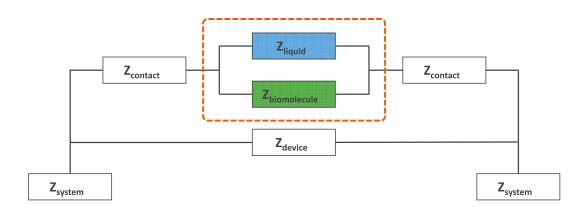
## A highly sensitive plasma-based amyloid-β detection system through medium-changing and noise cancellation system for early diagnosis of the Alzheimer's disease

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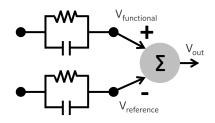


Fig. S1. Equivalent circuit of IME sensor and cancellation principle.

The designed interdigitated microelectrode was used for  $A\beta$  protein detection with signal processing systems. The interaction between  $A\beta$  protein and  $A\beta$  antibody, which is immobilized at the functional electrode of the sensor, led to changes in the impedance. Fig. S1. (a) shows an equivalent circuit of IME sensor in buffer solution before the functional electrode for accurate measurement of impedance changes by the interaction between  $A\beta$  protein and  $A\beta$  antibody ( $Z_{biomolecule}$ ). The biomolecule-containing liquid has high impedance. The designed

system was utilized to cancel out the impedance of liquid ( $Z_{liquid}$ ) and the specified parasitic impedance caused by the system and device. The  $Z_{system}$  and  $Z_{contact}$ , which respectively represent impedance due to the measurement system and measuring probe and electrode, were considered in the equivalent circuit. The  $Z_{device}$  represents the impedance between electrodes in a single device. As shown in Fig. S1, the reference electrode was used to cancel out these all impedances for enhancement of sensitivity. As shown in Fig. S1(b), the voltages from the functional electrode ( $V_{functional}$ ) and reference electrode ( $V_{reference}$ ) were calculated to cancel out other impedances for the accurate measurement of impedance changes by only the  $Z_{biomolecule}$  with the system. The output voltage ( $V_{out}$ ), which is due to the  $Z_{biomolecule}$ , was also amplified with the amplifier after the cancellation between the voltages of functional and reference electrodes as differential amplifier works.

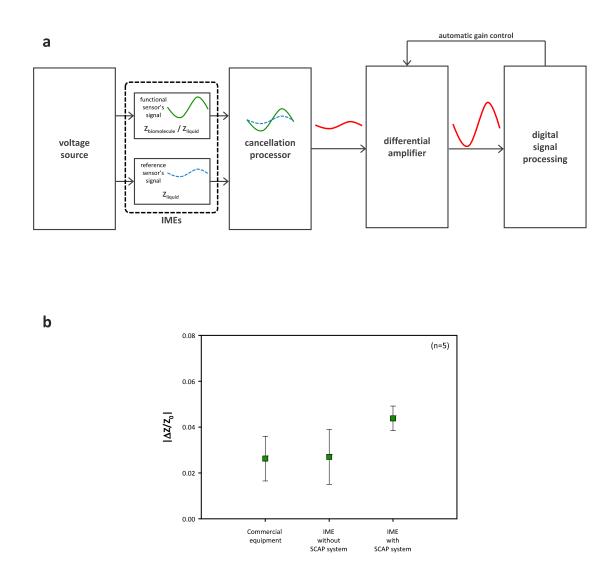


Fig. S2. Performance of signal cancellation and amplification process system embedded measurement system.

After obtaining an A $\beta$  antibody layer on SiO<sub>2</sub>, the interaction between the immobilized A $\beta$  antibody and A $\beta$  antigen could be measured using the designed IME sensing system. The designed sensing system, which has a signal cancellation and amplification process (SCAP) system embedded in the measurement system, was accomplished as shown in Fig. S2(a) in order to enhance sensitivity along with noise removal. Generally, the noise occurred by a biomolecule-containing solution and the structure of IME, which has a relatively long electrode length between electrodes. The Z<sub>liquid</sub> and Z<sub>biomolecule</sub> marked in Fig. S2(a) indicate the impedance of solution, including the effect of IME structures and impedance of target biomolecules,

respectively. The  $Z_{liquid}$  and  $Z_{biomolecule}$  were more dominant than other impedance components, as shown in an equivalent circuit (see Fig. S1(a) for detatils.). The effect of  $Z_{liquid}$  was approximately 1000–2000 fold greater than that of  $Z_{biomolecule}$ . Therefore, we developed a cancellation and amplification process to remove  $Z_{liquid}$  and other impedance components. Functional and reference electrodes were utilized. The functional electrode could detect  $Z_{biomolecule}$ , including the effect of liquid,  $Z_{liquid}$ . The reference electrode only detected  $Z_{liquid}$ . Therefore, we loaded the biomolecule-containing solution at the functional electrode and the same liquid without biomolecules at the reference electrode. The same conditions, voltage, and frequency were applied at both electrodes. After measurement of two impedimetric signals by the functional and reference electrodes, the two signals ( $Z_{biomolecule}/Z_{liquid}$  and  $Z_{liquid}$ ) were subtracted, to obtain the changes that were due to biomolecules ( $Z_{biomolecule}$ ). The amplification was also applied after the cancellation. Finally, we acquired amplified signals obtained only due to biomolecules ( $Z_{biomolecule}$ ) with the designed measurement systems. Other modes that do not apply cancellation and amplification could also be used.

