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**Supplemental Information**

**An Integrated Stochastic Model of Matrix-Stiffness-Dependent Filopodial Dynamics**

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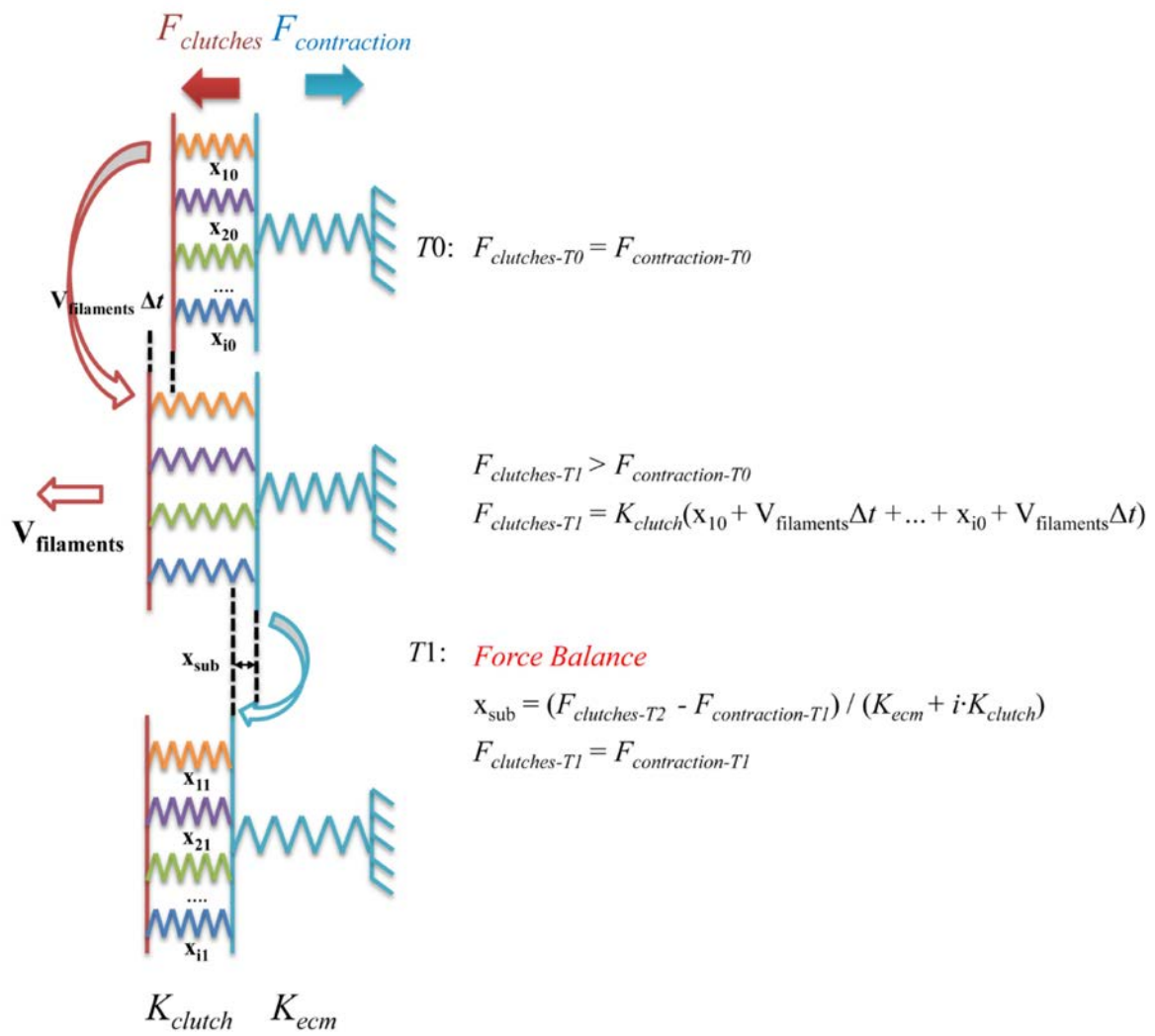


Figure S2. Diagram for calculation of force balance between molecular clutch and substrate.

