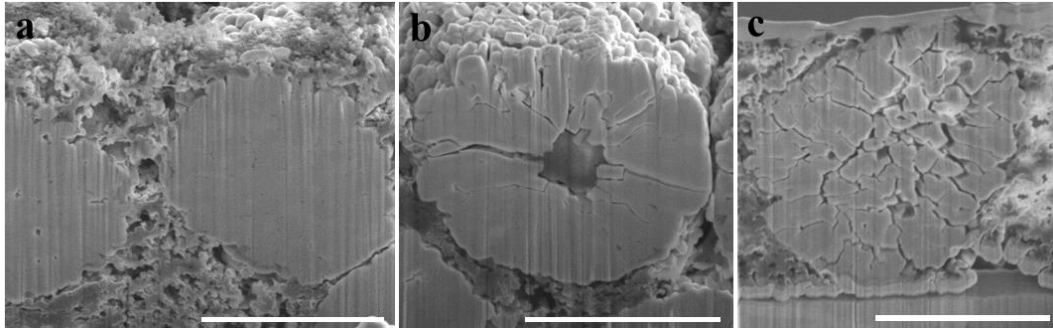
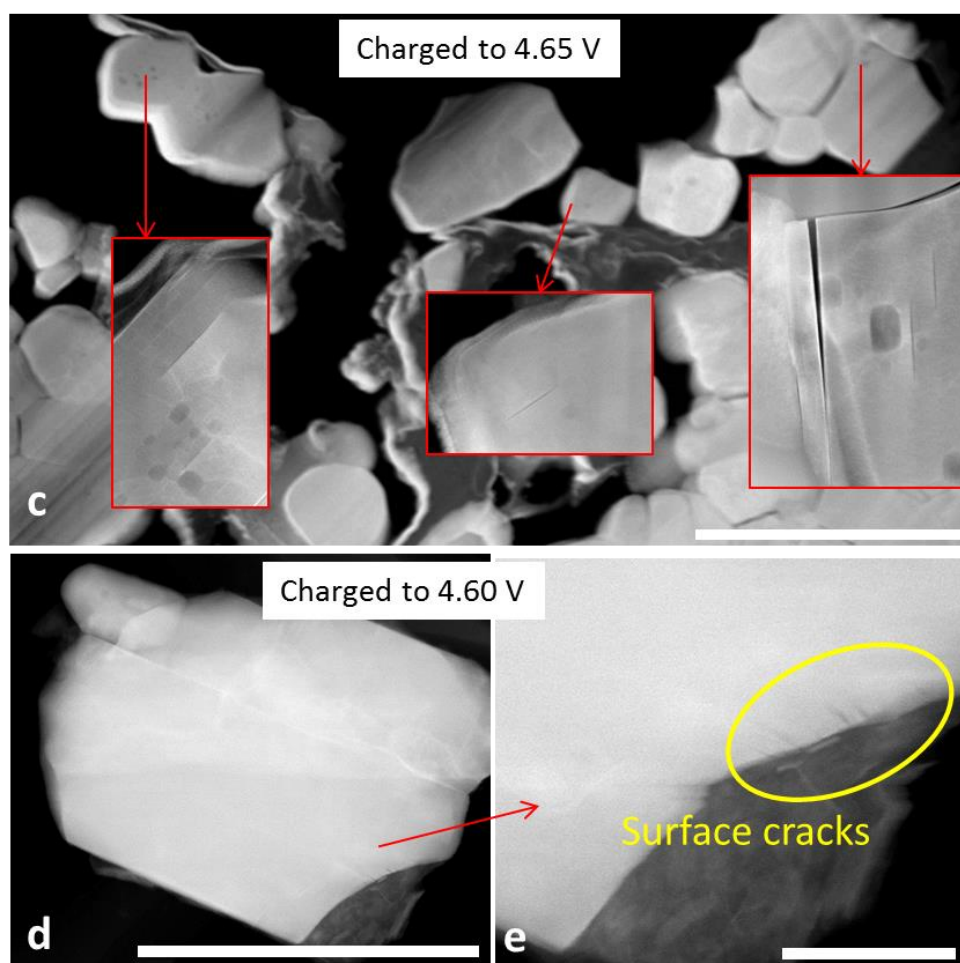
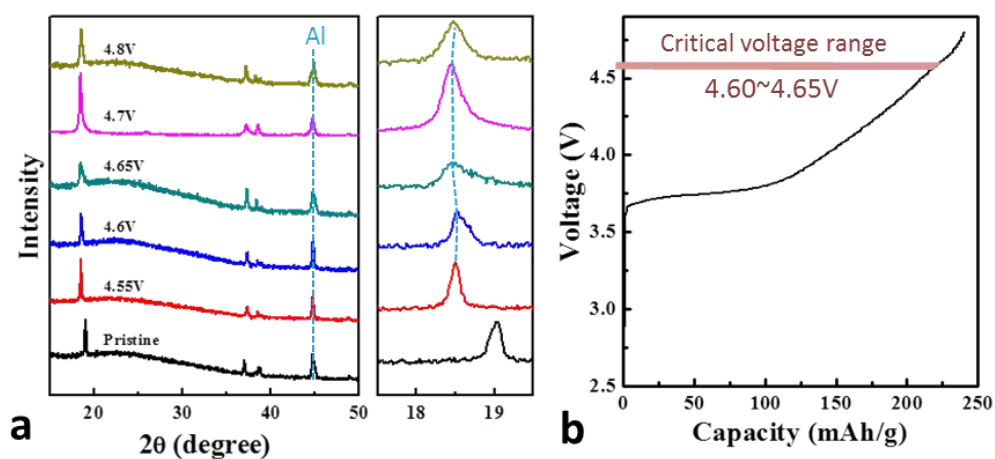


