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# **Supplemental Information**

# Cell Surface Mechanochemistry and the Determinants of Bleb Forma-

## tion, Healing, and Travel Velocity

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### **1** Summary of experimental predictions

The model makes several testable predictions throughout the Results section. For convenience, we tabulate these predictions here. Note that these predictions presume that the cell is exhibiting blebs before the perturbation.

Experimental perturbation	Parameter	Prediction
Increasing hydrostatic pressure	$P\uparrow$	Larger blebs
Increasing molecular size of adhesion molecules	$D\uparrow$	Abolish blebbing
Decreasing molecular size of adhesion molecules	$D\downarrow$	Slower bleb healing
Increasing myosin contractility	$M\uparrow$	Abolish blebbing
Decreasing myosin contractility	$M\downarrow$	Slower bleb healing
Increasing membrane tension	$\gamma_M \uparrow$	Faster bleb travel
Increasing abundance of adhesions	$k_{\mathrm{on}}\uparrow$	Slower bleb travel

Table S1: Model predictions for experimental perturbations.

### 2 Details of geometry of cortical and cytoplasmic actin

In 3D, the cell surface and cortex are curved, discontinuous two-dimensional manifolds and the cytoplasm is a 3D field. In full generality, the cortex and cytoplasmic actin network have a density at each point in space. We assume that actin-myosin contractility is isotropic and generates local stress proportional to the local density of cortical actin c. This stress therefore has two components: a tangential component due to connection with nearby cortex

$$\sigma_t = \sigma_M w_c c \nabla y_C, \tag{S1}$$

and a normal stress due to connection with the cytoplasmic actin network

$$\sigma_n = \sigma_M c y_C. \tag{S2}$$

We find that the normal contractile force is necessary for asymetric bleb healing, as occurs during bleb travel. This necessity can be understood from Fig. 1A: In the absence of cytoplasmic actin, the tangential stress pulls the membrane tangentially, but there is no force driving the cortex into the place of the cell. Our goal is to understand in 3D. To this end, we find it informative to study simplified 2D systems and 1D systems as an analytical tool. The 2D model is equivalent to either the geometries shown in Supplemental Fig. 1C



Figure S1: Approximations of cortex and cytoplasmic actin geometry in 3D. (A-B) Bleb geometry in 3D including only tangential cortical contractility (A), and both tangential and normal contractility (B). (C-D) Representation of 2D model. (E) Hypothetical 1D "non-spatial" model corresponding to ODE system used in Main Text.

or D. The 1D model, which we refer to as the ODE model in the Main Text, corresponds to the geometry shown in Supplemental Fig. 1E.

Model parameter	Estimated value	Source
r	0.1/s	(11)
$k_{ m on}$	$100/\mu\mathrm{m}^2\cdot\mathrm{s}$	(21)
$k_{ m off}$	1/s	(11)
$k_A$	$10\mathrm{pN}/\mu m$	(21)
$\sigma_M$	$0.1 \mathrm{Pa}/\mu\mathrm{m}^2$	(21)
$\hat{\Pi}$	$100 \mathrm{Pa}/\mathrm{\mu m}$	(21)
$y_M^0$	$3\mu{ m m}$	(8)
$\gamma_M$	$100\mathrm{pN}/\mathrm{\mu m}$	(45)

Table S2: Estimates of parameters used in non-dimensionalization.

### **3** Parameter estimation

Using these estimates, the correspondence between dimensional and nondimensional parameters are given by

$$x = \chi \cdot 0.2 \,\mu\mathrm{m} \tag{S3}$$

$$t = \tau \cdot 10s \tag{S4}$$

$$a = A \cdot 100/\mu m^2 \tag{S5}$$

$$y_M = Y_M \cdot 3\,\mu\mathrm{m} \tag{S6}$$

$$y_C = Y_C \cdot 3\,\mu\mathrm{m}.\tag{S7}$$

Note that model parameters not included in Table S2 do not impact the non-dimensionalization.

### 4 Model variants

### 4.1 Bending

The inclusion of higher-order derivatives in the mechanical energy transform the system into a higher-order boundary value problem. For example, the bending energy term transforms the membrane shape equation to a fourthorder equation. We simulate the base model with the addition of bending terms  $\beta > 0$ , shown in Fig. S2. We find that the excitable parameter regime and traveling parameter regimes are unchanged. For  $\beta = 100$ , the velocity of travel is increased by approximately two-fold and healing is delayed compared to no bending.



Figure S2: Influence of membrane bending rigidity. (A) Traveling bleb on a uniform surface with no bending energy  $\beta = 0$ . (B) Traveling bleb with large bending rigidity  $\beta = 100$ . The bleb velocity is increased by approximately two-fold and healing is delayed (but eventually occurs, not shown).

### 5 Details of numerical method

### 5.1 Base model

The base model, Eqs. 10-13, comprise a two-dimensional boundary value problem of elliptic type at each instant in time, coupled to two first-order (in time) partial differential equations. To solve the base model, we discretize space into a uniform grid of width  $\Delta \chi = 0.1$  and time step size  $\Delta t = 0.01$ . We use a standard five-point stencil finite difference method in space and forward-Euler in time.