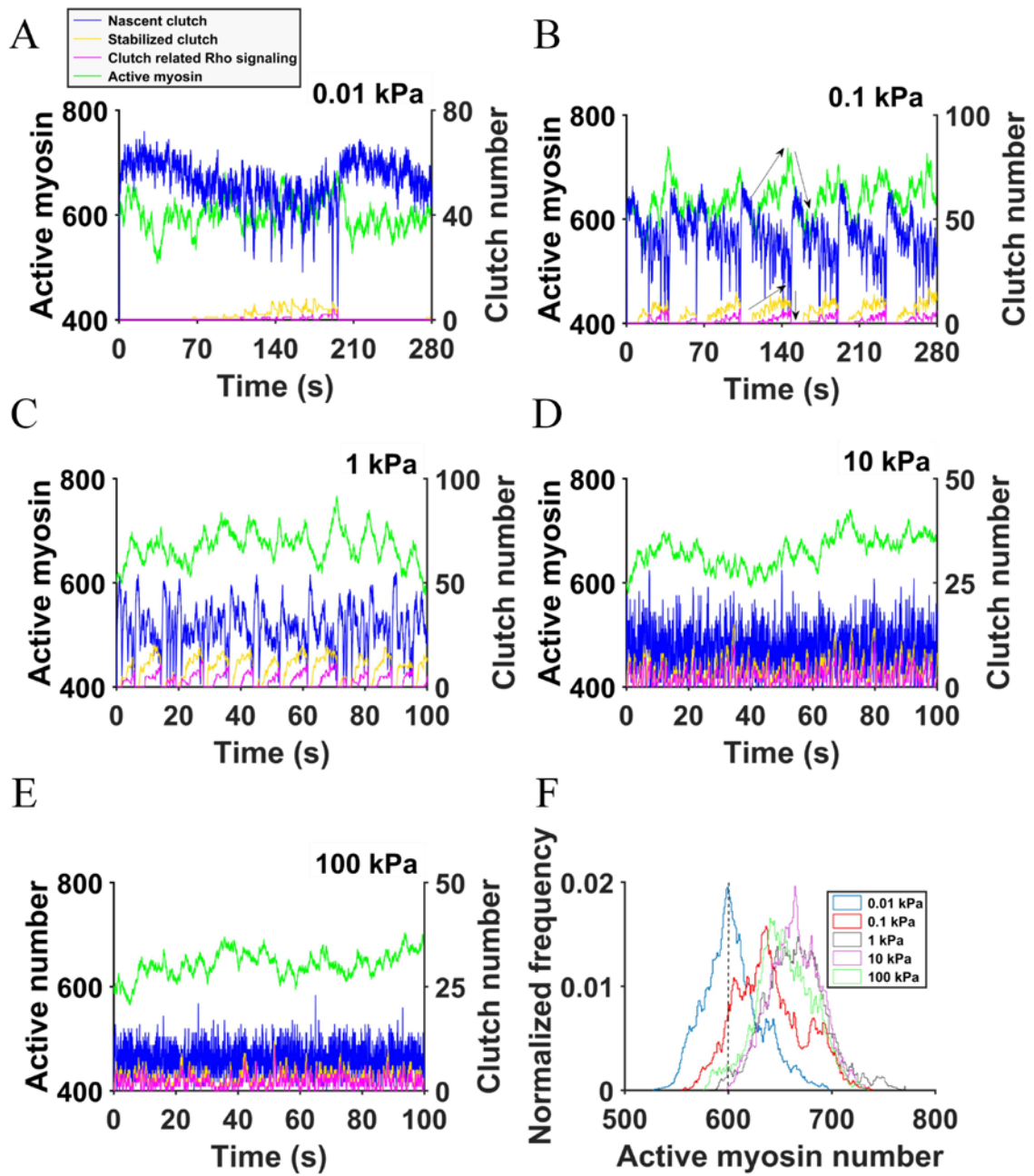
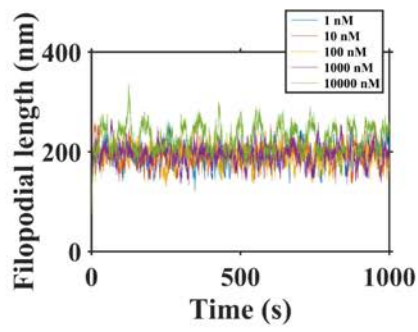
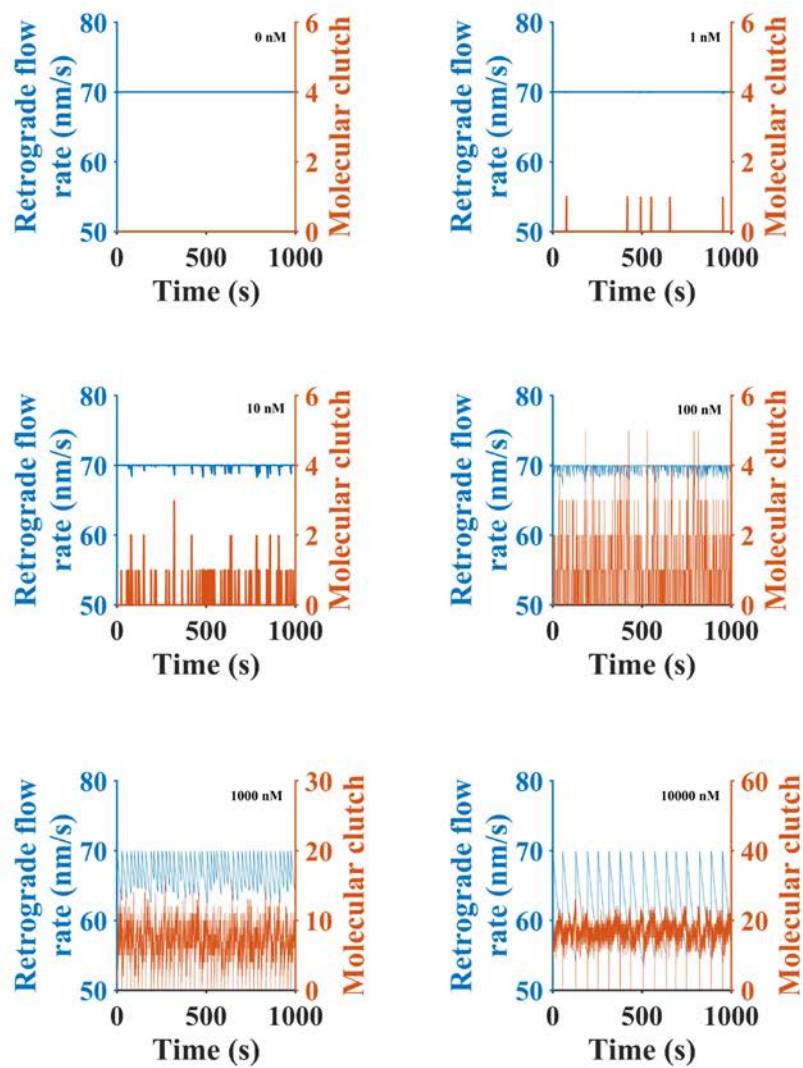


