

Supplemental Material

**General expressions for $R_{1\rho}$ relaxation for N -site chemical exchange
and the special case of linear chains**

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I. Reduction of the 12×12 linear four-site mechanism evolution matrix to a 3×3 matrix

The evolution matrix for the linear four-site exchange mechanism is:

$$\mathbf{L} + \mathbf{K} = \begin{pmatrix} \mathbf{L}_A & 0 & 0 & 0 \\ 0 & \mathbf{L}_B & 0 & 0 \\ 0 & 0 & \mathbf{L}_C & 0 \\ 0 & 0 & 0 & \mathbf{L}_D \end{pmatrix} + \begin{pmatrix} -k_{12} & k_{21} & 0 & 0 \\ k_{12} & -k_{21} - k_{13} & k_{31} & 0 \\ 0 & k_{13} & -k_{31} - k_{34} & k_{43} \\ 0 & 0 & k_{34} & -k_{43} \end{pmatrix} \otimes \mathbf{I} \quad (\text{S1})$$

The first application of the matrix determinant lemma yields:

$$\begin{aligned} 0 &= |\mathbf{L} + \mathbf{K} - \lambda \mathbf{I}| \\ &= |\mathbf{L}_A - \lambda \mathbf{I}| |\mathbf{L}_B - \lambda \mathbf{I}| |\mathbf{L}_C - \lambda \mathbf{I}| |\mathbf{L}_D - \lambda \mathbf{I}| \\ &\quad \times \left| \mathbf{I} + \begin{pmatrix} -k_{12} & k_{21} & 0 & 0 \\ 0 & -k_{13} & k_{31} & 0 \\ 0 & 0 & -k_{34} & k_{43} \end{pmatrix} \begin{pmatrix} (\mathbf{L}_A - \lambda \mathbf{I})^{-1} & 0 & 0 & 0 \\ 0 & (\mathbf{L}_B - \lambda \mathbf{I})^{-1} & 0 & 0 \\ 0 & 0 & (\mathbf{L}_C - \lambda \mathbf{I})^{-1} & 0 \\ 0 & 0 & 0 & (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ -1 & 1 & 0 \\ 0 & -1 & 1 \\ 0 & 0 & -1 \end{pmatrix} \right| \\ &= |\mathbf{L}_A - \lambda \mathbf{I}| |\mathbf{L}_B - \lambda \mathbf{I}| |\mathbf{L}_C - \lambda \mathbf{I}| |\mathbf{L}_D - \lambda \mathbf{I}| \\ &\quad \times \left| \begin{pmatrix} \mathbf{I} - k_{12}(\mathbf{L}_A - \lambda \mathbf{I})^{-1} - k_{21}(\mathbf{L}_A - \lambda \mathbf{I})^{-1} & k_{21}(\mathbf{L}_B - \lambda \mathbf{I})^{-1} & 0 \\ k_{13}(\mathbf{L}_B - \lambda \mathbf{I})^{-1} & \mathbf{I} - k_{13}(\mathbf{L}_B - \lambda \mathbf{I})^{-1} - k_{31}(\mathbf{L}_C - \lambda \mathbf{I})^{-1} & k_{31}(\mathbf{L}_C - \lambda \mathbf{I})^{-1} \\ 0 & k_{34}(\mathbf{L}_C - \lambda \mathbf{I})^{-1} & -k_{34}(\mathbf{L}_C - \lambda \mathbf{I})^{-1} - k_{43}(\mathbf{L}_D - \lambda \mathbf{I})^{-1} \end{pmatrix} \right| \\ &= |\mathbf{L}_A - \lambda \mathbf{I}| |\mathbf{L}_B - \lambda \mathbf{I}| |\mathbf{L}_C - \lambda \mathbf{I}| |\mathbf{L}_D - \lambda \mathbf{I}| \\ &\quad \times \left| \begin{pmatrix} \mathbf{I} - k_{12}(\mathbf{L}_A - \lambda \mathbf{I})^{-1} & 0 & 0 \\ 0 & \mathbf{I} & 0 \\ 0 & 0 & \mathbf{I} - k_{43}(\mathbf{L}_D - \lambda \mathbf{I})^{-1} \end{pmatrix} \right. \\ &\quad \left. + \begin{pmatrix} \mathbf{I} - k_{21}(\mathbf{L}_B - \lambda \mathbf{I})^{-1} & k_{21}(\mathbf{L}_B - \lambda \mathbf{I})^{-1} & 0 \\ k_{13}(\mathbf{L}_B - \lambda \mathbf{I})^{-1} & \mathbf{I} - k_{13}(\mathbf{L}_B - \lambda \mathbf{I})^{-1} - k_{31}(\mathbf{L}_C - \lambda \mathbf{I})^{-1} & k_{31}(\mathbf{L}_C - \lambda \mathbf{I})^{-1} \\ 0 & k_{34}(\mathbf{L}_C - \lambda \mathbf{I})^{-1} & -k_{34}(\mathbf{L}_C - \lambda \mathbf{I})^{-1} \end{pmatrix} \right| \end{aligned} \quad (\text{S2})$$

The second application of the matrix determinant lemma yields:

$$\begin{aligned}
0 &= |\mathbf{L}_A - \lambda \mathbf{I}| |\mathbf{L}_B - \lambda \mathbf{I}| |\mathbf{L}_C - \lambda \mathbf{I}| |\mathbf{L}_D - \lambda \mathbf{I}| \left| \mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1} \right| \left| \mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \right| \\
&\quad \times \left| \mathbf{I} + \begin{pmatrix} -(\mathbf{L}_B - \lambda \mathbf{I})^{-1} & (\mathbf{L}_B - \lambda \mathbf{I})^{-1} & 0 \\ 0 & (\mathbf{L}_C - \lambda \mathbf{I})^{-1} & -(\mathbf{L}_C - \lambda \mathbf{I})^{-1} \end{pmatrix} \right| \\
&\quad \times \left(\begin{array}{ccc} \mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1} & 0 & 0 \\ 0 & \mathbf{I} & 0 \\ 0 & 0 & \mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \end{array} \right) \begin{pmatrix} k_{21} & 0 \\ -k_{13} & -k_{31} \\ 0 & k_{34} \end{pmatrix} \\
&= |\mathbf{L}_A - \lambda \mathbf{I}| |\mathbf{L}_B - \lambda \mathbf{I}| |\mathbf{L}_C - \lambda \mathbf{I}| |\mathbf{L}_D - \lambda \mathbf{I}| \left| \mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1} \right| \left| \mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \right| \\
&\quad \times \left(\begin{array}{ccc} \mathbf{I} - k_{21} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} (\mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1}) - k_{13} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} & & -k_{31} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} \\ & -k_{13} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} & \\ & & \mathbf{I} - k_{31} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} - k_{34} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} (\mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1}) \end{array} \right) \\
&= |\mathbf{L}_A - \lambda \mathbf{I}| |\mathbf{L}_B - \lambda \mathbf{I}| |\mathbf{L}_C - \lambda \mathbf{I}| |\mathbf{L}_D - \lambda \mathbf{I}| \left| \mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1} \right| \left| \mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \right| \\
&\quad \times \left(\begin{array}{ccc} \mathbf{I} - k_{21} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} (\mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1}) & 0 & \\ 0 & & \mathbf{I} - k_{34} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} (\mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1}) \end{array} \right) - \begin{pmatrix} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} \\ (\mathbf{L}_C - \lambda \mathbf{I})^{-1} \end{pmatrix} \begin{pmatrix} k_{13} & k_{31} \end{pmatrix} \\
\end{aligned} \tag{S3}$$

