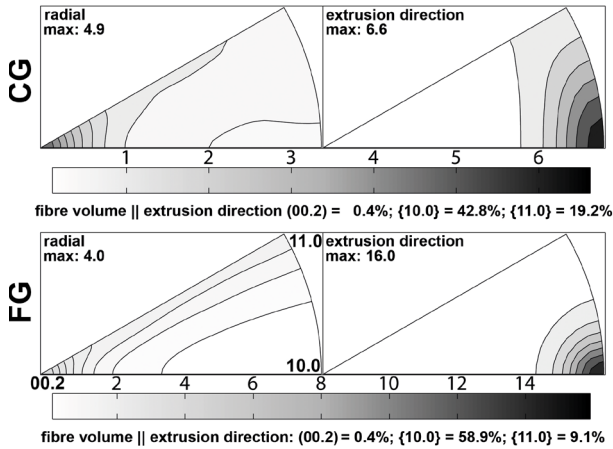
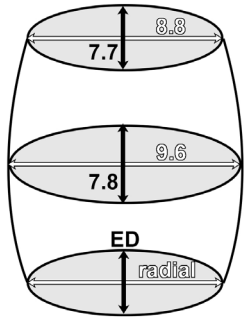


## Supplementary Information

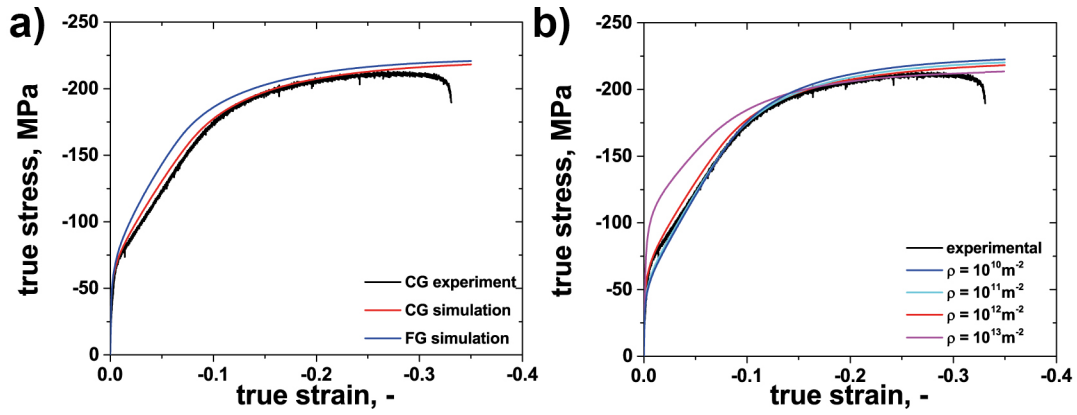
### Supplementary Figures



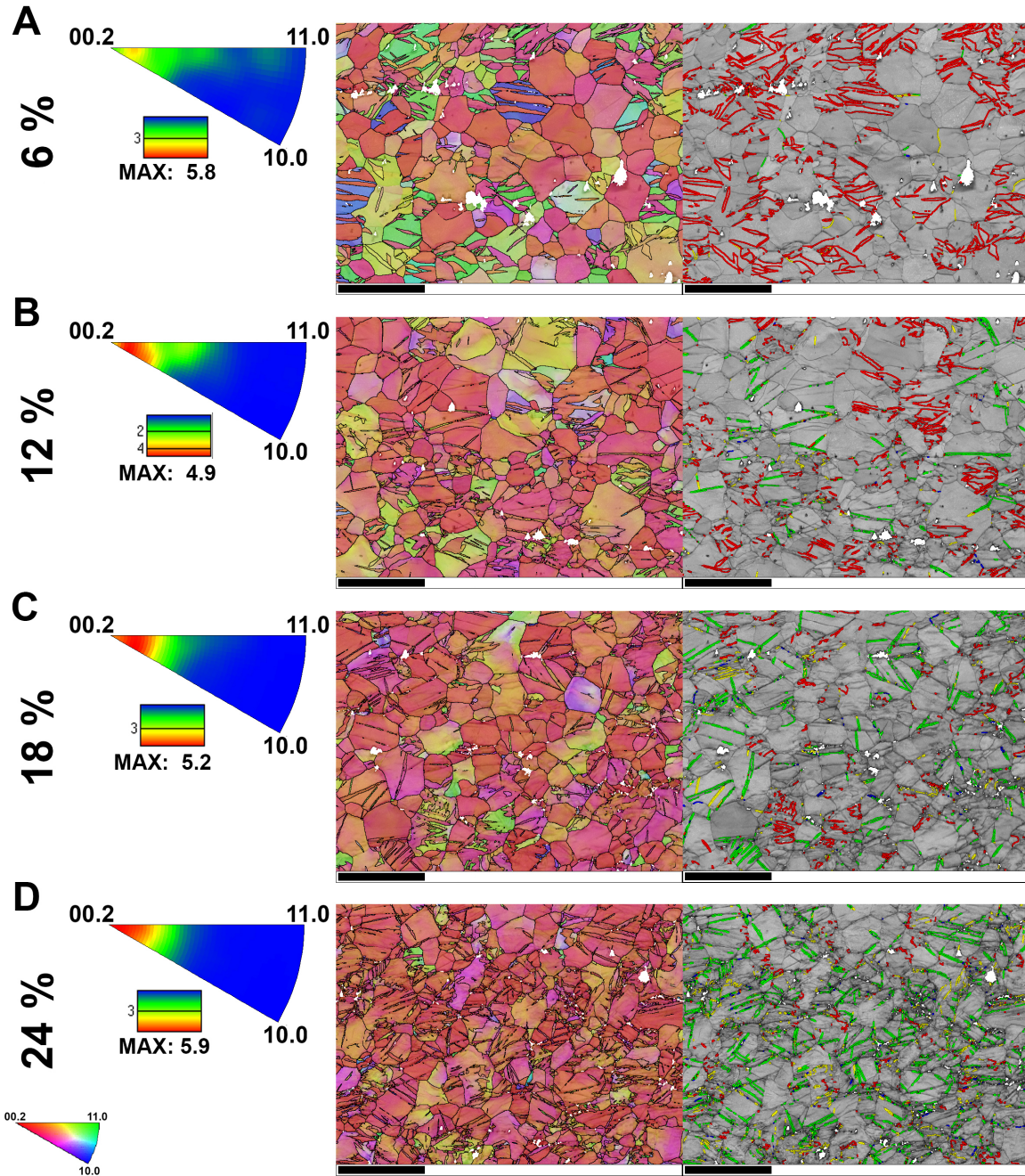
**Supplementary Figure 1 | Inverse pole figures representing the as-extruded texture parallel to radial and extrusion direction.** The textures of both materials are qualitatively similar, but differ in sharpness. Calculating the fiber volume fraction within  $15^\circ$  about the extrusion direction confirms a strengthened  $\langle 10.0 \rangle$  texture component parallel to ED in the FG material.