**Coupling of electrochemically triggered thermal and mechanical effects to aggravate failure in a layered cathode**

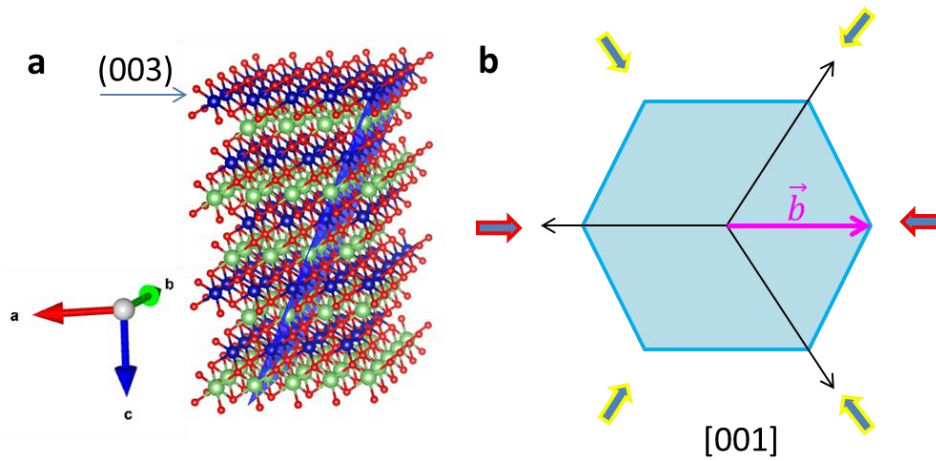
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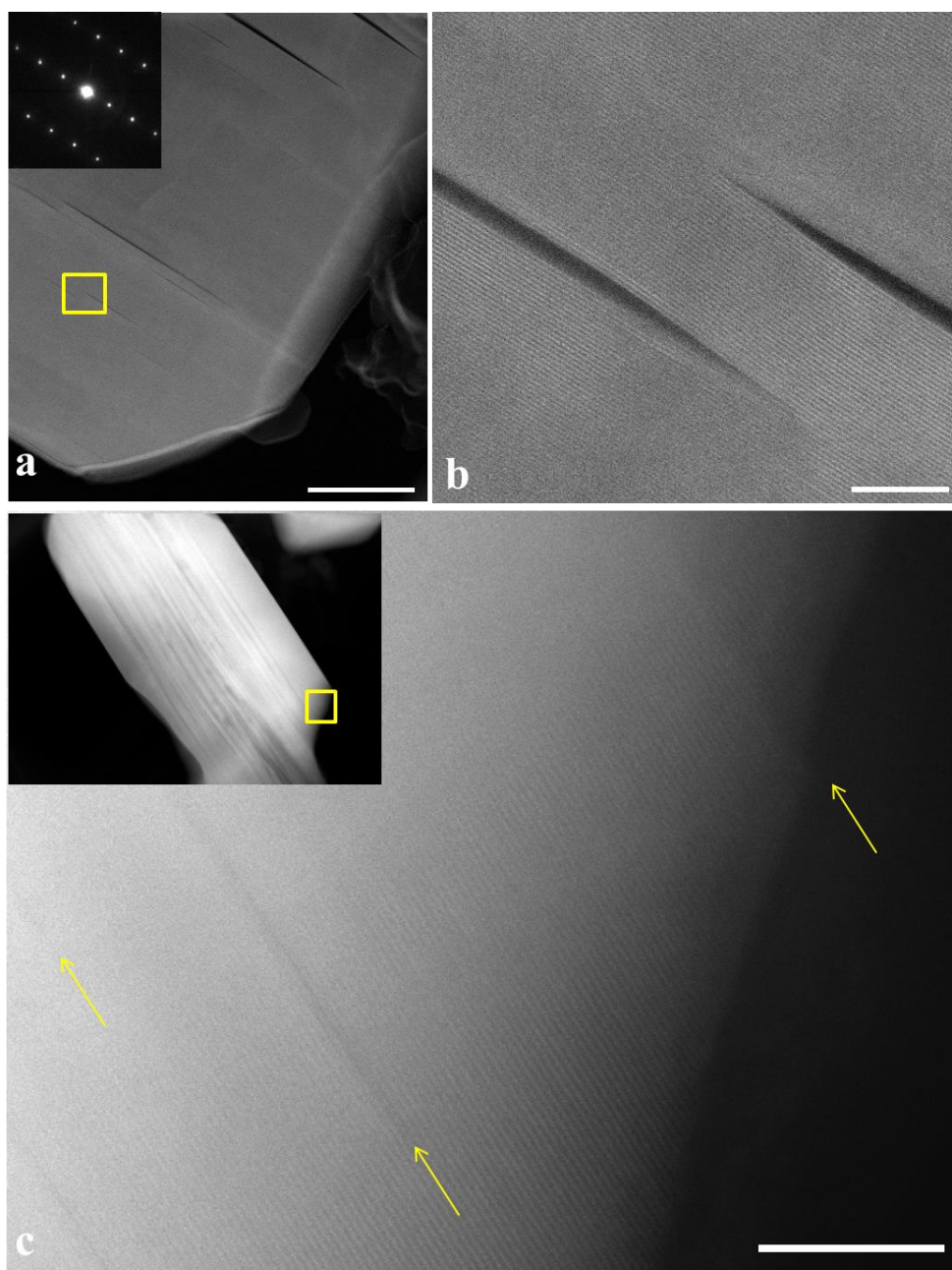
**Supplementary Figure 1. Cross sectional images by scanning electron microscopy (SEM). a**, pristine sample; **b**, after 100 cycles at 2.7–4.5 V; **c**, after 100 cycles at 2.7–4.8 V. The scale bars are 5 μm.