The third and last application of the matrix determinant lemma yields:

$$\begin{aligned}
0 &= |\mathbf{L}_A - \lambda \mathbf{I}| |\mathbf{L}_B - \lambda \mathbf{I}| |\mathbf{L}_C - \lambda \mathbf{I}| |\mathbf{L}_D - \lambda \mathbf{I}| \left| \mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1} \right| \left| \mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \right| \\
&\quad \times \left| \mathbf{I} - k_{21} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} (\mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1})^{-1} \right| \left| \mathbf{I} - k_{34} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} (\mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1})^{-1} \right| \\
&\quad \times \left| \mathbf{I} - \begin{pmatrix} k_{13} & k_{31} \end{pmatrix} \begin{pmatrix} \left(\mathbf{I} - k_{21} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} (\mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1})^{-1} \right)^{-1} & 0 \\ 0 & \left(\mathbf{I} - k_{34} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} (\mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1})^{-1} \right)^{-1} \end{pmatrix} \right| \\
&\quad \times \begin{pmatrix} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} \\ (\mathbf{L}_C - \lambda \mathbf{I})^{-1} \end{pmatrix} \\
&= |\mathbf{L}_A - \lambda \mathbf{I}| |\mathbf{L}_B - \lambda \mathbf{I}| |\mathbf{L}_C - \lambda \mathbf{I}| |\mathbf{L}_D - \lambda \mathbf{I}| \left| \mathbf{I} - k_{12} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} \right| \left| \mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \right| \\
&\quad \times \left| \mathbf{I} - k_{21} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} (\mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1})^{-1} \right| \left| \mathbf{I} - k_{34} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} (\mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1})^{-1} \right|
\end{aligned}$$

$$\begin{aligned}
& \left| \begin{array}{l} \mathbf{I} - k_{13} \left(\mathbf{I} - k_{21} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} \left(\mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1} \right)^{-1} \right)^{-1} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} \\ \times \\ -k_{31} \left(\mathbf{I} - k_{34} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} \left(\mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \right)^{-1} \right)^{-1} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} \end{array} \right| \\
& = \left| (\mathbf{L}_A - \lambda \mathbf{I}) \left(\mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1} \right) \right| \left| (\mathbf{L}_D - \lambda \mathbf{I}) \left(\mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \right)^{-1} \right| \\
& \left| (\mathbf{L}_B - \lambda \mathbf{I}) - k_{21} \left(\mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1} \right)^{-1} \right| \left| (\mathbf{L}_C - \lambda \mathbf{I}) - k_{34} \left(\mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \right)^{-1} \right| \\
& \left| \begin{array}{l} \mathbf{I} - k_{13} \left(\mathbf{I} - k_{21} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} \left(\mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1} \right)^{-1} \right)^{-1} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} \\ \times \\ -k_{31} \left(\mathbf{I} - k_{34} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} \left(\mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \right)^{-1} \right)^{-1} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} \end{array} \right| \\
& = \left| (\mathbf{L}_A - \lambda \mathbf{I} - k_{12} \mathbf{I}) \left((\mathbf{L}_B - \lambda \mathbf{I}) - k_{21} \left(\mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1} \right)^{-1} \right) \right| \\
& \times \left| (\mathbf{L}_D - \lambda \mathbf{I} - k_{43} \mathbf{I}) \left((\mathbf{L}_C - \lambda \mathbf{I}) - k_{34} \left(\mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \right)^{-1} \right) \right| \\
& \left| \begin{array}{l} \mathbf{I} - k_{13} \left(\mathbf{I} - k_{21} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} \left(\mathbf{I} - k_{12} (\mathbf{L}_A - \lambda \mathbf{I})^{-1} \right)^{-1} \right)^{-1} (\mathbf{L}_B - \lambda \mathbf{I})^{-1} \\ \times \\ -k_{31} \left(\mathbf{I} - k_{34} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} \left(\mathbf{I} - k_{43} (\mathbf{L}_D - \lambda \mathbf{I})^{-1} \right)^{-1} \right)^{-1} (\mathbf{L}_C - \lambda \mathbf{I})^{-1} \end{array} \right| \tag{S4} \\
& \left| \left\{ (\mathbf{L}_A - \lambda \mathbf{I} - k_{12} \mathbf{I}) (\mathbf{L}_B - \lambda \mathbf{I}) - k_{21} (\mathbf{L}_A - \lambda \mathbf{I}) \right\} \left\{ (\mathbf{L}_D - \lambda \mathbf{I} - k_{43} \mathbf{I}) (\mathbf{L}_C - \lambda \mathbf{I}) - k_{34} (\mathbf{L}_D - \lambda \mathbf{I}) \right\} \right| \\
& = \left| \begin{array}{l} -k_{13} (\mathbf{L}_A - \lambda \mathbf{I} - k_{12} \mathbf{I}) \left((\mathbf{L}_D - \lambda \mathbf{I} - k_{43} \mathbf{I}) (\mathbf{L}_C - \lambda \mathbf{I}) - k_{34} (\mathbf{L}_D - \lambda \mathbf{I}) \right) \\ -k_{31} (\mathbf{L}_D - \lambda \mathbf{I} - k_{43} \mathbf{I}) \left((\mathbf{L}_A - \lambda \mathbf{I} - k_{12} \mathbf{I}) (\mathbf{L}_B - \lambda \mathbf{I}) - k_{21} (\mathbf{L}_A - \lambda \mathbf{I}) \right) \end{array} \right| \\
& = \left| (\mathbf{L}'_A - \lambda \mathbf{I}) (\mathbf{L}'_B - \lambda \mathbf{I}) (\mathbf{L}'_C - \lambda \mathbf{I}) (\mathbf{L}'_D - \lambda \mathbf{I}) + k_{12} k_{21} k_{34} k_{43} \mathbf{I} - k_{34} k_{43} \left| (\mathbf{L}'_A - \lambda \mathbf{I}) (\mathbf{L}'_B - \lambda \mathbf{I}) \right| \right. \\
& \left. - k_{13} k_{31} \left| (\mathbf{L}'_A - \lambda \mathbf{I}) (\mathbf{L}'_D - \lambda \mathbf{I}) \right| - k_{12} k_{21} \left| (\mathbf{L}'_C - \lambda \mathbf{I}) (\mathbf{L}'_D - \lambda \mathbf{I}) \right| \right|
\end{aligned}$$

