

Supplemental Materials Online

In-vivo Imaging of Magnetic Fields Induced by Transcranial Direct Current Stimulation (tDCS) in Human Brain using MRI

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S1: Detection Limit of the Proposed Technique

Equation (2) in main text can be rewritten as:

$$\Delta B_z = \frac{\Delta \Phi_m}{\gamma \times \Delta TE} \quad (S1)$$

where the quantities are as those defined in *Equation (2)*, and Δ represents the fact that we are considering the phase difference between two TE's (The phase difference is utilized in actual analyses, since it removes a confound, see *Supplemental S5*). The modulo- 2π operation has been removed reflecting the fact that the phase angles have been unwrapped. In an ideal scenario without noise, the minimum (unbiased) detectable field corresponds to the smallest possible non-zero phase change generated by the smallest applied current (0.5mA). Because the full phase range of 0 to 2π radians is divided into 4096 discrete levels in MRI, the smallest non-zero phase change evaluates to $\left(\frac{2\pi}{4096}\right)$ radians. Together with the experimental parameter ΔTE (chosen as 9.84 msec for all our experiments), the minimum (unbiased) detectable field equates to 0.58nT at 0.5mA, or $\sim 1.2\text{nT/mA}$. It should be noted that this detection limit is specific to the present implementation. In other words, it is possible to lower this limit using a larger ΔTE , and to some extent, different applied currents. A larger ΔTE can be achieved by minimizing TE_1 , or, increasing TE_2 permitted by SNR.

23

24 **S2: MRI is only sensitive to magnetic field disturbances along B_z**

25 Here we show why MRI is only sensitive to magnetic field disturbances along the static
26 magnetic field (B_z). Any perturbation of the magnetic field ($\Delta\vec{B}$) can be written as a sum of two
27 orthogonal components: one along B_z , and the other perpendicular to B_z (indicated by $(\Delta B_{\parallel})\widehat{B}_z$
28 and $(\Delta B_{\perp})\widehat{B}_{\perp,z}$ respectively).

29 The total magnetic field can be written as a vector sum of B_z and the perturbation:

$$30 \quad \vec{B}_{total} = (B_z + \Delta B_{\parallel})\widehat{B}_z + (\Delta B_{\perp})\widehat{B}_{\perp,z} \quad (S2)$$

31 or equivalently, as a vector of length B_{mag} , at an angle θ to \widehat{B}_z :

$$32 \quad B_{mag} = \sqrt{(B_z + \Delta B_{\parallel})^2 + (\Delta B_{\perp})^2} \quad ; \quad \theta = \tan^{-1}\left(\frac{\Delta B_{\perp}}{B_z + \Delta B_{\parallel}}\right) \quad (S3)$$

33 For perturbations on the order of ppm, it can be seen that θ is almost zero i.e., \vec{B}_{total} is along \widehat{B}_z .

34 Under the same ppm perturbations, B_{mag} can be approximated using the Taylor Series expansion

35 as

$$36 \quad B_{mag} \cong B_z + \Delta B_{\parallel} + \frac{B_z}{2} \left\{ \left(\frac{\Delta B_{\parallel}}{B_z}\right)^2 + \left(\frac{\Delta B_{\perp}}{B_z}\right)^2 \right\} + \dots \quad (S4)$$

37 Relative to ΔB_{\parallel} , the contribution of ΔB_{\perp} is on the order of ppm (since it is scaled by a factor of

38 B_z^{-1}) and can thus be neglected. Thus, it can be said that (1) the magnetic field deviations

39 measured by MRI field mapping reflect ΔB_{\parallel} , i.e. the component of the field disturbances

40 along \widehat{B}_z and (2) the resultant field is along the MRI static field ($\because \theta \approx 0$).

41

42 **S3: Simulations of Phantom Experiment**

43 In the phantom experiment, the current density at each point of the current carrying tube can be

44 estimated. In such a special case involving known DC current densities, the Biot-Savart law can
45 be used to calculate current-induced magnetic fields (*Equation (3)* in main text).