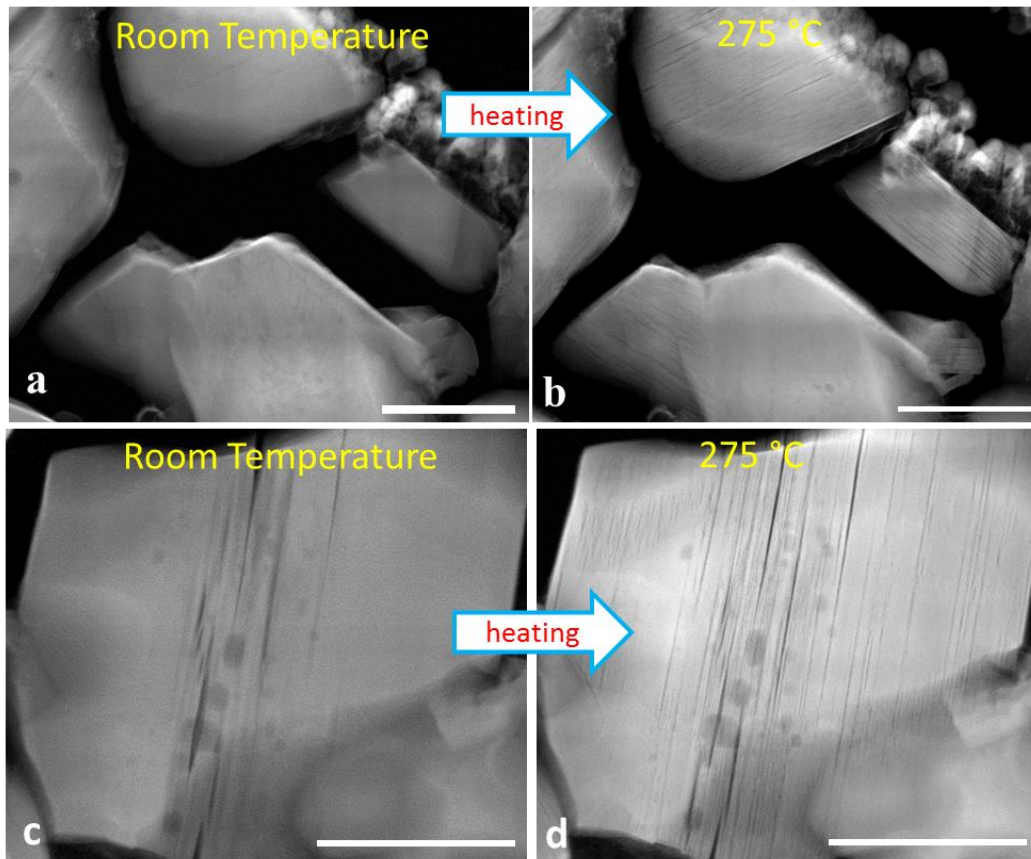
**Supplementary Figure 2. Identify the critical onset voltage for intragranular cracks.** **a**, X-ray diffraction (XRD) results of pristine sample and samples charged to 4.55 V, 4.60 V, 4.65 V, 4.70 V and 4.80 V (vs Li metal). **b**, the charge curve and estimated critical voltage range for intragranular cracks. **c**, High angle annular dark field (HAADF) observations on sample charged to 4.65 V. Cracks are shown insets. **d**, Sample charged to 4.60 V does not have intragranular cracks, but it has surface cracks shown in **e** (cycled area). The scale bars are 2  $\mu\text{m}$  in **c**, 1  $\mu\text{m}$  in **d**, and 200 nm in **e**.



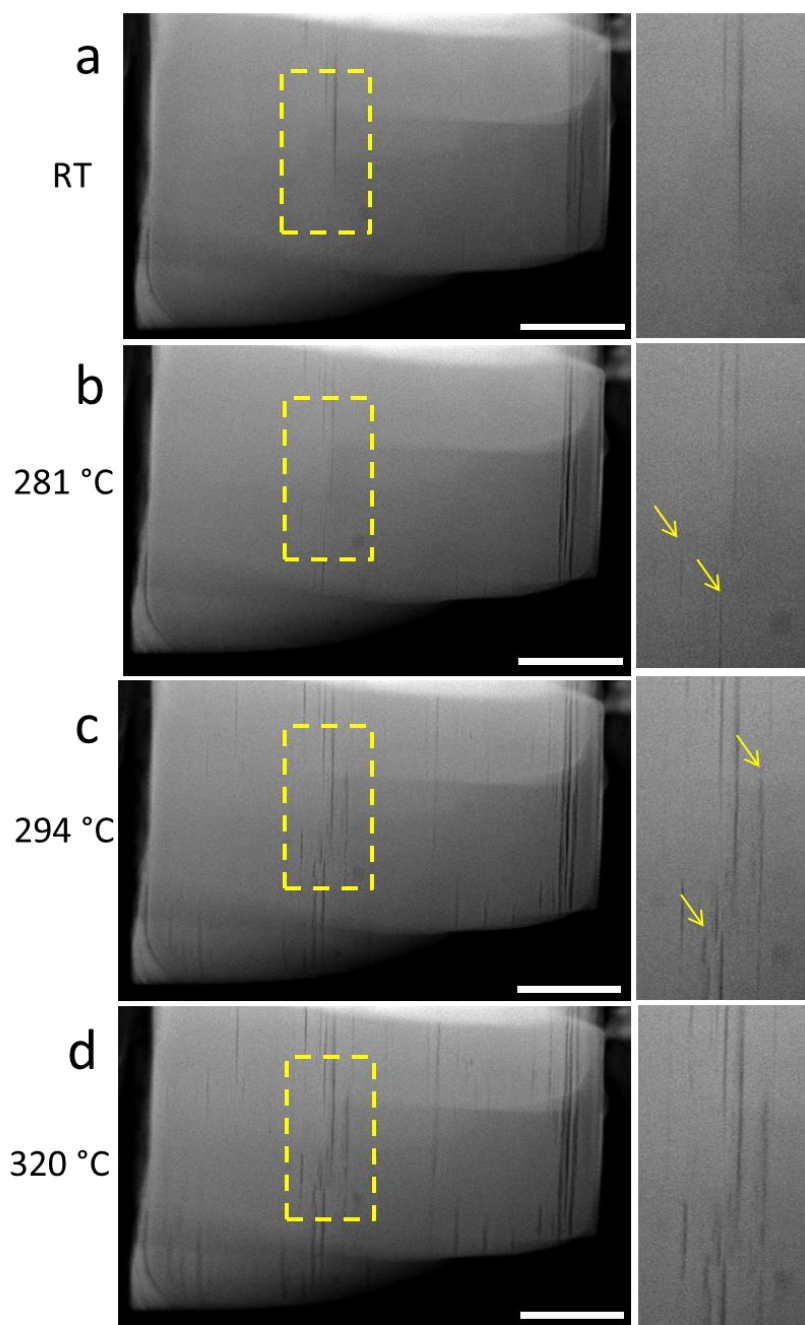
**Supplementary Figure 3. Schematically crystallographic analysis.** **a**, The blue plane denotes a (102) plane in layered structure. **b**, Top view from [001] zone axis, red arrows indicate two directions that cannot see extra (102) plane as they are parallel to the Burger's vector  $\vec{b}$ . Yellow directions can see the extra plane.



