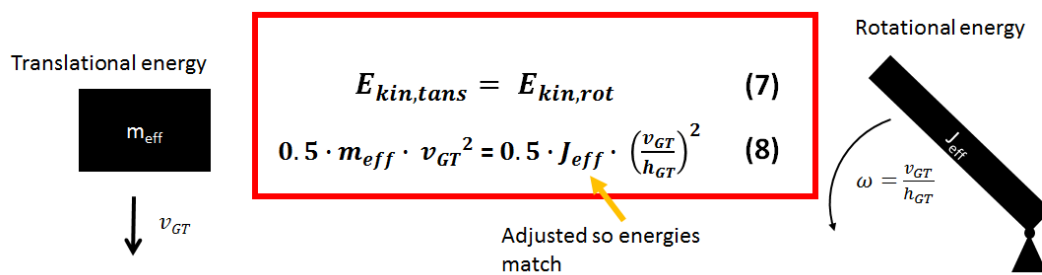


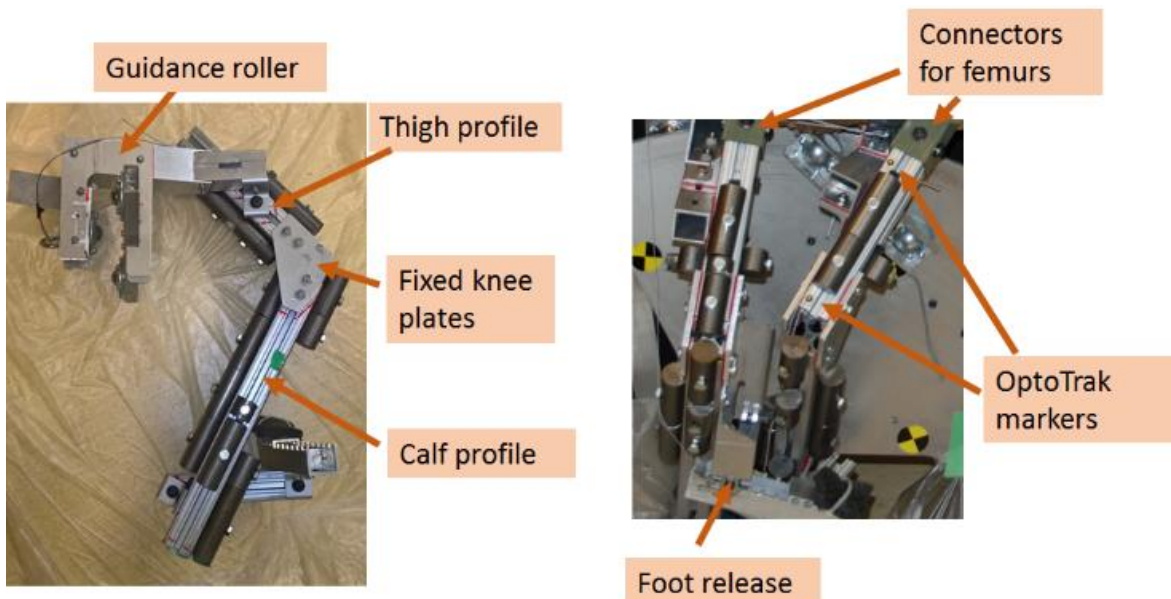
## 1 Energy calculation

2 We converted translational impact energy to rotational energy for the inverted pendulum (S1 Fig). The  
3 energy input and a greater trochanter impact velocity of 3.0 m/s were used as target to adjust the  
4 pendulum's inertia. The pendulum's mass ( 52 % body mass), including lower limb constructs, soft  
5 tissue, cadaveric parts and rollers, that was necessary to achieve the desired inertia was much higher  
6 than the effective mass (38 % body mass) of a translational sDOF model. The required mass  
7 corresponded to the mass of lower limbs and abdominal region based on literature. (1)



9 **S1 Fig translation from sDOF energy input (translational energy) to pendulum energy input (rotational energy).** The  
10 pendulum height was fixed for the experiment and the greater trochanter velocity was kept constant. As a result, the  
11 pendulum inertia was the parameter that was adjusted depending on the theoretical effective mass of the specimen.

