

# S2 Text: Calculation of the SAS variance

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## 1 Autocovariance

We start with the calculation of the autocovariance

$$V_{ij}(d^\circ) \equiv \mathbb{V} \left( \frac{\sin(q_i d)}{q_i d}, \frac{\sin(q_j d)}{q_j d} \right) \quad (1)$$

Define

$$g(d) \equiv \frac{\sin(q_1 d)}{q_1 d} \quad h(d) \equiv \frac{\sin(q_2 d)}{q_2 d} \quad f(d) \equiv g(d)h(d) \quad (2)$$

Then, to second order around  $d' \equiv d^\circ + \frac{\tau^2}{d^\circ}$

$$f(d) \simeq f + f'(d - d') + f'' \frac{(d - d')^2}{2} \quad (3)$$

where functions without arguments are understood as being evaluated at  $d'$ , *i.e.*,  $f$  stands for  $f(d')$  *etc.* For  $d \equiv d_{kl}$ ,  $\tau$  is understood as  $\tau_{kl}$ . Therefore

$$\mathbb{E}(f(d)) \equiv \int_0^{+\infty} f(d) p_\chi(d|d^\circ, \tau) dd = f + f'T_1 + f''T_2 \quad (4)$$

where the coefficients  $T_1$  and  $T_2$  are

$$T_1 \equiv \mathbb{E}(d - d') = 0 \quad (5)$$

$$T_2 \equiv \mathbb{E} \left( \frac{(d - d')^2}{2} \right) = \frac{\tau^2}{2} \quad (6)$$

The expressions for  $g$  and  $h$  are similar with the same  $T_i$  coefficients. Note that these coefficients have the same value with the exact distribution or with its approximation since we matched the first two moments. The previous equation thus reduces to

$$\mathbb{E}(f(d)) = f + f''T_2 \quad (7)$$

We now express the derivatives of  $f$  as a function of those of  $g$  and  $h$

$$f = gh \quad (8)$$

$$f' = g'h + gh' \quad (9)$$

$$f'' = g''h + gh'' + 2g'h' \quad (10)$$

Now to second order

$$\mathbb{E}(g(\mathbf{d}))\mathbb{E}(h(\mathbf{d})) = gh + (g''h + gh'')T_2 \quad (11)$$

Finally, the autocovariance is

$$V_{ij}(\mathbf{d}^\circ) = \tau^2 q_i q_j \sigma(q_i \mathbf{d}^\circ) \sigma(q_j \mathbf{d}^\circ) \quad (12)$$

with  $\sigma$  the derivative of sinc.

## 2 Cross-covariance

Now, we derive the cross-covariance

$$V_{ij}(\mathbf{d}_{kl}^\circ, \mathbf{d}_{kn}^\circ) \equiv \mathbb{V} \left( \frac{\sin(q_i \mathbf{d}_{kl})}{q_i \mathbf{d}_{kl}}, \frac{\sin(q_j \mathbf{d}_{kn})}{q_j \mathbf{d}_{kn}} \right) \quad (13)$$

Similarly to the autocovariance, define

$$g(\mathbf{d}) \equiv \frac{\sin(q_1 \mathbf{d})}{q_1 \mathbf{d}} \quad h(\mathbf{d}) \equiv \frac{\sin(q_2 \mathbf{d})}{q_2 \mathbf{d}} \quad f(\mathbf{d}) \equiv g(\mathbf{d}_{kl})h(\mathbf{d}_{kn}) \quad (14)$$

Then, to second order around  $\mathbf{d}'$

$$f(\mathbf{d}) \simeq f + \nabla^\top f(\mathbf{d} - \mathbf{d}') + \frac{1}{2}(\mathbf{d} - \mathbf{d}')^\top \Delta f(\mathbf{d} - \mathbf{d}') \quad (15)$$

where functions without arguments are understood as being evaluated at  $\mathbf{d}'$ , *i.e.*,  $f$  stands for  $f(\mathbf{d}')$  *etc.* Therefore

$$\mathbb{E}(f(\mathbf{d})) \equiv \int_0^{+\infty} f(\mathbf{d}) p_\chi(\mathbf{d}|\mathbf{d}^\circ, \tau) d\mathbf{d} = f + \nabla^\top f \mathbf{R}_1 + \text{tr}(\Delta f \mathbf{R}_2) \quad (16)$$

where the coefficients  $\mathbf{R}_1$  and  $\mathbf{R}_2$  are computed using the approximated distribution

$$\mathbf{R}_1 \equiv \mathbb{E}(\mathbf{d} - \mathbf{d}') = 0 \quad (17)$$

$$\mathbf{R}_2 \equiv \frac{1}{2} \mathbb{E} \left( (\mathbf{d} - \mathbf{d}')(\mathbf{d} - \mathbf{d}')^\top \right) = \frac{1}{2} \Sigma_\rho \quad (18)$$

with  $\rho = \cos \theta$ . The expressions for  $g$  and  $h$  are similar

$$\mathbb{E}(g(\mathbf{d}_{kl})) = g + g'' \frac{\tau_{kl}^2}{2} \quad (19)$$

$$\mathbb{E}(h(\mathbf{d}_{kn})) = h + h'' \frac{\tau_{kn}^2}{2} \quad (20)$$

with  $g$  understood as  $g(\mathbf{d}_{kl}^\circ)$  and  $h$  as  $h(\mathbf{d}_{kn}^\circ)$  respectively. We express the derivatives of  $f$  as a function of those of  $g$  and  $h$

$$f = gh \quad \nabla f = \begin{pmatrix} g'h \\ gh' \end{pmatrix} \quad \Delta f = \begin{pmatrix} g''h & g'h' \\ g'h' & gh'' \end{pmatrix} \quad (21)$$

Now to second order, we have

$$\mathbb{E}(g(\mathbf{d})) \mathbb{E}(h(\mathbf{d})) = f + g''h \frac{\tau_{kl}^2}{2} + gh'' \frac{\tau_{kn}^2}{2} \quad (22)$$

Finally, the cross-covariance is

$$V_{ij}(\mathbf{d}_{kl}^\circ, \mathbf{d}_{kn}^\circ) = \rho \tau_k^2 q_i q_j \sigma(q_i \mathbf{d}_{kl}^\circ) \sigma(q_j \mathbf{d}_{kn}^\circ) \quad (23)$$

with  $\sigma$  the derivative of sinc and  $\rho = \frac{\mathbf{d}_{kl}^\circ \cdot \mathbf{d}_{kn}^\circ}{d_{kl}^\circ d_{kn}^\circ}$ .