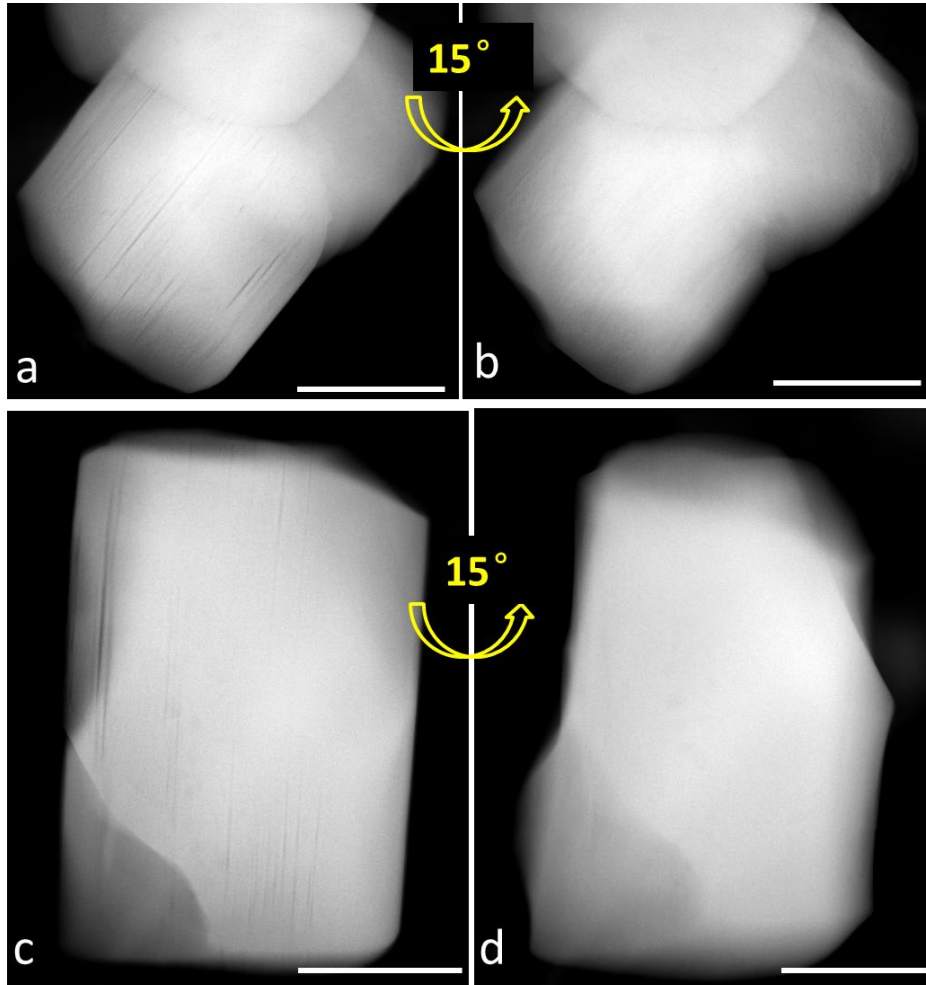
**Supplementary Figure 4. Intragranular cracks in delithiated  $\text{LiNi}_{0.6}\text{Mn}_{0.2}\text{Co}_{0.2}\text{O}_2$ .** Cross sectional high angle annular dark field (HAADF) images showing real cracks in **a** and **b**, incubation cracks in **c** (yellow arrows). Inset diffraction in **a** confirms the layered structure. The scale bars are 200 nm in **a**, 10 nm in **b** and **c**.



**Supplementary Figure 5. In situ heating triggers new cracks.** High angle annular dark field (HAADF) images showing cracks formation after heating of delithiated  $\text{LiNi}_{0.6}\text{Mn}_{0.2}\text{Co}_{0.2}\text{O}_2$  particles from room temperature **a, c** to 275 °C **b, d**. The Scale bars are 500 nm.