## 12 Lower limb construction



14 **S2 Fig lower limb design.** (left) left lower limb construction with masses for a heavy specimen. (right) lower limb  
15 constructions in the setup with a specimen connected at the top end and OptoTrak markers fixed to the left leg.

16 Aluminium profiles for thigh and calf with stiff plates at the knee that fixed the angle. Cylindrical masses  
17 to adjust the weight according to subject mass

## 18 **Mass adjustment**

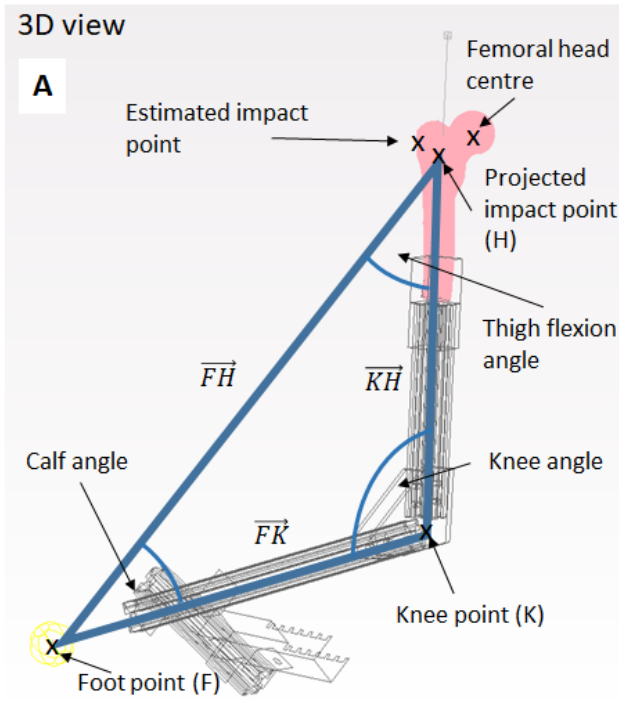
19 S1 Table target masses for body segments.

Body segment	Adjusted mass	Literature (1)
Foot and Calf	6 % body mass	6.4 % body mass
Lower thigh (leg construction)	4% body mass	10 % body mass
Upper thigh (bone and gel)	6% body mass	
Abdomen (up to naval)	20 % body mass	Based on target impact energy

20 Grey shaded rows highlight the leg construction. Orange shaded rows highlight the cadaveric specimen and soft tissue  
21 surrogate.

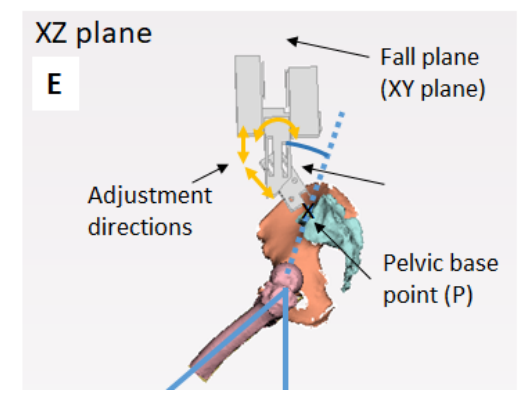
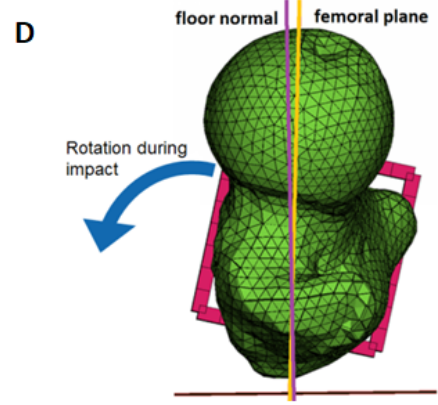
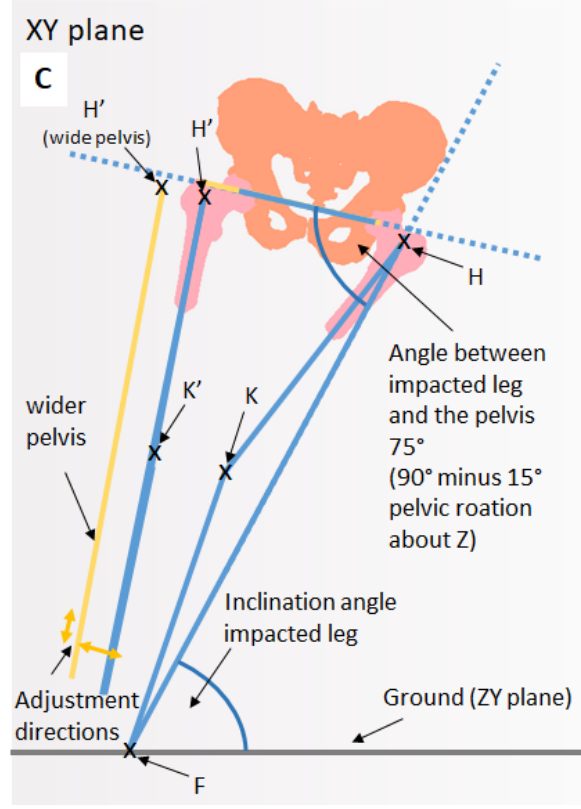
## 22 **Target alignment**

