

**Supplementary Figure 1.** The local coordination environment in MAF-49·H<sub>2</sub>O (probability drawn at 30%). \* represents symmetrically generated atoms.



Supplementary Figure 2. TG curve of MAF-49·H<sub>2</sub>O.



**Supplementary Figure 3**. PXRD patterns of MAF-49 after heating/adsorption/desorption treatments.



**Supplementary Figure 4**. (a)  $C_2H_6$ , (b)  $C_2H_4$ , (c)  $CO_2$  and (d)  $CH_4$  adsorption (solid) and desorption (open) isotherms of MAF-49 measured at 298 (blue), 307 (black) and 316 (red) K.



**Supplementary Figure 5**. Virial fitting (lines) of the (a)  $C_2H_6$ , (b)  $C_2H_4$ , (c)  $CO_2$  and (d)  $CH_4$  adsorption isotherms (points) of MAF-49 measured at 298 (blue), 307 (black) and 316 (red) K.



**Supplementary Figure 6**. Langmuir–Freundlich fitting (lines) of the (a)  $C_2H_6$ , (b)  $C_2H_4$ , (c)  $CO_2$  and (d)  $CH_4$  adsorption isotherms (points) of MAF-49 measured at 316 K.



**Supplementary Figure 7.** Mixed isotherms and selectivity in MAF-49 predicted by IAST for equimolar mixtures of (a)  $C_2H_6/C_2H_4$ , (b)  $C_2H_6/CO_2$  and (c)  $C_2H_6/CH_4$  at 316 K.



**Supplementary Figure 8**. The steric hindrance and electrostatic repulsion between the two C-H moieties of the two methylene groups from the host channel neck and the guest  $C_2H_4$  (C3A···C6 = 3.88 Å, H31A···H62 = 2.10 Å) in MAF-49·C<sub>2</sub>H<sub>4</sub>.



**Supplementary Figure 9.** Comparison of the channel neck sizes (defined by The N8····C3 separation as shown in Figure 3) of MAF-49, MAF-49·C<sub>2</sub>H<sub>6</sub>, MAF-49·C<sub>2</sub>H<sub>4</sub>, MAF-49·CO<sub>2</sub> obtained by computational simulations and single-crystal X-ray diffraction.



**Supplementary Figure 10.** Comparison of the preferential (a)  $C_2H_6$ , (b)  $C_2H_4$  and (c)  $CO_2$  adsorption sites (Zn purple, C dark gray, H light gray, N blue, hydrogen atoms are omitted for clarity) observed by single-crystal X-ray diffraction (red) and PDFT calculation (green). Left and Right, the structures are projected along the channel neck and perpendicular to the channel neck, respectively.



**Supplementary Figure 11**. PXRD patterns of (a) HKUST-1, (b) MOF-74-Mg, (c) MOF-74-Co, (d) UiO-66, (e) MAF-3, (f) MAF-4 and (g) IRMOF-8 samples used in this work. Note that the IRMOF-8 sample adopt an interpenetrated structure, which has been commonly obtained in the literature and used for gas (such as  $H_2^{1}$  and  $C_2H_6/C_2H_4^{2,3}$ ) adsorption studies.



**Supplementary Figure 12**. Breakthrough curves of Figure 4 expressed using time (min) and specific breakthrough time (min g<sup>-1</sup>) as abscissa.



**Supplementary Figure 13.** Breakthrough curves of (a) 4:1 CH<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> mixture, (b) 1:1 CO<sub>2</sub>/C<sub>2</sub>H<sub>6</sub> mixture, and (c) 1:1 C<sub>2</sub>H<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> mixture for MAF-49. Left, specific injection amount (mmol g<sup>-1</sup>) as abscissa. Right, specific breakthrough time (min g<sup>-1</sup>) and breakthrough time (min) as abscissa. Lines are drawn to guide eyes.  $C_i$  and  $C_o$  are the concentrations of each gas at the inlet and outlet, respectively.



**Supplementary Figure 14**. The  $C_2H_6$  adsorption isotherms (left, lines are drawn to guide eyes) and Virial fitting (right, lines are fitting results) of (a) MAF-3, (b) MAF-4 and (c) IRMOF-8.



**Supplementary Figure 15**. Breakthrough curves of Figure 5 expressed using breakthrough time (min) and specific breakthrough time (min g<sup>-1</sup>) as abscissa.