Expanding the above expression and collecting powers of λ yields:

$$\begin{aligned}
0 &= \mathbf{L}'_A \mathbf{L}'_B \mathbf{L}'_C \mathbf{L}'_D - k_{34} k_{43} \mathbf{L}'_A \mathbf{L}'_B - k_{13} k_{31} \mathbf{L}'_C \mathbf{L}'_D + k_{12} k_{21} k_{34} k_{43} \\
& - \lambda \left\{ \begin{array}{l} \mathbf{L}'_A \mathbf{L}'_B \mathbf{L}'_C + \mathbf{L}'_A \mathbf{L}'_B \mathbf{L}'_D + \mathbf{L}'_A \mathbf{L}'_C \mathbf{L}'_D + \mathbf{L}'_B \mathbf{L}'_C \mathbf{L}'_D \\ - (k_{13} k_{31} + k_{34} k_{43}) \mathbf{L}'_A - k_{34} k_{43} \mathbf{L}'_B - k_{13} k_{31} \mathbf{L}'_C - (k_{12} k_{21} + k_{13} k_{31}) \mathbf{L}'_D \end{array} \right\} \tag{S5} \\
& + \lambda^2 \left\{ \sum_{\substack{i,j \\ j>i}} \mathbf{L}'_i \mathbf{L}'_j - k_{12} k_{21} - k_{13} k_{31} - k_{34} k_{43} \right\} + \lambda^3 \left\{ \mathbf{L}'_A + \mathbf{L}'_B + \mathbf{L}'_C + \mathbf{L}'_D \right\} + \lambda^4
\end{aligned}$$

Keeping only the three lowest order terms in λ yields Eq. (42).

II. Woodbury approximation for the triangular three-site scheme

In the following, “first” refers to the first order approximation, “second” to the second order approximation. The first order approximation of R_{ex} in a triangular three-site exchange situation can be written as (Eq. 48)

$$R_{ex}^{triang,first} = R_{ex}^{linear,first} \left[\frac{1}{1 + \sin^2 \theta R_{ex}^{linear,first} Tr\{\mathbf{Z}\}} \right] \quad (S6)$$

The inverse of R_{ex} is:

$$\frac{1}{R_{ex}^{triang,first}} = \frac{1}{R_{ex}^{linear,first}} \left[1 + \sin^2 \theta R_{ex}^{linear,first} Tr\{\mathbf{Z}\} \right] \quad (S7)$$

The absolute value of differences of reciprocal R_{ex} values can be used to obtain a new approximation for $R_{ex}^{triang,exact}$, which we call $R_{ex}^{triang,new}$:

$$\begin{aligned} \left| \frac{1}{R_{ex}^{triang,new}} - \frac{1}{R_{ex}^{triang,exact}} \right| &< \left| \frac{1}{R_{ex}^{triang,first}} - \frac{1}{R_{ex}^{triang,exact}} \right| \\ \Leftrightarrow \left| \frac{1}{R_a} \left[1 + \sin^2 \theta R_b Tr\{\mathbf{Z}\} \right] - \frac{1}{R_{ex}^{triang,exact}} \right| &< \left| \frac{1}{R_{ex}^{triang,first}} - \frac{1}{R_{ex}^{triang,exact}} \right| \end{aligned} \quad (S8)$$

in which R_a and R_b must be determined and in which vertical bars denote absolute values. The two cases in which $R_{ex}^{triang,new}$ is smaller or larger than $R_{ex}^{triang,exact}$ must be considered separately.

Note that $R_{ex}^{triang,exact} > R_{ex}^{triang,first}$ and $R_{ex}^{linear,exact} > R_{ex}^{linear,first}$.

$$\begin{aligned} \text{In the first case, } R_{ex}^{triang,new} < R_{ex}^{triang,exact} \text{ and } R_{ex}^{triang,first} < R_{ex}^{triang,exact} : \\ \frac{1}{R_a} \left[1 + \sin^2 \theta R_b Tr\{\mathbf{Z}\} \right] - \frac{1}{R_{ex}^{triang,exact}} &< \frac{1}{R_{ex}^{triang,first}} - \frac{1}{R_{ex}^{triang,exact}} \\ \Leftrightarrow \frac{1}{R_a} \left[1 + \sin^2 \theta R_b Tr\{\mathbf{Z}\} \right] &< \frac{1}{R_{ex}^{triang,first}} \end{aligned} \quad (S9)$$

Setting R_a to $R_{ex}^{linear,exact}$ and R_b to $R_{ex}^{linear,first}$ yields

$$\frac{1}{R_{ex}^{linear,exact}} < \frac{1}{R_{ex}^{linear,first}} \Leftrightarrow R_{ex}^{linear,exact} > R_{ex}^{linear,first} \quad (S10)$$

which is true as noted above. Setting both R_a and R_b to $R_{ex}^{linear,exact}$ usually violates the condition $R_{ex}^{triang,new} < R_{ex}^{triang,exact}$, as shown empirically.

In the second case, $R_{ex}^{triang,new} > R_{ex}^{triang,exact}$ and $R_{ex}^{triang,first} < R_{ex}^{triang,exact}$:

$$\begin{aligned} -\frac{1}{R_a} [1 + \sin^2 \theta R_b Tr\{\mathbf{Z}\}] + \frac{1}{R_{ex}^{triang,exact}} &< \frac{1}{R_{ex}^{triang,first}} - \frac{1}{R_{ex}^{triang,exact}} \\ \Leftrightarrow \frac{2}{R_{ex}^{triang,exact}} - \frac{1}{R_{ex}^{triang,first}} &< \frac{1}{R_a} [1 + \sin^2 \theta R_b Tr\{\mathbf{Z}\}] \\ \Leftrightarrow \frac{2}{R_{ex}^{triang,exact}} - \frac{1}{R_{ex}^{triang,first}} &< \frac{1}{R_a} + \frac{R_b}{R_a} \left[\frac{1}{R_{ex}^{triang,first}} - \frac{1}{R_{ex}^{linear,first}} \right] \end{aligned} \quad (S11)$$

