Camphor-Engine-Driven Micro-Boat Guides Evolution of Chemical Gardens

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Supplementary Video: Heliciform precipitates formed under the self-propulsion of the micro-boat.

Supplementary Figure S1. **a - The filament typical for chemical gardens is shown; the magnification is ×600; b - The same filament cut lengthwise; c - The butt of the filament; the magnification is ×750.**

Supplementary Figure S2. **The time dependence of changes in geometrical parameters of the precipitate** (the concentration of $K_4Fe(CN)_6$ *c*=2 wt.%).

Supplementary Figure S3. **Temporal (a) and spatial (b) temperature distributions during the self-propulsion. a** - The time dependence of the temperature of the boat front (*c*=0.25 wt.%). The temperature jump in the initial period of self-locomotion is clearly seen. **b** - The temperature distribution along the micro-boat surface (*c*=0.250 wt.%). The blue rectangle represents the micro-boat in its real dimensions.

The rotational motion of the micro-boat along the rim of the Petri dish should be addressed within the model developed in Ref. 51. Let the vertical axis *Z* be coinciding with the inner side of the rim of the Petri dish, as shown in Supplementary Figure S4.

Supplementary Figure S4. **The cross-section of the PVC tubing (micro-boat) driven by the camphor engine is depicted with yellow color.** The contact angle *θ* formed by the potassium hexacyanoferrate aqueous solution and the rim of the Petri dish is shown.

The micro-boat rotates in the Petri dish at the distance of *ca*. 1 cm from the rim ($y_0 \approx 1$ *cm* in Fig 6 and Supplementary Fig. S4). Assume that the meniscus formed by the potassium hexacyanoferrate aqueous solution with the rim has the contact angle *θ* (established experimentally with the goniometer as $\theta = 35 \pm 1^\circ$; the contact angle hysteresis⁵² is neglected). Bush et al. demonstrated that in this case, the lateral force *Fy* \rightarrow acts on the micro-boat⁵¹ (Fig 6 and Supplementary Fig. S4):

$$
\left|\vec{F}_{y}\right| = -T\cot\theta\exp(-\frac{y_0}{l_{ca}}),\tag{6}
$$

where *T* is the modulus of the vertical force exerted by a floating body on a liquid/vapor interface, and $l_{ca} = \sqrt{\gamma/\rho g}$ is the capillary length.⁵² In our case, the lateral force \vec{F}_y \rightarrow is the centripetal force acting on the micro-boat; thus we obtain:

$$
T \cot \theta \exp\left(-\frac{y_0}{l_{ca}}\right) \approx \frac{mv_{cm}^2}{R - y_0},\tag{7}
$$

where R is the internal radius of the Petri dish. Assuming for the sake of a very rough estimation: $\theta \approx 35^\circ$; $y_0 \approx 1$ *cm*, $l_{ca} \approx 0.271$ *cm*; $R = 5$ *cm*; $T \approx y_2 m g$ yields:

$$
v_{cm} \approx \sqrt{\frac{1}{2}(R - y_0)g \exp\left(-\frac{y_0}{l_{ca}}\right)} \approx 8.5 \frac{cm}{s},\tag{8}
$$

which is an overestimated value (friction is neglected) but reasonable, when compared with the experimentally observed characteristic velocity of rotation of micro-boats.