Data Path : H:\LiaoPQ-GC-MS-20150526-R2\ Data File : MAF-49-1-1-C2H4-C2H6-MS-017.D Acq On : 31 Mar 2015 20:58 Operator : Sample Misc ALS Vial : 1 Sample Multiplier: 1 Integration Parameters: rteint.p Integrator: RTE Smoothing : ON Filtering: 5 Sampling : 1 Min Area: 3 % of largest Peak Start Thrs: 0.2 Max Peaks: 100 Stop Thrs : 0 Peak Location: TOP If leading or trailing edge < 100 prefer < Baseline drop else tangent > Peak separation: 5 Method : E:\data\Jennifer\Flow throught system\GC methods\5PAHs\_3Pesticides\_liquid injection\_splitless.M Title : Signal : EIC Ion 28.00 (27.70 to 28.70): MAF-49-1-1-C2H4-C2H6-MS-017.D\data.ms peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total --- ----- ---- ---- --- ----- ----1 0.919 306 321 394 rM 4 2402897 64363059 100.00% 100.000% Sum of corrected areas: 64363059 Signal : EIC Ion 30.00 (29.70 to 30.70): MAF-49-1-1-C2H4-C2H6-MS-017.D\data.ms peak R.T. first max last PK peak corr. corr. % of

# min scan scan scan TY height area % max. total

1 0.912 307 318 363 rM 4 3536 9848 100.00% 100.000%

Sum of corrected areas: 9848

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**Supplementary Figure 16**. GC-MS spectra of the outlet gas (top:  $C_2H_4$ , bottom  $C_2H_6$ ) showing  $C_2H_4$  purity of 99.98% given by MAF-49 for a single breakthrough operation using 1:1  $C_2H_4/C_2H_6$  as input.

Data Path : H:\LiaoPQ-GC-MS-20150526-R2\ Data File : MAF-3-1-1-C2H4-C2H6-010.D Acq On : 3 Apr 2015 8:20 Operator : Sample Misc ALS Vial : 1 Sample Multiplier: 1 Integration Parameters: rteint.p Integrator: RTE Smoothing : ON Filtering: 5 Min Area: 3 % of largest Peak Sampling : 1 Max Peaks: 100 Start Thrs: 0.2 Stop Thrs : 0 Peak Location: TOP If leading or trailing edge < 100 prefer < Baseline drop else tangent > Peak separation: 5 Method : E:\data\Jennifer\Flow throught system\GC methods\5PAHs\_3Pesticides\_liquid injection\_splitless.M Title Signal : EIC Ion 28.00 (27.70 to 28.70); MAF-3-1-1-C2H4-C2H6-010.D\data.ms peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total 1 0.973 336 351 407 rBV3 7522564 136112261 100.00% 100.000% Sum of corrected areas: 136112261 : EIC Ion 30.00 (29.70 to 30.70): MAF-3-1-1-C2H4-C2H6-010.D\data.ms Signal peak R.T. first max last PK peak corr. corr. % of

# min scan scan scan TY height area % max. total

1 0.973 340 351 376 rVB3 47344 497102 100.00% 100.000%

Sum of corrected areas: 497102

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**Supplementary Figure 17**. GC-MS spectra of the outlet gas (top:  $C_2H_4$ , bottom  $C_2H_6$ ) with  $C_2H_4$  purity of 99.5% given by MAF-3 for a single breakthrough operation using 1:1  $C_2H_4/C_2H_6$  as input.

Data Path : H:\LiaoPQ-GC-MS-20150526-R2\ Data File : MAF-4-1-1-C2H4-C2H6-001.D Acq On : 1 Apr 2015 17:34 Operator : Sample Misc ALS Vial : 1 Sample Multiplier: 1 Integration Parameters: rteint.p Integrator: RTE Smoothing : ON Filtering: 5 Sampling : 1 Min Area: 3 % of largest Peak Start Thrs: 0.2 Max Peaks: 100 Peak Location: TOP Stop Thrs : 0 If leading or trailing edge < 100 prefer < Baseline drop else tangent > Peak separation: 5

Method : E:\data\Jennifer\Flow throught system\GC methods\5PAHs\_3Pesticides\_liquid injection\_splitless.M Title :