Figure S3. The effect of Rho signaling on myosin motor activation on substrate with different stiffness (0.01 kPa ~ 100 kPa).

A



B



**Figure S4. The effect of talin concentration on filopodial dynamics.**(A) Five individual trajectories are shown from stochastic simulations within 0  $\mu$ M ~10  $\mu$ M talin. (B) Retrograde flow is strongly influenced by the molecular clutch formation at 1 and 10  $\mu$ M talin.

### Simulation algorithm:

The stochastic filopodial dynamics model was implemented using a variable time step Gillespie Stochastic Simulation Algorithm (SSA), also known as a Kinetic Monte Carlo simulation. The simulation is allowed to run for  $10^8$  time steps ( $>1000s$ ) to ensure the simulation has reached steady-state before statistics are calculated in **Fig. 2-4**. 20 trajectories were generated for each set of parameter values in **fig. 5** for different substrate stiffness. For most results, we report the mean values obtained by averaging over the duration of at least one simulation.

1. The order of events in filopodial dynamics model was:

(1) Calculate the unbinding rate for each nascent and stabilized clutch, based on the current tension on clutch (product of clutch deformation and clutch stiffness). Talin-actin bond was modeled as a slip bond (one exponential with a positive exponent) and integrin-FN bond was modeled as a catch bond (the sum of two exponentials, one with positive exponent and the other with negative exponent). The parameters of such bonds were obtained after fitting the curve to previously experimental data (Fig1C, lifetime data in the figure correspond to the inverse of  $k_{off}$ ).

(2) Calculate the event time  $t_i$  for each possible reaction in each loop by Eq.S1

$$t_i = \frac{-\ln(RAN_i)}{k_i}, \quad (S1)$$

where  $RAN_i$  is a uniformly distributed random number between zero and one, and  $k_i$  is the kinetic rate for the following reactions:

- a) Active talin binding with inactive integrin forming talin-integrin complexes; talin-integrin complexes dissociation.