Again, setting $R_a = R_{ex}^{linear,exact}$ and $R_b = R_{ex}^{linear,first}$ yields:

$$\begin{aligned} \frac{2}{R_{ex}^{triang,exact}} - \frac{1}{R_{ex}^{triang,first}} &< \frac{1}{R_{ex}^{linear,exact}} + \frac{R_{ex}^{linear,first}}{R_{ex}^{linear,exact} R_{ex}^{triang,first}} - \frac{1}{R_{ex}^{linear,exact}} \\ \Leftrightarrow \frac{2}{R_{ex}^{triang,exact}} &< \frac{R_{ex}^{linear,first}}{R_{ex}^{linear,exact} R_{ex}^{triang,first}} + \frac{1}{R_{ex}^{triang,first}} \\ \Leftrightarrow \frac{R_{ex}^{triang,first}}{R_{ex}^{triang,exact}} &< \frac{R_{ex}^{linear,first}}{2R_{ex}^{linear,exact}} + \frac{1}{2} \end{aligned} \quad (S12)$$

which establishes a boundary condition that is frequently, but not always met. In contrast, setting $a = R_{ex}^{linear,exact}$ and $b = R_{ex}^{linear,exact}$ lead to a boundary condition, which is, as empirically shown, usually not met:

$$\begin{aligned}
& \frac{2}{R_{ex}^{triang,exact}} - \frac{1}{R_{ex}^{triang,first}} < \frac{1}{R_{ex}^{linear,exact}} + \frac{1}{R_{ex}^{triang,first}} - \frac{1}{R_{ex}^{linear,first}} \\
& \Leftrightarrow \frac{2}{R_{ex}^{triang,exact}} + \frac{1}{R_{ex}^{linear,first}} < \frac{2}{R_{ex}^{triang,first}} + \frac{1}{R_{ex}^{linear,exact}} \\
& \Leftrightarrow 2 \left(\frac{1}{R_{ex}^{triang,exact}} - \frac{1}{R_{ex}^{triang,first}} \right) > \frac{1}{R_{ex}^{linear,exact}} - \frac{1}{R_{ex}^{linear,first}}
\end{aligned} \tag{S13}$$

The new approximation for the triangular three-site scheme performs better than the first-order approximation if the boundary condition Eq. S12 is met.

As a result of the above considerations, the new approximation for R_{ex} is:

$$R_{ex}^{triang,new} = R_{ex}^{linear,exact} \left[\frac{1}{1 + \sin^2 \theta R_{ex}^{linear,first} Tr\{\mathbf{Z}\}} \right] \tag{S14}$$

and $R_{ex}^{linear,exact}$ can be substituted by $R_{ex}^{linear,second}$, giving the Woodbury approximation:

$$R_{ex}^{triang,Woodbury} = R_{ex}^{linear,second} \left[\frac{1}{1 + \sin^2 \theta R_{ex}^{linear,first} Tr\{\mathbf{Z}\}} \right] \tag{S15}$$

III. Fitting three-state models

Aspects of using the above expressions for fitting to experimental data are described below for three-state models; extension to more complex topologies are straightforward. The exchange contribution to relaxation is

$$-\lambda = \sin^2 \theta R_{ex} = -1 / Tr \left\{ (\mathbf{L} + \mathbf{K})^{-1} \right\} \quad (\text{S16})$$

and for a triangular three-state model,

$$\mathbf{L} = \begin{bmatrix} \mathbf{L}_A & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathbf{L}_B & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \mathbf{L}_C \end{bmatrix} \quad (\text{S17})$$

in which

$$\begin{aligned} L_A &= \begin{bmatrix} 0 & -\delta_A & 0 \\ \delta_A & 0 & -\omega_1 \\ 0 & \omega_1 & 0 \end{bmatrix} \\ &= \begin{bmatrix} 0 & -\Delta\Omega + p_B\Omega_{BA} + (1-p_A-p_B)\Omega_{CA} & 0 \\ \Delta\Omega - p_B\Omega_{BA} - (1-p_A-p_B)\Omega_{CA} & 0 & -\omega_1 \\ 0 & \omega_1 & 0 \end{bmatrix} \\ L_B &= \begin{bmatrix} 0 & -\delta_B & 0 \\ \delta_B & 0 & -\omega_1 \\ 0 & \omega_1 & 0 \end{bmatrix} \\ &= \begin{bmatrix} 0 & -\Delta\Omega - (1-p_B)\Omega_{BA} + (1-p_A-p_B)\Omega_{CA} & 0 \\ \Delta\Omega + (1-p_B)\Omega_{BA} - (1-p_A-p_B)\Omega_{CA} & 0 & -\omega_1 \\ 0 & \omega_1 & 0 \end{bmatrix} \\ L_C &= \begin{bmatrix} 0 & -\delta_C & 0 \\ \delta_C & 0 & -\omega_1 \\ 0 & \omega_1 & 0 \end{bmatrix} \\ &= \begin{bmatrix} 0 & -\Delta\Omega + p_B\Omega_{BA} - (p_A+p_B)\Omega_{CA} & 0 \\ \Delta\Omega - p_B\Omega_{BA} + (p_A+p_B)\Omega_{CA} & 0 & -\omega_1 \\ 0 & \omega_1 & 0 \end{bmatrix} \end{aligned} \quad (\text{S18})$$

$$\begin{aligned}
\mathbf{K} &= \begin{bmatrix} -k_{12} - k_{13} & k_{21} & k_{31} \\ k_{12} & -k_{21} - k_{23} & k_{32} \\ k_{13} & k_{23} & -k_{31} - k_{32} \end{bmatrix} \otimes \mathbf{I} \\
&= \begin{bmatrix} -\frac{p_B k_{AB}}{p_A + p_B} - \frac{(1-p_A-p_B)k_{AC}}{1-p_B} & \frac{p_A k_{AB}}{p_A + p_B} & \frac{p_A k_{AC}}{1-p_B} \\ \frac{p_B k_{AB}}{p_A + p_B} & -\frac{p_A k_{AB}}{p_A + p_B} - \frac{(1-p_A-p_B)k_{BC}}{1-p_A} & \frac{p_B k_{BC}}{1-p_A} \\ \frac{(1-p_A-p_B)k_{AC}}{1-p_B} & \frac{(1-p_A-p_B)k_{BC}}{1-p_A} & -\frac{p_A k_{AC}}{1-p_B} - \frac{p_B k_{BC}}{1-p_A} \end{bmatrix} \otimes \mathbf{I}
\end{aligned} \tag{S19}$$

$$\Omega_{mA} = \Omega_m - \Omega_A, k_{AB} = k_{12} + k_{21}, k_{AC} = k_{13} + k_{31}, \text{ and } k_{BC} = k_{23} + k_{32}.$$