To verify IME impedance measuring system, we repeatedly compared SCAP system with commercial equipment (PGSTAT302N, Metrohm Autolab), as shown in Fig. S2(b). After 10 pg mL-1 A $\beta$ -A $\beta$  antibody interaction, the impedance change of the same IME was monitored using each measurement system. About 2.6%, 2.7%, and 4.3% of impedance changes were measured using commercial equipment, IME without SCAP system, and IME with SCAP system, respectively; approximately 1.9%, 2%, and 1% standard deviations, respectively, were calculated for the impedance changes. By utilizing IME with SCAP system, we achieved a 1.6-fold higher impedance change and a half lower standard deviation compared with other systems. We also confirmed that the IME with SCAP system for A $\beta$  detection was more suitable than the other systems.

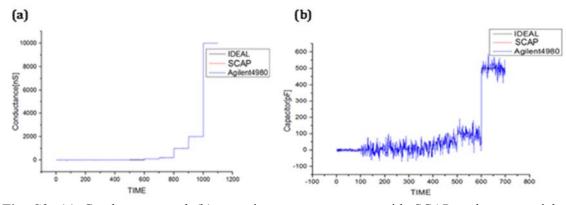


Fig. S3. (a) Conductance and (b) capacitance measurement with SCAP and commercial equipment (Agilent 4980).

Capacitance	Error ratio (%)		
(pF)	SCAP	commercial	
10	0.59	64.908	
50	0.15	1.293	
100	0.47	4.361	
500	0.38	0.177	
average	0.39	17.68	

Table. The error ratio estimation of measuring conductance and capacitance

Resistance	Error ratio (%)		
(MΩ)	SCAP	commercial	
200	9.47	31.89	
100	5.06	13.94	
50	10.14	15.89	
10	2.52	4.06	
5	0.39	1.37	
1	0.29	0.07	
0.5	0.26	0.09	
0.1	0.08	0.05	
average	3.52	8.42	

Before the application for IME sensor, the impedance measuring system with SCAP is evaluated. First, we prepared and compounded the electrical components (resistor of 0.1, 0.5, 1, 5, 10, 50, 100, 200 M $\Omega$  and capacitor of 10, 50, 100, 500 pF). The conductance and capacitance were monitored with SCAP and commercial equipment (Agilent 4980) as shown Fig. S3. When the conductance and the capacitance measured, the ratio of error of conductance and capacitance with SCAP is reduced as described in Table. Furthermore, IME's resistance of approximately 0.4 M $\Omega$  and capacitance of 170 pF were measured, respectively. In the capacitance of range 100 to 500 pF and resistance of range 0.1 to 0.5 M $\Omega$ , the impedance measuring system with SCAP is more appropriate with low measuring error.

## Table S1. Biosensors for the detection of $A\beta$

## Reference

Sensing platform	Simplicity	Detection range	Real bio-fluidics were utilized?	Reference
rGO-FET	Label-free	1 fM to 100 pM	No	1
CNT-MESFET	Label-free	1 pg/mL to 1 ng/mL	Synthetic analytes in human serum	2
GO-based fluorescence	fluorescence label	10 nM to 2 mM	No	3
QCM	Label-free	50 pg/mL to 5 µg/mL	No	4
DVP	labeled	100 pM to 50 nM	Synthetic Aβ in CSF of both normal and AD rats	5
Cyclic voltammetry	fluorescence label	20 pM to 1.50 nM	Synthetic Aβ added into artificial CSF	6
Cyclic voltammetry with N- doped graphene modified Au electrodes	FITC label	5 pg/mL to 800 pg/mL	No	7
SERS	Labe-free	500 fg/mL to 6 pg/mL	Synthetic Aβ spiked in rabbit whole blood.	8
EIS	Label-free	l pM to l μM	Cell-derived natural Aß oligomers in culture medium	9
EIS with carbon disposable electrochemical printed chip	Label-free	10 pM to 200 μM	No	10
This work	Label-free	100 fg/mL to 1 ng/mL (synthetic Aβ)	Synthetic Aβ in mouse plasma	

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