- b) Talin-integrin complexes binding with FN forming talin-integrin-FN complexes; talin-integrin-FN complexes dissociation.
- c) Talin-integrin complexes binding with actin forming talin-integrin-actin complexes; talin-integrin-actin complexes dissociation.
- d) Talin-integrin-FN complexes binding with actin forming actin-talin-integrin-FN complexes (nascent clutch); actin-talin-integrin-FN complexes unbinding at talin-actin interface.
- e) Talin-integrin-actin complexes binding with FN forming actin-talin-integrin-FN complexes (nascent clutch); actin-talin-integrin-FN complexes unbinding at integrin-FN interface.
- f) Talin in molecular clutch unfolding and refolding.
- g) Vinculin binding with unfolding talin's VBS site resulting in Actin-talin-vinculin-integrin-FN complexes (stabilized clutch).
- h) Integrin-FN interface in stabilized clutch unbinding leading to clutch bond break.
- i) Activation or inactivation of myosin.
- j) Actin and talin diffusion within in filopodium.
- k) Actin polymerization and depolymerization. Actin polymerization under membrane force was derived earlier (3),

$$k_{ona} = k_{ona0} e^{\left(-\frac{F_{mem}\delta}{k_B T}\right)}. \quad (S2)$$

- (3) Advance time by the minimum calculated event time.
- (4) Execute the reaction corresponding to the minimum calculated event time.
- (5) Calculate F-actin retrograde flow rate based on the current substrate deformation and

membrane force using the linear force-velocity relationship,

$$V_{retro} = V_u \left( 1 - \frac{F_{substrate}}{N_m F_b + F_{mem}} \right), \quad (S3)$$

$$F_{substrate} = K_{substrate} X_{substrate}. \quad (S4)$$

(6) Advance engaged clutch positions by the product of the F-actin retrograde flow rate and time step.

(7) Calculate substrate position through a force balance between the substrate and clutch springs (**Fig.S2**).

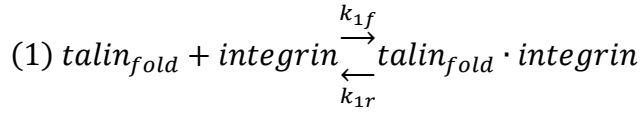
(8) Calculate filopodial length based on retrograde flow. If the barbed end resides beyond the last compartment, then update the number of compartments.

(9) Return to step 1.

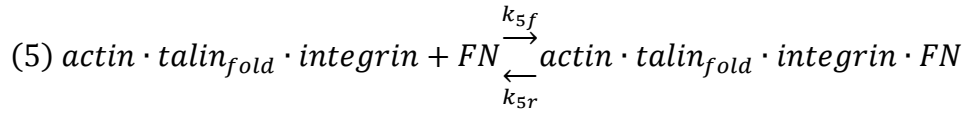
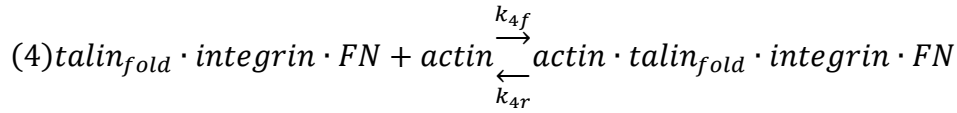
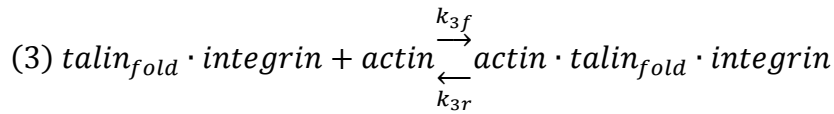
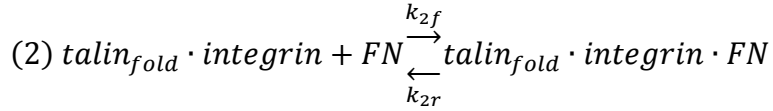


## Reactions of clutch adhesions in Gillespie set:

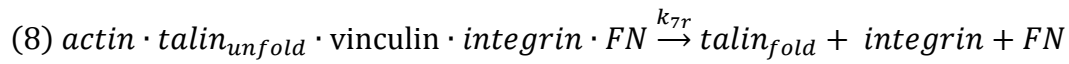
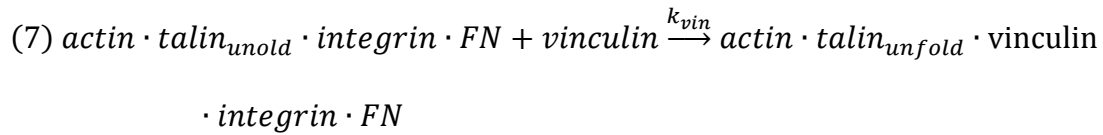
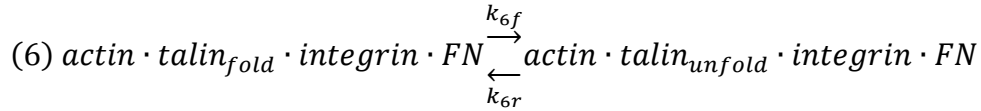
1. Inside-out activation of integrins by active talin