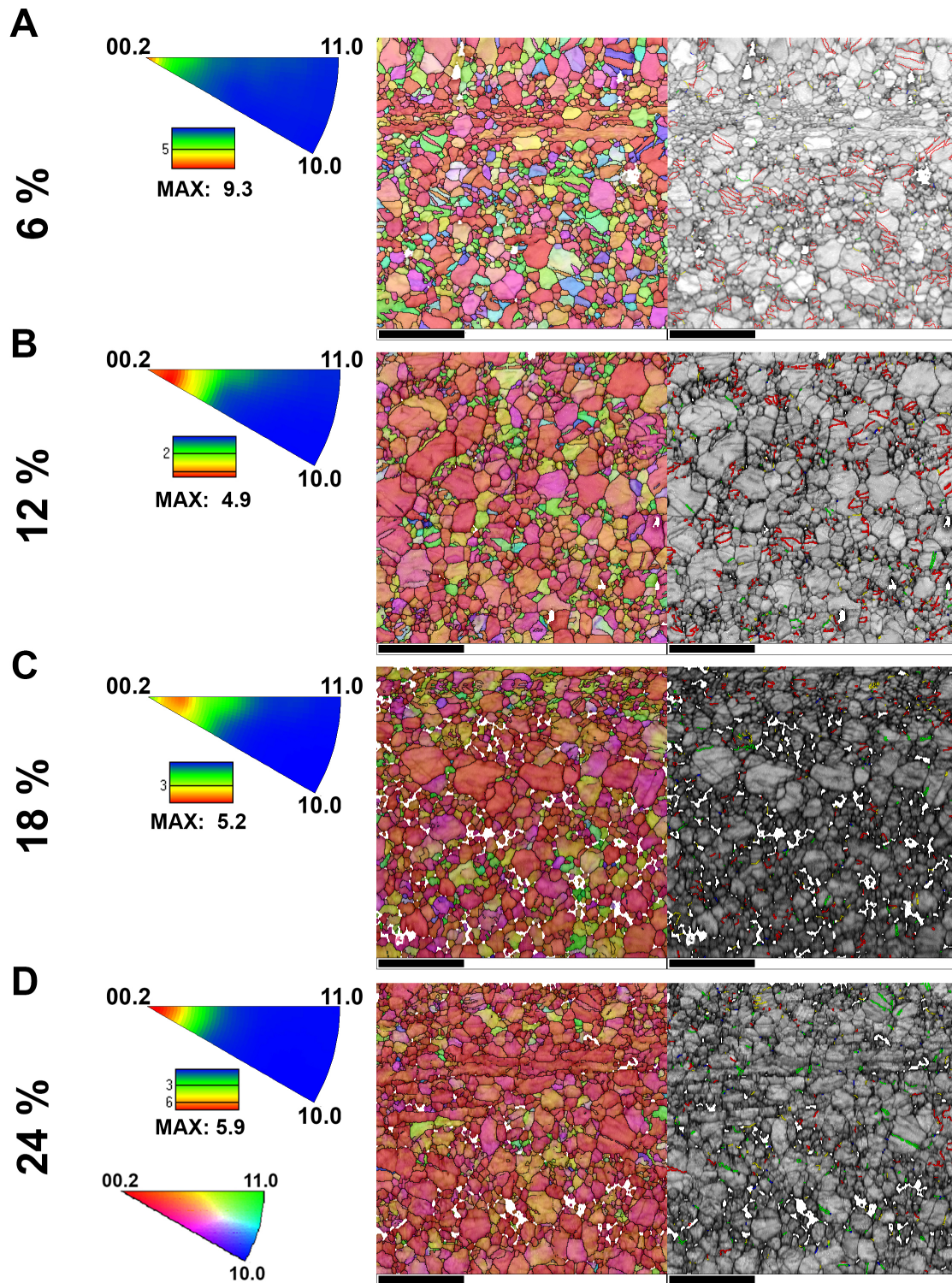
**Supplementary Figure 2 | Exemplary schematic of the barreling of a compression sample at 29.5% strain.** Non-uniform deformation featuring a more pronounced lateral extension perpendicular to the ED direction. This non-uniform deformation is introduced by the as-extruded texture and the selected strain path, while the barreling of the samples is minor.



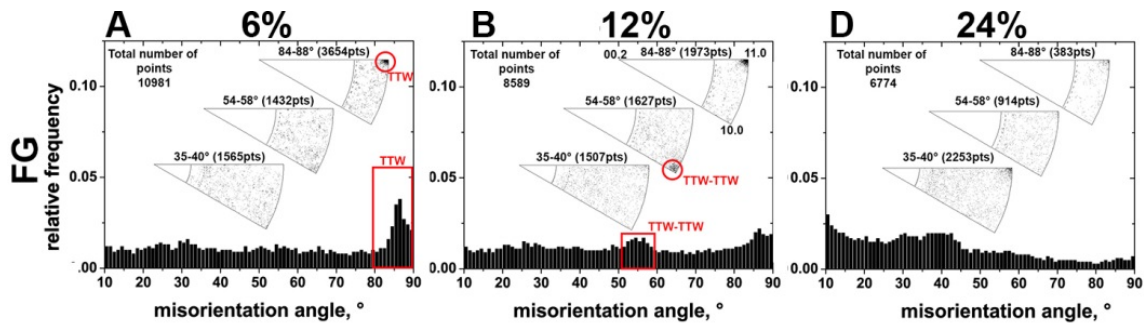
**Supplementary Figure 3 | EPSC simulations displaying the effect of the different starting textures and dislocation densities.** a) The difference in texture results in minor changes of the flow curve. b) The impact of different dislocation densities is negligible considering low dislocation densities, which are reasonably assumed based on the recrystallized microstructure of both materials.



