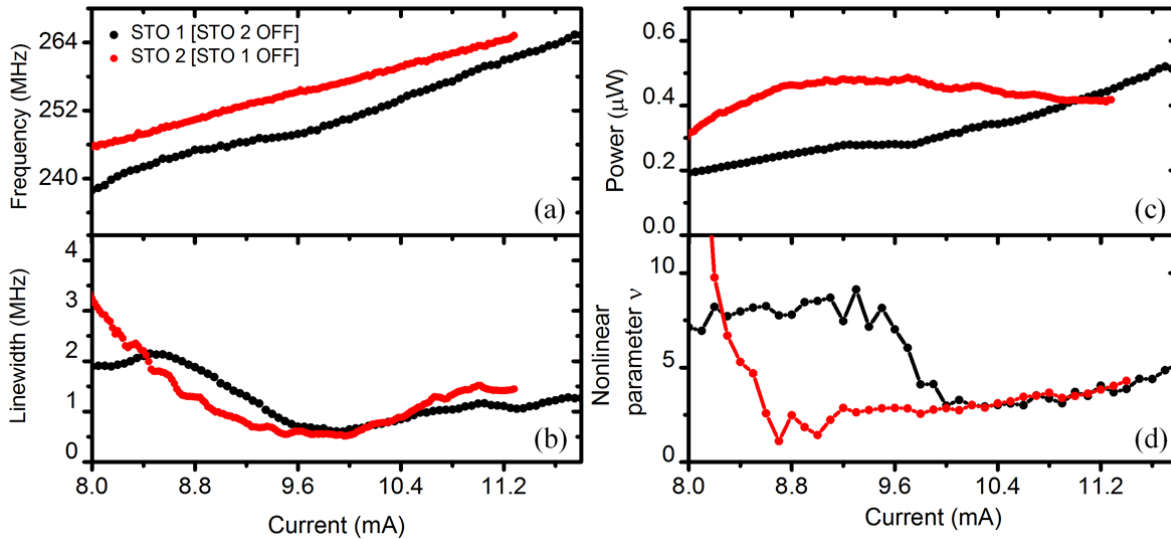


1 Supplement note 1: Characteristics of the non-interacting spin torque oscillators (STOs)

2 **Supplementary Figure 1** shows the properties of each non-interacting STOs. In the measurements
3 presented in the main text, the dc-current $I_{DC,2}$ of the oscillator n°2 (STO 2) is fixed to $I_{DC,2} = +10.6$ mA,
4 while the dc-current of the oscillator n°1 (STO 1) is swept from +10.5 to +11.8 mA. For these conditions,
5 the properties of the rf emitted signal are similar i.e. the spectral linewidth (STO 2 \approx 1.15 MHz, STO 1 \approx
6 1-1.25 MHz), the emitted power (STO 2 \approx 0.44 μ W, STO 1 \approx 0.35-0.52 μ W) and their nonlinear
7 parameter ν (STO 2 \approx 3.4, STO 1 \approx 3-4.8). Having chosen these dc current values permits us to stand in
8 the hypothesis of “almost identical” oscillators¹, a condition that is particularly true in the middle of the
9 synchronization bandwidth.

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Supplementary Figure 1: Properties of the non-interacting STOs. Frequency (a), Linewidth (b), Power (c) and nonlinear parameter ν (d) for each non interacting oscillator (STO 1 and STO 2) as a function of I_{DC} in their respective current source. These measurements have been obtained at room temperature and zero field.