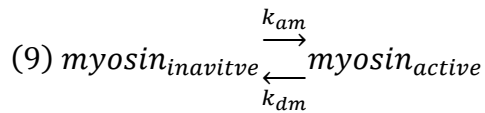
2. Formation of Mechanosensing links



3. Talin unfolding/refolding, vinculin binding, integrin-FN break and vinculin dissociation



4. Myosin activation



**The mathematical representation of reactions in clutch model:**

$$\frac{dC_{T\cdot I}}{dt} = k_{1f}C_T C_{ti} + k_{2r}C_{TIF} + k_{3r}C_{ATI} - (k_{1r} + k_{2f} + k_{3f})C_{T\cdot I} \quad (S5)$$

$$\frac{dC_{TIF}}{dt} = k_{2f}C_{T\cdot I} + k_{4r}C_{A\cdot T\cdot I\cdot F} - (k_{2r} + k_{4f})C_{TIF} \quad (S6)$$

$$\frac{dC_{ATI}}{dt} = k_{3f}C_{T\cdot I} + k_{5r}C_{A\cdot T\cdot I\cdot F} - (k_{3r} + k_{5f})C_{ATI} \quad (S7)$$

$$\frac{dC_{A\cdot T\cdot I\cdot F}}{dt} = k_{4f}C_{TIF} + k_{5f}C_{ATI} + k_{6r}C_{A\cdot T\cdot I\cdot F} - (k_{4r} + k_{5r} + k_{6f})C_{A\cdot T\cdot I\cdot F} \quad (S8)$$

$$\frac{dC_{A\cdot TU\cdot I\cdot F}}{dt} = k_{6f}C_{A\cdot T\cdot I\cdot F} - k_{6r}C_{A\cdot T\cdot I\cdot F} - k_{vin}C_{A\cdot TU\cdot I\cdot F} \quad (S9)$$

$$\frac{dC_{A\cdot T\cdot V\cdot I\cdot F}}{dt} = k_{vin}C_{A\cdot TU\cdot I\cdot F} - k_{7r}C_{A\cdot T\cdot V\cdot I\cdot F} \quad (S10)$$

$$\frac{dC_{Ma}}{dt} = k_{am}C_{Mina} - k_{dm}C_{Ma} \quad (S11)$$

In these equations,  $C_T$  represents the concentration of folding talin,  $C_{ti}$  represents the concentration of integrin,  $C_{T\cdot I}$  represents the concentration of talin·integrin complexes,  $C_{TIF}$  represents the concentration of talin·integrin·fibronectin complexes,  $C_{ATI}$  represents the concentration of actin·talin·integrin complexes,  $C_{A\cdot T\cdot I\cdot F}/C_{A\cdot TU\cdot I\cdot F}$  represents the concentration of actin·talin(fold/unfold)·integrin·fibronectin complexes,  $C_{A\cdot T\cdot V\cdot I\cdot F}$  represents the concentration of actin·talin·vinculin·integrin·fibronectin complexes,  $C_{Mina}/C_{Ma}$  represents the concentration of inactive/active myosin.