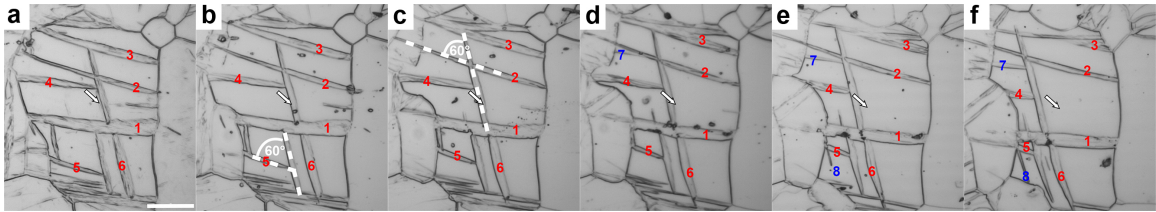
**Supplementary Figure 4 | EBSD analysis of the coarse-grained material.** EBSD analysis using inverse pole figures (IPF), IPF maps superimposed by band contrast (BC) and twin boundaries (TB) superimposed by (BC) maps of CG samples for different strain levels. TTW boundaries = red, CTW = yellow, type 1 DTW = green, type 2 DTW = blue. The scale bars correspond to 100  $\mu\text{m}$ .



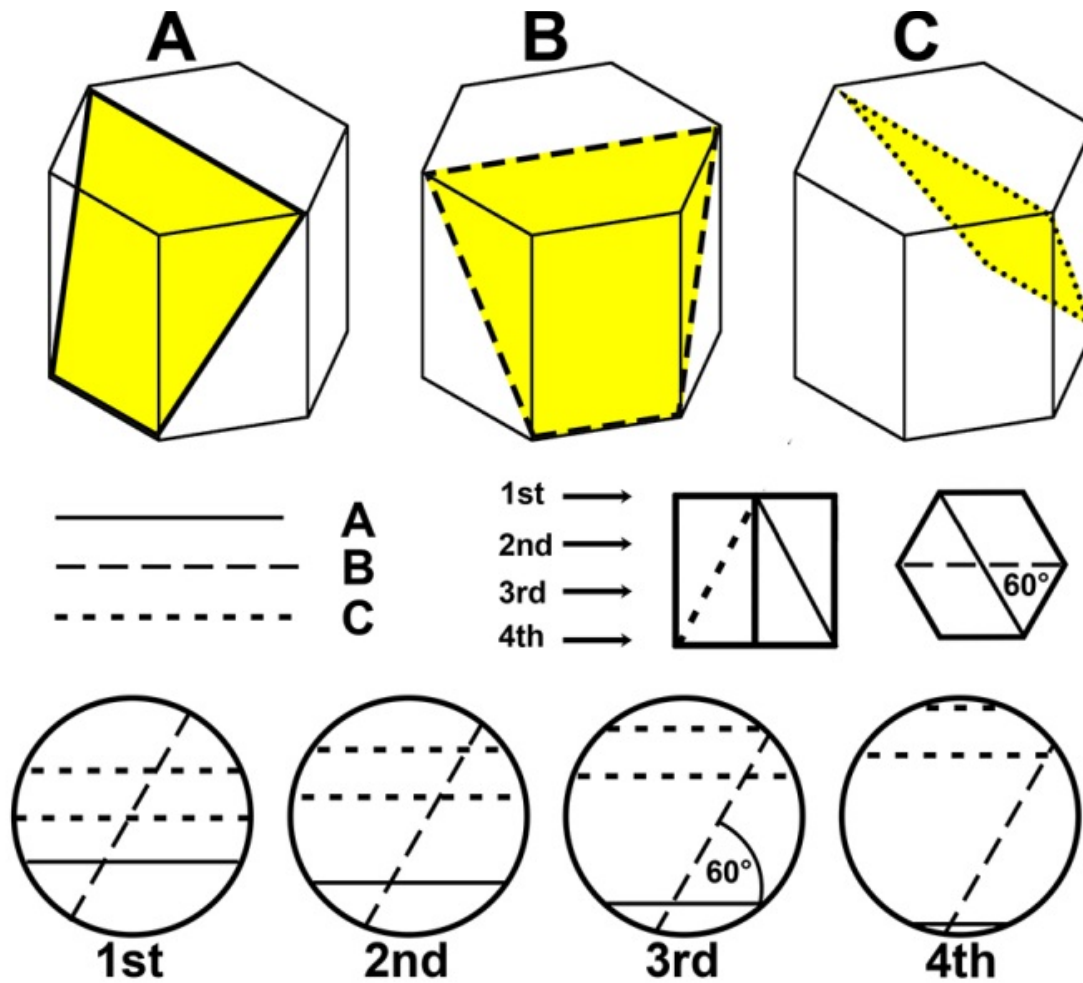
**Supplementary Figure 5 | EBSD analysis of the fine-grained material.** EBSD analysis using inverse pole figures (IPF), IPF maps superimposed by band contrast (BC) and twin boundaries (TB) superimposed by (BC) maps of FG samples for different strain levels. TTW boundaries = red, CTW = yellow, type 1 DTW = green, type 2 DTW = blue. The scale bars correspond to 50  $\mu\text{m}$ .