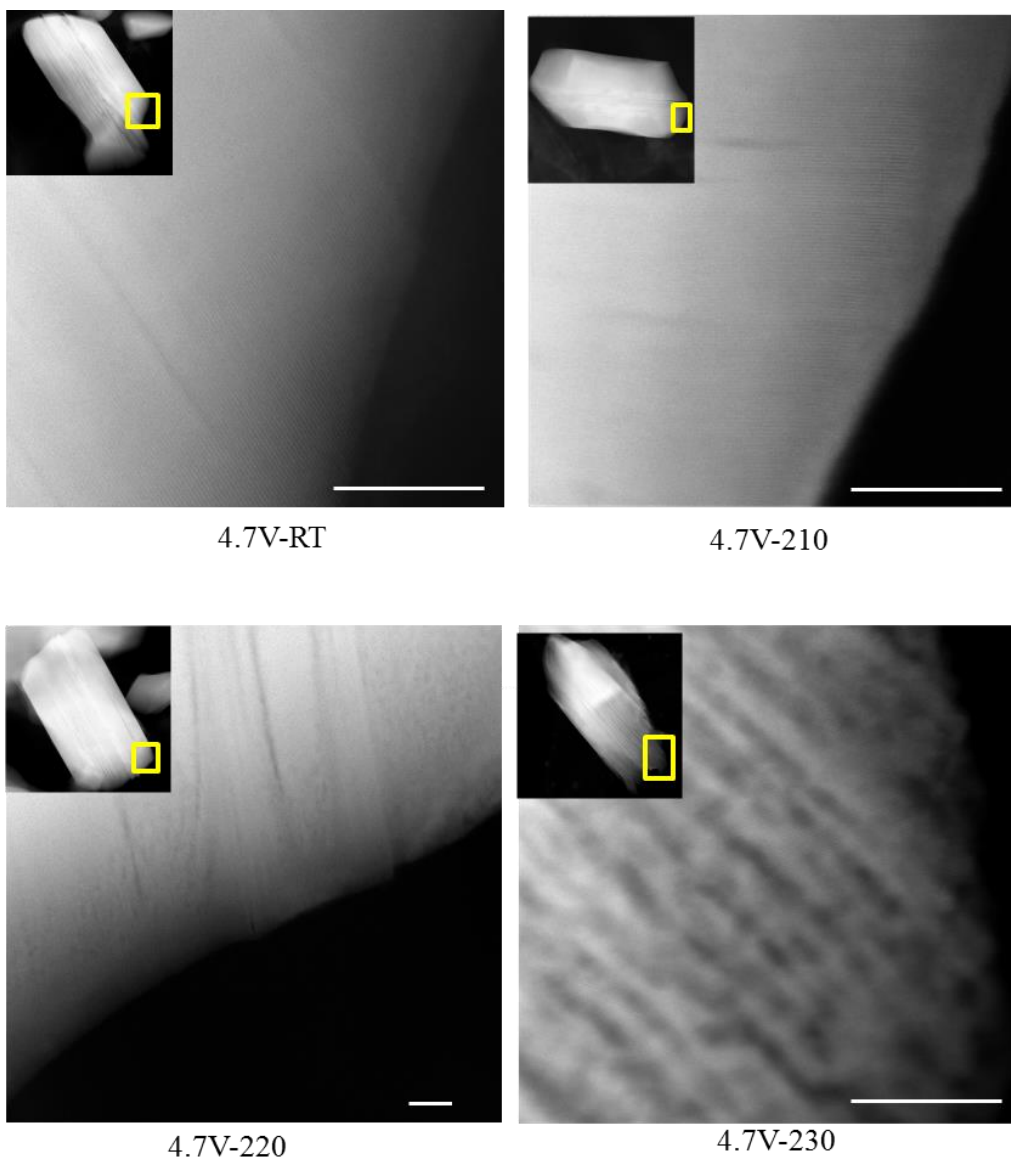


**Supplementary Figure 6. Snapshots during in situ heating.** A delithiated  $\text{LiNi}_{0.6}\text{Mn}_{0.2}\text{Co}_{0.2}\text{O}_2$  particle (charged to 4.7 V vs Li metal) is heated from room temperature **a** to 281 °C **b**, 294 °C **c**, and 320 °C **d**. Yellow arrows indicate new cracks. The scale bars are 200 nm.

