

## Supplementary information

### Contactless Fluid Manipulation in Air:

### Droplet Coalescence and Active Mixing by Acoustic Levitation

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#### Calculation method of sound field

The distributed point source method (DPSM)<sup>1, 2</sup> is used to model a sound field without a computational mesh by distributing point sources of sound at the boundary. Emitters and reflectors are discretized by point sources to represent the sound field. The sound pressure  $p_m$  and the velocity  $v_m$  at a distance  $r_{mn}$  generated by a sound wave radiated from the point source  $m$  is given by

$$p_m(r_{mn}) = A_m \frac{\exp i(kr_{mn} - \omega t_m)}{r_{mn}} = A_m G(r_{mn}), \quad (\text{S1})$$

$$v_m(r_{mn}) = \frac{\mathbf{n} \cdot \mathbf{r}_{mn}}{i\omega\rho_G} \frac{\partial p}{\partial r} = A_m M(r_{mn}), \quad (\text{S2})$$

where  $A_m$  is the strength of the  $m$ -th point,  $k = 2\pi/\lambda$  is the wavenumber,  $\omega$  is the angular frequency and  $\rho_G$  is the density of air. For an ultrasonic phased array, sound waves radiated from each transducer are excited at different time intervals  $\Delta t_m$  to focus sound waves. Thus, the term  $t_m$  in Eq. (S1) can be expressed in terms of the phase difference from a reference time  $t$ :

$$t_m = t - \Delta t_m. \quad (\text{S3})$$

If there are  $N$  point sources, the total value at point  $x$  is given by

$$p(x) = \sum_{m=1}^N p_m(r_{mn}), \quad (\text{S4})$$

$$v(x) = \sum_{m=1}^N v_m(r_{mn}). \quad (\text{S5})$$

If there is a secondary sound source such as a reflector, the amplitudes of the sound sources are determined to satisfy the boundary condition.  $N$  point sources whose amplitude is unknown are distributed over both the primary sound source (e.g., transducers) and the secondary sound source (e.g., reflector). Here, it is assumed that the sound sources are spheres of radius  $r_s$ , and the radiation points are located at positions retracted by  $r_s$  from the boundary. By giving the velocity  $V_0$  to the primary sound sources and velocity 0 to the secondary sources, the following equation is obtained:

$$\{v_m\} = {}^t\{V_0, \dots, V_0, 0, \dots, 0\}, \quad (\text{S6})$$

$$\{A_m\} = [M_{mn}]^{-1}\{v_m\}. \quad (\text{S7})$$

Because  $N$  equations are given for  $N$  unknown sound sources, the amplitudes of the unknown sound sources are determined.

### **Supplementary Video S1**

This video shows the contactless coalescence of acoustically levitated droplets by an ultrasonic phased array. The record speed was 8000 fps, and the play speed was 60 fps.

### **Supplementary Video S2**

This video shows the mixing behavior inside the droplet without mode. The record speed was 500 fps, and the play speed was 240 fps.

### **Supplementary Video S3**

This video shows the mixing behavior inside the droplet with 6<sup>th</sup> mode. The record speed was 500 fps, and the play speed was 240 fps.

## References

1. Ahmad, R., Kundu, T. and Placko, D., Modeling of phased array transducers, *J. Acoust. Soc. Am.*, **117**, 1762-1776 (2005).
2. Wada, Y., Yuge, K., Nakamura, R., Tanaka, H. & Nakamura, K., Dynamic analysis of ultrasonically levitated droplet with moving particle semi-implicit and distributed point source method, *Jpn. J. Appl. Phys.*, **54**, 07HE04 (2015).