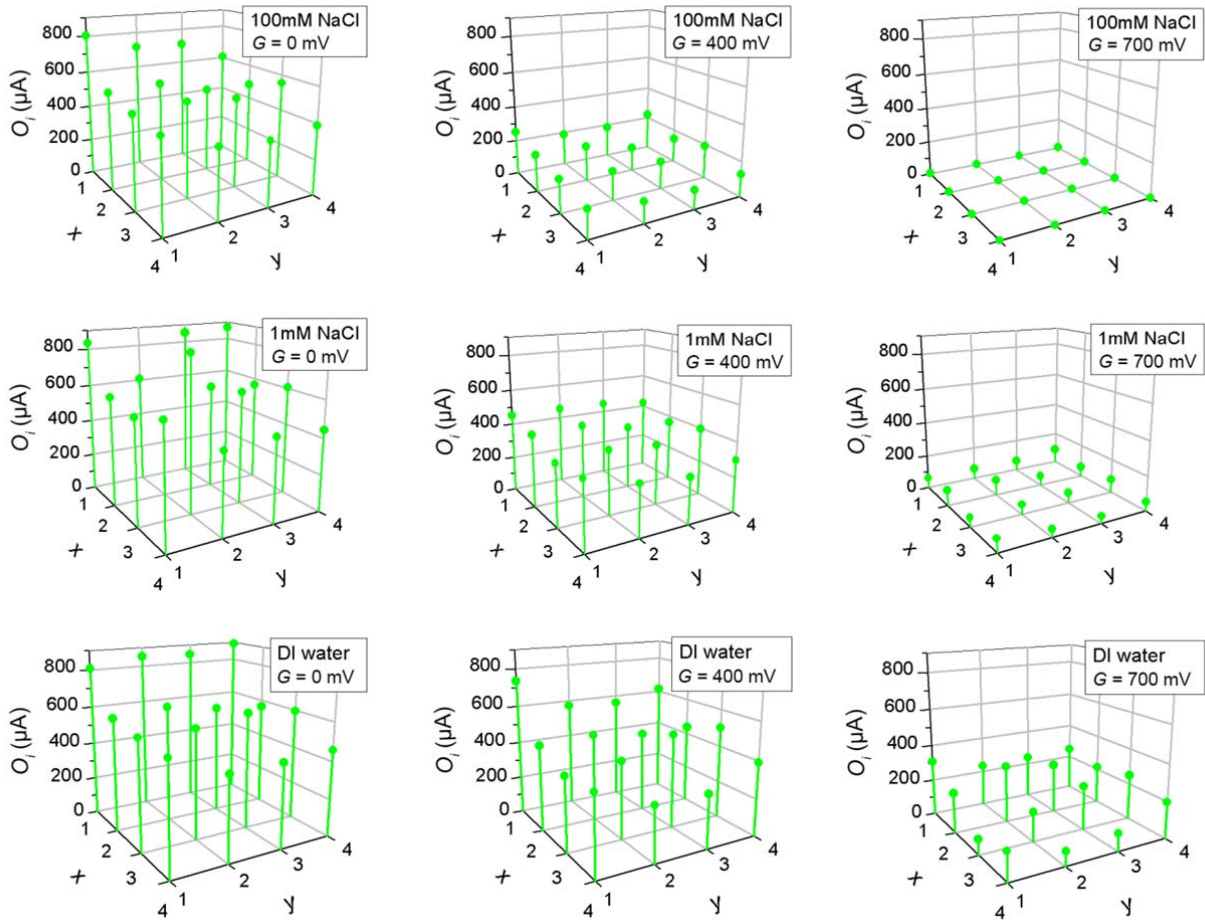


1 Supplementary Figures



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3 **Supplementary Figure 1. Gate voltage vs electrolyte concentration spatial mappings of output O_i .** A
4 pulse is applied at every local input I_i (amplitude of 100 mV, width of 50 ms) and the amplitude of the
5 corresponding output O_i is determined for different global DC gate voltages ($G = 0 - 700$ mV) and
6 electrolyte concentrations (DI water – 100 mM NaCl). More effective global gating is observed through
7 the 'diagonal' direction of the mappings (for high voltages and high electrolyte concentrations).