### 5.2 Non-uniform tension

The inclusion of non-uniform tension changes the boundary value problem to a non-uniform elliptic equation. The equations takes the form

$$P = f(\chi_1, \chi_2) Y_M(\chi_1, \chi_2) - \nabla \cdot (\Gamma(\chi_1, \chi_2) \nabla Y_M(\chi_1, \chi_2))$$
(S8)

where f and  $\Gamma$  are spatially varying. We use a uniform grid in space and set  $\Delta \chi = 0.1$ . The functions  $f, Y_M$  and  $\Gamma$  all live at cell edges  $(f|_{i,j} = f(i\Delta\chi, j\Delta\chi), i = 1, 2, ..., 2000)$  and we impose periodic boundary conditions. The parameter functions f and  $\Gamma$  must be interpolated to the edges, which we do by uniform averaging. The resulting discretization stencil is given by

$$P = \left(f|_{i,j} + \frac{1}{2\Delta x^2} \left(\gamma|_{i+1,j} + \gamma|_{i-1,j} + \gamma|_{i,j+1} + \gamma|_{i,j-1} + 4\gamma|_{i,j}\right) \mathbf{Y}_{\mathbf{M}}|_{\mathbf{i},\mathbf{j}} - \frac{1}{2\Delta x^2} \left((\gamma|_{i+1,j} + \gamma|_{i,j}) \mathbf{Y}_{\mathbf{M}}|_{\mathbf{i}+1,\mathbf{j}} + (\gamma|_{\mathbf{i},\mathbf{j}} + \gamma|_{\mathbf{i},\mathbf{j}-1}) \mathbf{Y}_{\mathbf{M}}|_{\mathbf{i}-1,\mathbf{j}}\right) - \frac{1}{2\Delta x^2} \left((\gamma|_{i,j} + \gamma|_{i,j+1}) \mathbf{Y}_{\mathbf{M}}|_{\mathbf{i},\mathbf{j}+1} + (\gamma|_{\mathbf{i},\mathbf{j}} + \gamma|_{\mathbf{i},\mathbf{j}-1}) \mathbf{Y}_{\mathbf{M}}|_{\mathbf{i},\mathbf{j}-1}\right)$$

Since this equation remains linear, it can be written into a sparse matrix and solved as a linear system.

### 5.3 Higher-order models including bending forces

Adding higher order terms, including bending forces, transforms the boundary value problem into a higher-order boundary value problem. The bending term, in particular, introduces a fourth-order bilaplacian operator. This significantly increases the computational cost of solving the equations, therefore we use a more sophisticated solver described here. We solve the following equations:

$$\frac{\partial C}{\partial t} = \alpha A - C \tag{S9}$$

$$\epsilon \frac{\partial A}{\partial t} = \frac{C}{1+C} \exp\left(-\left(\frac{1}{D}\frac{MC}{A+MC}Y_m\right)\right) - A \exp\left(\frac{1}{F_0}\frac{MC}{A+MC}Y_m\right)$$

$$I + C \qquad (DA + MC) \qquad (F_0A + MC) \qquad (S10)$$

$$P = hY_m - \nabla \cdot (\Gamma \nabla Y_m) + B \nabla^4 Y_m \tag{S11}$$

$$h = \frac{AMC}{A + MC} + P,\tag{S12}$$

where  $\alpha = 57, \epsilon = 0.1, D = 0.15, F_0 = 1, M = 0.007$  and P = 0.1. The nondimensional bending modulus is  $B \equiv \beta/\gamma x_c^3$ . In non-uniform tension models, B = 0 and the non-uniform tension term  $\Gamma = 1 + \theta C$  where  $\theta = 0.1$  or  $\theta = 0.2$ . For bending models,  $\Gamma = 1$  and  $B \in \{10^{-2}, 10^{-1}, 1, 10^1, 10^2\}$ .

All variables satisfy periodic conditions at all boundaries. The initial condition for  $Y_m$  and C is their steady state value  $Y_m^{ss} = 0.5582$  and  $C^{ss} = 15.8236$ . A is also set to steady state  $A^{ss} = 0.2776$  except that A = 0 where  $r = \sqrt{x^2 + y^2} < 5$ .

The system is solved in a square computational domain  $[-200, 200]^2$ . The domain is initialized to a  $64 \times 64$  mesh with a maximum of 5 refinement levels. At the finest level, grid length is  $400/(64 \times 2^5) \approx 0.2$ . The time step is  $10^{-2}$ .

We use the implicit second order Crank-Nicholson scheme for time discretization in Eqs. (S9) and (S10). Spatial derivatives are discretized using central difference approximations. Eq. (S11) is reformulated as a system of two second order equations. Block structured Cartesian refinement is used to efficiently resolve the multiple spatial scales. In particular, the mesh is refined in regions with large spatial gradients of  $Y_m$  (typically around the bleb). The equations at implicit time level are solved by the adaptive nonlinear multigrid method developed in (46).

### 6 Description of Supplemental Movies

- Supplemental Movie 1. We simulate the 2D model with boundary conditions at the top and bottom (12-o-clock and 6-o-clock). Corresponds to parameters in Fig. 4A
- Supplemental Movie 2. Stationary bleb in 3D. Corresponds in Fig 2B.
- Supplemental Movie 3. Traveling bleb in 3D on a uniform surface. Travel is unrestricted and the excitation spreads in all directions.
- Supplemental Movie 4. Traveling bleb with surface heterogeneity. Corresponds to Fig. 4B.
- Supplemental Movie 5. Traveling bleb with global pressure. Corresponds to Fig. 6A.

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