Signal : EIC Ion 28.00 (27.70 to 28.70): MAF-4-1-1-C2H4-C2H6-001.D\data.ms

peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total --- ------

1 0.965 329 347 389 rM 5 3243520 44270812 100.00% 100.000%

Signal : EIC Ion 30.00 (29.70 to 30.70): MAF-4-1-1-C2H4-C2H6-001.D\data.ms

peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total

 $1 \quad 0.963 \quad 335 \quad 346 \quad 366 \ \text{rM} \ 5 \quad 68997 \quad 142241 \ 100.00\% \ 100.000\%$ 

Sum of corrected areas: 142241

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**Supplementary Figure 18**. GC-MS spectra of the outlet gas (top:  $C_2H_4$ , bottom  $C_2H_6$ ) with  $C_2H_4$  purity of 99.6% given by MAF-4 for a single breakthrough operation using 1:1  $C_2H_4/C_2H_6$  as input.

Data Path : H:\LiaoPQ-GC-MS-20150526-R2\ Data File : IRMOF-8-1-1-C2H4-C2H6-MS-05.D Acq On : 31 Mar 2015 23:07 Operator Sample Misc ALS Vial : 1 Sample Multiplier: 1 Integration Parameters: rteint.p Integrator: RTE Smoothing : ON Filtering: 5 Sampling : 1 Min Area: 3 % of largest Peak Start Thrs: 0.2 Max Peaks: 100 Stop Thrs : 0 Peak Location: TOP If leading or trailing edge < 100 prefer < Baseline drop else tangent > Peak separation: 5 Method : E:\data\Jennifer\Flow throught system\GC methods\5PAHs\_3Pesticides\_liquid injection\_splitless.M Title Signal : EIC Ion 28.00 (27.70 to 28.70): IRMOF-8-1-1-C2H4-C2H6-MS-05.D\data.ms peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total --- ----- ----- ---- ---- ----- -----1 0.884 288 308 423 rM 4 6957820 549710224 100.00% 100.000% Sum of corrected areas: 549710224 Signal : EIC Ion 30.00 (29.70 to 30.70): IRMOF-8-1-1-C2H4-C2H6-MS-05.D\data.ms peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total

1 0.892 297 311 370 rM 4 10959 439160 100.00% 100.000%

Sum of corrected areas: 439160

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**Supplementary Figure 19**. GC-MS spectra of the outlet gas (top:  $C_2H_4$ , bottom  $C_2H_6$ ) with  $C_2H_4$  purity of 99.9% given by IRMOF-8 for a single breakthrough operation using 1:1  $C_2H_4/C_2H_6$  as input.



**Supplementary Figure 20**. Breakthrough curves of a complete adsorption-desorption cycle using 1:1  $C_2H_4/C_2H_6$  mixture for MAF-49 (1.346 g sample was used, corresponding to an apparent density of 0.811 g cm<sup>-3</sup> a column voidage of 0.452; The mixed gas and He flow rates are both 0.6 cm<sup>3</sup> min<sup>-1</sup>). Solid symbols:  $C_2H_4$ , Open symbols:  $C_2H_6$ . Lines are drawn to guide eyes.  $C_i$  and  $C_o$  are the concentrations of each gas at the inlet and outlet, respectively.

Data Path : H:\LiaoPQ-GC-MS-20150526-R2\ Data File : MAF-49-15-1-C2H4-C2H6-011.D Acq On : 4 Apr 2015 21:11 Operator : Sample Misc ALS Vial : 1 Sample Multiplier: 1 Integration Parameters: rteint.p Integrator: RTE Smoothing : ON Filtering: 5 Sampling : 1 Min Area: 3 % of largest Peak Start Thrs: 0.2 Max Peaks: 100 Stop Thrs : 0 Peak Location: TOP If leading or trailing edge < 100 prefer < Baseline drop else tangent > Peak separation: 5 Method : E:\data\Jennifer\Flow throught system\GC methods\5PAHs\_3Pesticides\_liquid injection\_splitless.M Title Signal : EIC Ion 28.00 (27.70 to 28.70); MAF-49-15-1-C2H4-C2H6-011.D\data.ms peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total -- ---- ---- ----- ------ -1 0.971 319 343 384 rM 2 4851775 135146886 100.00% 100.000% Sum of corrected areas: 135146886 Signal : EIC Ion 30.00 (29.70 to 30.70): MAF-49-15-1-C2H4-C2H6-011.D\data.ms peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total 1 0.971 320 343 365 rM 2 2723 5575 100.00% 100.000%

Sum of corrected areas: 5575

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**Supplementary Figure 21**. GC-MS spectra of the outlet gas (top:  $C_2H_4$ , bottom  $C_2H_6$ ) with  $C_2H_4$  purity of 99.995% given by MAF-49 for a single breakthrough operation using 15:1  $C_2H_4/C_2H_6$  as input.