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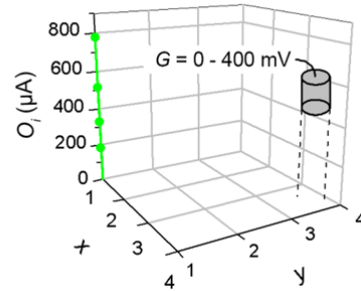
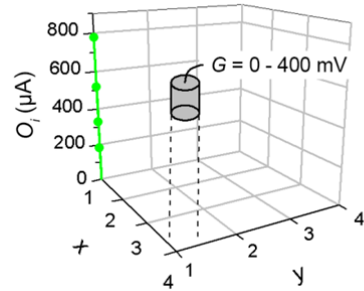
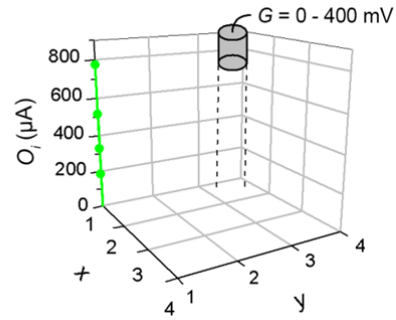
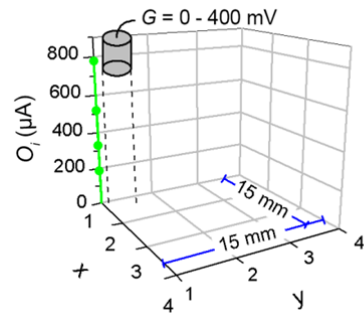
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15 **Supplementary Figure 2. Influence of the gate-device distance on global gating.** Output O_i of the
 16 device at coordinates (1, 1) for the application of a pulse at the local input I_i (amplitude of 100 mV, width
 17 of 50 ms), global gate voltages $G = 0 - 400$ mV and various gate-channel distances on the 4×4 grid.

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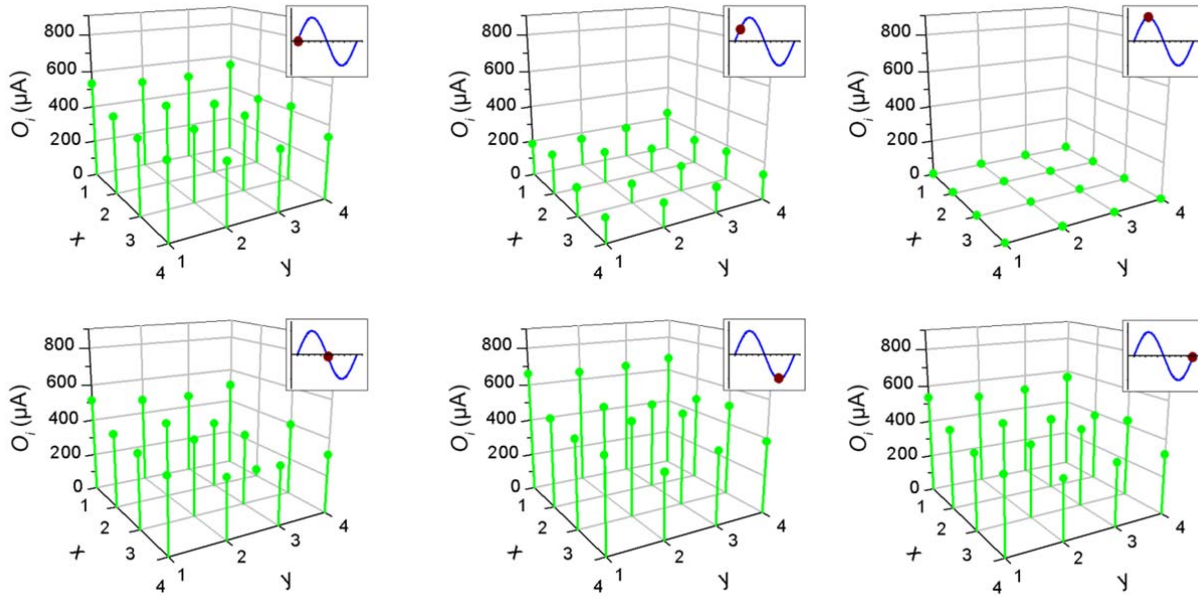
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27 **Supplementary Figure 3. Gating the device grid in a global electrolyte with an AC signal.** Spatial