**Supplementary Figure 6 | Misorientation distribution functions of the FG material at different strains.** At  $\epsilon_E = 6\%$  TTW-ing is predominant, although it is hindered in comparison to the CG material. DTWs were observed only very occasionally within the investigated strain range. The very weak peak at  $\sim 55^\circ$  can be attributed to TTW-TTW intersections.

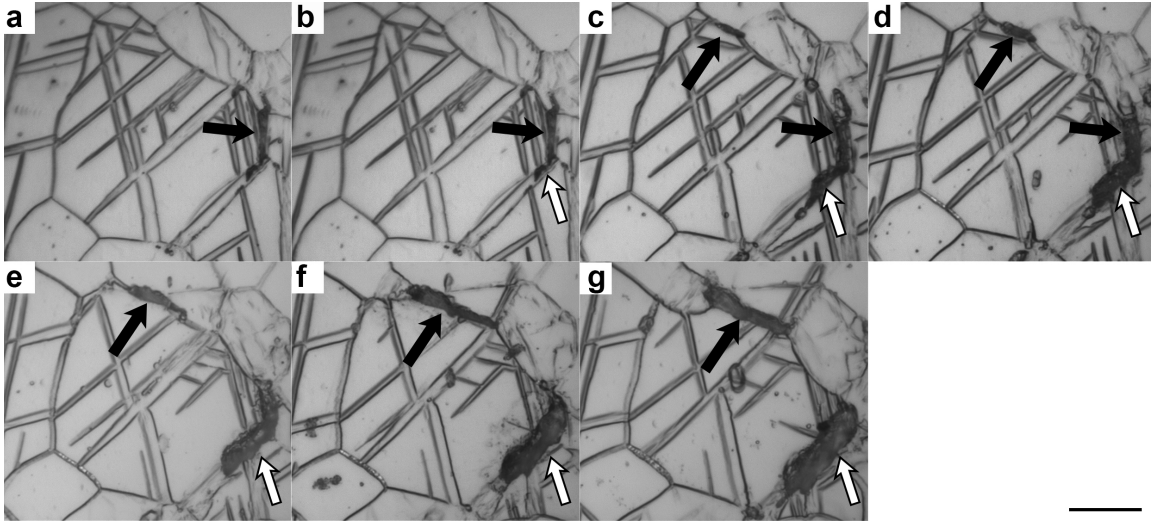


**Supplementary Figure 7 | Slices illustrating the 3D arrangement of several contraction twins.** The white arrow is used as a reference point facilitating the tracking of twin boundary shifts. Several contraction twins are labeled with red numbers to facilitate the relocation of the twins in each of the sections. In addition blue numbers label contraction twins, which were not visible initially and appeared during sectioning. The scale bar corresponds to 20  $\mu\text{m}$ .

