Coexistence of multiple minor states of fatty acid binding protein and their functional relevance

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## Calculation of RD rates and CEST intensities for exchange models I and IV

The theoretical relaxation rate at a given CPMG field strength ( $v_{CPMG}$ ) was calculated by

$$R_n^{cal} = \frac{-\ln[M_{n\tau}(2)/M_0(2)]}{T_{CPMG}},$$
[1]

where  $T_{CPMG} = 4n\tau$  and  $v_{CPMG} = n/T_{CPMG}$ ,  $T_{CPMG}$  is the total time of the CPMG period,  $\tau$  is half of the delay between the centers of two successive 180° pulses, 2n is number of CPMG pulses;  $M_{n\tau}(2)$  and  $M_0(2)$  are the second element of magnetization vector  $M_{n\tau}$  and  $M_0$ , respectively,  $M_0 = [p_1 \ p_2 \ p_3]^T$  or  $[p_1 \ p_2 \ p_3 \ p_4]^T$  for 3state or 4-state exchange,  $p_j$  is the population of state j (j=1, 2, 3, 4; which correspond to state I<sub>1</sub>, N, I<sub>2</sub>, and I<sub>3</sub> in scheme 1 in the main text);  $M_{n\tau}$  is given by

$$M_{n\tau} = [\exp(-B\tau)^* \exp(-B^*\tau)^* \exp(-B^*\tau)^* \exp(-B\tau)]^n * M_0,$$
[2]

where B is the exchange matrix and  $B^*$  is the conjugate of B. For a 3-state exchange (model I), B is given by

$$B = \begin{bmatrix} R_{21} + k_{12} + i\Omega_1 & -k_{21} & 0\\ -k_{12} & R_{22} + k_{21} + k_{23} + i\Omega_2 & -k_{32}\\ 0 & -k_{23} & R_{23} + k_{32} + i\Omega_3 \end{bmatrix}.$$
[3]

For a 4-state exchange (model IV), B is given by

$$B = \begin{bmatrix} R_{21} + k_{12} + i\Omega_1 & -k_{21} & 0 & 0 \\ -k_{12} & R_{22} + k_{21} + k_{23} + k_{24} + i\Omega_2 & -k_{32} & -k_{42} \\ 0 & -k_{23} & R_{23} + k_{32} + i\Omega_3 & 0 \\ 0 & -k_{24} & 0 & R_{24} + k_{42} + i\Omega_4 \end{bmatrix}.$$
 [4]

In eqs. 3 and 4,  $R_{2j}$  and  $\Omega_j$  are the transverse relaxation rate and resonant frequency (in radians per second) of a spin at state j, respectively;  $k_{jk}$  is the conversion rate from state j to state k;  $i = \sqrt{-1}$ .

The theoretical intensity of a spin at state N (or state 2) at a given weak rf field was calculated by

$$I^{cal} = M(6), \tag{5}$$

where M(6) is the 6<sup>th</sup> element of magnetization vector M. M is given by

$$M = \exp(-At)M_0,$$
[6]

where  $M_0$  is the initial magnetization vector and equal to  $[0\ 0\ p_1\ 0\ 0\ p_2\ 0\ 0\ p_3]^T$  for a 3-state exchange and  $[0\ 0\ p_1\ 0\ 0\ p_2\ 0\ 0\ p_3\ 0\ 0\ p_4]^T$  for a 4-state exchange; t is the saturation time; A is an exchange matrix. For a 3-state model (model I), A is given by