28 output current mapping of O_i , at different moments of time of the AC global signal (frequency of 1 mHz

29 and amplitude 600 mV). A voltage pulse is applied at every local input I_i (amplitude of 100 mV, width of

30 50 ms) and the output current O_i of every device is measured as a function of time. Every graph

31 corresponds to a moment of time of the AC signal (inset).

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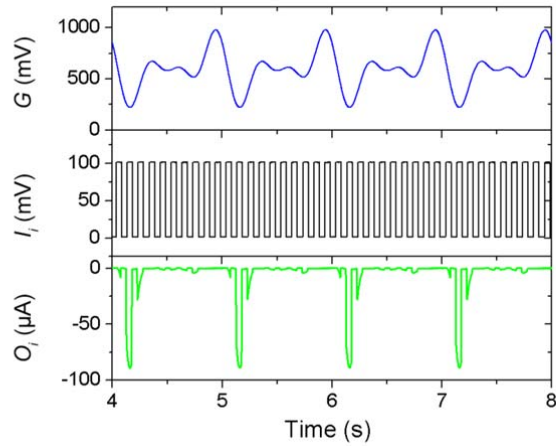
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41 **Supplementary Figure 4. Synchronization function.** Resulting output current O_i , with the application
 42 of a global input G with higher harmonics (amplitude modulation of a sine wave of frequency of 2 Hz,
 43 amplitude of 500 mV and offset of 600 mV, with a second sine wave of frequency of 1 Hz, AM depth of
 44 120%), and a train of voltage pulses (amplitude of 100 mV, width of 50 ms, period of 100 ms) at local
 45 input I_i . The steeper oscillation leads to higher output current O_i .