46

47 An implementation of the Biot-Savart law for line currents (33) was modified in-house and
48 extended to volumetric finite element currents. The implementation of the finite element
49 simulation was carried out in two steps:

50 1. Magnetic field estimation:

51 Magnetic fields (along B_z) were estimated over a grid (henceforth referred to as the ‘Sampled
52 grid’, *Supplemental Fig. S2(a)*) designed to match the spatial resolution of the MRI phantom
53 experiment $\Delta x \times \Delta y \times \Delta z = 2 \times 2 \times 3 \text{ mm}^3$. It should be noted that while MRI
54 measurements represent the average magnetic field in a voxel, magnetic fields calculated
55 using the Biot-Savart law estimate the field at a point and hold no information about the
56 neighborhood. To address this, the magnetic field at each point on the sampled grid was
57 calculated as an average over fields calculated on a 3D ‘super-sampled’ grid (*Supplemental*
58 *Fig. S2(b)*, shown as 2D for simplicity). The spatial resolution of the 3D super-sampled grid
59 was 0.5 mm isotropic and the magnetic field value at each point was calculated using the
60 Biot-Savart Law (*Equation (3)* in main text).

61

62 2. Electric Current modeling:

63 Assuming the salt-water electrolyte to be isotropic with uniform conductivity, the electric
64 current is expected to travel in parallel ‘streamlines’ between the electrodes. Utilizing the
65 inherent symmetries in the system, these streamlines were discretized to a non-Cartesian grid
66 as shown in *Supplemental Fig. S2(c)*. The discretized grid had a spatial resolution of

67 ~0.125mm isotropic. In other words, at least 64 points would be enclosed by a volume with
68 the size of a single voxel on the super-sampled grid (discussed in 1 above).

69

70 Each streamline is an electric current flowing through an ohmic resistor. Thus, the system is
71 electrically equivalent to a current-divider circuit (shown in *Supplemental Fig. S2(d)*), with
72 each branch of the circuit representing a streamline and the input being the total applied
73 current. The resistance of each branch is equal to the resistivity of the electrolyte multiplied
74 by the ratio of the length of the streamline to its cross-sectional area. While the length of a
75 particular streamline is known from phantom geometry, the cross-sectional area is
76 determined during the discretization process. The circuit was solved to compute the current
77 through each streamline by choosing the total applied current to be 1mA. It should be noted
78 that the resistivity of the electrolyte is not needed for this calculation. The choice of 1mA
79 enabled direct comparison between the simulated fields and those detected using MRI (the
80 latter being the induced magnetic fields per unit mA applied-current). The average current
81 density within the conducting tube 'A' was 0.79 mA/cm^2 (1mA, $\frac{1}{2}$ inch tube diameter).

82

83 **S4: Simulations of Limb Experiment (Calf)**

84 Laplace's equation governs the voltage distribution in a purely resistive volume during constant
85 current flow. The calf structural MR images were segmented into compartments representing the
86 gel, skin, fat, muscle and bone using a combination of automated and manual segmentation
87 routines (17). The stimulation electrodes were imported as CAD models and positioned within
88 the image data. Volumetric meshes were subsequently generated from the compartments
89 (SIMPLEWARE Ltd, Exeter, UK) and imported to a commercial finite element solver

90 (COMSOL Inc, MA, USA). Isotropic conductivity values were used (electrode: 5.99×10^7 , gel: 1.4
91 S/m, skin: 0.465, fat: 0.001, muscle: 0.16, bone: 0.01) and the Laplace equation was solved to
92 generate a spatial map of current density. The conductivity values used have been previously
93 reported in (34) (skin and bone) and (35)(muscle and fat).

94

95 The Biot-Savart law (*Equation 3* in main text) was used to calculate magnetic field due the
96 calculated static current densities. The Biot-Savart law was implemented as a 3D convolution, as
97 previously reported in (21).