Data Path : H:\LiaoPQ-GC-MS-20150526-R2\ Data File : MAF-3-15-1-C2H4-C2H6-013.D Acq On : 5 Apr 2015 9:02 Operator : Sample Misc ALS Vial : 1 Sample Multiplier: 1 Integration Parameters: rteint.p Integrator: RTE Smoothing : ON Filtering: 5 Sampling : 1 Min Area: 3 % of largest Peak Max Peaks: 100 Start Thrs: 0.2 Stop Thrs : 0 Peak Location: TOP If leading or trailing edge < 100 prefer < Baseline drop else tangent > Peak separation: 5 Method : E:\data\Jennifer\Flow throught system\GC methods\5PAHs\_3Pesticides\_liquid injection\_splitless.M Title Signal : EIC Ion 28.00 (27.70 to 28.70): MAF-3-15-1-C2H4-C2H6-013.D\data.ms peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total --- ----- ----- ---- ---- ----- -----1 0.989 339 351 400 rBV2 291584 2571186 100.00% 100.000% 2571186 Sum of corrected areas: Signal : EIC Ion 30.00 (29.70 to 30.70): MAF-3-15-1-C2H4-C2H6-013.D\data.ms peak R.T. first max last PK peak corr. corr. % of

# min scan scan scan TY height area % max. total

1 0.989 343 351 374 rM 2 5191 8602 100.00% 100.000%

Sum of corrected areas: 8602

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**Supplementary Figure 22**. GC-MS spectra of the outlet gas (top:  $C_2H_4$ , bottom  $C_2H_6$ ) with  $C_2H_4$  purity of 99.6% given by MAF-3 for a single breakthrough operation using 15:1  $C_2H_4/C_2H_6$  as input.

Data Path : H:\LiaoPQ-GC-MS-20150526-R2\ Data File : MAF-4-15-1-C2H4-C2H6-011.D Acq On : 5 Apr 2015 8:57 Operator : Sample Misc ALS Vial : 1 Sample Multiplier: 1 Integration Parameters: rteint.p Integrator: RTE Smoothing : ON Filtering: 5 Sampling : 1 Min Area: 3 % of largest Peak Start Thrs: 0.2 Max Peaks: 100 Stop Thrs : 0 Peak Location: TOP If leading or trailing edge < 100 prefer < Baseline drop else tangent > Peak separation: 5 Method : E:\data\Jennifer\Flow throught system\GC methods\5PAHs\_3Pesticides\_liquid injection\_splitless.M Title Signal : EIC Ion 28.00 (27.70 to 28.70): MAF-4-15-1-C2H4-C2H6-011.D\data.ms peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total --- ---- ---- ---- ---- ----1 0.995 347 359 449 rM 2 4881389 22194158 100.00% 100.000% Sum of corrected areas: 22194158 : EIC Ion 30.00 (29.70 to 30.70): MAF-4-15-1-C2H4-C2H6-011.D\data.ms Signal peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total . .... .... ....

1 0.997 349 360 383 rM 2 6935 12090 100.00% 100.000%

Sum of corrected areas: 12090

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**Supplementary Figure 23**. GC-MS spectra of the outlet gas (top:  $C_2H_4$ , bottom  $C_2H_6$ ) with  $C_2H_4$  purity of 99.9% given by MAF-4 for a single breakthrough operation using 15:1  $C_2H_4/C_2H_6$  as input.

Data Path : H:\LiaoPQ-GC-MS-20150526-R2\ Data File : IRMOF-8-15-1-C2H4-C2H6-MS-009.D Acq On : 31 Mar 2015 20:39 Operator : Sample Misc ALS Vial : 1 Sample Multiplier: 1 Integration Parameters: rteint.p Integrator: RTE Smoothing : ON Filtering: 5 Sampling : 1 Min Area: 3 % of largest Peak Start Thrs: 0.2 Max Peaks: 100 Stop Thrs: 0 Peak Location: TOP If leading or trailing edge < 100 prefer < Baseline drop else tangent > Peak separation: 5 Method : E:\data\Jennifer\Flow throught system\GC methods\5PAHs\_3Pesticides\_liquid injection\_splitless.M Title Signal : EIC Ion 28.00 (27.70 to 28.70): IRMOF-8-15-1-C2H4-C2H6-MS-009.D\data.ms peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total --- ----- ----- ---- ---- -----1 0.929 319 332 410 rM 4 2778384 76935635 100.00% 100.000% Sum of corrected areas: 76935635 : EIC Ion 30.00 (29.70 to 30.70): IRMOF-8-15-1-C2H4-C2H6-MS-009.D\data.ms Signal peak R.T. first max last PK peak corr. corr. % of # min scan scan scan TY height area % max. total 1 0.948 316 340 372 rM 4 12216 26104 100.00% 100.000%