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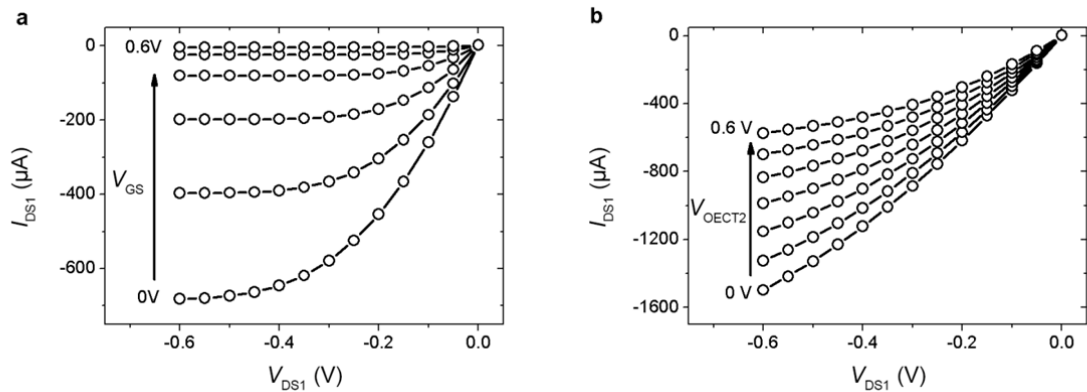
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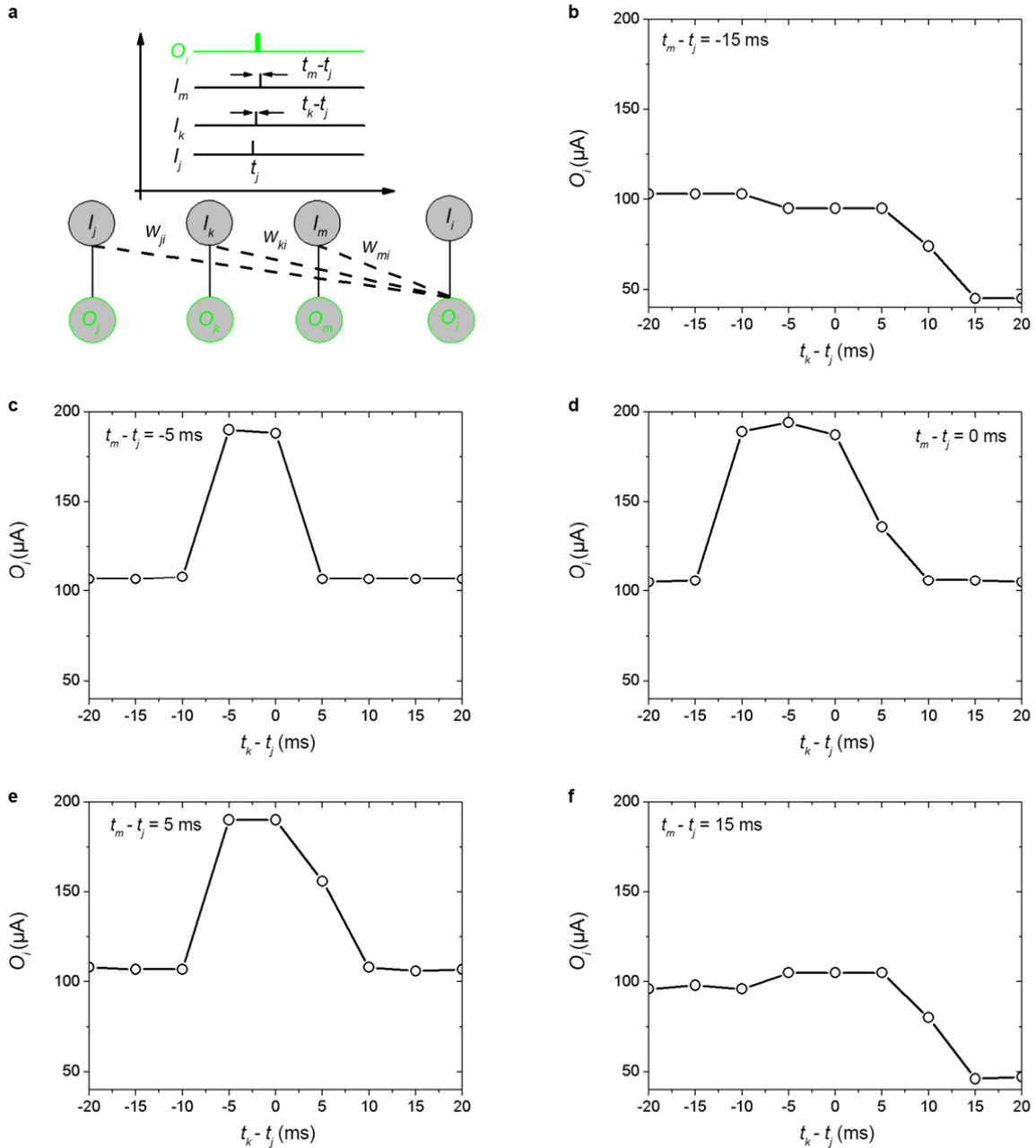
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59 **Supplementary Figure 5. OEECT characteristic curves.** (a) $I_{DS} - V_{DS}$ measurements in typical 3-
 60 terminal transistor configuration for the OEECT1 using a AgCl gate electrode ($V_{DS} = 0 - -0.7$ V, $V_{GS} = 0 -$
 61 0.6 V). (b) $I_{DS} - V_{DS}$ measurements in typical 3-terminal transistor configuration for the OEECT1 using
 62 another transistor OEECT2 as a gate electrode ($V_{DS} = 0 - -0.7$ V, $V_{OEECT2} = 0 - 0.6$ V).



