

SUPPLEMENTARY INFORMATION

Computationally Informed Design of a Multi-Axial Actuated Microfluidic Chip Device

Alessio Gizzi,^a Sara Maria Giannitelli,^a Marcella Trombetta,^a Christian Cherubini,^{a,b} Simonetta Filippi,^{a,b} Adele De Ninno,^c Luca Businaro,^c Annamaria Gerardino,^c and Alberto Raineri^{*a,c}

PDMS mechanical characterization

Customized molds were purposely manufactured to investigate the mechanical response of the PDMS both in tension and compression. The degassed mixtures (10:1 v/v and 15:1 v/v prepolymer-to-curing agent ratio) were poured into the molds and cured using a digitally controlled oven, allowing precise control of the operating temperature. Since the influence of curing process on PDMS mechanical properties is clearly documented^{1,2}, curing time and temperatures were set in order to exactly reproduce the thermal steps experienced by the material during device fabrication.

Mechanical tests were performed on a universal tester (model 3365, Instron Corporation, Issaquah, WA, USA) equipped with a 500 N f.s. load cell. Unconfined compression tests were performed on cylindrical samples up to 50% strain. Uniaxial tensile tests were conducted until failure on rectangular specimens. For each experimental condition, at least three specimens were tested, stress-strain curves were acquired and averaged, and results were used for tuning of the *in silico* model.

Definition of the PM geometry

Different geometries were analyzed to identify the optimal MCD design (see Fig. S1). In Fig. S2, a direct comparison among three representative geometries

under equibiaxial stretching is provided: displacement field (a), strain (b) and stress (c) patterns, equivalent stiffness (d). Color codes are homogenized over the three configurations.

Addendum to: Multiaxial Loading Simulations

Figure S3 shows von Mises strain field (a) and equivalent stiffness (b) induced on the optimized porous membrane (PM) under uniaxial (left), equibiaxial (center) and biaxial 3:5 (right) loading patterns for a maximum pressure $p = -500\text{ mbar}$. Figure S4 compares the equibiaxial displacement field components (u, v horizontal and vertical, respectively) measured on the MCD with those obtained by numerical simulations for the three material models (NLE, MR, OGD). Three different points placed at $(0^\circ, 45^\circ, 90^\circ)$ along a circular region with radius $750\ \mu\text{m}$ from the center of the PM have been represented.

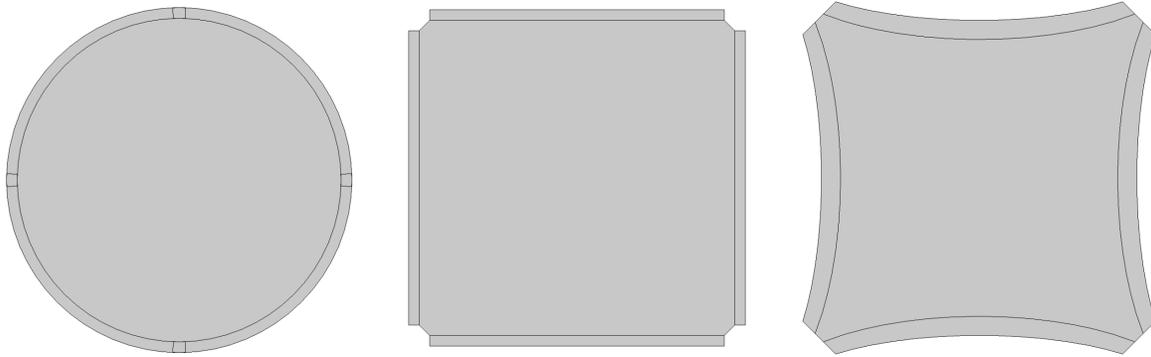
References

- 1 D. T. Eddington, W. C. Crone and D. J. Beebe, 7th International Conference on Miniaturized Chemical and Biochemical Analysis Systems, 2003.
- 2 I. D. Johnston and et al., *Journal of Micromechanics and Microengineering*, 2014, **24**, 035017.