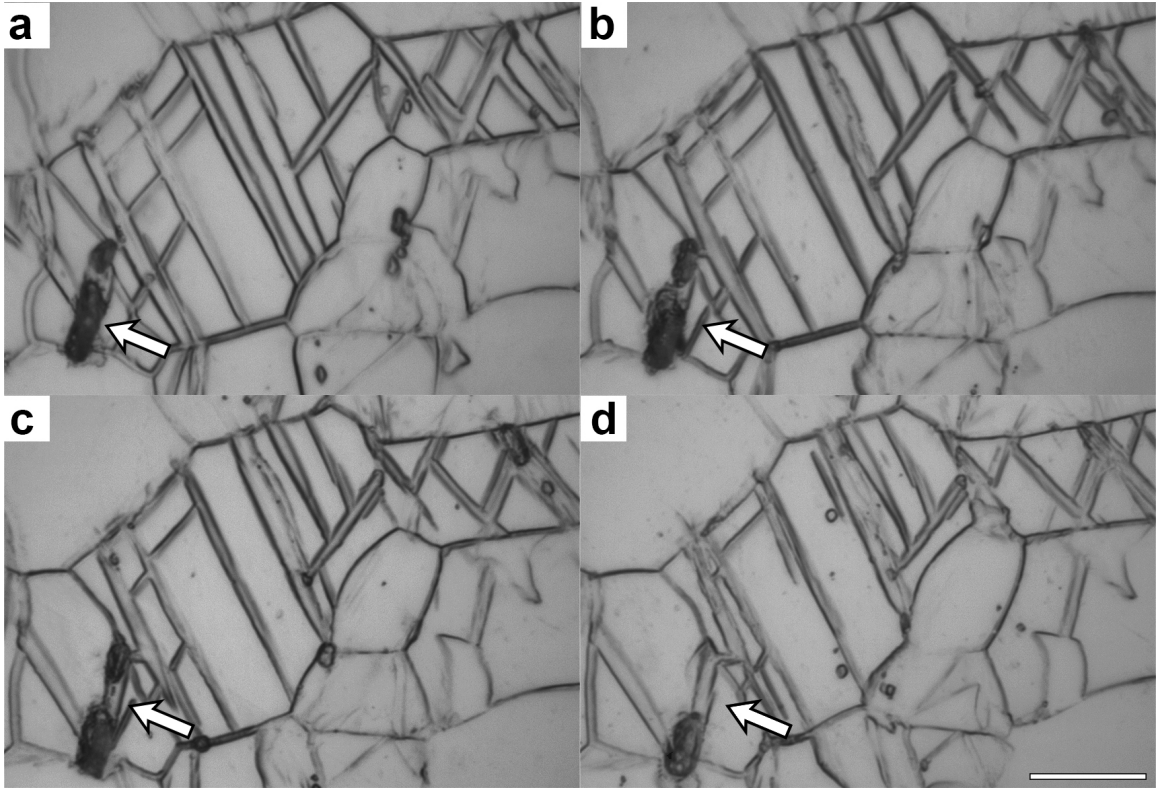


**Supplementary Figure 8 | Schematic displaying contraction twin networks.** Schematic illustrating the 3D network given in Fig 4 a-c and Supplementary Fig. 7. Twin 1 corresponds to A, twin 6 corresponds to B and twins 2, 3, 5 correspond to C. Twins A and C share a  $\langle 11.0 \rangle$  zone axis and hence appear to be parallel in each section; however, sectioning reveals different variants through the increasing distance between the twins. Twin B does not share a  $\langle 11.0 \rangle$  zone axis with the twins A and C. This twin variant is rotated by 60° about a  $\langle 00.2 \rangle$  axis with respect to twins A and C. This 60° angle is maintained through serial sectioning.