In the above equations, the known quantities are $\Delta\Omega$ and ω_1 ; the parameters to be optimized are p_A , p_B , Ω_{AB} , Ω_{AC} , k_{AB} , k_{AC} , and k_{BC} . Use of these variables incorporates the constraints that $p_A + p_B + p_C = 1$ and that the change in free-energy around the reaction cycle must be zero (which constrains k_{23}/k_{32} given the other rate constants). The exchange matrix for the linear three-site model in which A is the middle state (A exchanges with B and C) is obtained by setting $k_{BC} = 0$. The exchange matrix for the linear three-site model in which A is the end state (A exchanges with B and B exchanges with C) is obtained by setting $k_{AC} = 0$. In practice, independent estimates of some of these parameters, such as limiting chemical shifts, may be necessary to reduce the complexity of data fitting. The derivative of $\sin^2\theta R_{ex}$ with respect to a parameter x is:

$$\frac{d(\sin^2\theta R_{ex})}{dx} = \frac{\text{Tr} \left\{ (\mathbf{L} + \mathbf{K})^{-2} \frac{d(\mathbf{L} + \mathbf{K})}{dx} \right\}}{\text{Tr}^2 \left\{ (\mathbf{L} + \mathbf{K})^{-1} \right\}} \tag{S20}$$

which is needed for gradient-based optimization methods. The derivative on the right-hand-side of Eq. S20 is obtained analytically from Eqs. S16-S19. For example,

$$\frac{d(\mathbf{L} + \mathbf{K})}{d\Omega_{BA}} = \begin{bmatrix} \frac{d\mathbf{L}_A}{d\Omega_{BA}} & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \frac{d\mathbf{L}_B}{d\Omega_{BA}} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} & \frac{d\mathbf{L}_C}{d\Omega_{BA}} \end{bmatrix} \quad (\text{S21})$$

$$\begin{aligned} \frac{d\mathbf{L}_A}{d\Omega_{BA}} &= \begin{bmatrix} 0 & -p_B & 0 \\ p_B & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \\ \frac{d\mathbf{L}_B}{d\Omega_{BA}} &= \begin{bmatrix} 0 & (1-p_B) & 0 \\ -(1-p_B) & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \\ \frac{d\mathbf{L}_C}{d\Omega_{BA}} &= \begin{bmatrix} 0 & -p_B & 0 \\ p_B & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \end{aligned} \quad (\text{S22})$$

As another example,

$$\frac{d(\mathbf{L} + \mathbf{K})}{dk_{AB}} = \frac{1}{p_A + p_B} \begin{bmatrix} -p_B & p_A & 0 \\ p_B & -p_A & 0 \\ 0 & 0 & 0 \end{bmatrix} \otimes \mathbf{I} \quad (\text{S23})$$

Note that Equations S16 and S20 are not expanded analytically (that is, algebraic expressions for the matrix inverses are not needed); rather, numerical values are calculated for each combination of parameters directly from these equations.

IV. Supplemental Figure Captions

Figure S1. $R_{1\rho}$ magnetization decay for two-site chemical exchange. Calculations were performed by numerical evaluation of the integrated Bloch-McConnell equation for each decay component in Eq. 6, using $a_i = \mathbf{d} \left| \mathbf{u}_i \right\rangle \left\langle \mathbf{u}_i^{-1} \right| \mathbf{M}(0)$. Parameters used for the calculations were $p_A = 0.5, p_B = 0.5, \omega_1 = 100 \text{ s}^{-1}, \Omega_B - \Omega_A = 1000 \text{ s}^{-1}, \Delta\Omega = 500 \text{ s}^{-1}, R_1 = 1.5 \text{ s}^{-1}, R_2 = 11 \text{ s}^{-1}$ and $k_{ex} = k_{12} + k_{21} = 1000 \text{ s}^{-1}$. Magnetization decay for the components associated with the (a) least negative, real eigenvalue and (b) the second real eigenvalue. (c) and (d) Real-valued magnetization decays obtained by addition of pairs of components for complex conjugate eigenvalues.

Figure S2. Offset dependence of the R_{ex} contribution to $R_{1\rho}$ for three-site exchange in the strong field limit. (Solid) Numerical calculation of $R_{ex} = -\lambda/\sin^2\theta$ from the least negative real eigenvalue of the 9×9 evolution matrix, (dashed) calculation from the first-order approximation from Eqs. 11, and (dotted) calculation from the second-order approximation from Eqs. 29 and 40. To center the graph, parameters were chosen so that $\delta_A = \Delta\Omega$. Parameters used for the calculations were $p_A = 0.85, p_B = 0.10, p_C = 0.05, k_{12}+k_{21} = 1550 \text{ s}^{-1}, k_{13}+k_{31} = 2500 \text{ s}^{-1}, \omega_1 = 1250 \text{ s}^{-1}, \Omega_B - \Omega_A = 750 \text{ s}^{-1}, \Omega_C - \Omega_A = -1500 \text{ s}^{-1}$.

Figure S3. Offset dependence of the R_{ex} contribution to $R_{1\rho}$ for linear three-site exchange in which the sites exchange in different exchange regimes. (Solid) Numerical calculation of $R_{ex} = -\lambda/\sin^2\theta$ from the least negative real eigenvalue of the 9×9 evolution matrix, (dashed) calculation from the first-order approximation from Eqs. 11, and (dotted) calculation from the second-order approximation from Eqs. 29 and 40. The inset exemplifies a region in which the results of the calculations differ. To center the graph, parameters were chosen so that $\delta_A = \Delta\Omega$. Parameters used for the calculations were (in partial analogy to Fig. 2) $p_A = 0.95, p_B = 0.035, p_C = 0.015, k_{12}+k_{21} = 200 \text{ s}^{-1}, k_{13}+k_{31} = 5000 \text{ s}^{-1}, \omega_1 = 500 \text{ s}^{-1}, \Omega_B - \Omega_A = 1500 \text{ s}^{-1}, \Omega_C - \Omega_A = -3500 \text{ s}^{-1}$.