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64 **Supplementary Figure 6. Time correlation mapping.** (a) Schematic of the measurement procedure.

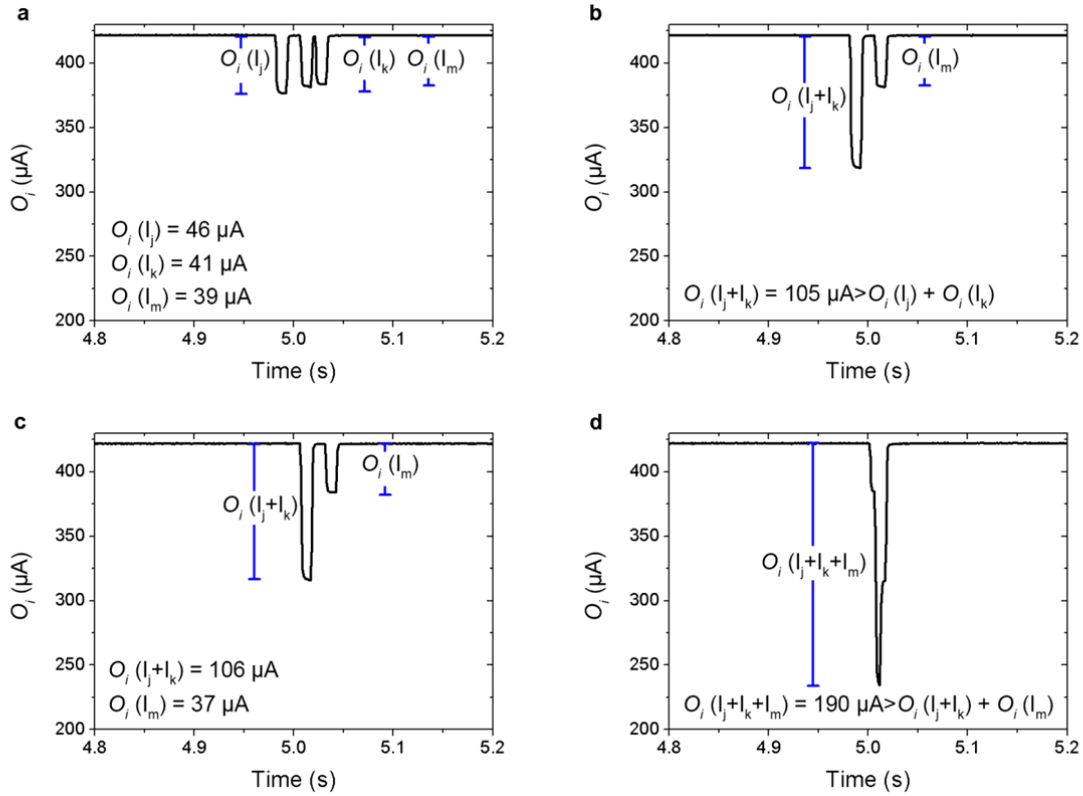
65 (b)-(f) Amplitude of O_i vs $t_k - t_j$ for different $t_m - t_j$ time intervals ($t_m - t_j = -15 - 15$ ms). Time correlation

66 mapping of Fig. 5(b) is constructed by combining the graphs of Supplementary Figure 3(b)-(f).

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71 **Supplementary Figure 7. Super-linear summation in coincidence detection measurements. (a)-(b)**

72 The sum two individual local inputs $O_i(I_j)$ and $O_i(I_k)$ ($\sim 87 \mu\text{A}$) is smaller than the overall output $O_i(I_j +$

73 $I_k)$ ($\sim 105 \mu\text{A}$). (c)-(d) The sum of $O_i(I_j + I_k)$ and $O_i(I_m)$ ($\sim 143 \mu\text{A}$) is smaller than the overall output $O_i(I_j$

74 $+ I_k + I_m)$ ($\sim 190 \mu\text{A}$).

