

- **Extracturing**, natural gas extraction
- $\frac{20}{27}$
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Analytical Methods

- *Sample Collection:* Groundwater wells were purged until temperature, pH, and electrical
- conductance readings were stable. Shallow groundwater samples were collected in pre-
- combusted 40-mL glass volatile organic analysis (VOA) vials containing 1-mL of 50%
- $\frac{33}{100}$ v/v hydrochloric acid (HCl), capped without headspace, and stored on ice or at $\frac{4}{10}$ until
- analysis. Samples were collected as close to the wellhead as possible and upstream of any water treatment systems.
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- *Volatile Organic Compounds (VOCs):* We used a modified version of EPA Method 624
- and 8015D as described in Getzinger et al. (2015) [1] for quantification and qualitative
- identification of 50 unique VOCs via GC-FID and GC-MS (Table S1). Briefly, a 5-mL
- aliquot of groundwater was purged with helium on a purge and trap concentrator and
- subsequently transferred to a GC-FID (quantification with retention time identity
- confirmation) or GC-MS (confirming qualitative identification) using a Restek
- 42 MegaMixTM standard mixture (Restek 502.2).
- *Gasoline Range Organic Compounds (GRO):* We quantified GRO with the sample
- preparation techniques described for the VOC analysis and used a GRO mix standard for
- quantification (Restek #30065), following EPA Method 8015D. Chromatographic peaks

eluting within the retention time window of 2-methylpentane and 1,2,4-trimethylbenzene

were integrated and added together for a total signal representative of the organic

compounds with boiling points within the defined gasoline range [2].

Diesel Range Organic Compounds (DRO): We used a liquid-liquid extraction technique

to quantify DRO with EPA Method 8015D, as described in Getzinger et al. (2015) [1].

- Approximately 500 mL of groundwater was extracted with 90:10
- dichloromethane:methanol three times before rotary evaporation down to a final volume
- of 1-1.5 mL. Samples were quantified with a Restek DRO mix standard (Restek 31064)

via GC-FID. Chromatographic peaks eluting within the retention time window of decane

- 55 $(r_{n}C_{10})$ and octacosane $(r_{n}C_{28})$ were integrated and added together for a total signal
- representative of the organic compounds with boiling points within the defined diesel range [2].
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- *Comprehensive two-dimensional gas chromatography:* Two Leco GC×GC systems were used in this study: one coupled with a time-of-flight mass spectrometer (TOF-MS; Leco used in this study: one coupled with a time-of-flight mass spectrometer (TOF-MS; Leco
- Pegasus 4D) and one coupled to a flame ionization detector (FID) detector. They were
- equipped with an Agilent 6890 GC (TOF-MS) and Agilent 7890 GC (FID system) and
- configured with split/splitless auto injectors (7683B series) and a dual stage cryogenic
- modulator (Leco, Saint Joseph, Michigan). Samples were injected in splitless mode. Two
- 64 capillary GC columns were fitted in each $GC \times GC$ instrument, with a cryogenic
- modulator between the two. The first-dimension column was a non-polar Restek Rxi-
- 1ms, (60 m length, 0.25 mm I.D., 0.25 µm film thickness) and the second-dimension
- separations were performed on a 50% phenyl polysilphenylene-siloxane column (SGE
- BPX50, 1.0 m length, 0.10 mm I.D., 0.1 µm film thickness). The modulator between the
- 69 two columns operates with a liquid N₂ cold jet and dry N₂ hot jet operated at 10-15 °C
- above the temperature of the main GC oven. Hydrogen was used as carrier gas at a

71 constant flow rate of 0.90 mL min⁻¹ on the GC×GC-FID and helium at a flow rate of 1.00 72 mL min⁻¹ on the GC×GC-TOF.

GC×GC-TOFMS Method:

75 The temperature program of the main oven started isothermal at 50 \degree C (15 min) and was 76 then ramped from 50 to 330 °C at 1.75 °C min⁻¹. The hot jet pulse width was 0.75 s and the modulation period was 10 s with a 4.25 s cooling period between stages. The second 78 dimension oven was programmed from 55 $\rm{^{\circ}C}$ (15 min) to 335 $\rm{^{\circ}C}$ at 1.75 $\rm{^{\circ}C}$ min⁻¹. The TOF-MS data were sampled at an acquisition rate of 50 spectra per second. The transfer line from the second oven to the TOFMS was deactivated fused silica (0.5 m length, 0.18 81 mm I.D.), constantly held at 315 °C. The TOF detector voltage was 1335 Volts and the 82 source temperature 220 °C. The mass spectrometer employs 70 eV electron ionization and operates at a push pulse rate of 5 kHz allowing sufficient signal averaging time to ensure good signal-to-noise ratios while still operating at a high enough data acquisition rate to accurately process (signal average) spectra from the peaks eluting from the second 86 dimension column in this high resolution separation technique (GC×GC-TOF second