Figure S4. Second-order approximations of $R_{1\rho}$ linear three-site exchange at different dominant site populations. (Left) Actual $R_{1\rho}$ plots, (Right) absolute difference between exact numerical and approximate results. (Solid) Numerical calculation of the least negative real eigenvalue of the 9×9 evolution matrix, (dashed) calculation from the second-order approximation from Eqs. 29 and 40, using R_{eff} from Eq. 13, (dotted) calculation from the second-order approximation from Eqs. 29 and 40, using R_{eff} from Eq. 12, (dashed-dotted) calculation from the second-order approximation from Eqs. 29 and 40, but replacing \mathbf{L}'_k with $\mathbf{L}'_k + \mathbf{R}$ in Eq. 40 and not using R_{eff} . To center the graph, parameters were chosen so that $\delta_A = \Delta\Omega$. Parameters used for calculation: $p_B = p_C = (1-p_A)/2$, $k_{12}+k_{21} = 100 \text{ s}^{-1}$, $k_{13}+k_{31} = 100 \text{ s}^{-1}$, $\omega_1 = 50 \text{ s}^{-1}$, $\Omega_B - \Omega_A = -300 \text{ s}^{-1}$, $\Omega_C - \Omega_A = 300 \text{ s}^{-1}$, $R_1 = 1 \text{ s}^{-1}$, $R_2 = 6 \text{ s}^{-1}$. (a) $p_A = 0.33$; (b) $p_A = 0.9$.

Figure S5. R_{ex} contribution to $R_{1\rho}$ in triangular 3-state chemical exchange. To center the graph, parameters were chosen so that $\delta_A = \Delta\Omega$. Parameters used for all calculations were $p_A = 0.85$, $p_B = 0.1$, $p_C = 0.05$, $k_{12}+k_{21} = 50 \text{ s}^{-1}$, $k_{13}+k_{31} = 2000 \text{ s}^{-1}$, $\Omega_B - \Omega_A = -1000 \text{ s}^{-1}$, $\Omega_C - \Omega_A = 2000 \text{ s}^{-1}$, $\omega_1 = 500 \text{ s}^{-1}$. Left: Triangular 3-state chemical exchange scheme and approximations of the R_{ex} contribution. (Solid) Numerical calculation of $R_{ex} = -\lambda/\sin^2\theta$ from the least negative real eigenvalue of the 9×9 evolution matrix, (dashed) calculation from the first order approximation (Eq. 11), (dotted) calculation from the Woodbury approximation (Eq. 50), (dashed-dotted) calculation from a less well performing variation of the Woodbury approximation in which all first order terms are replaced by second order terms; additional parameter: $k_{23}+k_{32} = 700 \text{ s}^{-1}$. Right: Difference in error (approximation – numerical value) between the Woodbury approximation and the first order approximation. Values greater than 0 mean that the first order approximation is more accurate than the Woodbury approximation. The value of $k_{23}+k_{32}$ has been varied. Smaller rate constants for $k_{23}+k_{32}$, relative to the other kinetic rate constants, give a more accurate Woodbury approximation.

Figure S6. Approximations for the pseudo-kite 4-site scheme at different population levels. To center the graph, parameters were chosen so that $\delta_A = \Delta\Omega$. Parameters used for all calculations were $p_B = 10/16 \cdot (1 - p_A)$, $p_C = 5/16 \cdot (1 - p_A)$, $p_D = 1/16 \cdot (1 - p_A)$, $k_{21} + k_{12} = 140 \text{ s}^{-1}$, $k_{31} + k_{13} = 350 \text{ s}^{-1}$, $k_{43} + k_{34} = 700 \text{ s}^{-1}$, $k_{41} + k_{14}$ (non-linear fragment) = 350 s^{-1} , $\Omega_B - \Omega_A = -850 \text{ s}^{-1}$, $\Omega_C - \Omega_A = 2550 \text{ s}^{-1}$, $\Omega_D - \Omega_A = -4250 \text{ s}^{-1}$, $\omega_1 = 350 \text{ s}^{-1}$. Left: 2-dimensional plots showing the performance of the approximations at three different population scenarios. (Solid) Numerical calculation of $R_{ex} = -\lambda/\sin^2\theta$ from the least negative real eigenvalue of the 12×12 evolution matrix of the pseudo-kite four-site scheme, (dashed) calculation from the first order approximation from Eq. 11, (dotted) Woodbury approximation (Eq. 50). Right: 3-dimensional plots showing the performance of the approximations at three different population scenarios ($0.2 \leq p_A \leq 0.99$). The absolute differences between the numerical result and the first-order approximation (top) and the Woodbury approximation are plotted.

Figure S7. Use of pseudo-sites to calculate the Woodbury approximation for complex schemes. Top: A pseudo-kite 4-site scheme (grey: non-linear component of the scheme) can be collapsed to a linear three-site scheme. In this example, D* is the pseudo-site which has the same chemical shift as site A. The population in D* can be set low and pseudo-exchange rates between A and D can be set to very large numbers. Middle: Equivalence of the linear three-site scheme and the pseudo-kite 4-site scheme. (Solid) Numerical calculation of $R_{ex} = -\lambda/\sin^2\theta$ from the least negative real eigenvalue of the 12×12 evolution matrix of the pseudo-kite four-site scheme, (dashed – overlapping with solid) numerical calculation of the 9×9 evolution matrix of the linear three-site scheme, (dotted) Woodbury approximation (Eq. 50) of the pseudo-kite four-site scheme. To center the graph, parameters were chosen so that $\delta_A = \Delta\Omega$. Parameters used for all calculations were $p_B = 0.1$, $p_C = 0.05$, $k_{12} + k_{21} = 10 \text{ s}^{-1}$, $k_{12} + k_{21} = 500 \text{ s}^{-1}$, $\omega_l = 100 \text{ s}^{-1}$, $\Omega_B - \Omega_A = -500 \text{ s}^{-1}$, $\Omega_C - \Omega_A = 200 \text{ s}^{-1}$. Additional parameters for three-site scheme: $p_A = 0.85$. Additional parameters for four-site scheme: $p_A = 0.84999$, $p_D = 0.00001$, $k_{14} + k_{41} = 10000 \text{ s}^{-1}$, $k_{34} + k_{43} = 10000 \text{ s}^{-1}$, $\Omega_D - \Omega_A =$

0 s^{-1} . Bottom: A pseudo-kite 5-site system can be used to obtain the Woodbury approximation for a star four-site system (grey: non-linear component of the scheme).

