



 $^{25}_{26}$ Figure S1: Variation of the slip weakening distance with depth applied in the dynamic simulations.

27 Above 50 km the  $d_c$  has a value of 1m. Depth is given relative to the point at which the fault reaches

- 28 the surface.
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Figure S2: Amplitude spectra for the initial stress (subplot a) and resulting slip (subplot b). In both 41 subplots the distributions have been grouped according to resulting magnitude with the amplitude

42 spectra calculated in wavenumber bins. **a)** the black dashed line represents the length of the fault for 43 which the normal stress is depth invariant (and the scaling the initial shear stress is uniform), the solid 44 black line represents a  $k^{-1}$  slope **b**) the black dash represents the maximum element size with the solid 45 black line representing a  $k^2$  slope.

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 $\frac{54}{55}$ Figure S3: comparison between slip distributions generated using a nucleation size smaller than in the original model. Taking 35 cases, we used the same initial conditions (i.e. stochastic shear stress distributions), the only difference is that the nucleation zone is halved. Of the 35 comparisons, 8 did not nucleate when the nucleation zone was halved, in the rest, the final slip distributions we similar. A selection of these are presented in this figure where the original slip distribution is represented by a red line an the dashed black line indicates slip in the case where the nucleation zone has been halved. 

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 **Figure S4**: Moment magnitude distribution from dynamic simulations assuming that the length scales 75 according to Eqn 3. Bin size are  $0.2 M_w$ , very small events have been excluded (i.e. simulations where



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88 **Figure S5:** Pre-stress and slip distributions subdivided into the magnitude bins  $8.4 - 8.6$  M<sub>w</sub>;  $8.6 - 8.8$ 89  $M_w$  and 8.8-9.0  $M_w$ . The subplots on the left side represent pre-stress distributions, the different coloured lines represent the different initial pre-stress distributions and the red lines are the yield stress .The right handside subplots are the resulting slip distributions from the corresponding pre-stress distributions on the right hand side. Again each colour represents a different simulation. The solid red line is the yield stress the drop in yield stress due to the nucleation patches are not draw in order to improve clarity of the initial stress distribution; the amplitude of the drop in the yield stress in the nucleation zone is depicted by the dashed line. The triangles represent the location of the nucleation zones.



99 **Figure S6:** Pre-stress and slip distributions subdivided into the magnitude bins 9. – 9.2 M<sub>w</sub>; 9.2 – 9.4

- 100  $M_w$  and 9.4 9.6  $M_w$ . The layout and colour code used in the subplots are similar to Fig. S5.
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115 **Figure S7**: testing the effect of introducing a more compliant wedge  $(v_p = 4.7 \text{ km/s}, v_s = 2.1 \text{ km/s}, \rho =$ 116 2.5 kg/m<sup>3</sup>) compared to the rest of the medium ( $v_p = 6.3$  km/s,  $v_s = 3.2$  km/s,  $\rho = 3000$  kg/m<sup>3</sup>). 35 117 sample case were taken where all other aspects of the model were the same. In general there was little alteration for small events (see top left sub-figure). For larger events, the addition of the wedge, on average induced larger amounts of slip near the surface, however the general shape of the slip is similar 120 in nearly all cases.

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**Figure S8**: transfer functions for each magnitude bin split depending on if rupture reaches the surface

- 128 (i.e. Surface) or does not (Deep). Choice of whether to use the deep or surface transfer function is
- defined based on the probability of it occurring in the simulations (see Table S1). The M 8.4-8.6 bin
- contains 19 events and therefore its sample size is not representative. The grey box denotes the wedge.
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 **Figure S9:** Earthquake magnitude distribution from dynamic simulations assuming that the seismic 148 moment is  $M_0 = \mu \bar{\delta} W^2$ . Bin size is 0.2 M<sub>w</sub>, and the majority of events range between M<sub>w</sub> 8.4-9.2,

- 149 based on this scaling.
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 $164 \over 165$ Figure S10: Comparison of max slip generated in 500 stochastic source simulations. The standard

 methodology produces a maximum slip (blue dots) range of 14.4 – 35.8 m with a mean of 22.6 m (solid blue line) applying the transfer function shifts the maximum slip range to 17.9 – 49.4 m with a mean of 168 30. m (solid red line). All slip distributions produce  $M_w$  9 events and have been used to generate  $H_{max}$  in Fig. 8 in the main text. 

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 **Figure S11**: Histograms of the location of the maximum slip in the stochastic models discussed in Fig. 175 S6 and Figure 8 in main text. The traditional stochastic source model produces a relatively even distribution with depth, featuring a slightly higher frequency of occurrence at depth relative to near the surface (blue histogram). With the application of the transfer function the maximum slip is shifted towards the surface (orange histogram). The red line represents the applied transfer function in the case where rupture reaches the surface, the blue is the transfer function when rupture does not reach the 180 surface both transfer functions were generated using the slip distributions in the  $M_w$  9 - 9.2 bin. The 181 choice of which transfer function to use is based on the probability of surface rupture occurring in the 182  $M_w$  9 - 9.2 bin, in this case 82.1 % of the ruptures reached the surface therefore a probability function of 0.821 to 0.178 was used in choosing between the surface transfer function and the deep rupture 184 transfer function. 









211 **Figure S13:** The effect of using the M<sub>w</sub> 9.2-9.4 transfer function for a M 9 event of calculating Hmax hazrd. **a)** Location of the fault (the subduction zone interface) relative to the Japanese coastline and receiver locations (denoted by black dots). Colours on the fault plane are the SPDF for the modified 214 stochastic source model using the  $M_w$  9.2-9.4 transfer function. Dashed lines across the fault plane 215 mark 50 km, 100 km, 150 km down dip distance from the top of the fault. Bold black line denotes tsunami receiver locations (see Methods). **b)** Conditional probability of exceedance of maximum wave 217 height along latitude, for the modified source model using the  $M_{w}$  9.2-9.4 transfer function for a M 9 event; and **c)** original stochastic source model, again for a M 9 earthquake. The logarithmic colour 219 scale is the same for both plots. The grey solid lines indicate the maximum and minimum  $H_{\text{max}}$  obtained 220 at each receiver. Blue diamonds are maximum tsunami wave height observed during the 2011  $M_w$  9 221 earthquake, as in panel d. **d**) observed maximum wave height and runup for 2011  $M_w$  9 Tohoku 222 earthquake, the 1896 M<sub>s</sub> 7.2 and 1933 M<sub>s</sub> 8.5 Sanriku earthquakes as described in Figure 7 in main text. 

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- 229 tranfer functions (see Figures 7, S12, S13)
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Table S1: probablity of rupture reaching the surface compared to earthquakes that do not.

246 The probablitites are based on the slip distributions produced in the dynamic rupture

247 simulations. With increasing magnitude there is an consistant trend of increasing likelihood of

248 surface rupture with increasing rupture. The 8.4 M-8.6 M bin has been omitted as it only

249 contained 19 events which is not enough to produce a representative result.