraction of tissue volume to vascular volume. The interval corresponds to a tissue volume of 97%-98% of total volume.  $\diamond$  To simplify, we assume negligible oxygen exchange between the venous compartment and tissue. \$ With this value the factor  $p_t/(K_m + p_t)$  primarily prevents  $p_t$  from becoming negative while having a relatively small impact on the oxygen metabolism since the relative difference between m and  $m^{max}$  is less than 1% if  $p_t > 0.1$  mmHg so  $m \approx m^{max}$ .

#### Temporal dynamics of input variables

The temporal development of relative changes in input variables used in the analysis of the data set of Vasquez et al. [18] was modeled by the function f(t). The function f(t) increases from baseline towards a maximum value of  $\theta_1$  according to an asymmetrical sigmoid function [19] between times  $t_{min}$  and  $t_{max}$ , decreases exponentially towards a plateau value of  $\theta_2$  between times  $t_{max}$  and  $t_{end}$ , and finally decreases exponentially towards baseline value after time  $t_{end}$ .  $t_{min}$  and  $t_{end}$  are start and end times of the stimuli respectively, and  $t_{max}$  is the time of maximum response.

$$f(t) = \begin{cases} f_1(t) + 1, & t_{min} < t \le t_{max} \\ f_2(t) + 1, & t_{max} < t \le t_{end} \\ f_3(t) + 1, & t > t_{end}, \end{cases}$$
(3)

$$f_1(t) = \theta_1 / [1 + g(t) \exp\{\theta_3 * (\theta_4 - t)\}$$
(4)

+ {1 - g(t)} exp{
$$\theta_5 * (\theta_4 - t)$$
}] (5)

$$f_2(t) = (s_1 - \theta_3) \exp\{\theta_6 * (t_{max} - t)\} + \theta_3$$
(6)

$$f_3(t) = s_2 \exp\{\theta_7 * (t_{end} - t)\},\tag{7}$$

where  $s_1 = f(t_{max})$ , and  $s_2 = f(t_{end})$ .  $g(t) = 1/[1 + \exp\{-\gamma(\theta_4 - t)\}]$  where  $\gamma = 2\theta_3\theta_5/|\theta_3 + \theta_5|$  and  $\theta$  holds model parameters.

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