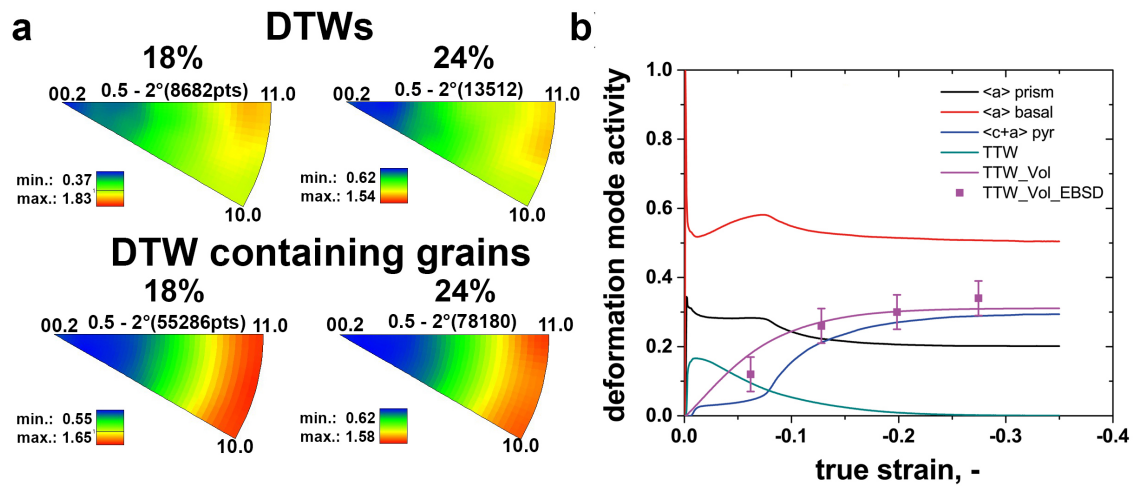




**Supplementary Figure 9 | Slices displaying crack formation.** Slices illustrating crack formation at grain boundaries (black arrows) and at contraction twin boundaries (white arrows). The scale bar corresponds to 20  $\mu\text{m}$ .



**Supplementary Figure 10 | Slices illustrating crack formation at contraction twin boundaries.** White arrows mark a crack, which was formed at a contraction twin boundary using consecutive slices. The scale bar corresponds to 20  $\mu\text{m}$ .



**Supplementary Figure 11 | Analysis of the active deformation modes.** a) IGMA distributions of the DTWs and DTW containing grains. The IGMA distributions are of  $\langle uvt0 \rangle$  type indicating a predominant activation of basal  $\langle a \rangle$  slip or coactivation of basal  $\langle a \rangle$  slip and pyramidal  $\langle c+a \rangle$  slip. b) Predicted deformation mode activity for the CG material indicating an important contribution of  $\langle c+a \rangle$  pyramidal slip at strains  $> 10\%$ .

## Supplementary Tables

**Supplementary Table 1 | Tension twin (TTW) volume fractions of the CG and the FG materials.** The TTW volume fractions have been calculated from the <00.2> texture component parallel to the compression direction (cf. Supplementary Notes - TTW volume fraction)

Compression strain	TTW volume fraction (CG)	TTW volume fraction (FG)
$\epsilon_E = 6\%$	12% $\pm$ 5%	12% $\pm$ 5%
$\epsilon_E = 12\%$	26% $\pm$ 5%	25% $\pm$ 5%
$\epsilon_E = 18\%$	30% $\pm$ 5%	24% $\pm$ 5%

### **Supplementary Note 1: Texture**

Fig. 1 displays the initial texture of the extrusion using pole figures and inverse pole figures (IPF) with respect to the radial direction ( $\perp$  ED). In order to provide a more detailed description of the texture Supplementary Fig. 1 displays IPFs parallel to the extrusion and the radial direction along with the fibre volume fraction of the relevant texture components. Both materials feature very similar textures, which only differ slightly in sharpness. Hence, texture effects are largely omitted in this study. In order to evaluate the remaining texture effects, elastic-plastic self-consistent simulations were conducted, which are displayed in Supplementary Fig. 3 a) and confirm a minor influence of the starting texture on the deformation behavior.

### **Supplementary Note 2: Tension twin volume fraction**

We calculate the fiber volume of the  $\langle 0002 \rangle$  texture component parallel to compression direction within an angular deviation of  $30^\circ$  and subtracting the initially present fiber volume. The results are summarized in Supplementary Table 1. Unfortunately, the determination of the initially present fiber volume introduces a notable error, which might conceal the commonly observed Hall-Petch effect on tension twinning.