- dimension peak widths range between 50 to 200 milliseconds).
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GC×GC-FID Method:

- 90 For the GC×GC-FID analysis, 1 μ L of each sample solution was injected into a 300 °C
91 splitless injector with a purge time of 0.5 min. The first-dimension column and the dual
- splitless injector with a purge time of 0.5 min. The first-dimension column and the dual
- stage cryogenic modulator resided in the main oven, whereas the second-dimension
- column was fitted in a separate oven, allowing for independent temperature control of all 94 three. The temperature program of the main oven started isothermal at 40 $^{\circ}$ C (10 min)
- 95 and was then ramped from 40 to 335 $^{\circ}$ C at 1.25 $^{\circ}$ C min⁻¹. The second dimension oven
- was programmed to remain isothermal at 45 °C for 10 minutes and then ramped from 45
- 97 to 340 °C at 1.25 °C min⁻¹. The hot jet pulse width was 0.50 seconds and the modulation
- period was 7.5 seconds with a 3.25 second cooling period between stages.
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Inorganic constituents: Inorganic compounds were analyzed from samples collected

- either simultaneously with or prior to sample collection campaigns for organic
- compounds. Analyses were performed via methods described by Warner et al. (2012) [3].
- *Methane:* Methane was analyzed from samples collected simultaneously with or prior to
- sample collection campaigns for organic compounds. Analyses were performed via
- methods described by Jackson et al. (2013) and Darrah et al. (2014) [4, 5].
- *Helium concentrations and noble gases:* Helium and heavier noble gases were analyzed
- from samples collected simultaneously with or prior to sample collection campaigns for
- organic compounds. Analyses were performed via methods described by Jackson et al.
- (2013) and Darrah et al. (2014) [4, 5].

Field Setting

- Samples were collected in northeastern Pennsylvania from three aquifers (Lock Haven,
- Catskill, and Alluvium) overlying the Marcellus Shale in the northern Appalachian Basin.
- Extensive descriptions of the geology and hydrogeologic settings can be found elsewhere
- [3-7].

116 **Groundwater Contaminant Transport Calculations**

- 117 Subsurface groundwater transport of bis(2-ethylhexyl) phthalate through an aquifer 118 representative of northeastern Pennsylvania hydrogeology was estimated based on
- 119 calculations and physical parameters (Table S2) from various sources [8-13]. 120
- 121 The compound-specific, sorption-retarded transport velocity, v_c , is given by:
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$$
v_c = \frac{v_w}{R}
$$
 Eq. SI

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124 where v_w is the bulk groundwater flow and *R* is the retardation factor given by: 125

$$
R = 1 + \rho_s \frac{1 - \phi}{\phi} K_d
$$
 Eq. S2

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127 and ρ_s is the sediment or soil bulk density, ϕ is the porosity, and K_d is the solid-water 128 distribution coefficient. Here, we assume K_d is dominated by sorption to non-black 129 carbon organic carbon phases [10], and so:

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K_d = K_{oc} * f_{oc}
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 Eq. S3

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132 where K_{oc} is the organic carbon partition coefficient and f_{oc} is the fraction of organic 133 carbon in the porous medium.

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136 **Modeling chemical transport across a polyethylene liner**

137 We deployed an analytical solution to calculate 1-D Fickian diffusion of bis(2-

138 ethylhexyl) phthalate (DEHP; diethylhexyl phthalate) across a 4-mm polyethylene (PE)

- 139 film, following Crank (1975) [14] and Schwarzenbach et al. (2002) [10]:
- 140

$$
C_{PE}(x,t) = C_{PE}^{*}erfc\left(\frac{x}{2(D_{PE}t)^{1/2}}\right)
$$
 Eq. S4