	$R_{21} + k_{12}$	$-\Delta \omega_{\rm l}$	$\mathcal{O}_{y}$	$-k_{21}$	0	0	0	0	0 ]	
	$\Delta \omega_{\rm l}$	$R_{21} + k_{12}$	$-\omega_x$	0	$-k_{21}$	0	0	0	0	
	$-\omega_{y}$	$\omega_{x}$	$R_{11} + k_{12}$	0	0	$-k_{21}$	0	0	0	
	$-k_{12}$	0	0	$R_{22} + k_{21} + k_{23}$	$-\Delta \omega_2$	$\mathcal{O}_{y}$	$-k_{32}$	0	0	. [7]
A =	0	$-k_{12}$	0	$\Delta \omega_{2}$	$R_{22} + k_{21} + k_{23}$	$-\omega_{x}$	0	$-k_{32}$	0	
	0	0	$-k_{12}$	$-\omega_{y}$	$\mathcal{O}_x$	$R_{12} + k_{21} + k_{23}$	0	0	$-k_{32}$	
	0	0	0	$-k_{23}$	0	0	$R_{23} + k_{32}$	$-\Delta \omega_{3}$	$\omega_{y}$	
	0	0	0	0	$-k_{23}$	0	$\Delta \omega_{3}$	$R_{23} + k_{32}$	$-\omega_x$	
	0	0	0	0	0	$-k_{23}$	$-\omega_{y}$	$\mathcal{O}_x$	$R_{13} + k_{32}$	

For a 4-state model (model IV), A is given by

	$R_{21} + k_{12}$	$-\Delta \varphi$	$\mathcal{O}_{y}$	$-k_{21}$	0	0	0	0	0	0	0	0 ]	
	$\Delta \varphi$	$R_{21} + k_{12}$	$-\omega_{x}$	0	$-k_{21}$	0	0	0	0	0	0	0	
	$-\omega_{y}$	$\mathcal{Q}_{x}$	$R_{11} + k_{12}$	0	0	$-k_{21}$	0	0	0	0	0	0	
	$-k_{12}$	0	0	$R_{22} + k_{21} + k_{23} + k_{24}$	$-\Delta q$	$\mathcal{Q}_{y}$	$-k_{32}$	0	0	$-k_{42}$	0	0	
	0	$-k_{12}$	0	$\Delta q_2$	$R_{22} + k_{21} + k_{23} + k_{24}$	$\mathcal{O}_{x}$	0	$-k_{32}$	0	0	$-k_{42}$	0	[8]
A=	0	0	$-k_{12}$	$-\omega_{y}$	$\mathcal{Q}_{x}$	$R_{12} + k_{21} + k_{23} + k_{24}$	0	0	$-k_{32}$	0	0	$-k_{42}$	. [0]
	0	0	0	$-k_{23}$	0	0	$R_{23} + k_{32}$	-Δığ	$\mathcal{O}_{\mathcal{Y}}$	0	0	0	
	0	0	0	0	$-k_{23}$	0	Δą	$R_{23}+k_{32}$	$-\omega_{x}$	0	0	0	
	0	0	0	0	0	$-k_{23}$	$-\omega_{y}$	$\mathcal{O}_{x}$	$R_{13} + k_{32}$	0	0	0	
	0	0	0	$-k_{24}$	0	0	0	0	0	$R_{24} + k_{42}$	$-\Delta q$	$\omega_{y}$	
	0	0	0	0	$-k_{24}$	0	0	0	0	$-\Delta q$	$R_{24} + k_{42}$	$-\omega_{x}$	
	0	0	0	0	0	$-k_{24}$	0	0	0	$-\omega_{y}$	$\mathcal{O}_{x}$	$R_{14} + k_{42}$	

In eqs. 7 and 8,  $\Delta \omega_j = \Omega_j - \omega_{rf}$ , where  $\omega_{rf}$  is the angular frequency of the weak rf field applied in CEST;  $\omega_x$  and  $\omega_y$  are the x and y components of the rf field strength (in radians per second); R<sub>1j</sub> is the longitudinal relaxation rate of a spin at state j.



Figure S1. Representative experimental and calculated CEST (left panel) and RD (right panel) profiles described well by model I (Q42). Experimental CEST points recorded with rf field strengths of 13.6 and 27.2 Hz are indicated by  $\circ$  and  $\Box$ , respectively. RD data points recorded on 800 and 500 MHz are indicated by  $\circ$  and  $\Box$ , respectively. The best fits obtained with model I are solid lines.