Sum of corrected areas: 26104

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**Supplementary Figure 24**. GC-MS spectra of the outlet gas (top:  $C_2H_4$ , bottom  $C_2H_6$ ) with  $C_2H_4$  purity of 99.96% given by IRMOF-8 for a single breakthrough operation using 15:1  $C_2H_4/C_2H_6$  as input.



Supplementary Figure 25. The column breakthrough experiment setup.

	CO <sub>2</sub>	CH <sub>4</sub>	C <sub>2</sub> H <sub>6</sub>	$C_2H_4$
Kinetic diameter (Å)	3.3	3.758	4.443	4.163
Polarizability (× $10^{25}$ cm <sup>3</sup> )	29.11	25.93	44.3-44.7	42.52
Quadruple moment ( $\times 10^{26}$ esu cm <sup>2</sup> )	4.30	0	0.65	1.50
Boiling point (K)	194.75	111.6	184.55	169.42

**Supplementary Table 1**. Physical parameters of CO<sub>2</sub>, C<sub>2</sub>H<sub>6</sub> and CH<sub>4</sub><sup>4, 5</sup>.

Supplementary Table 2. Crystal Data and Structure Refinement results.

Complex	MAF-49	MAF-49·H <sub>2</sub> O	$MAF-49 \cdot C_2 H_4$	MAF-49·CO <sub>2</sub>	$MAF-49 \cdot C_2 H_6$
Formula	C <sub>5</sub> H <sub>6</sub> N <sub>8</sub> Zn	$C_5H_7N_8O_{0.5}Zn$	$C_{5.78}H_{7.56}N_8Zn$	$C_{5.14}H_6N_8O_{0.27}Zn$	$C_{5.67}H_8N_8Zn$
Formula weight	243.57	252.56	254.50	249.56	253.62
Temperature (K)	195(2)	195(2)	195(2)	195(2)	195(2)
Space group	P3 <sub>1</sub> 21	P3 <sub>1</sub> 21	P3 <sub>1</sub> 21	<i>P</i> 3 <sub>1</sub> 21	P3 <sub>1</sub> 21
a/Å	9.6963(15)	9.6767(14)	9.6896(16)	9.7682(15)	9.663(3)
c/Å	20.126(3)	20.172(3)	20.153(4)	20.100(4)	20.224(5)
V/Å <sup>3</sup>	1638.7(4)	1635.8(4)	1638.6(5)	1660.9(5)	1635.2(8)
Z	6	6	6	6	6
$D_{\rm c}/{\rm g~cm^{-3}}$	1.481	1.538	1.547	1.499	1.550
$R_{ m int}$	0.0192	0.0340	0.0254	0.0393	0.0529
$R_1[I > 2\sigma(I)]$	0.0184	0.0369	0.0337	0.0422	0.0448
$wR_2$ (all data)	0.0438	0.0994	0.1028	0.1313	0.1203
GOF	1.060	1.051	1.059	1.052	1.008
Flack	0.003(10)	-0.02(2)	-0.01(2)	-0.01(3)	-0.02(3)
Peak and hole (e Å <sup><math>-3</math></sup> )	0.293 and -0.249	0.579 and -0.405	0.986 and -0.368	1.281 and -0.423	0.656 and -0.633

 $R_1 = \sum ||F_0| - |F_c|| / \sum |F_0|. \ wR_2 = [\sum w(F_0^2 - F_c^2)^2 / \sum w(F_0^2)^2]^{1/2}.$ 

Compound	From adsorption isotherms (kJ mol <sup>-1</sup> )	From GCMC/PDFT simulation (kJ mol <sup>-1</sup> )
MAF-49·CO <sub>2</sub>	30	31
MAF-49· $C_2H_4$	48	47
MAF-49·C <sub>2</sub> H <sub>6</sub>	60	56