**Table S1. Baseline model parameters**

Parameter	Symbol	Value	Source	sensitivity
Integrin activation by talin	$k_{1f}$	$3.3 \text{ s}^{-1}$	(1)	
Talin-integrin dissociation	$k_{1r}$	$0.0042 \text{ s}^{-1}$	(1)	
Talin-integrin binding with FN	$k_{2f}$	$1.5 \text{ s}^{-1}$	(1)	
Talin-integrin-FN dissociation	$k_{2r}$	$0.1 \text{ s}^{-1}$	(1)	
Talin-integrin binding with actin	$k_{3f}$	$1.5 \text{ s}^{-1}$	(1)	
Talin-integrin-actin dissociation	$k_{3r}$	$0.1 \text{ s}^{-1}$	(1)	
Talin-integrin-FN binding with actin	$k_{4f}$	$1.5 \text{ s}^{-1}$	(1)	
Actin-talin bond dissociation	$k_{4r}$	<i>slip bond</i>	(2)	
Talin-integrin-FN binding with actin	$k_{5f}$	$1.5 \text{ s}^{-1}$	(1)	
Integrin-FN bond dissociation in nascent clutch	$k_{5r}$	<i>catch bond</i>	(2)	
Talin unfolding	$k_{6f}$	<i>slip bond</i>	(2)	
Talin refolding	$k_{6r}$	<i>slip bond</i>	(2)	
Vinculin on-rate	$k_{onv}$	$1 \text{ s}^{-1}$	$0.1 \sim 10 \text{ s}^{-1}$	1.04
Integrin-FN bond dissociation in stabilized clutch	$k_{7r}$	<i>catch bond</i>	(2)	
Actin-talin bond rupture force	$F_{tb}$	2 pN	$0.5 \sim 2.5 \text{ pN}$	0.86
Clutch spring constant	$K_t$	1 pN/nm	(2)	
Concentration of actin at the filopodial base	$C_A$	10 $\mu\text{M}$	(3)	
Concentration of talin at the filopodial base	$C_T$	0 ~ 10 $\mu\text{M}$	(3)	
Integrin density per compartment	$C_{ii}$	0.1	(1)	
Half of actin monomer size	$\delta$	2.7 nm	(3)	
Diffusion rate	$k_D$	$5/16 \mu\text{m}^2 \text{ s}^{-1}$	(4)	
Actin polymerization rate	$k_{ona}$	$50 \text{ s}^{-1}$	(5)	
Actin depolymerization rate	$k_{offa}$	$1.4 \text{ s}^{-1}$	(6)	
Membrane force	$F_{mem}$	10 pN	(3)	
Initial number of active motors	$C_a$	600	set	
Number of inactive motors in cytoplasm	$C_{ina}$	120	set	
Motor stall force	$F_b$	2 pN	(2)	

Motor unloaded retrograde flow velocity	$V_u$	110 nm/s	(2)	
Maximum motor binding rate	$\alpha k_{am0}$	$0.05 \text{ s}^{-1}$	(7)	
Minimum motor binding rate	$k_{am0}$	$0.01 \text{ s}^{-1}$	(7)	
Motor unbinding rate	$k_{dm0}$	$0.002 \text{ s}^{-1}$	(7)	
Characteristic force, activated adhesion signalling	$F_R$	10~25 pN	(7)	
Saturation constant, Rho effect on myosin activation	$\lambda$	0.1	0~1	0.0
Radius of circular adhesion site	$a$	550 nm	(8)	

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**Table S2. Model parameters range for Fig. 2-5 and Fig. S3**

Figure	Actin-talin bond rupture force $F_{tb}$ (pN)	Vinculin binding $k_{vm}^{-1}$ (s)	Integrin clustering		Rho effect on myosin activation $\lambda$	Integrin density $C_{ii}$	Clutch spring constant $K$ (pN/nm)
			1. linearity function	2. Gaussian function - no clustering			
Fig.2	0.5~2.5	-	-	-	-	0.1	1
Fig.3A	1.5	0.1/1/10	-	-	-	0.1	1
Fig. 3B	1.5	0.1/1/10	-	-	-	1	1
Fig. 3C	1.5	10	-	-	-	0.1/1	1
Fig. 3D	1.5	10	-	-	-	0.1/1	1
Fig. 3H (red line)	1.5	10	1	-	-	-	1
Fig. 3H (blue line)	1.5	10	2	-	-	-	1
Fig. 3H (black line)	5	10	-	-	-	0.1	1700
Fig. 4	1.5	10	-	-	0~1	0.1	1
Fig. S3	1.5	10	-	-	0.1	0.1	1

**Table S3. Statistical significance tests for Fig. 5**

Figure panel	Statistical significance
Fig. 5A	$P < 0.05$ between $E_{ecm} = 0.1$ kPa, 1 kPa, 10 kPa, 100 kPa only above 1000 nM
Fig. 5B	$P < 0.02$ between $F_{mem} = 0$ pN, 5 pN, 10 pN in the range of 0.1 kPa ~ 100 kPa
Fig. 5C	$P < 0.05$ between $F_{unf} = 5$ pN, 10 pN, 30 pN only below 15.8 kPa
Fig. 5D	$P < 0.05$ between $F_{Rho} = 10$ pN, 15 pN, 20 pN only below 4 kPa

## Supplementary References

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