141 where $C_{PF}(x,t)$ (mass/cm³) is the concentration in the PE x cm from the side in contact 142 with retention pond water at some time, $t(s)$, C_{PE}^* is the concentration at the boundary of 143 the PE equilibrated with water in the retention pond, and D_{PE} (cm²/s) is the diffusivity of DEHP within the PE. By neglecting the additional resistances to mass transport provided by a water-side diffusive boundary layer, diffusion within the soil porous media, and retardation within the PE caused by pigments (e.g., carbon black, commonly used to color the black PE liners used in containment ponds), this mathematical model simulates the furthest possible distance the concentrations front could reach within the PE film. *D_{PE}* for DEHP was estimated at $10^{-11.3}$ cm²/s, based on a relationship between molar 150 volume (MV) and $log D_{PE}$ (Eq. S5) obtained from measured D_{PE} for PAHs (polycyclic aromatic hydrocarbons) and PCBs (polychlorinated biphenyls) [15] and molar volume

estimated using the Sparc Performs Automated Reasoning in Chemistry (SPARC)

chemical property estimator.

$$
log D_{PE} (cm^2/s) = -0.014 \, MV \, (cm^3/mol) - 6.1 \qquad Eq. S5
$$

Using these values, DEHP will only diffuse 1 mm into the PE liner after 4 years (and

157 only 2×10^{-27} % of the original concentration). Using an even more conservative

158 calculation, employing 100-fold faster diffusion (D_{PE} =10^{-9.3} cm²/s) indicates that only 2%

of DEHP could cross a 4-mm thick PE liner by 12 months.

We confirmed the application of the analytical solution by running an explicit, finite-

difference model to simulate transport across the PE using a previously prepared Matlab

 code modified to reflect boundary conditions relevant to a pond-PE-porous media system [16].

Table ST. Detection minus for DKO, GKO, and the targeted VOCs. Compound	LOD (ppb)	Compound	LOD (ppb)
DRO	0.09	1,2-Dibromoethane	0.17
GRO	0.03	chlorobenzene	1.8
1,1-Dichloroethene	0.84	Ethylbenzene	2.9
Methylene chloride	1.0	m-Xylene+p-xylene	5.0
1,1-Dichloroethane	0.47	o-xylene	2.4
trans-1,2-Dichloroethene	1.2	styrene	0.26
2,2-Dichloropropane	2.4	bromoform	9.0
cis-1,2-dichloroethene	2.4	1,2,3-Trichloropropane	0.32
chloroform	2.7	Bromobenzene	0.54
Bromochloromethane	1.5	1,1,2,2-Tetrachloroethane	1.2
carbon tetrachloride	0.83	n-Propylbnezene	0.34
1,1,1-trichloroethane	0.83	2-Chlorotoluene	0.39
1,1-dichloropropene	0.83	1,3,5-Trimethylbenzene	0.19
Benzene	0.20	tert-Butylbenzene	0.37
1,2-dichloroethane	0.53	1,2,4-Trimethylbenzene	0.35
Trichloroethene	1.2	sec-Butylbenzene	0.42
1,2-Dichloropropane	0.70	1,3-Dichlorobenzene	0.55
bromodichloromethane	4.2	1,4-Dichlorobenzene	0.24
Dibromomethane	4.1	4-isopropyltoluene	0.24
cis-1,3-Dichloropropene	0.91	1,2-Dichlorobenzene	0.56
toluene	0.26	n-Butylbenzene	0.50
trans-1,3-Dichloropropene	1.2	1,2-Dibromo-3-chloropropane	7.2
1,1,2-Trichloroethane	1.5	1,2,4-Trichlorobenzene	1.0
Tetrachloroethene	0.41	Hexachlorobuatdiene	2.6
1,3-Dichloropropane	0.66	Napthalene	0.88
dibromochloromethane	0.10	1,2,3-Trichlorobenzene	1.1

Table S1. Detection limits for DRO, GRO, and the targeted VOCs.

169 **Table S2.** Parameters used for subsurface transport calculations of bis(2-ethylhexyl) phthalate.

phthalate.

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 $\frac{173}{174}$ Figure S1. Ranked comparison of DRO (left) and GRO (right) between active and non-

175 active zones (active zone defined as < 1 km from a shale gas well). There was a statistical 176 difference in DRO between zones ($p = 0.01$, Mann-Whitney U test) and no difference in

177 GRO between zones ($p = 0.90$).

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 $\frac{181}{182}$ **Figure S2.** Ranked comparison of DRO (left) and GRO (right) with respect to different shallow groundwater types. Type D water has influence of Marcellus formation brine via natural connectivity [3]. There were no statistical differences in DRO or GRO between 185 types (DRO, $p > 0.05$; GRO, $p > 0.05$; Kruskal-Wallis test).

measurements taken either during the same sampling campaign or at a previous time.

 Statistical analysis showed no correlation (DRO, p > 0.05; GRO, p > 0.05, Spearman correlation).

- 196 time. Statistical analyses showed no correlation (DRO, $p > 0.05$; GRO $p > 0.05$,
- Spearman correlation).