Figure S2. Representative experimental and calculated CEST (left panel) and RD (right panel) profiles described well by model IV rather than by model I (F55). Experimental CEST points recorded with rf field strengths of 13.6 and 27.2 Hz are indicated by  $\circ$  and  $\Box$ , respectively. RD data points recorded on 800 and 500 MHz are indicated by  $\circ$  and  $\Box$ , respectively. The best fits obtained with model I (3-state) are black solid lines, while the fits obtained with model IV (4-state) are red lines.



Figure S3. Representative CEST (a, c, e, and g) and RD (b, d, f, and h) profiles recorded at 0.7 mM hIFABP. The experimental CEST data at rf field fields of 13.6 and 27.2 Hz are indicated by "o" and "•", respectively. The experimental RD data at 800 are indicated by "o". The solid lines are best fits obtained with model I (a, b, c, d, g, and h) and model IV (e and f). Note that the  $R2^{eff}$  values shown here were recorded with the continuous wave decoupling CPMG scheme, which are significantly smaller than those shown in Figure 1 that were acquired with the relaxation compensated scheme.



Figure S4. Experimental and calculated CEST (left panel) and RD (right panel) profiles of E107. Experimental CEST points recorded with rf field strengths of 13.6 and 27.2 Hz are indicated by  $\circ$  and  $\Box$ , respectively. RD data points recorded on 800 and 500 MHz are indicated by  $\circ$  and  $\Box$ , respectively. The solid lines were calculated with model I by assuming  $v(I_1) - v(N) = -0.41$  ppm and  $v(I_2) - v(N) = -1.83$  ppm.



Figure S5. The experimental data used are the same as those shown in Fig. S4. However, the solid lines were calculated with model I by assuming  $v(I_1) - v(N) = -0.41$  ppm and  $v(I_2) - v(N) = +1.83$  ppm.



Figure S6. The experimental data used are the same as those shown in Fig. S4. Only the region from 116-128 ppm are displayed for better view. The red lines were calculated by assuming  $v(I_1) - v(N) = -0.41$  ppm and  $v(I_2) - v(N) = 1.83$  ppm, while the blue lines were obtained by assuming  $v(I_1) - v(N) = +0.41$  ppm and  $v(I_2) - v(N) = 1.83$  ppm.