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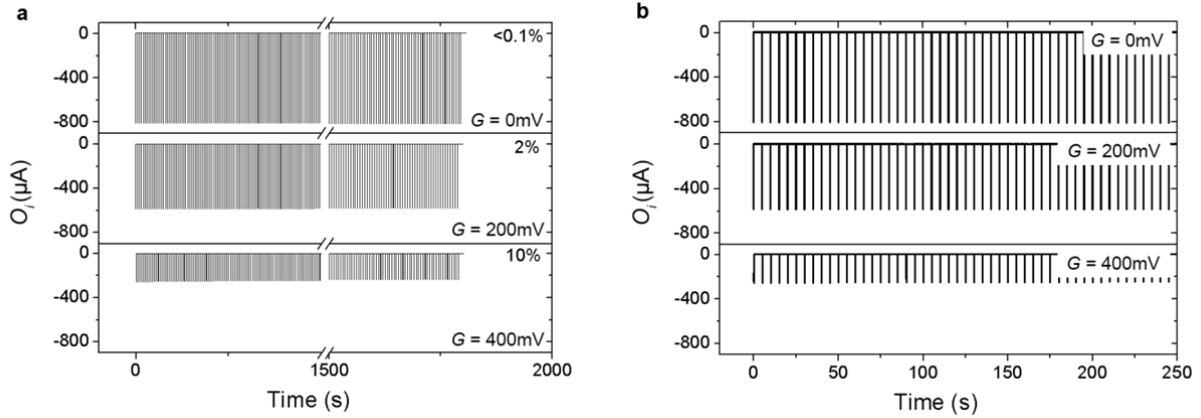
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85 **Supplementary Figure 8. Endurance measurements.** Endurance measurements of the output O_i for

86 applying a train of pulses (amplitude of 100 mV, width of 50 ms and period of 5 s) at the local input I_i (at

87 coordinates (1, 1)) for global gate voltages $G = 0 - 400$ mV. **(a)** $N = 360$ cycles. **(b)** $N = 50$ cycles.

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104 **Supplementary Notes**

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106 **Supplementary Note 1 - Gate voltage vs electrolyte concentration spatial mappings of local output** 107 **O_i**

108 Ionic concentration vs gate voltage spatial mappings are presented in **Supplementary Fig. 1**. A pulse is
109 applied at every local input I_i (amplitude of 100 mV, width of 50 ms) and the amplitude of the
110 corresponding output O_i is determined for different global DC gate voltages ($G = 0 - 700$ mV) and
111 electrolyte concentrations (DI water – 100 mM NaCl). The global gating regulates more efficiently the
112 I/O transmission for larger global voltages and with the presence of higher concentrations of ionic
113 species. Thus the most effective route for the global regulation of every local I/O transmission is through
114 the 'diagonal' of the diagram of **Supplementary Fig. 1**.

115

116 **Supplementary Note 2 - Influence of the location of the gate on global gating**

117 Regarding location of the gate in the device grid, two extreme regimes can be referred here. One extreme
118 is when the gate electrode has much smaller dimensions than the PEDOT:PSS active area of a device and
119 this regime was recently studied.¹ In the latter work, the output of the OECT was dependent on the
120 distance between the gate and the drain electrode, and this dependency allowed the demonstration of
121 orientation selectivity with a multi-gated OECT. The channel dimensions of the multi-gated device were
122 in the range of \sim cm and the gates were approximately 4 times smaller. The opposite extreme is studied in
123 the present work. Here, the channel width and length is $W \times L = 50 \times 50 \mu\text{m}^2$, while the gate dimensions
124 are much larger and in the range of \sim mm. In this case, the output of the device is practically independent
125 on the distance between the global gate and the channel.