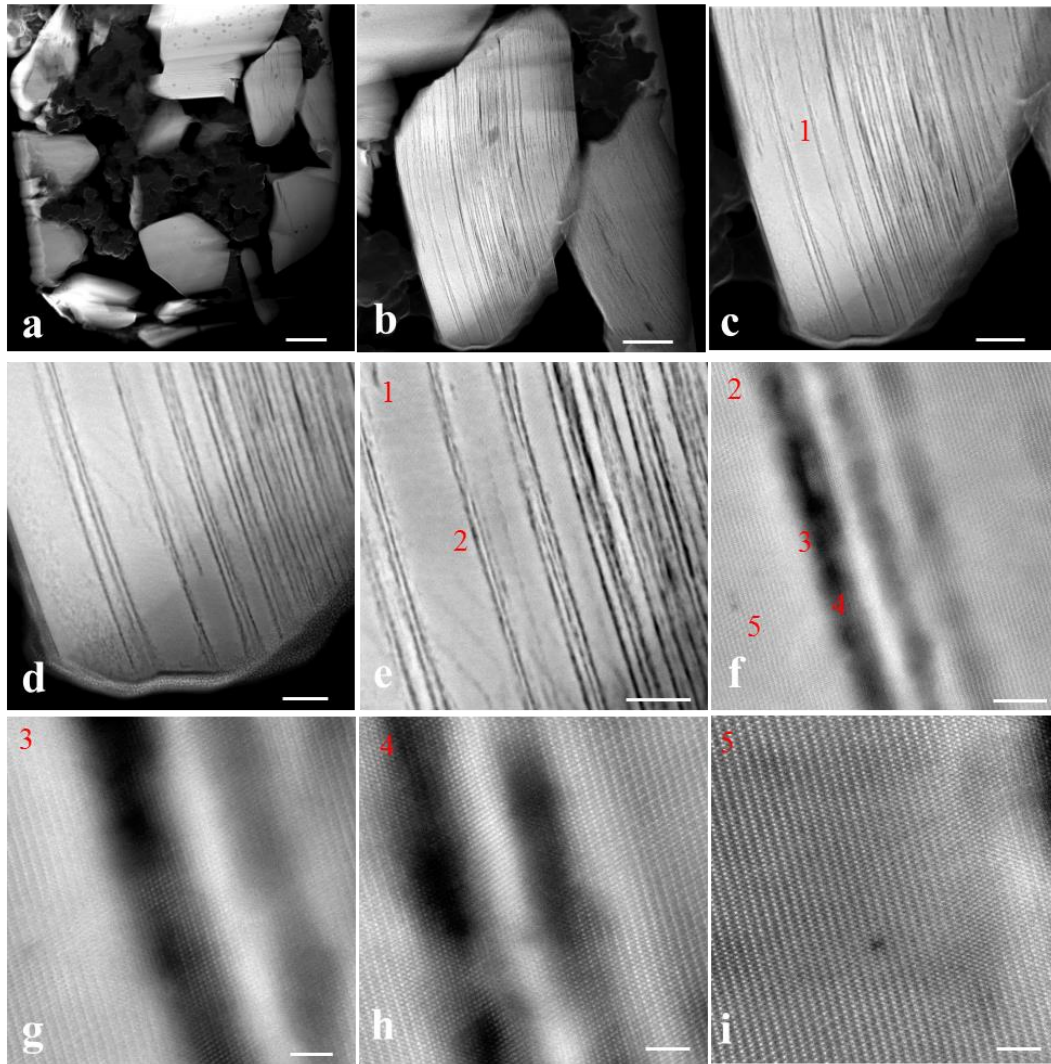


**Supplementary Figure 7. Orientation matters crack imaging.** Two examples **a, b** showing tilting the observation directions can lead to cracks invisible. The scale bars are 200 nm in **a, b** and 500 nm in **c, d**.