23 A triangle between the foot point (F), knee point (K) and a point created by projecting the estimated  
24 impact point onto the femoral shaft axis (H), was used to define a lower limb triangle for both legs (S3  
25 Fig, A). Segment length ratios (1) and the calf angle (2) were taken from literature and used to calculate  
26 hip flexion and knee flexion (Figure 3 B).



B	Impacted femur	[°]	Ref
	Hip flexion angle *	37.6	
	Calf angle	33.4	[2]
	Knee angle*	109	
	Internal rotation**	15	
	Femur anteversion angle	-13	[3]
	Contralateral femur	[°]	Ref
	Hip flexion angle *	37.6	
	Calf angle	33.4	[2]
	Knee angle*	109	
	Internal rotation**	0	
	Femur anteversion angle	-13	[3]
	Pelvis	[°]	Ref
	Pelvis rotation about Z**	15	
	Pelvic tilt	12	[4]

\* Calculated value, \*\* chosen value



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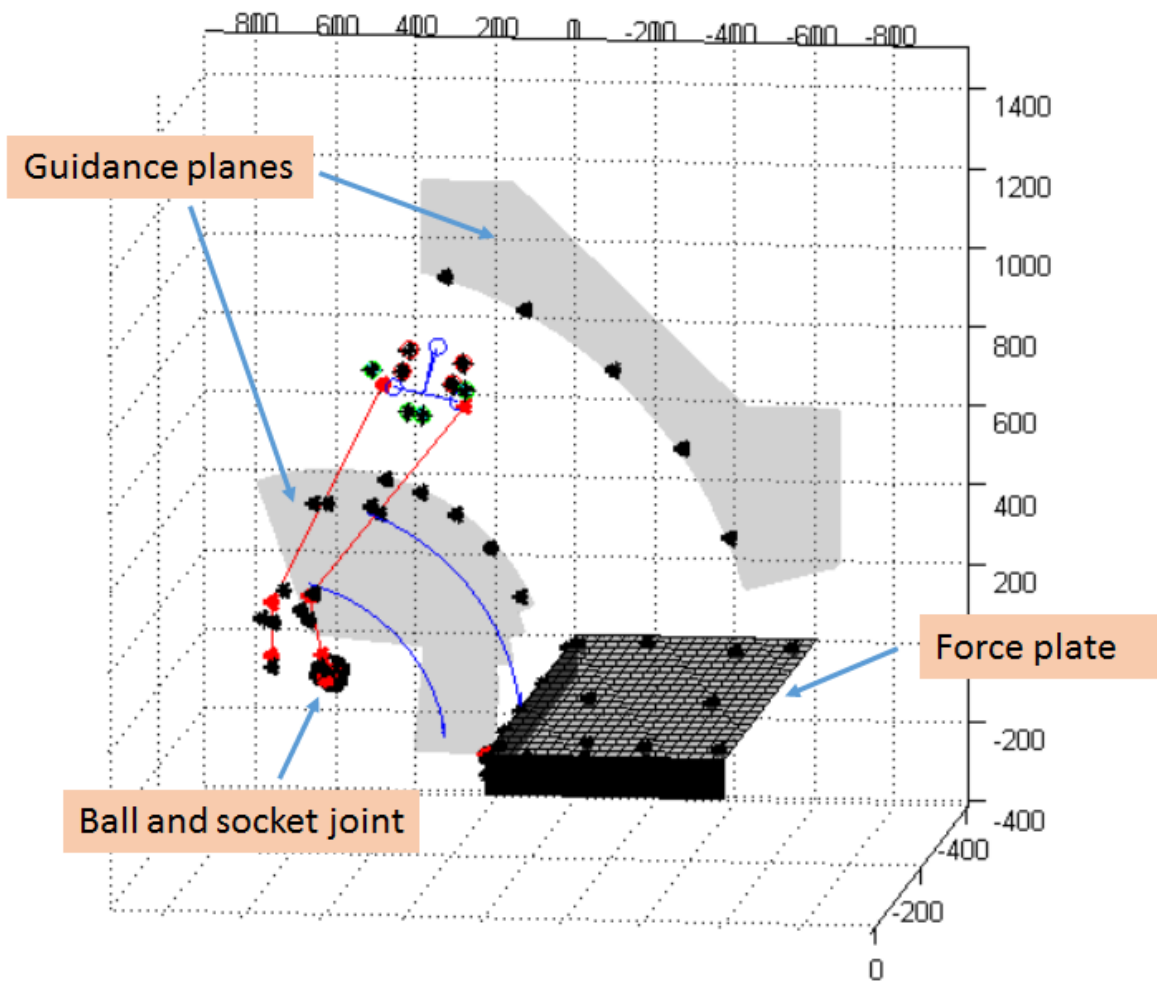
28 **S3 Fig Body posture and detailed alignment.** (A) Schematic triangle for lower limb angle calculation. (B) Target angles for  
 29 both limbs and the pelvis. (C) schematic of angles and adjustment options of the specimen in the setup (D) pelvic tilt and  
 30 pelvic roller adjustment options (E) femoral neck alignment right before impact