Res		<sup>15</sup> N chemical shifts (ppm)					Amide hydrogen exchange		
	N	I <sub>1</sub>	I <sub>2</sub>	I <sub>3</sub>	Ua	$k_{obs}(s^{-1})^b$	$P (k_{rc}/k_{ex})^{c}$		
F2*	113.63	111.84	116.45		119.13	0.6	13.3		
D3	119.26	118.35	120.65		122.39	0.4	20.0		
S4*	120.99	122.35	116.24		116.69	0.3	71.3		
T5*	116.24	115.02	114.19		116.05	1.2	19.6		
W6*	128.75	129.19	125.75		123.48	1.20x10 <sup>-4</sup>	$7.10 \times 10^4$		
K7	123.47	123.86	120.98		122.10	1.44x10 <sup>-4</sup>	$6.80 \times 10^4$		
V8*	128.39	126.62	127.58		121.34	-	-		
D9	128.19	128.61	127.38		124.65	7.20x10 <sup>-4</sup>	$6.98 \times 10^3$		
R10	112.92	112.66	113.65		121.91	1.26x10 <sup>-3</sup>	$8.72 \times 10^3$		
S11	113.75	112.78	113.12		117.74	3.3	16.3		
E12*	122.62	121.25	123.18		122.85	1.84x10 <sup>-2</sup>	$4.63 \times 10^2$		
Y14	121.14	121.79	119.71		120.55	1.7	9.1		
D15	118.59	-	-		123.00	-	-		
K16*	119.69	120.68	119.12		121.55	0.7	11.9		
F17	121.43	n	n		121.30	2.23x10 <sup>-4</sup>	$4.71 \times 10^4$		
M18	118.21	118.39	117.55		122.14	1.55x10 <sup>-4</sup>	$1.00 \times 10^5$		
E19	120.13	n	n		122.24	2.51x10 <sup>-4</sup>	$2.19 \times 10^4$		
K20	123.12	n	n		122.43	6.14x10 <sup>-4</sup>	$1.45 \times 10^4$		
M21	115.43	n	n		121.31	6.07x10 <sup>-4</sup>	$2.94 \times 10^4$		
G22	108.30	108.85	107.75		110.14	0.3	110.7		
V23	121.53	120.84	120.96		120.18	0.4	10.2		
N24*	126.50	127.65	127.69		123.01	6.0	5.1		
I25*	121.19	122.75	122.34		121.16	4.7	1.1		
V26*	121.67	120.31	122.09		124.68	0.7	2.3		
K27	119.32	n	n		125.80	2.3	4.0		
R28	119.52	n	n		122.67	3.4	6.4		
K29	119.50	118.79	119.05		122.86	6.6	3.2		
L30	119.71	119.28	119.06		123.18	1.4	3.4		
A31	120.15	121.30	121.02		124.74	1.9	4.5		
A32*	117.17	119.57	116.31		123.04	3.4	4.1		
H33*	116.88	115.56	117.90		117.92	5.0	2.2		
D34*	119.08	120.77	118.31		121.75	3.0	3.2		
N35*	119.17	120.69	118.08		118.95	3.9	7.2		
L36*	119.55	120.84	120.37		122.64	0.3	25.4		
K37*	126.41	128.31	125.69		121.79	0.01-0.1	78-780		
L38*	123.06	125.75	125.55		123.26	2.20x10 <sup>-4</sup>	$2.18 \times 10^4$		
T39*	121.29	117.83	122.42		114.69	3.13x10 <sup>-4</sup>	$2.32 \times 10^4$		
I40	128.58	129.17	126.47		123.27	$2.42 \times 10^{-3}$	$1.69 \times 10^3$		
T41*	121.31	122.97	119.88		118.14	4.56x10 <sup>-4</sup>	$1.52 \times 10^4$		
Q42*	128.53	126.46	126.85		122.80	0.3	84.0		
E43	128.65	128.05	127.83		122.47	0.2	34.0		
G44	117.63	-	-		109.79	-	-		
N45	113.18	112.45	114.48		118.74	9.9	6.4		
K46	120.89	n	n	n	121.57	8.87x10 <sup>-3</sup>	$2.97 \times 10^3$		

Table S1. <sup>15</sup>N chemical shifts of major state (N) and minor states (I<sub>1</sub>, I<sub>2</sub>, and I<sub>3</sub>) and amide hydrogen exchange rates (k<sub>obs</sub>) and protection factors