 Figure S5. Relationship of DRO (left) and GRO (right) with the number of days since the 201 nearest shale gas well was drilled. Statistical analyses showed no correlation (DRO, p > 202 0.05; GRO, $p > 0.05$, Spearman correlation). Note that only three groundwater wells were sampled repeatedly over a period of time (shown in color), and most of the data are

- individual wells that were sampled once during our three-year period.
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 $\begin{array}{c} 207 \\ 208 \end{array}$ **Figure S6.** Relationship of DRO (left) and GRO (right) with bromide (top) and chloride 209 (bottom). Statistical analyses showed no correlation (DRO and bromide, $p > 0.05$; GRO (bottom). Statistical analyses showed no correlation (DRO and bromide, $p > 0.05$; GRO 210 and bromide, $p > 0.05$; DRO and chloride, $p > 0.05$; GRO and chloride, $p > 0.05$). 211

Figure S7. The 1-dimensional Fickian diffusion model for transport of bis(2-

 ethylhexyl)phthalate through a 4-mm thick polyethylene liner using a reasonable, 216 estimated diffusivity of $10^{-11.3}$ cm²/s (a) and a 100-fold faster diffusion of $10^{-9.3}$ cm²/s (b). Note that this model represents the fastest-possible transport times, as we neglected resistances to mass transport provided by a water-side diffusive boundary layer, diffusion within the soil porous media, and retardation within the PE caused by pigments (e.g., carbon black, commonly used to color the black PE liners used in containment ponds).

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222 **GRO and DRO Fingerprinting**

 GRO/DRO ratios could be used as a tracer of these waters or potentially as an indicator of deep formation water migration. Noting that only a small number of samples (*n* = 5) had detectable levels of both GRO *and* DRO, it is clear that there is no discernable GRO/DRO "fingerprint" (Figure 2, inset, main text) in groundwater in from this region. Similarly, flowback water showed variable GRO/DRO ratios, with total GRO and DRO abundance much higher than that observed in groundwater (SI Fig. S8). Thus, GRO/DRO fingerprinting and enrichments are not viable candidates for tracing flowback water migration from either faulty well casings or leaking containment pits. 231

233 Figure S8. Comparison of GRO and DRO concentrations in shallow groundwater 235 samples and flowback waters samples. Note that the flowback water samples (colored 236 triangles) have much higher GRO and DRO (a), whereas groundwater samples (open 237 circles) have comparatively low levels for GRO and DRO (b). There is no discernable 238 GRO/DRO fingerprint in either groundwater or flowback water, as both exhibit a high 239 degree of variability.

242 Figure S9. Relationship of DRO (left) and GRO (right) concentrations with sampled 243 groundwater well depth and the distance to the nearest shale gas well. There was no

- 244 statistical relationship between concentration and well depth (DRO $p > 0.05$, GRO $p >$ \mathbf{C} \mathcal{O}
- 245 0.05). The samples with the highest concentrations were found in areas with relatively
- 246 shallow well depths and close to shale gas wells.
- 247

249 **Figure S10.** Spatial relationship of DRO (left) and GRO (right) concentrations with the

250 distance to the nearest leaking underground storage tank (LUST) as reported by

251 Pennsylvania Department of Environmental Protection (PA DEP). Statistical analyses

252 showed no correlation (DRO, $p > 0.05$; GRO, $p > 0.05$). LUST location data available at

253 http://www.depreportingservices.state.pa.us/ReportServer/Pages/ReportViewer.aspx?/Cle
254 anup/Tank Cleanup Incidents. Accessed on November 2, 2014. anup/Tank Cleanup Incidents. Accessed on November 2, 2014.

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Figure S11. GCxGC-TOFMS analysis of gasoline, diesel fuel, and a hydraulic fluid 258 common in industrial and agricultural applications, along with a groundwater samples 259 (PAS 311C) that contained elevated levels of DRO. Note that the instrument response in 260 the DRO region of the groundwater sample is dominated by the phthalate and unlike 261 those of the fuels.

Figure S12. GCxGC-TOF-MS analysis of five (out of 23 total) low-but-detectable-DRO containting groundwater samples and a field blank indicated no detectable levels of bis(2- ethyhexyl) phthalate. These results demonstrate that phthalates, while ubiquitous in industrial products (e.g., plastics and piping material), do not often appear in groundwater

268 in this region. The complimentary analysis of two high-DRO containing groundwater

269 samples appears in the main text and shows the presence bis(2-ethylhexyl) phthalate.

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