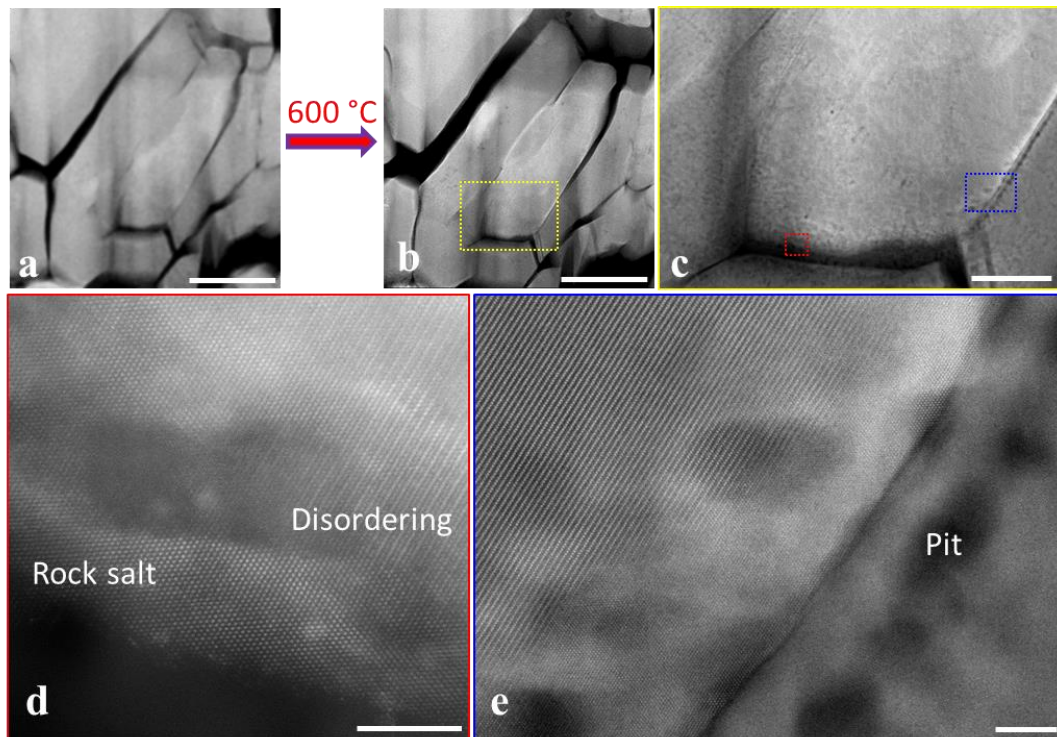




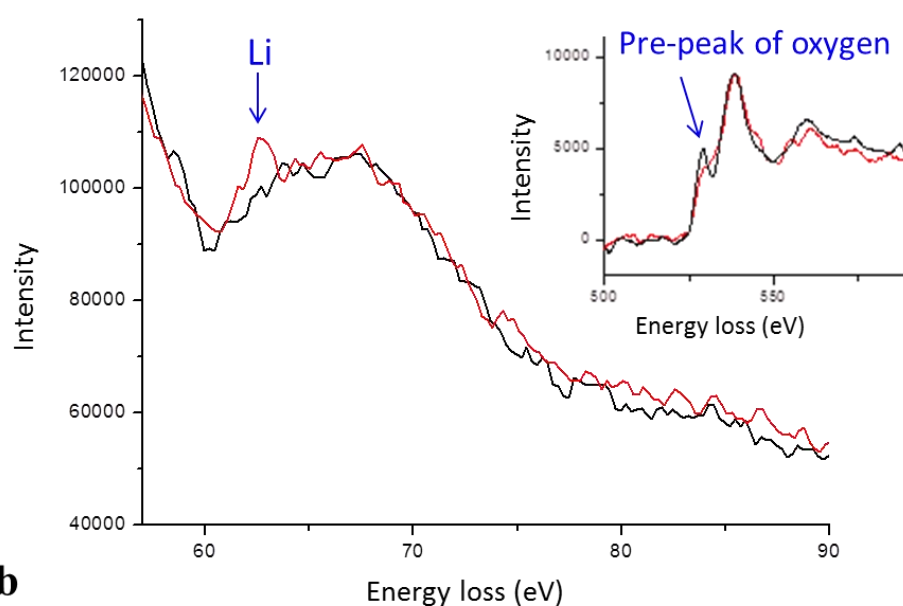
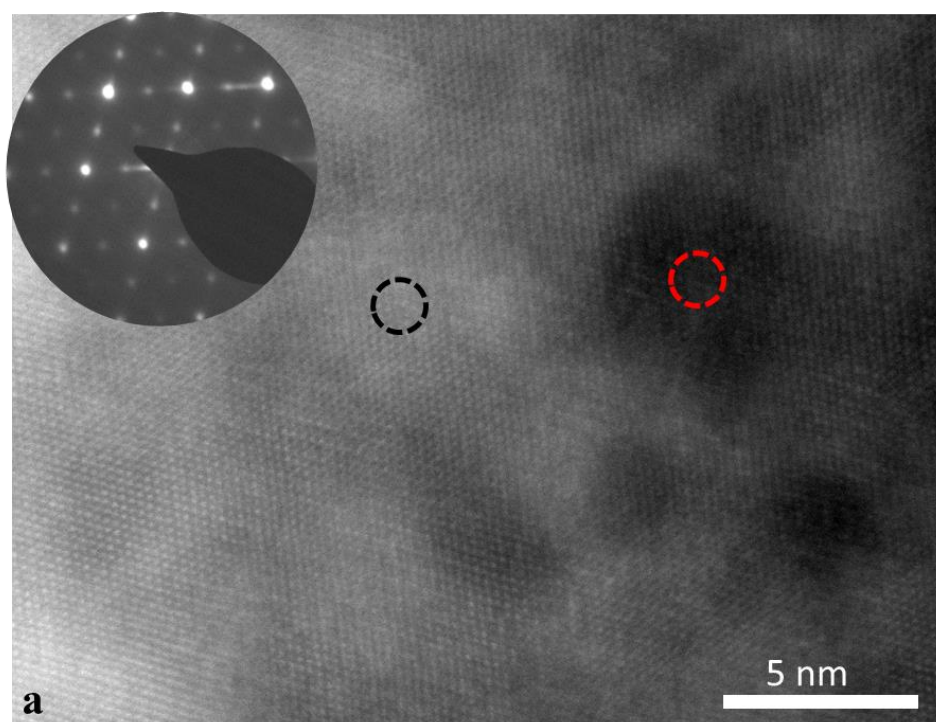
**Supplementary Figure 8. Identify the starting temperature point for intragranular cracking and decomposition.** High angle annular dark field (HAADF) observations reveal the transition temperature range is 210 °C to 230 °C. The scale bars are 20 nm.



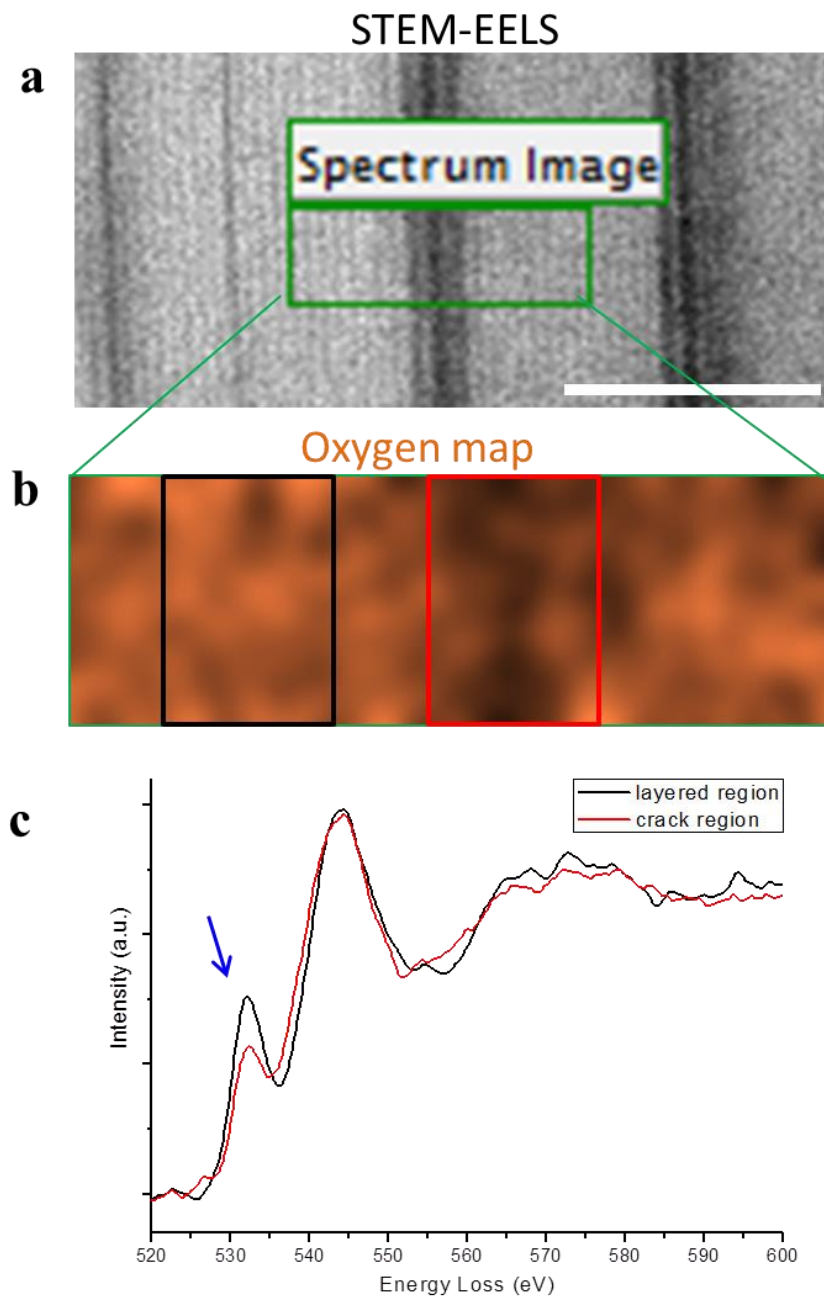
**Supplementary Figure 9. Confirming bulk cracking mechanism.** Cross sectional observation by high angle annular dark field (HAADF) on FIB milled particles. The sample is heated to 230 °C. Intragranular cracking and thermal decomposition are clearly observed. The scale bars are 500 nm in **a**, 200 nm in **b**, **c**, 50 nm in **d** and **e**, 5 nm in **f**, 2 nm in **g**, **h** and **i**.