**Supplementary Table 3**. Comparison for the binding energies between adsorption isotherms and GCMC/PDFT simulations.

$C_2H_6$ $C_2H_4$				$CO_2$							
	D…A	Н…А	∠D-H…A		D····A	Н…А	∠D-H…A		D…A	Н…А	∠D-H…A
	(Å)	(Å)	(°)		(Å)	(Å)	(°)		(Å)	(Å)	(°)
C6-H61N8	3.23	2.15	168					C6…N8	2.91		
C7-H71N1A	3.47	2.40	162	C6-H61N8	3. 58	2.54	161	C6…N8A	2.91		
C6-H62···N8A/N3A	2.86/3.38	2.15/2.70	120/120	C7-H71N2A	3.57	2.65	142	С3-Н31…О1	3.34	2.46	135
C6-H63…N2	4.15	3.26	140					СЗА-НЗ1А…О1А	3.34	2.46	135
C7-H72…N6B	4.59	3.59	152	C6-H62…N6	5.20	4.41	134				
C7-H73··N4C	5.05	4.03	155	C7-H71…N3	6.51	5.52	154				

Supplementary Table 4. The interactions between the gas molecules and host framework in MAF-49.

Symmetric codes: A = 1+*x*-*y*, 2-*y*, 0.6667-*z*; B = 1+*x*-*y*, 1-*y*, 0.6667-*z*; C = -1-*x*+*y*, 1-*x*, -0.33333+*z*; D = *x*-*y*, 1-*y*, 0.6667-*z*.

Materials	Sample weight	Crystal density	Apparent density	Apparent density	
	(g)	$(g \text{ cm}^{-3})$	$(g \text{ cm}^{-3})$	Column voidage	(cm <sup>3</sup> )
MAF-49	1.873	1.481	1.128	0.238	0.395
IRMOF-8	1.063	0.896	0.640	0.285	0.474
MAF-4	1.316	1.067	0.793	0.257	0.427
MAF-3	1.472	1.241	0.887	0.285	0.473
HKUST-1	1.119	0.879	0.674	0.233	0.387
MOF-74-Mg	1.147	0.920	0.691	0.249	0.413
MOF-74-Co	1.374	1.170	0.827	0.293	0.485
UiO-66	1.531	1.198	0.922	0.230	0.382

**Supplementary Table 5**. Comparing the parameters of the breakthrough columns studied in this work.

Apparent density = Sample weight / Column volume

Column voidage = 1 - Sample weight / Crystal density / Column volume

Column free space = Column volume × Column voidage

		Gravimetric/Volumetric productivity (mmol g <sup>-1</sup> /mmol cm <sup>-3</sup> ) with					
			different purities				
Matorials	Crystal density	00.05%	00.5%	000/			
Materials	$(g \text{ cm}^{-3})$	99.9370+	99.370+	9970 <del>-</del>			
MAF-49	1.480	0.28/0.42	0.30/0.45	0.32/0.47			
IRMOF-8	0.896	0/0	0.05/0.04	0.11/0.10			
MAF-4	1.067	0/0	0.02/0.02	0.03/0.03			
MAF-3	1.241	0/0	0.004/0.005	0.01/0.01			

**Supplementary Table 6**. Comparing the  $C_2H_4$  productivities of  $C_2H_6$  selective adsorbents for a single breakthrough operation using 1:1  $C_2H_4/C_2H_6$  as input.

**Supplementary Table 7**. Comparing the  $C_2H_4$  productivities of  $C_2H_6$  selective adsorbents for a single breakthrough operation using 15:1  $C_2H_4/C_2H_6$  as input.

		Gravimetric/Volumetric productivity (mmol g <sup>-1</sup> /mmol cm <sup>-3</sup> ) with					
		different puritties					
Materials	Crystal density (g cm <sup>-3</sup> )	99.995%+	99.95%+	99.5%+	99%+		
MAF-49	1.480	1.48/2.17	1.68/2.48	2.07/2.97	2.46/3.70		
IRMOF-8	0.896	0/0	0.06/0.05	0.15/0.13	0.22/0.21		
MAF-4	1.067	0/0	0/0	0.004/0.004	0.015/0.016		
MAF-3	1.241	0/0	0/0	0.001/0.001	0.006/0.008		

# Supplementary Methods.

## **Calculations of adsorption enthalpies**

The coverage-dependent adsorption enthalpy profiles were calculated from the sorption data measured at 298, 307 and 316 K by the Virial fitting method and Clausius-Claperyron equation.