126 The difference between these two regimes can be understood quantitatively according to a previously
127 published work by D. A. Bernards, G. G. Malliaras et., al.² According to this work, the relation between
128 the electrolyte potential V_{EL} and the gate potential V_{G} is given by:

$$129 \quad V_{EL} = \frac{V_G}{1 + \frac{C_C}{C_G}} \quad (1)$$

130 where C_C and C_G is the channel and the gate capacitance respectively. For large difference in the
 131 dimensions between the gate and the channel (i.e., the present case), $C_G \gg C_C$ and thus $V_E \sim V_G$. This
 132 means that the whole gate voltage drops to the channel and the electrolyte resistance (or the gate-channel
 133 distance) is not a determinative parameter for the output of the device. For comparable dimensions (not
 134 applicable in this case) between the gate and the channel, capacitances C_C and C_G are also comparable
 135 and $V_E < V_G$. This results in a partial drop of the V_G at the electrolyte, and in this case gate-channel
 136 distance affects the output response of the device.¹

137 **Supplementary Fig. 2** shows the output O_i of the device at coordinates (1, 1) for the application of a
 138 pulse at the local input I_i (amplitude of 100 mV, width of 50 ms) and for various locations of the gate on
 139 the 4×4 grid (with dimensions of $\sim 15 \times 15 \text{ mm}^2$). The output O_i is practically independent on the exact
 140 location of the gate, at least within the dimensions of the grid.

141

142 **Supplementary Note 3 - AC signals as global clocks**

143 The I/O transmission of the grid of 4×4 devices for a global, AC signal is investigated in the
 144 **Supplementary Fig. 3**. Similarly to the single device measurements of **Fig. 3**, a train of pulses is applied
 145 at the I_i terminal of every device (amplitude of 100 mV, width of 50 ms, period of 5 s), a global AC signal
 146 is applied at G terminal (amplitude of ± 600 mV, frequency of 1 mHz) and the resulting spiking output
 147 response O_i of every device is measured as a function of time. The mapping of every local output
 148 amplitude O_i of the grid, at different moments of time of the global AC signal is depicted in
 149 **Supplementary Fig. 3**. The output response of the grid is regulated globally in a synchronized manner
 150 and the I/O transmission can be modulated with a periodicity between the extreme values $0 - O_{MAX}$.
 151 Therefore, the AC signal is considered as synchronization function, or a global clock.

152 **Supplementary Note 4 - Synchronization functions**

153 The global oscillation of **Fig. 3(c)** is a result of the amplitude modulation (AM) of a 1 Hz signal with a 3
154 Hz signal. According to the formulation, the overall result of AM of a carrier signal (with frequency f_c)
155 with a modulation signal (with frequency f_m) without phase difference φ ($= 0$) is given by:³

$$156 \quad y(t) = ct_1 \cdot \sin(2\pi f_c t) + ct_2 \left[\sin(2\pi(f_c + f_m)t) + \sin(2\pi(f_c - f_m)t) \right] \quad (\text{S2})$$

157 Where ct_i is a constant and t is time. For $f_c = 1$ Hz and $f_m = 3$ Hz, it comes out the resulting AM
158 modulation exhibits the harmonics of $f_c = 1$ Hz, $f_c + f_m = 4$ Hz and $|f_c - f_m| = 2$ Hz. In fact, these are the
159 basic harmonics that are observed in **Fig. 3(c)**.

160 In **Fig. 3 (c)**, a global oscillation with a positive offset (in the range 500 mV to 900 mV) is chosen, in
161 order to operate the device in the sub-threshold regime (i.e., $G > 600$ mV, or the 'OFF' state, see also **Fig.**
162 **1(d)**) during the majority of the global oscillation, and only during the basic harmonic of the AC signal
163 (i.e., 1 Hz) the device is operated close to the threshold regime ($G \sim 600$ mV). This definition of the
164 global oscillation is the key feature for synchronization of an input train of pulses at the local input I_i ,
165 with the basic harmonic of the global oscillation at 1 Hz, close the threshold regime. The output current
166 O_i can dramatically be increased by using a steeper global oscillation below the threshold voltage (see
167 **Supplementary Fig. 4**).

168

169 **Supplementary Note 5 - OECT characteristic curves**

170 **Supplementary Fig. 5(a)** shows typical, single device, $I_{DS} - V_{DS}$ measurements in typical transistor
171 configuration (3-terminal configuration). The $I_{DS} - V_{DS}$ characteristic of the OECT1 is modulated by
172 using a V_{GS} voltage (using a AgCl gate electrode), which exhibits a typical OECT behavior.⁴ Regarding
173 the present work, the I/O suppression with a global gate voltage, can be understood quantitatively by
174 taking into account the typical $I_{DS} - V_{DS}$ of **Supplementary Fig. 5(a)**.