F47*	126.35	124.45	127.05	125.30	121.53	1.31x10 <sup>-2</sup>	$8.01 \times 10^2$
T48*	115.81	119.18	116.25	113.76	116.22	3.85x10 <sup>-4</sup>	$3.51 \times 10^4$
V49	127.81	128.12	127.27	126.24	123.15	2.21x10 <sup>-4</sup>	$1.98 \times 10^4$
K50*	128.28	123.79	127.42	126.59	125.76	3.06x10 <sup>-4</sup>	$2.99 \times 10^4$
E51*	127.07	127.90	129.33	124.69	122.03	$2.87 \times 10^{-3}$	$1.96 \times 10^{3}$
S52*	120.40	119.69	121.73	120.26	117.11	_	_
S53*	121.42	115.37	122.12	119.73	118.23	0.4	161.6
A54*	120.59	126.83	119 64	122.58	125 72	5.5	5.0
F55*	112 39	116 68	111 77	114 36	119 43	16	5.0
R56*	114 46	118 17	113 09	116 84	123 31	0.9	21.2
N57	120.44	-	-	-	120.41	-	
158*	118.54	117.01	117.03	120.59	121.11	0.3	17.9
E59*	124 54	126.00	123 25	126.86	124 93	11	23
V60*	127.55	125.01	128.90	123.15	121.58	0.01-0.1	19.5-195
V61	125 72	126.03	125.53	123 62	124 43	$6.14 \times 10^{-3}$	$3.25 \times 10^2$
F62*	121.44	123.32	121.11	122.71	124.55	$3.09 \times 10^{-5}$	$1.87 \times 10^5$
E63	120.25	120.66	120.63	118.84	122.61	$6.72 \times 10^{-3}$	$7.30 \times 10^2$
L64*	125.14	123.20	125.26	122.95	123.10	$1.49 \times 10^{-3}$	$1.73 \times 10^{3}$
G65	108 76	109 78	108.59	110.08	109.57	$5.15 \times 10^{-3}$	$3.08 \times 10^3$
V66*	122.47	121.25	122.49	120.72	120.48	$4.38 \times 10^{-5}$	$9.32 \times 10^4$
T67*	129.48	128.14	128.67		118.05	7.3	1.1
F68	127.05	n	n		122.60	$1.38 \times 10^{-4}$	$9.14 \times 10^4$
N69	117.23	117.70	116.55		120.52	0.3	163.6
Y70*	122.32	125.87	123.26		120.71	0.2	77.5
N71	121.02	121.81	123.41		121.00	1.0	48.0
L72*	121.99	120.70	122.84		122.57	3.53x10 <sup>-3</sup>	$2.15 \times 10^3$
G75	108.22	107.93	109.04		109.54	2.6	6.5
T76	119.99	n	n		113.92	2.0	8.7
E77*	129.02	127.99	129.57		123.05	0.3	22.7
L78	126.09	125.70	125.29		123.04	1.54x10 <sup>-4</sup>	$1.67 \times 10^4$
R79	119.40	n	n		122.12	5.48x10 <sup>-6</sup>	2.95x10 <sup>6</sup>
G80	116.32	115.77	115.56		110.77	4.45x10 <sup>-5</sup>	9.61x10 <sup>5</sup>
T81	107.05	107.91	106.47		113.75	3.21x10 <sup>-5</sup>	5.43x10 <sup>5</sup>
W82	120.37	119.79	121.63		123.36	-	-
S83	115.84	n	n		116.33	5.29x10 <sup>-6</sup>	$4.76 \times 10^{6}$
L84	125.63	n	n		124.07	0.2	36.2
E85	127.85	128.43	127.30		121.60	0.2	13.2
G86	117.63	-	-		109.79	-	-
N87*	122.87	121.32	122.21		118.74	9.6	6.5
K88	118.32	n	n		121.65	2.33x10 <sup>-3</sup>	$1.13 \times 10^{4}$
L89*	123.76	121.59	122.83		123.02	<5x10 <sup>-6</sup>	>3.6x10 <sup>6</sup>
190	125.39	n	n		121.35	<5x10 <sup>-6</sup>	$>1.2 \times 10^{7}$
G91	122.27	121.90	121.46		113.06	<5x10 <sup>-6</sup>	$>5.2 \times 10^{6}$
K92	128.45	128.82	127.59		120.87	3.34x10 <sup>-4</sup>	5.59x10 <sup>4</sup>
F93	121.93	n	n		121.52	1.01x10 <sup>-4</sup>	7.53x10 <sup>4</sup>
K94	119.69	n	n		123.53	1.83x10 <sup>-5</sup>	7.92x10 <sup>5</sup>
R95	122.40	122.86	123.32		122.67	0.4	54.7
T96	116.23	115.77	117.23		115.56	1.1	17.7
D97	121.02	n	n		122.67	0.4	27.5
N98	117.04	n	n		119.35	0.5	56.4
G99	108.15	n	n		109.26	0.3	179.3

