Bifurcation Analysis on a Variation of the FitzHugh-Nagumo (FHN) Model

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Bifurcation analysis

The variation of the FHN equations is represented as

$$
\frac{\partial v_{\mathbf{m}}}{\partial t} = \frac{1}{\varepsilon_1 c_{\mathbf{m}}} (k(v_{\mathbf{m}} - v_1)(v_2 - v_{\mathbf{m}})(v_{\mathbf{m}} - v_3) - w + \nu) \triangleq f_1(v_{\mathbf{m}}, w), \tag{1}
$$

$$
\frac{\partial w}{\partial t} = \varepsilon_2 (\beta v_m - \gamma w + \delta) \triangleq f_2(v_m, w). \tag{2}
$$

The nullclines of the FHN model are given by the following two equations

$$
f_1(v_m, w) = 0,\t\t(3)
$$

$$
f_2(v_m, w) = 0.\t\t(4)
$$

The $v_{\rm m}$ -nullcline is a cubic function of $v_{\rm m}$, which is shown as

$$
w = k(v_m - v_1)(v_2 - v_m)(v_m - v_3) + \nu,
$$
\n(5)

and the w-nullcline is a straight line as follows:

$$
w = \frac{\beta}{\gamma}v_{\rm m} + \frac{\delta}{\gamma}.\tag{6}
$$

The equilibrium of the FHN system is the intersection of these two nullclines, which is defined as (v_m^*, w^*) . The stimulus amplitude ν can then be denoted as a function of the equilibrium v_m^* with other parameters fixed:

$$
\nu(v_m^*) = -k(v_m^* - v_1)(v_2 - v_m^*)(v_m^* - v_3) + (\beta v_m^* + \delta)/\gamma.
$$
 (7)

We are interested in the case when there is always only one equilibrium in the FHN system whatever the stimulus amplitude ν , for which the slope of the w-nullcline should be greater than the maximal slope of the $v_{\rm m}$ -nullcline. The slope of the straight w-nullcline is $\frac{\beta}{\gamma}$, while the maximal slope of the v_m-nullcline is found at the point $v_{\rm m} = \frac{v_1 + v_2 + v_3}{3}$ $\frac{y_2 + v_3}{3}$ and it is equal to $\frac{k(v_1 + v_2 + v_3)^2}{3}$ $\frac{v_2 + v_3}{3} - k(v_1v_2 + v_1v_3 + v_2v_3)$. The condition for the existence and uniqueness of equilibrium is therefore given by:

$$
\Delta_1 \triangleq (v_1 + v_2 + v_3)^2 - 3(v_1v_2 + v_1v_3 + v_2v_3) - \frac{3\beta}{k\gamma} < 0. \tag{8}
$$

The local stability of the equilibrium is determined by linearization of the nonlinear FHN model at the equilibrium, which is given by

$$
\frac{\partial}{\partial t}\mathbf{x} = \mathbf{D}\mathbf{x},\tag{9}
$$

where $x =$ $\sqrt{ }$ $\overline{ }$ $v_{\rm m} - v_{\rm m}^*$ $w - w^*$ \setminus , and **D** is the Jacobian matrix at the equilibrium $(v_m^*, w^*),$ which is shown as follows:

$$
\mathbf{D} = \begin{pmatrix} \frac{\partial f_1(v_m, w)}{\partial v_m} & \frac{\partial f_1(v_m, w)}{\partial w} \\ \frac{\partial f_2(v_m, w)}{\partial v_m} & \frac{\partial f_2(v_m, w)}{\partial w} \end{pmatrix} \Bigg|_{(v_m^*, w^*)} \triangleq \begin{pmatrix} f_{1v_m} & f_{1w} \\ f_{2v_m} & f_{2w} \end{pmatrix}
$$

$$
= \begin{pmatrix} \frac{q(v_m^*, v_1, v_2, v_3, k)}{\varepsilon_1 c_m} & -\frac{1}{\varepsilon_1 c_m} \\ \varepsilon_2 \beta & -\varepsilon_2 \gamma \end{pmatrix},
$$
(10)

where $q(v_m^*, v_1, v_2, v_3, k) = -3kv_m^{*2} + 2k(v_1 + v_2 + v_3)v_m^* - k(v_1v_2 + v_1v_3 + v_2v_3)$. The solution of Eq. [\(9\)](#page-1-0) can be represented as

$$
\boldsymbol{x}(t) = \exp(\lambda t) \; \boldsymbol{v}, \tag{11}
$$

where λ is the eigenvalue of the Jacobian matrix \boldsymbol{D} and \boldsymbol{v} is its corresponding eigenvector. By solving the characteristic equation

$$
\det(\mathbf{D} - \lambda \mathbf{I}) = 0,\tag{12}
$$

we obtain the relationship between eigenvalue λ and the equilibrium v_m^* , which is given as follows:

$$
\lambda^{2} - (f_{1v_{\rm m}} + f_{2w})\lambda + (f_{1v_{\rm m}}f_{2w} - f_{1w}f_{2v_{\rm m}}) = 0.
$$
\n(13)

Depending on the values of eigenvalues, we can determine whether the equilibrium is stable or not. Since we are interested in characterizing the stability of equilibrium as a function of model parameters, we need to compute eigenvalues as a function of these parameters and so we assess stability through the evaluation of two conditions as presented in Table [1.](#page-2-0)