Figure S1

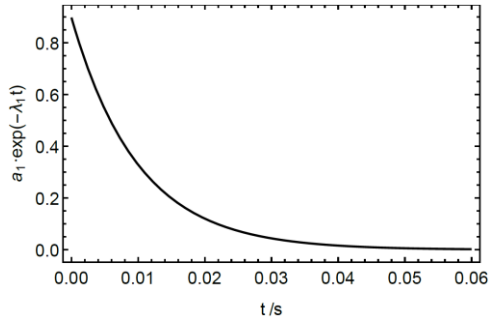
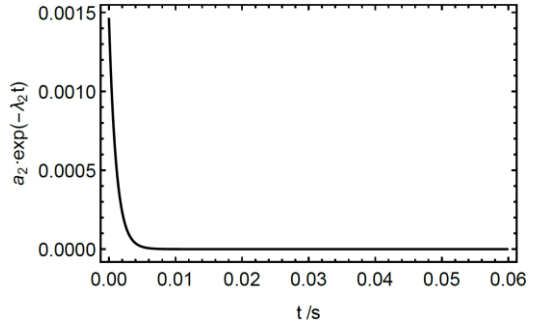
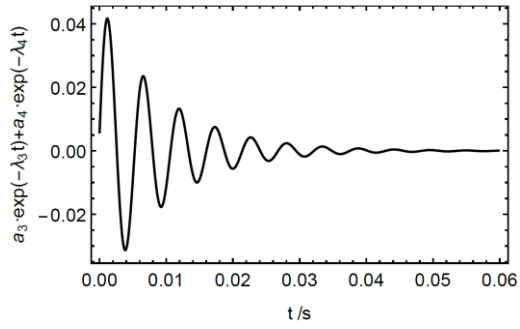
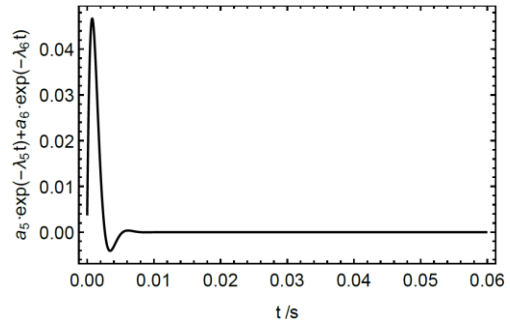
A**B****C****D**

Figure S2

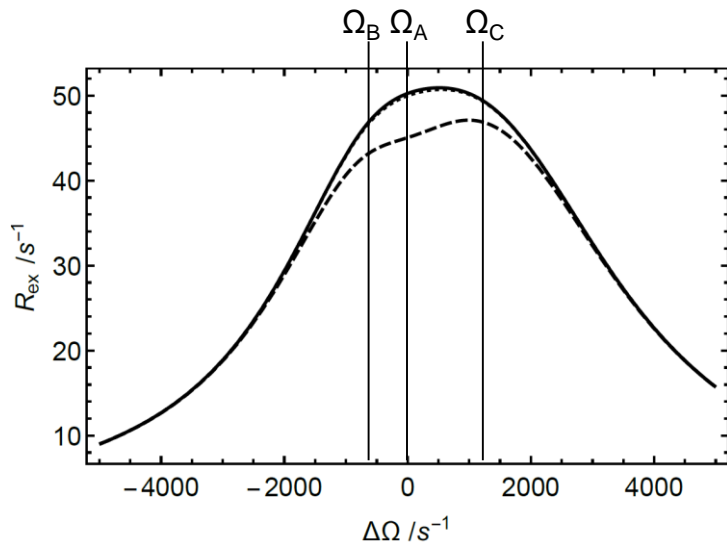


Figure S3

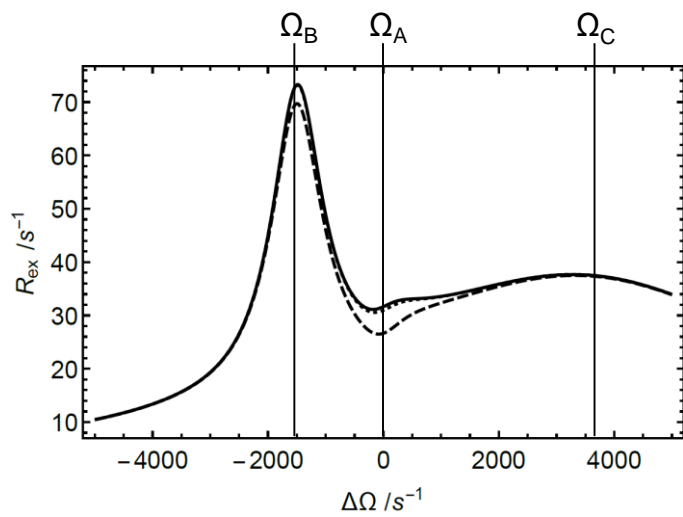
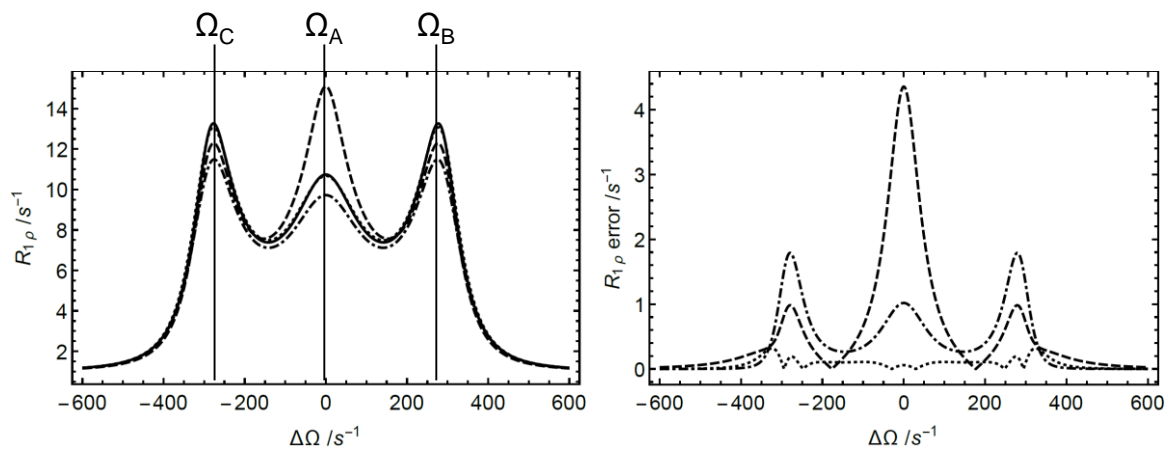