N100	119.63	n	n	118.57	9.75x10 <sup>-3</sup>	$6.48 \times 10^3$
E101	120.36	n	n	121.07	0.01-0.1	89.3-893
L102	124.63	125.25	125.35	122.88	3.57x10 <sup>-5</sup>	$7.22 \times 10^4$
N103	124.71	124.33	124.09	119.58	1.98x10 <sup>-4</sup>	$1.33 \times 10^{5}$
T104	118.71	118.71	117.66	114.68	2.09x10 <sup>-4</sup>	$1.177 \times 10^{5}$
V105	127.27	n	n	123.02	4.45x10 <sup>-5</sup>	$9.83 \times 10^4$
R106	124.58	n	n	125.70	4.08x10 <sup>-5</sup>	$2.95 \times 10^{5}$
E107	121.53	121.12	123.36	122.51	4.53x10 <sup>-5</sup>	$1.57 \times 10^{5}$
I108	124.86	-	-	121.57	-	-
I109	130.26	n	n	124.72	5.14x10 <sup>-4</sup>	$2.95 \times 10^3$
G110	119.37	n	n	112.61	11.8	1.3
D111	124.86	-	-	120.11	-	-
E112	118.68	n	n	121.05	1.34x10 <sup>-4</sup>	$2.11 \times 10^4$
L113	123.96	n	n	123.06	1.58x10 <sup>-5</sup>	$1.63 \times 10^5$
V114	128.30	128.63	127.59	121.15	$<5x10^{-6}$	$>3.4 \times 10^{5}$
Q115	130.73	n	n	124.81	9.19x10 <sup>-5</sup>	$1.25 \times 10^{5}$
T116*	122.04	120.92	120.53	115.34	1.22x10 <sup>-4</sup>	$1.53 \times 10^{5}$
Y117	126.24	125.77	125.32	122.86	1.01 x10 <sup>-4</sup>	$1.16 \text{ x} 10^5$
V118	120.17	120.79	120.89	122.75	7.09x10 <sup>-5</sup>	$4.37 \times 10^4$
Y119	128.22	n	n	124.63	9.83x10 <sup>-5</sup>	$5.47 \times 10^4$
E120	126.26	n	n	123.50	0.2	24
G121	127.72	n	n	109.96	0.01-0.1	182.3-1823
V122	123.70	n	n	120.30	2.56x10 <sup>-4</sup>	$1.59 \times 10^4$
E123	126.68	n	n	125.27	2.27x10 <sup>-2</sup>	$1.36 \times 10^{2}$
A124	126.38	125.83	127.05	125.20	3.04x10 <sup>-4</sup>	$3.22 \times 10^4$
K125	116.66	117.39	115.96	120.65	7.37x10 <sup>-4</sup>	$1.71 \times 10^{4}$
R126*	120.50	121.69	119.64	122.43	2.06x10 <sup>-4</sup>	$1.06 \times 10^5$
I127	123.59	123.17	122.96	121.94	1.17x10 <sup>-4</sup>	$3.65 \times 10^4$
F128	126.90	n	n	124.41	1.83x10 <sup>-4</sup>	$2.56 \times 10^4$
K129	118.80	118.42	120.38	123.66	1.97x10 <sup>-4</sup>	$7.35 \times 10^4$
K130	123.72	123.20	125.54	122.29	5.48x10 <sup>-3</sup>	$3.03 \times 10^{3}$
D131*	130.32	129.16	131.01	na	7.16x10 <sup>-3</sup>	$1.28 \times 10^{3}$

n: No RD dispersion was observed on the 800 MHz spectrometer, indicating the chemical shifts in the native and intermediate states are very similar.

-: due to peak overlap or weak peak, the data are not available.

na: the prediction value is not available.

\*: CEST profiles displayed two obvious dips (>80 Hz) and as well in RD profiles  $R_{ex} > 2 s^{-1}$  on 500 MHz NMR.

<sup>a:</sup> The shifts in the unfolded state were predicted using the ncIDP predictor tool (http://nmr.chem.rug.nl/ncIDP/).

<sup>b:</sup> For the exchange rates larger than 0.1 s<sup>-1</sup>, they were measured by the amide hydrogen exchange method in 95% H<sub>2</sub>O and 5% D<sub>2</sub>O. For the rates smaller than 0.01 s<sup>-1</sup>, they were measured by the H-D exchange method. For those between 0.01 and 0.1 s<sup>-1</sup>, they were estimated based on the dead time (180 s) of the H-D exchange experiment and the lower limit of the amide hydrogen exchange method. The H-D exchange data were recorded for 5.5 hours at pH 7.1, 30 °C. So the exchange rates could not be measured accurately if they are smaller than  $5 \times 10^{-6} \text{ s}^{-1}$ .

<sup>c:</sup> krc was predicted using an online software tool (http://sblab.sastra.edu/cintx.html).