98

99 **S5: Experimental Procedures**

100 ***Concurrent tDCS-MRI***

101 An MRI compatible tDCS system was constructed to enable concurrent tDCS-MRI experiments.
102 Quad-shielded coaxial cables were used to carry the applied current from the tDCS stimulator
103 (kept in the MRI control room) to the electrodes (in the scanner room). The battery-powered
104 “ActivaDose Iontophoresis Delivery Unit” (ActivaTek, Salt Lake City, UT) was used to drive
105 the current. Similar to (13), a filter box and in-line resistors of 10k-ohm were installed at the
106 stimulator and electrode ends respectively to provide protection from potential voltage
107 fluctuations due to gradient switching during MRI scans.

108

109 ***Experiments***

110 **A. Phantom:**

111 The phantom was constructed in three parts –

112 (i) Bulk phantom: A standard Siemens cylindrical phantom ($3.75\text{g NiSO}_4 \times 6\text{H}_2\text{O} + 5\text{g NaCl}$ per

113 1000gm H₂O, 0.5 Gallon, 10.6 cm diameter) was used. Available in a sealed plastic container,
114 the contents are insulated from external currents.

115 (ii) Current-Carrying tube (Tube 'A', **Fig. 1a**): A flexible plastic tube (ID=1/2 inch) was bent
116 into a U-shape and wrapped around the long axis of (i) at its midline. The tube was filled with
117 salt water (electrolyte), and fitted with copper electrodes at both ends. The electrodes were
118 connected to the tDCS stimulator. All applied currents travel through this tube.

119 (iii) 'Control' Tube (Tube 'B', **Fig. 1a**): A second plastic tube (ID=3/8 inch) constructed using
120 the same material and electrolytes, was placed similar to (ii) at the distal end of (i). This tube was
121 designed to serve as an intra-session control and accordingly, the electrodes were not connected
122 to the tDCS stimulator.

123

124 B. Calf:

125 Round carbon rubber electrodes (2" inch diameter) were secured laterally on each side of the left
126 calf. Conductivity gel (Cadwell, P/N# 202153-000) was used to make electrical contacts.

127

128 C. Head:

129 Sponge electrodes were placed bilaterally over the C3/C4 position (anode C4 and cathode C3),
130 according to the international 10/20 system to target the motor cortices. The electrodes were
131 rectangular (4.5x9cm) in shape with their long axes in A \leftrightarrow P direction. The same conductivity
132 gel as the calf experiment (Cadwell, P/N# 202153-000) was used to make electrical contacts.

133

134 ***Data Acquisition***

135 MRI data were acquired using a product single channel Tx/Rx quadrature volume coil. The

136 phantom and calf data were acquired on a Siemens 3T PRISMA system, while the head data
137 were acquired on a Siemens 3T Trio TIM system. It should be noted that MRI shimming was
138 performed only once at the start of each session. Shimming is a pre-scan preparatory step that
139 corrects for field deviations from B_z and may cancel out current induced fields. Potentially
140 uncorrected field deviations, unrelated to electrical current, were explicitly modeled out (see
141 Φ_{drift} below).

142

143 *Pre-Processing*

144 Stochastic noise in a single voxel of the phase image is approximately zero-mean Gaussian for
145 (magnitude) SNR ≥ 3 (36). A Gaussian noise is necessary for phase unwrapping as well as for
146 GLM modeling of the preprocessed data (especially since at the other extreme of SNR=0, voxel
147 noise in the phase image is uniformly distributed). The threshold of 3 is mathematically
148 equivalent to a p-value (since the distribution of the noise is known). This p-value threshold was
149 adjusted (Bonferroni corrected) to account for the total number of voxels being tested, and
150 voxels under the threshold were excluded.

151

152 Thresholded phase data was unwrapped using the Region growing algorithm implemented in the
153 PhaseTools toolbox (37) (available as a plug-in for Fiji (38)). Unwrapping was carried out at the
154 individual volume level, followed by unwrapping within each slice. Using SPM8, volumes were
155 then realigned to the first (volume) to account for inter-scan motion. The realignment parameters
156 were estimated using the magnitude data from the first echo (TE_1). The realignment step was
157 skipped for the phantom.