Table 1. Conditions for the stability of equilibrium saddle unstable $\lambda_1 > 0$, $\lambda_2 < 0$ or $\lambda_1 < 0$, $\lambda_2 > 0$ $\lambda_1 \lambda_2 < 0$

Type		Stability Eigenvalues $(\lambda_1$ and $\lambda_2)$	\mid Condition 1 \mid Condition 2	
saddle	unstable	$\lambda_1 > 0$, $\lambda_2 < 0$ or $\lambda_1 < 0$, $\lambda_2 > 0$ $\lambda_1 \lambda_2 < 0$		
$node/focus$ stable		$Re(\lambda_1) < 0$, $Re(\lambda_2) < 0$	$\lambda_1 \lambda_2 > 0$	$\lambda_1 + \lambda_2 < 0$
node/focus unstable		$Re(\lambda_1) > 0$, $Re(\lambda_2) > 0$	$\lambda_1\lambda_2>0$	$\lambda_1 + \lambda_2 > 0$

When the node or focus loses stability, it is possible to construct a bounding surface around the unstable equilibrium. According to the Poincaré-Bendixson theorem $[1]$, a limit cycle must exit in the FHN system when the node or focus is unstable. In other words, the behavior of the FHN system changes qualitatively from a stable equilibrium to a limit cycle. Therefore, in order to identify the ranges of v_m^* so that the FHN system has a limit cycle, we need to compute condition 1 and condition 2 in Table [1](#page-2-0) under which the node or focus is unstable, that is,

$$
\lambda_1 \lambda_2 = f_{1v_m} f_{2w} - f_{1w} f_{2v_m}
$$
\n
$$
= -\varepsilon_2 \gamma \frac{q(v_m^*, v_1, v_2, v_3, k)}{\varepsilon_1 c_m} + \frac{\varepsilon_2 \beta}{\varepsilon_1 c_m} > 0,
$$
\n(14)

$$
\lambda_1 + \lambda_2 = f_{1v_m} + f_{2w} \n= \frac{q(v_m^*, v_1, v_2, v_3, k)}{\varepsilon_1 c_m} - \varepsilon_2 \gamma > 0.
$$
\n(15)

With the condition [\(8\)](#page-1-1), the discriminant of inequality [\(14\)](#page-2-1) is negative. Therefore,

inequality [\(14\)](#page-2-1) is satisfied for all v_m^* so that we only need to consider inequality [\(15\)](#page-2-2). If the discriminant of the quadratic polynomial in inequality [\(15\)](#page-2-2) is negative, the inequality is also satisfied for all v_m^* . In this work, we are interested in the case when the quadratic polynomial has positive discriminant, i.e.,

$$
\Delta_2 > 0,\tag{16}
$$

where $\Delta_2 = (v_1 + v_2 + v_3)^2 - 3(v_1v_2 + v_1v_3 + v_2v_3) - \frac{3\varepsilon_1\varepsilon_2c_m\gamma}{k}$ $\frac{2C_{\text{m}}}{k}$, in which case inequality [\(15\)](#page-2-2) is satisfied if

$$
\frac{v_1 + v_2 + v_3 - \sqrt{\Delta_2}}{3} < v_m^* < \frac{v_1 + v_2 + v_3 + \sqrt{\Delta_2}}{3}.\tag{17}
$$

In a word, the equilibrium is unstable and instead the FHN system has a limit cycle if the equilibrium satisfies inequality [\(17\)](#page-3-0) with the parameters $v_1, v_2, v_3, k, \beta, \gamma, \varepsilon_1, \varepsilon_2$, c_m satisfying inequalities [\(8\)](#page-1-1) and [\(16\)](#page-3-1). Together with Eq. [\(7\)](#page-1-2) and inequality [\(17\)](#page-3-0), we finally obtain the range of the stimulus amplitude ν to produce a limit cycle.

At the transition point (the point at which equilibrium loses stability), the real parts of eigenvalues vanish and the eigenvalues are

$$
\lambda_{1,2} = \pm i \sqrt{f_{1v_{\rm m}} f_{2w} - f_{1w} f_{2v_{\rm m}}}.
$$
\n(18)

These eigenvalues correspond to an oscillatory solution, i.e., spike trains, with a frequency given by

$$
\omega = \sqrt{f_{1v_{\rm m}} f_{2w} - f_{1w} f_{2v_{\rm m}}}
$$
\n
$$
= \sqrt{\frac{\varepsilon_2}{\varepsilon_1 c_{\rm m}}} \sqrt{-\gamma q(v_{\rm m}^*, v_1, v_2, v_3, k) + \beta}.
$$
\n(19)

According to Eq. [\(7\)](#page-1-2), v_m^* in the above equation is a function of $v_1, v_2, v_3, k, \beta, \delta, \gamma, \nu$. Hence, the frequency can be represented as

$$
\omega = \sqrt{\frac{\varepsilon_2}{\varepsilon_1 c_{\rm m}}} g(v_1, v_2, v_3, k, \beta, \delta, \gamma, \nu), \tag{20}
$$

where $g(v_1, v_2, v_3, k, \beta, \delta, \gamma, \nu) = \sqrt{-\gamma q(v_m^*, v_1, v_2, v_3, k) + \beta}$, which is a function of v_1 ,

 $v_2, v_3, k, \beta, \delta, \gamma, \nu.$

References

1. Hale JK, Buttanri H, Kocak H. Dynamics and Bifurcations. Texts in Applied Mathematics. Springer New York; 1996.