**Supplementary Figure 10. In situ heating of fully discharged sample.** The  $\text{LiNi}_{0.6}\text{Mn}_{0.2}\text{Co}_{0.2}\text{O}_2$  sample is cycled 100 times with cycle window as 2.7-4.5 V. **a** the sample area under room temperature, **b–e** after heating to 600 °C. **c** is from the yellow frame in **b**. **d** and **e** are from **c**, respectively. Heating resulted phase transformation and pit formation are only located at surface layer. The scale bars are 500 nm in **a** and **b**, 100 nm in **c**, 5 nm in **d** and **e**.



**Supplementary Figure 11. Characterizing pit position.** **a**, High angle annular dark field (HAADF) image and corresponding selective area electron diffraction (SAED) pattern from thermal decomposed region. HAADF image shows pit formation due to material decomposition. SAED shows a typical spinel featured pattern but without other crystal phase, indicating lithia is in amorphous state rather than crystalline. The scale bar is 5 nm. **b**, Electron energy loss spectroscopy (EELS) measurement from the pit region (red) and original region (black). Pit region shows higher Li concentration evidenced by the boosted Li K-edge. Inset oxygen K-edge also shows a depressed pre-peak which is from lithia.



**Supplementary Figure 12. Measure oxygen concentration at crack region. a,** High angle annular dark field (HAADF) image of cycle induced cracks. The scale bar is 10 nm. **b,** corresponding oxygen map of the region in **a.** **c,** Electron energy loss spectroscopy to compare the crack region (red) and crack-free region (black). The depressed pre-peak of oxygen indicates oxygen vacancies in crack region.

**Supplementary Table 1** Mechanical material constants of NMC622 and LiNMC622<sup>3-5</sup>

	NMC622	LiNMC622
$E_1$	186.7 GPa	229.3 GPa
$E_2$	186.7 GPa	229.3 GPa
$E_3$	54.2 GPa	152 GPa
$\nu_{12}$	0.3	0.3
$\nu_{23}$	0.24	0.24
$\nu_{31}$	0.24	0.24
$G_{12}$	71.5 GPa	95.3 GPa
$G_{23}$	20.8 GPa	63.2 GPa
$G_{31}$	20.8 GPa	63.2 GPa

## Supplementary Methods

### Simulation methods

We developed a mechanics model to elucidate the different origins of the driving forces for crack propagation in the  $\text{LiNi}_{0.6}\text{Mn}_{0.2}\text{Co}_{0.2}\text{O}_2$  (NMC622) particles. The total strain here is additive of three components, the chemical ( $\varepsilon_{ij}^c$ ), thermal ( $\varepsilon_{ij}^t$ ), and elastic ( $\varepsilon_{ij}^e$ ) one, as  $\varepsilon_{ij} = \varepsilon_{ij}^c + \varepsilon_{ij}^t + \varepsilon_{ij}^e$ , where the subscripts  $i, j = 1, 2, 3$  represent the [100], [010], and [001] directions of materials. The chemical strain is induced by lithium insertion, which is assumed to be proportional to the normalized lithium concentration ( $c$ ) by fully lithiated state, as  $\varepsilon_{ij}^c = \beta_{ij}c$ . The diagonal tensor,  $\beta_{ij}$ , represents the lithiation expansion coefficients. As for NMC622, we set  $\beta_{11} = \beta_{22} = 2.8\%$ ,  $\beta_{33} = -4.0\%$ , and  $\beta_{ij} = 0$  for the other entries.<sup>1</sup> The thermal strain is linearly dependent on the increment of temperature,  $\varepsilon_{ij}^e = \alpha_{ij}\Delta T$ , with the room temperature set as the reference (25 °C). For layered structured phase (NMC622), we set  $\alpha_{11} = \alpha_{22} = 3.34 \times 10^{-6}$  and  $\alpha_{33} = 6.3 \times 10^{-6}$  to present anisotropic thermal expansion,<sup>2</sup> whereas the isotropic thermal expansion of RS phase is set as  $\alpha = 3.4 \times 10^{-6}$ . As an orthotropic crystal, the stiffness tensor of the layered structure depends on nine independent material constants. We set the material constants of NMC622 ( $c = 0$ ) and LiNMC622 ( $c = 1$ ) in the model, as shown in **Supplementary Table 1**, and assume that the stiffness tensor of the intermediate stages linearly scales with the lithium concentration ( $c$ ). However, in an isotropic material like RS phase, the stiffness tensor only depends on two independent constants (i.e. Young's modulus  $E$  and Poisson's ratio  $\nu$ ). Here we set  $E_{RS} = 180\text{Gpa}$  and  $\nu_{RS} = 0.3$ . This mechanics model is numerically implemented in the finite element package ABAQUS/standard.

## Supplementary References

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