158

159 ***Model for Measured Phase***

160 Measured phase was modeled as:

161
$$\Phi_m = \Phi_{Current}(TE, i(s)) + \Phi_0(s) + \Phi_{Non-Current}(TE) + \Phi_{drift}(TE, s) + \Phi_{noise} \quad (S5)$$

162 where Φ_m is the measured phase, $\Phi_{Current}$ is the phase due to current-induced fields, TE is the
163 echo-time, “ s ” refers to the fact that the data is from the s^{th} scan in the current session and $i(s)$ is
164 the current applied during the “ s -th” scan. Φ_0 is the baseline phase, $\Phi_{Non-Current}$ is the phase due to
165 field deviations unrelated to applied current but steady between scans (eg. off-resonance), Φ_{drift} is
166 the phase due to inter-scan field-deviations caused by the time-varying drift of the main magnetic
167 field and Φ_{noise} is the phase due to (Gaussian) noise.

168

169 The phase difference ($\Delta\Phi_m$) between the two TEs was computed. This step eliminates Φ_0 . $\Delta\Phi_m$
170 was subsequently included as the dependent variable in a general linear model (GLM) with
171 applied current ($i(s)$) as the predictor. This is based on the assumption that the current path
172 remains the same for all applied currents. $\Delta\Phi_{Non-Current}$ by definition does not vary with applied
173 current and is implicitly incorporated into the GLM intercept.

174

175 On the other hand, $\Delta\Phi_{drift}$ was explicitly modeled by a polynomial function that was fitted least
176 squares wise to phase measured during zero-current scans. This is consistent with the model for
177 measured phase (***Equation (S5)***) wherein the phase fluctuations for zero-current scans should be
178 purely due to drift and noise. The degree (d^*) of the polynomial was selected to optimally match
179 the characteristics of the residual with those of Φ_{noise} to prevent overfitting. Φ_{noise} for each voxel
180 was estimated using the magnitude image (36).

181

182 The regression coefficient for applied current (β_{Current}) obtained from the GLM analysis can be
183 interpreted as the phase gained per 1mA applied-current. This was converted to induced
184 magnetic field per mA current using *Equation (2)*. Obtained mA-current induced magnetic field
185 maps were subsequently thresholded at $p < 0.05$ and cluster corrected (using AlphaSim (39))
186 following standard statistical procedures for fMRI.

187

188 ***Group Level Analyses***

189 Current-induced field maps of individual subjects were coregistered to the corresponding
190 structural images and subsequently normalized to the MNI space using SPM8. Normalized field
191 maps were used to perform a one-sample t-test for both ‘Active’ and ‘Sham’ sessions. Results
192 were thresholded at $p < 0.05$ and cluster corrected for multiple comparisons using AlphaSim (39).

193

194 ***Region-of-interest (ROI)-Analysis***

195 ROIs were constructed as spheres with a radius of 1cm centered at projections of C3/C4 on the
196 cortex (as reported by (23)), thresholded to exclude all out of brain voxels. Each ROI enclosed
197 equal number of voxels (178). $\Delta\Phi_{\text{Current}}$ within each ROI was averaged over all voxels, and was
198 used in a linear fit with applied current as the predictor. The slope of such a fit can be interpreted
199 as the ROI-averaged current-induced field. These were subsequently used to perform a one-
200 sample t-test for both ‘Active’ and ‘Sham’ sessions. Significant current induced magnetic fields
201 were observed for the ‘Active’ session, both at C3 and C4 (corresponding to Cathode and Anode
202 respectively). No fields were observed for the ‘Sham’ session (See *Supplemental Fig. S1*).
203 Additionally, the field changes under anode and cathode had the same sign; which is intuitive

204 given that the direction of tDCS current flow is the same (from anode to cathode) at both
205 electrodes. Note that the sign of the fields matches that of the results obtained through voxel-
206 wise analysis.