**Virial fitting:** A Virial-type expression was used (eq. 1), which is composed of parameters  $a_i$  and  $b_i$ , which are independent of temperature. In eq. 1, *P* is the pressure in atm, *N* is the adsorbed amount in mmol g<sup>-1</sup>, *T* is the temperature in Kelvin,  $a_i$  and  $b_i$  are the Virial coefficients, and *m* and *n* represent the numbers of coefficients required to adequately describe the isotherms.

$$\ln p = \ln n + \frac{1}{T} \sum_{i=0}^{l} a_{i} n^{i} + \sum_{j=0}^{m} b_{j} n^{j} \qquad (1)$$
$$K_{H} = \exp(-b_{0}) \times \exp(\frac{-a_{0}}{T}) \qquad (2)$$

The adsorption enthalpy ( $\Delta H$ ) is obtained from the following equation derived from the Clausius-Clapeyron equation (eq. 3).

$$Q_{st} = -R \left[ \frac{\partial \ln p}{\partial (1/\mathrm{T})} \right]_n = -R \sum_{i=0}^l a_i n^i \quad (3)$$

### Breakthrough measurements.

A stainless-steel column with a length of 10 cm and an internal diameter of 0.46 cm ( $V_{column} = 0.23 \times 0.23 \times 3.14 \times 10.0 = 1.66 \text{ cm}^3$ ) was packed with microcrystalline sample. The sample in each column was compressed as much as possible to obtain the best separation performance, and column voidages are similar for different samples. As shown in the above scheme, the column was connected to the GC by stainless-steel pipes with a combined length of 40 cm and an internal diameter of 0.30 cm ( $V_{tube} = 0.150 \times 0.150 \times 3.14 \times 40 = 2.84 \text{ cm}^3$ ). The column and most parts of the pipelines between the injection and sampling ports were placed in a temperature-controlling oven. The flow rates (cm<sup>3</sup> min<sup>-1</sup> at 298.15 K and 1 bar) of pure gases were regulated by mass flow controllers. Before breakthrough experiments, the columns were heated at 323 K for 10 hours and then cooled to the measurement temperature of 313(1) K, during which pure He flow (2.0 cm<sup>3</sup> min<sup>-1</sup>) was kept passing through the columns. Pure gases were mixed by passing through the gas-mixing jar and then used

directly. Except otherwise specified, the mixed gas flow rates are 0.8, 0.2, and 1.6 cm<sup>3</sup> min<sup>-1</sup> for the breakthrough operations using 1:1:1:1 CH<sub>4</sub>/CO<sub>2</sub>/C<sub>2</sub>H<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>, 1:1 C<sub>2</sub>H<sub>4</sub>/C<sub>2</sub>H<sub>6</sub>, and 15:1 C<sub>2</sub>H<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> as inputs, respectively. The gas stream at the outlet of the column was analyzed on line by using a chromatographic analyzer (Agilent 7890A) with a thermal conductivity detector (TCD) and an HP-AL/S column or an Agilent 5975C Mass Spectrometer (MS) with the injection mode in manual.

Absolute and relative concentrations of each gas at the inlet and outlet are expressed by molar ratio. To compare the performances of different materials unambiguously, the specific injection amount  $\tau$  (mmol g<sup>-1</sup>) was used as the abscissa, meaning that the breakthrough time (min) was not only divided by the adsorbent weight (g) but also multiplied by the flow rate of the injection gas (mmol min<sup>-1</sup>). For comparison, breakthrough curves using breakthrough time (min) and specific breakthrough time (min g<sup>-1</sup>) as abscissa were also provided in the supplementary information.

The breakthrough curves were expressed by

$$f(\tau) = \frac{C_{o}(\mathbf{j}, \tau)}{C_{i}(\mathbf{j})}$$
(4)

Where  $C_o(j, \tau)$  is the TCD peak area of gas j at the outlet at  $\tau$  and  $C_i(j)$  is the TCD peak area of gas j at the inlet (not change with  $\tau$ ). The purity of gas j (*i.e.* the molar ratio of gas j in the outlet gas mixture containing n types of gases) can be expressed by

$$g(\tau) = \frac{C_{o}(j, \tau)}{\sum_{j=1}^{n} C_{o}(j, \tau)} \times 100\%$$
 (5)