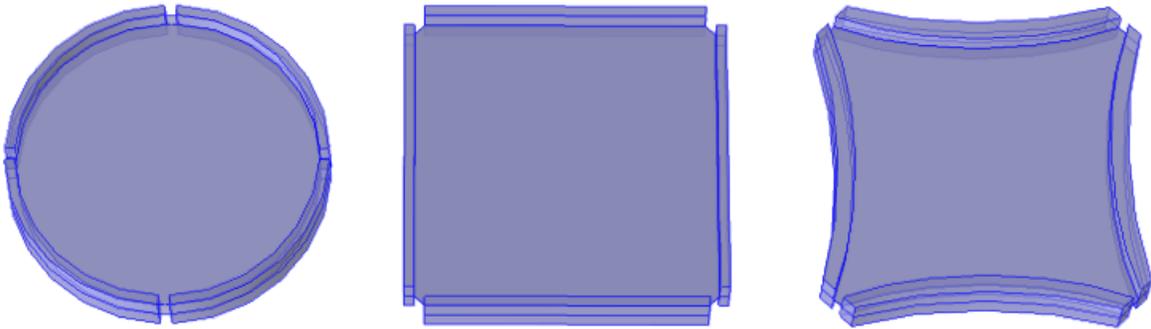
^a Department of Engineering, Università Campus Bio-Medico di Roma, Rome, Italy. E-mail: a.raineri@unicampus.it

^b International Center for Relativistic Astrophysics (ICRA), Rome, Italy.

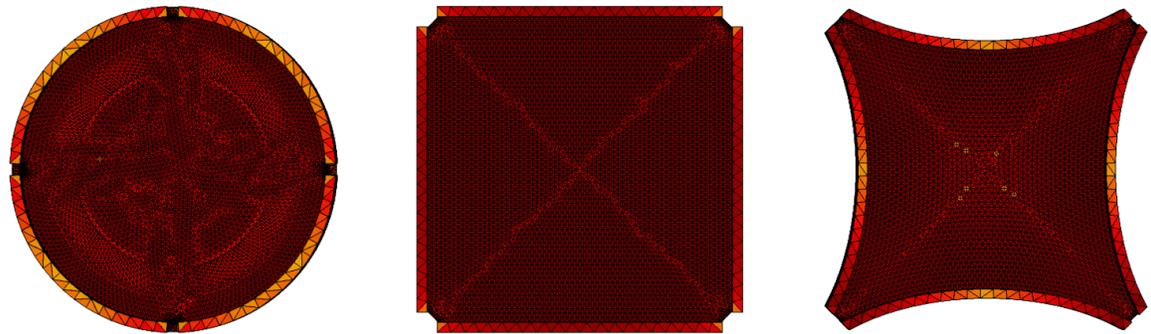
^c Institute for Photonics and Nanotechnology, National Research Council, Rome, Italy.



(a)



(b)



(c)

Fig. S1 Comparison of different designs for the PM: a) planar section; b) three-dimensional view; c) mesh quality.