207

208 **S6: Ampere's Law for Biological Tissues**

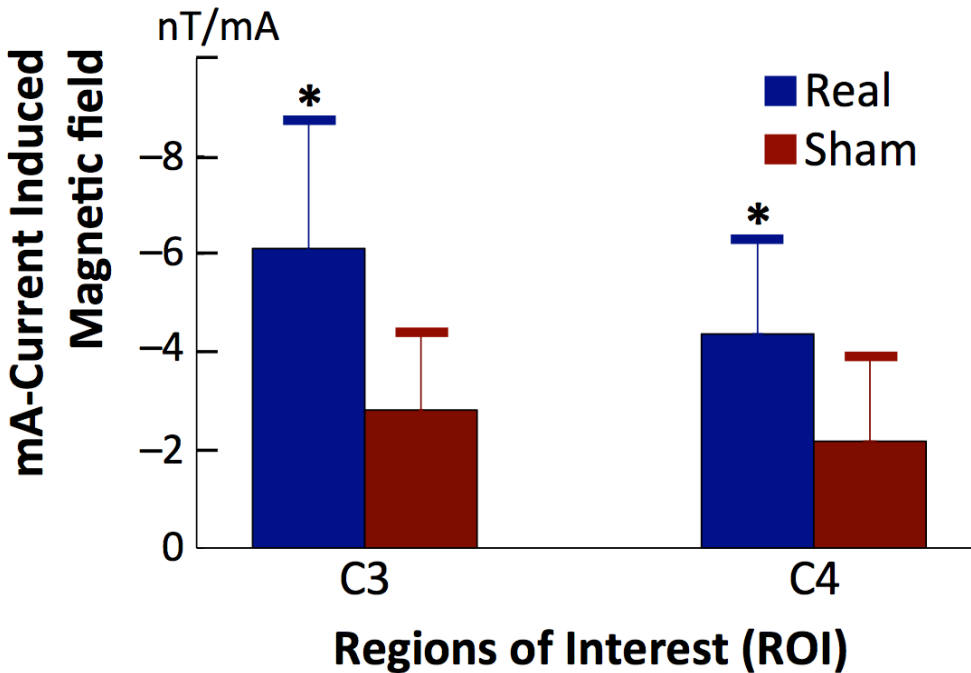
209 The general form of Ampere's Law is:

$$210 \quad \nabla \times \vec{H} = \vec{j} + \frac{\delta}{\delta t} \vec{D} \quad (S6)$$

211 where \vec{H} is the magnetizing field, \vec{j} is the applied current, \vec{D} is the displacement field, t is time
212 and ∇ is the curl operator. The time-varying term can be ignored for our DC case. Our
213 experiment consists of applying a current to biological tissues, which induces magnetic field
214 perturbations $\leq \mu\text{T}$ around a 3T static field (B_0) of the MRI. Under these conditions, it is
215 appropriate to replace \vec{H} according to

$$216 \quad \vec{B} = \mu \vec{H} \quad (S7)$$

217 where \vec{B} is the induced magnetic field, and μ is the magnetic permeability of the biological tissue
218 (26). Under the same conditions, μ is reported to be a scalar, varying on the order of ppm
219 between tissues (26). By using *Equation (S7)* in *Equation (S6)*, *Equation (1)* in main text can be
220 derived. A key point to note is that for the reported tissue μ , the relationship between applied
221 current \vec{j} and induced magnetic field \vec{B} is linear. Note that the linearity relationship holds even if
222 μ is a tensor. In fact, the independence of μ from \vec{B} or \vec{H} is a sufficient condition for linearity to
223 hold.



227 **Figure S1:** Results of one-sample t-test performed on ROI-averaged current-induced field.