To achieve a sufficient resolution for GC capillary column before TCD analyses, the outlet gas analytes need to be diluted by large amounts of protective gas He. Therefore, gas j could not be detected by TCD when the  $g(\tau)$  is lower than about 1%. To obtain the accurate concentrations and purities for the C<sub>2</sub>H<sub>4</sub>/C<sub>2</sub>H<sub>6</sub> breakthrough experiments, the MS peak areas of C<sub>2</sub>H<sub>4</sub> and C<sub>2</sub>H<sub>6</sub> were used, in which the C<sub>2</sub>H<sub>4</sub> purity was expressed by

$$g(\tau) = \frac{M_{o}(C_{2}H_{4}, \tau)}{M_{o}(C_{2}H_{4}, \tau) + M_{o}(C_{2}H_{6}, \tau)/0.8} \times 100\%$$
(6)

Where  $M_0(C_2H_4, \tau)$  and  $M_0(C_2H_6, \tau)$  are the MS peak areas of  $C_2H_4$  and  $C_2H_6$  at  $\tau$ , respectively.

The C<sub>2</sub>H<sub>4</sub> productivity (*q*) is defined by the breakthrough amount of C<sub>2</sub>H<sub>4</sub>, which is calculated by integration of the breakthrough curve  $f(\tau)$  during a period from  $\tau_1$  to  $\tau_2$  where the C<sub>2</sub>H<sub>4</sub> purity is higher than or equal to a threshold value *p* (such as 99.95%):

$$q = \frac{C_{i}(C_{2}H_{4})}{C_{i}(C_{2}H_{4}) + C_{i}(C_{2}H_{6})} \times (\int_{\tau_{1}}^{\tau_{2}} f(\tau)d\tau), \ (g(\tau) \ge p)$$
(7)

### **Computational Details.**

All simulations/calculations were performed by the Materials Studio 5.5 package. The preferred sorption locations were searched through Grand Canonical Monte Carlo (GCMC) simulations by using the fixed loading task and Metropolis method in the sorption calculation module. For all the GCMC simulations, the simulation box was set with 8 ( $2 \times 2 \times 2$ ) unit cells while all the frameworks and the gas molecules were described by the universal forcefield (UFF). Both the framework and the gas molecules were regarded as rigid model and the QEq partial charges and QEq charges were employed to the atoms of the framework and guest molecules, respectively. The cutoff distance was set to 18.5 Å for the Lennard-Jones (LJ) interactions, and the electrostatic interactions and the van der Waals interactions were handled using the Ewald and Atom based summation method, respectively. The loading steps, equilibration steps and the production steps were all set to  $1.0 \times 10^7$ . The saturation/maximum uptakes were modeled at 316 K using the fixed pressure task and Metropolis method with  $2.0 \times 10^7$  equilibration steps, followed by  $2.0 \times 10^7$  production steps for computing the ensemble averages.

All energies were calculated by the periodic density functional theory (PDFT) method by the Dmol<sup>3</sup> module. Before the energy calculations, full geometry optimizations with fixed cell parameters were performed to the host-guest systems based on the adsorption conformations obtained from GCMC simulation. The widely used generalized gradient approximation (GGA) with the Perdew-Burke-Ernzerhof (PBE) functional and the double numerical plus d-functions (DNP) basis set, TS for DFT-D correction as well as the Effective Core Potentials (ECP) were used. The energy, force and displacement convergence criterions were set as  $1 \times 10^{-5}$  Ha,  $2 \times 10^{-3}$  Ha and  $5 \times 10^{-3}$  Å, respectively. The energy balance is expressed by the following equations:

$$\Delta E_{\rm ads} = E_{\rm host+guest} - E_{\rm apohost} - E_{\rm guest} \tag{8}$$

$$\Delta E_{\rm trans} = E_{\rm host} - E_{\rm apohost} \tag{9}$$

$$\Delta E_{\rm fitting} = E_{\rm host+guest} - E_{\rm host} - E_{\rm guest} \tag{10}$$

Where  $\Delta E_{ads}$  is the adsorption enthalpy,  $\Delta E_{trans}$  is the energy change of the host framework after adsorption of guest,  $\Delta E_{fitting}$  is the interaction energy between the guest and the final host framework, and  $E_{host+guest}$ ,  $E_{guest}$ ,  $E_{apohost}$  and  $E_{host}$  are the energies of the final host-guest system, the free guest, the guest-free host framework, and the transformed host framework after adsorption, respectively.

### **Supplementary References**

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