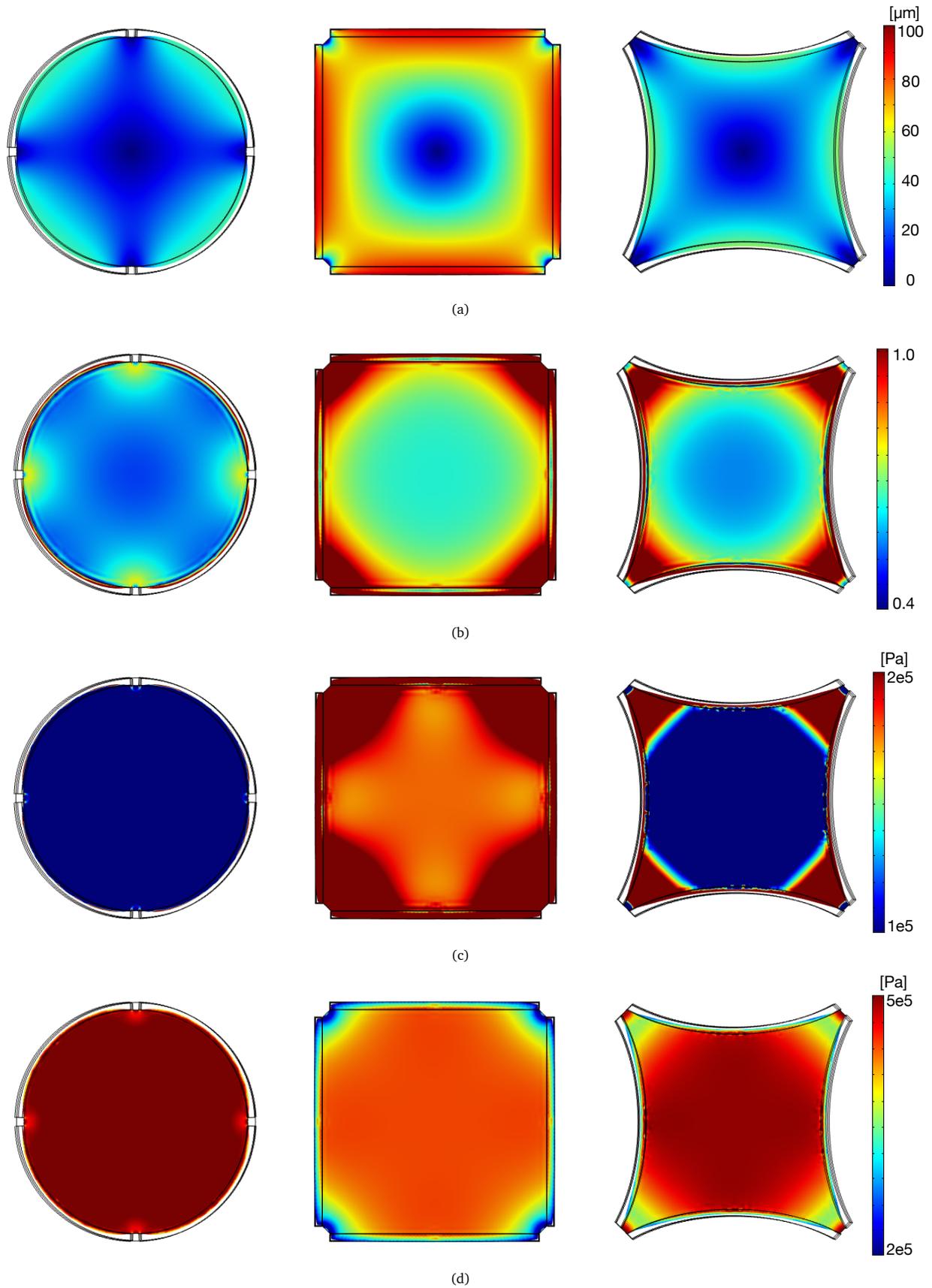


Fig. S2 Comparison of different designs for the PM under equibiaxial loading in terms of: a) displacement field; b) strain distribution of the first invariant of deformation; c) von Mises stress; d) equivalent stiffness.