175 Moreover, another device (i.e., OECT2) can be used for gating the OECT1. **Supplementary Fig. 5(b)**
176 shows similar $I_{DS} - V_{DS}$ measurements (for OECT1) for different 'gate' voltages at the OECT2, V_{OECT2}
177 (applied at the source terminal of OECT2, while the drain is floating). **Supplementary Fig. 5(b)** shows
178 that every OECT in the grid (in this case OECT2) effectively acts as a gate electrode for OECT1 through
179 the electrolyte. Although this 'secondary' gating is less effective when compared with the AgCl electrode
180 case (the $I_{DS} - V_{DS}$ is partially suppressed), it provides a quantitative explanation of the soft connectivity
181 between individual devices through the electrolyte continuum.

182

183 **Supplementary Note 6 - Measurement procedure of coincidence detection**

184 The measurement procedure of the construction of the time correlation mapping of the output O_i , $t_k - t_j$ vs
185 $t_m - t_j$ (refer also to **Fig. 5(b)**) is described thereafter. A voltage pulse ($V_1 = 0.5$ V, $t_p = 10$ ms) is applied at
186 three local inputs (I_j , I_k , I_m) with variable time intervals $t_k - t_j$ (for the I_k input) and $t_m - t_j$ (for the I_m input)
187 in respect to a reference time t_j of the I_j input and the output amplitude O_i of the i^{th} device (for $V_O = 0.05$
188 V) is determined in every case (**Supplementary Fig. 6(a)**). The time correlation mapping of **Fig. 5(b)**
189 was constructed following the procedure that is described below: the time interval of the pair of pulses at
190 I_m and I_j terminals ($= t_m - t_j$) was kept constant and the time interval of the I_k terminal was varied, creating
191 ($t_m - t_j = \text{constant}$, $t_k - t_j$) arrays. Following the above procedure, for different $t_m - t_j = \text{constant}$ intervals,
192 the surface of **Fig. 5(b)** is scanned and constructed (**Supplementary Fig. 6(b)-(f)**), O_i vs $t_k - t_j$ for
193 different $t_m - t_j$ time intervals).

194

195 **Supplementary Note 7 - Super-linear summation**

196 An example of the raw data of the measurement of coincidence detection is presented in **Supplementary**
197 **Fig. 7**, as resulted by applying pulses at the local inputs I_j , I_k and I_m for various time intervals and by
198 defining the amplitude of the output current O_i . **Supplementary Fig. 7(a)** and **(b)**, show that the sum two

199 individual local inputs $O_i(I_i)$ and $O_i(I_k)$ is smaller than the overall output $O_i(I_i + I_k)$, when inputs I_j and I_k
200 are time-synchronized. Similarly, in **Supplementary Fig. 7(c)** and **(d)**, the sum of $O_i(I_j + I_k)$ and $O_i(I_m)$ is
201 also smaller than the overall output $O_i(I_i + I_k + I_m)$. Therefore, the overall output response O_i is slightly
202 super-linear summation of the individual local inputs.

203

204 **Supplementary Note 8 - Endurance measurements**

205 **Supplementary Fig. 8(a)** shows the endurance measurements of the output O_i as a function of time for
206 applying a train of pulses ($N = 360$ cycles, amplitude of 100 mV, width of 50 ms and period of 5 s) at the
207 local input I_i (at coordinates (1, 1)) for global gate voltages $G = 0 - 400$ mV. **Supplementary Fig. 8(b)**
208 shows the same measurement in more detail ($N = 50$ cycles). The output of the device is quite stable after
209 360 cycles. For $G = 0$ mV, the amplitude of O_i is quite stable ($< 0.1\%$ degradation), while for $G = 400$
210 mV the amplitude of O_i displays only a small degradation ($\sim 10\%$).

211

212 **Supplementary References**

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