27 **Supplement note 2: Characteristic of the phase noise in the synchronized state**

28 In the optimized synchronized state, corresponding to the largest synchronized bandwidth, i.e. $\psi_{\Delta\tau} -$
 29 $\psi_e \approx n\pi [\pi]$, the phase sum and difference are defined by the following system of **Supplementary**
 30 **Equation 1** (see Ref²):

$$\begin{cases} \frac{d\Phi}{dt} = -2\bar{\omega} + \xi_1(t) + \xi_2(t) & (1) \\ \frac{d\psi}{dt} = -\Delta\omega - 2F_e \sin \psi + \xi_1(t) - \xi_2(t) & (2) \end{cases}$$

31 where $\xi_1(t)$ and $\xi_2(t)$ are the white noise source in each STO, $2\bar{\omega}$ the sum of the two STO frequencies
 32 $\Delta\omega$ the frequency detuning and F_e the strength of the locking force. For almost identical oscillators, the
 33 intensities of noise are equivalent (leading to similar spectral linewidths) and described by
 34 **Supplementary Equation 3**:

$$\langle \xi_1(t) | \xi_2(t') \rangle = 2\sigma_0^2 \delta_{1,2} \delta(t - t') \quad (3)$$

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 36 Contrary to the phase difference, the phase sum Φ has no retroaction process. Thus, the diffusion of the
 37 phase sum turns out to be much larger than the diffusion of the phase difference with a diffusion constant
 38 $D_\Phi = 2\sigma_0^2 \gg D_\psi$. Given that the phases of each synchronized oscillator are $\phi_1 = (\Phi + \psi)/2$ and
 39 $\phi_2 = (\Phi - \psi)/2$, their diffusion constants are then $D_{s,1} = D_{s,2} = \sigma_0^2$. Note that when the two STOs are
 40 not interacting, their diffusion constants are $D_1 = D_2 = 2\sigma_0^2$. We thus deduce that the phase noise of the
 41 synchronized STOs should decrease by a factor 2 compared to the value when they are independent.

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 43 **Supplement note 3: Estimation of the synchronization bandwidth**

44 As mentioned earlier, the two STOs are almost identical. In this case, the rf-current emitted by one STO
 45 that will drive the second oscillator can be estimated by **Supplementary Equation 3**:

$$I_{rf,STO} = \frac{I_{rf,STO}}{\pi R^2} = \frac{\sqrt{P_{int}/R_{STO}}}{\pi R^2} \quad (3)$$

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 47 with R the dot radius of the STO, R_{STO} the STO resistance and P_{int} the power emitted by the STO. In our
 48 experimental setup, the presence of a power divider used to detect the emitted power on a spectrum
 49 analyzer results in a decrease by 6 dBm of the effective synchronizing signal that is applied on each
 50 oscillator. The impedance mismatch between the circuit resistance (50 Ω) and the oscillator resistance (32
 51 Ω) is also contributing to the decrease of the actual synchronizing rf-current. We estimate for this
 52 effective synchronizing current $I_{rf,eff} = (1 - R_{re})I_{rf,STO}/2$ with $R_{re} = (50-32)/(50+32)$.

53 The synchronization bandwidth is then expressed in the best conditions, i.e for $\psi_{\Delta\tau} - \psi_e = n\pi [\pi]$, by
 54 **Supplementary Equation 5**:

$$\Delta\omega_{sync} = 2 \frac{\sqrt{1+v^2} \sqrt{\Lambda_{SL}^2 + \Lambda_{FL}^2}}{\sqrt{p_0}} I_{rf,eff} \quad (4)$$

55
 56 and the normalized power by **Supplementary Equation 5**³:

$$p_0 = \frac{18P_{int}}{R_{load}} \left(\frac{R_{load} + R_{STO}}{I_{dc} \Delta R_{TMR}} \right)^2 \quad (5)$$

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 58
 59 For the presented measurements, $I_{rf,STO} = 0.5 \text{ mA}$, $R_{STO} = 32 \Omega$, $v = 3.4 - 3.7$, $p_0 = 0.21$
 60 ($\Delta R_{TMR}(I_{dc}) \sim 14 \Omega$, $R_{load} = 50 \Omega$, $R_{STO} = 30 \Omega$, $I_{dc} = 11 \text{ mA}$), $R = 150 \text{ nm}$, and Λ_{FL}^2 and Λ_{SL}^2 are taken
 61 from Reference⁴. Injecting these parameters, we deduce $\Delta\omega_{sync} \sim 1.6 - 2.1 \text{ MHz}$. Note that this value is
 62 in excellent agreement with our experimental observations (2.2 MHz).
 63

64 **Supplement References**

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