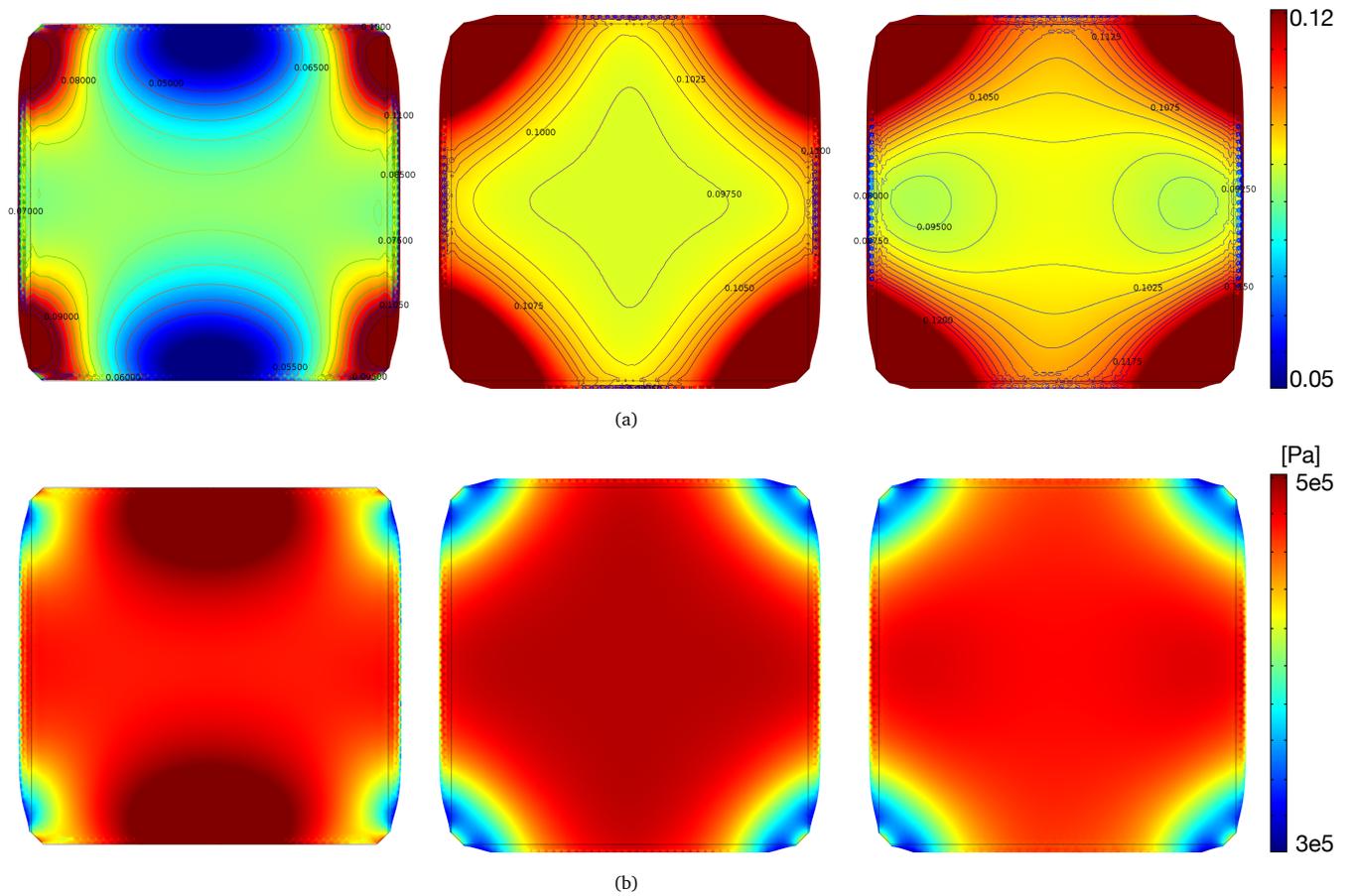
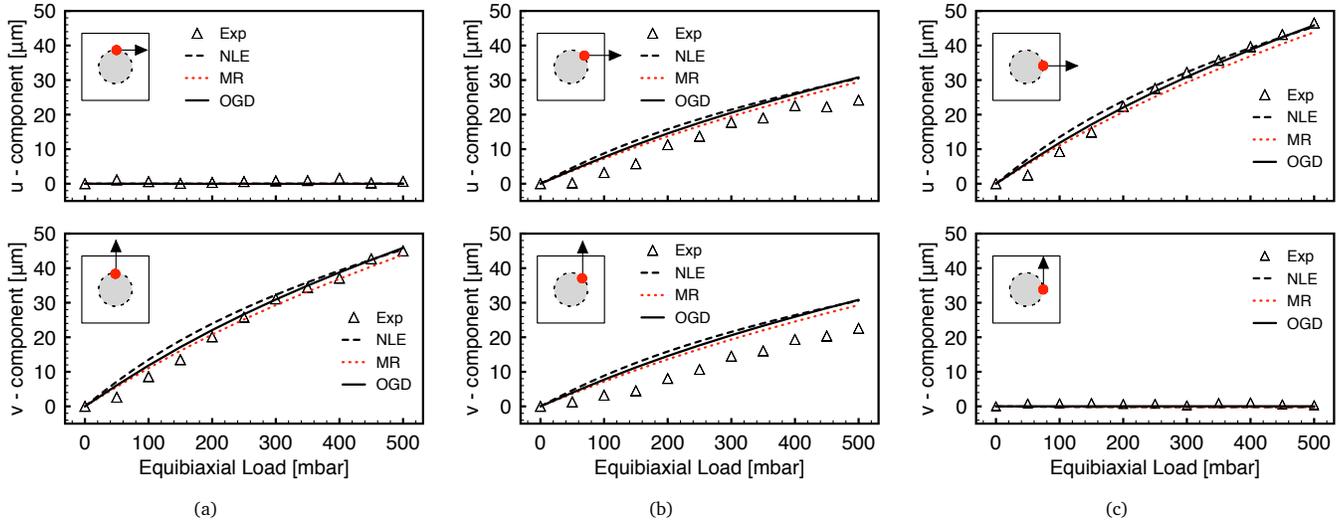


Fig. S3 a) von Mises strain induced on the PM under uniaxial (left), equibiaxial (center) and biaxial 3:5 (right) loading patterns for a maximum pressure $p = -500 \text{ mbar}$. A limited range of strain values $[0.05 \div 0.12]$ is displayed. b) Equivalent stiffness for the corresponding loading patterns. A limited range of stiffness values $[(3 \div 5 \cdot 10^5) \text{ Pa}]$ is displayed.



| Radius [μm] | r.m.s. error [%] | | |
|--------------------|------------------|------|------|
| | NLE | MR | OGD |
| 750 | 10.8 | 10.8 | 11.2 |

Fig. S4 Model validation under equibiaxial loading (negative pressure). Displacement field components (horizontal and vertical, u, v , respectively) taken at $r = 750 \mu m$ (a-c) from the center of the porous membrane (PM) for three representative points. 'Exp' refers to measured data; NLE, MR and OGD refer to nonlinear elastic, Moonery-Rivlin and Ogden material models, respectively. The insets indicate the position of the points with coordinates (origin is set in the center of the membrane): (a) (0, 750), (b) (530, 530), (c) (750, 0). The table reports the average percentage error of the displacement over the three selected locations for the peak pressure (500 mbar) vs. the three material models.