Figure S4

A



B

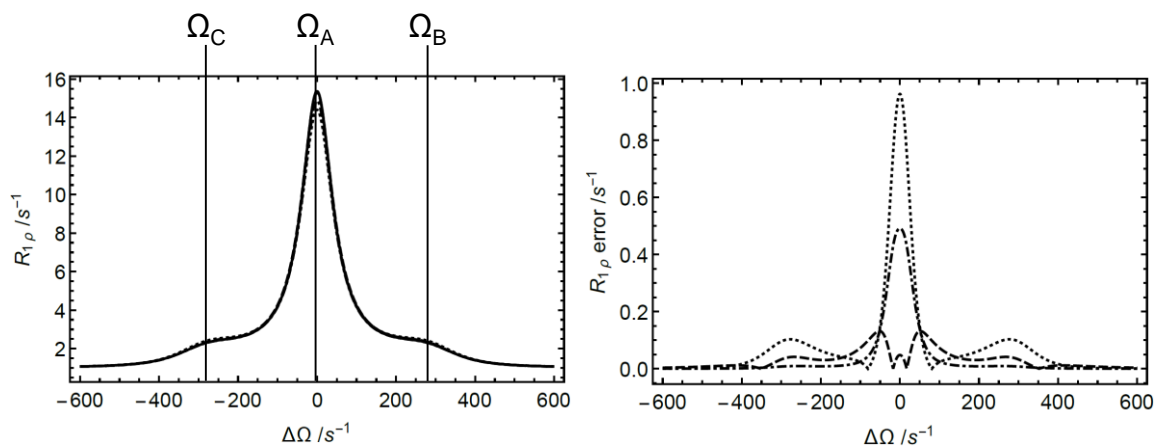


Figure S5

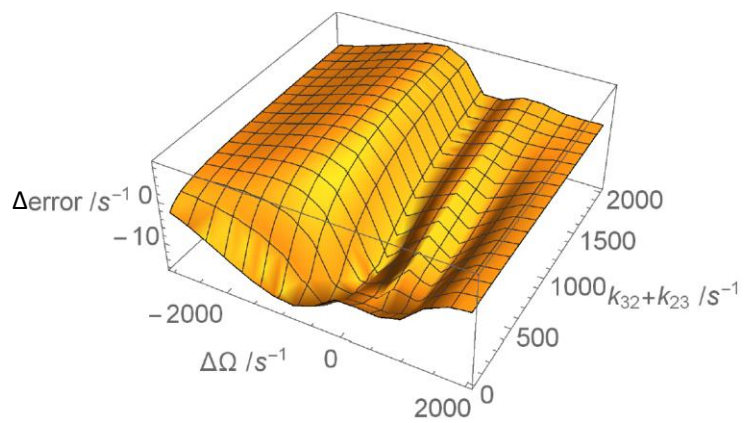
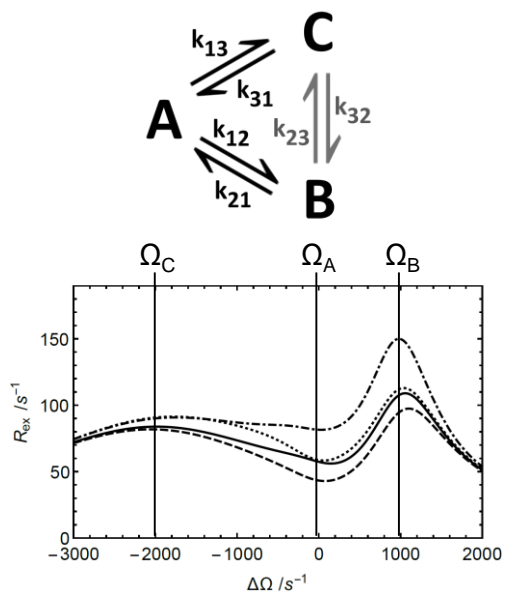


Figure S6

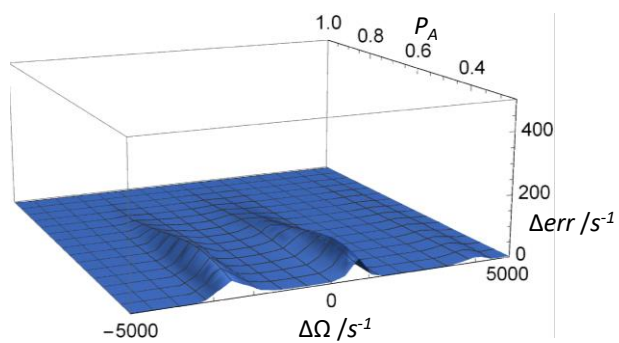
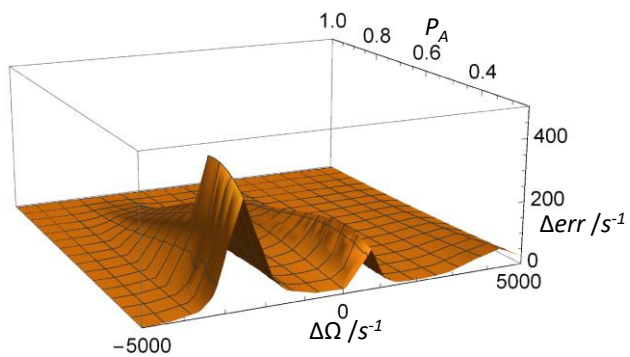
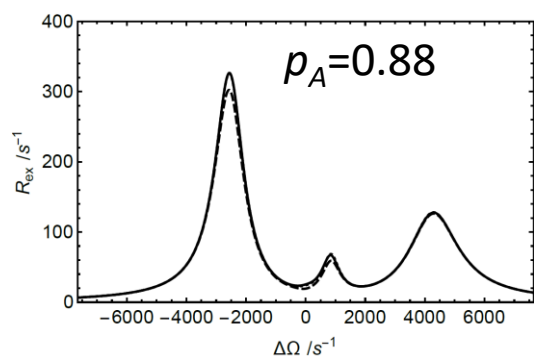
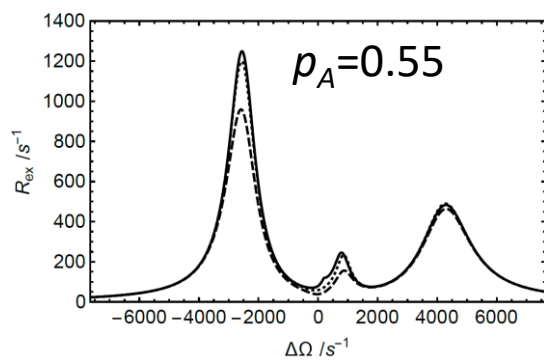
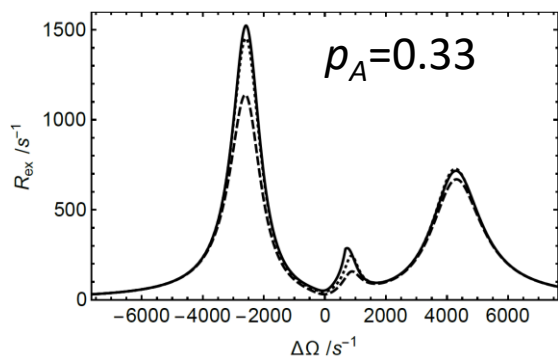


Figure S7