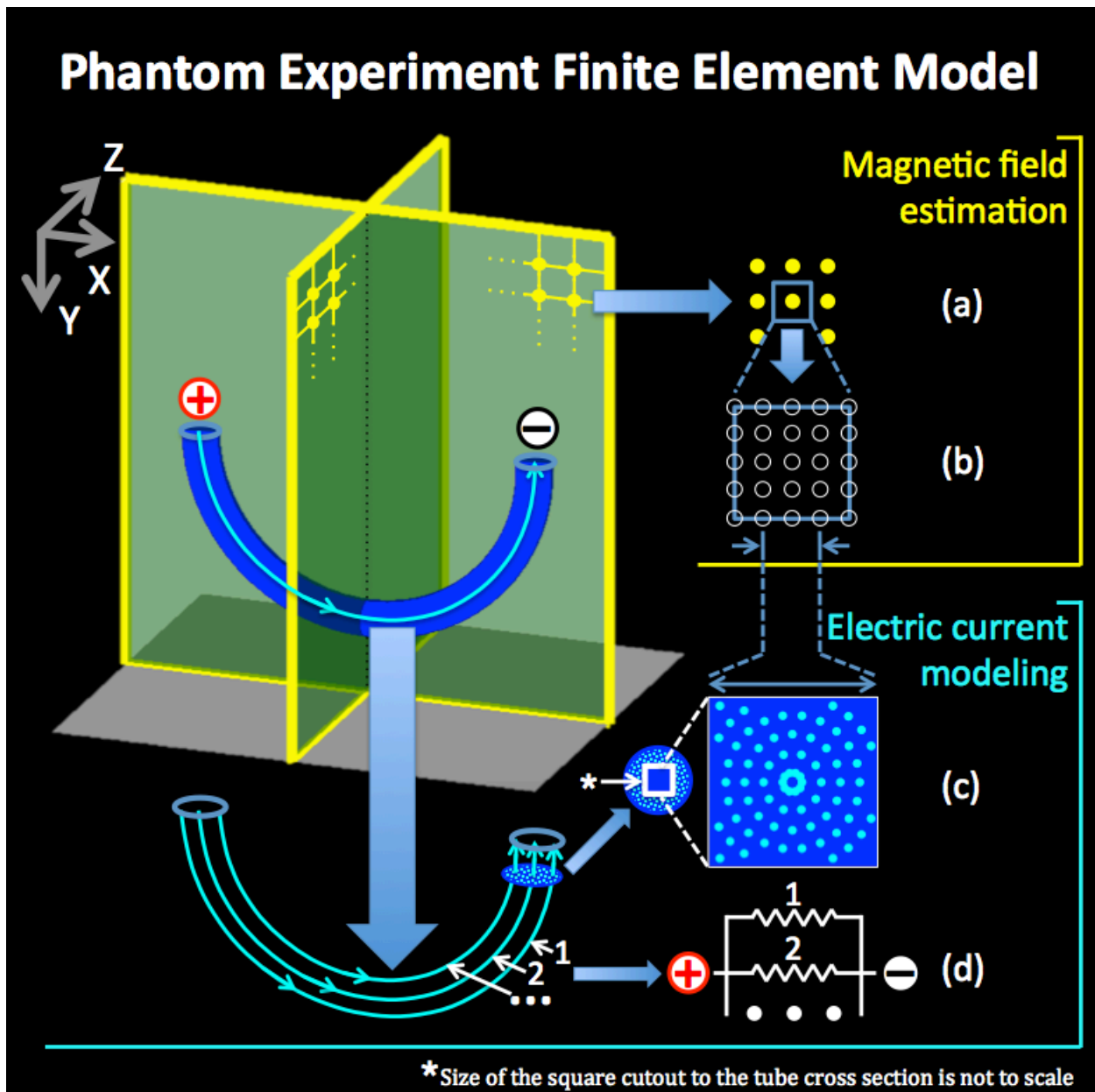
228 Significant current-induced magnetic field reductions were detected at the C3 and C4 ROIs for

229 the ‘Active’ session ($\beta = -6.1$ nT/mA, -4.4 nT/mA; $p = 0.036, 0.044$ respectively; $N = 12$

230 subjects). No significant fields were detected for the ‘Sham’ session ($\beta = -2.8$ nT/mA, -2.2

231 nT/mA; $p = 0.104, 0.233$ respectively). Also shown are error bars for the one-sample t-tests. See

232 *Supplemental S5* for detailed methods for ROI analysis.



233

234 **Figure S2:** Finite Element modeling of the phantom experiment: (a) shows the grid where the
 235 magnetic field was calculated as an average over points on a ‘super-sampled’ grid (b), to emulate
 236 the fact that MRI measures the average behavior in a voxel. The applied current was modeled as
 237 streamlines, which were subsequently discretized as shown in (c). Current through each
 238 streamline was calculated from the equivalent circuit as depicted in (d)

239