31 A femoral anteversion angle of 13 ° was chosen. (3) To lift the knee off the ground a combination of  
 32 internal rotation and adduction was applied. A 2 ° bigger internal rotation than femoral anteversion

33 angle was chosen to ensure that the femoral neck passed through a vertical alignment with the ground  
34 during the impact (S3 Fig, D). The contralateral limb was assumed to mirror the impacted limb's thigh  
35 flexion and knee angle, but not the internal rotation and adduction.

36 Both femoral head centres were aligned to be in the same XY plane (S3 Fig, E). The pelvic tilt was set  
37 to 12 °. (4) A fall alignment with the upper body flexed only in the same fall plane was assumed.  
38 Therefore, a pelvic rotation in the coronal plane of 15 ° was selected for this study. This angle was  
39 assumed to be one part of the upper body to ground angle (2) which is a combination of pelvic rotation  
40 with respect to the ground and lateral spine bending. The upper body superior to the base of sacrum  
41 was not modelled.

42 To confirm the experimental alignment and position of the specimen in the rig, a virtual experimental  
43 rig was created in MATLAB (Mathworks, Natick, MA, USA). Digitized points and markers in combination  
44 with CT based marker locations and bony landmarks were used to measure the position of the femurs  
45 and pelvis with respect to the setup and with respect to each other (S4 Fig).



46

47 **S4 Fig Virtual experimental setup.** Virtual reconstruction, used to calculate specimen alignment prior to releasing the  
 48 pendulum. *Black points:* digitized points; *red elements:* lower limb reconstruction; *blue lines above the legs:* pelvic  
 49 alignment reconstruction based on digitized markers; *blue circle segments:* tracked active markers over the fall phase.

50 Adjustable angles were iteratively changed until they were within 5 ° of the target value prior to  
 51 releasing the specimen (S2 Table). Subject specific differences in the distance between the femoral  
 52 heads and the height of the pelvis required some adjustment options to position specimens into similar  
 53 alignments. Angles that had not to be adjusted between specimens were thigh flexion, knee and calf  
 54 angle of each lower limb, thigh internal rotation angle for both lower limbs, and thigh adduction of the  
 55 impacted limb. Thigh adduction of the contralateral leg was adjusted based on the distance between  
 56 the femoral head centres of the specimen. The pelvic rotation about the Z-axis was also adjusted with  
 57 a slider at the pin release between impacted and contralateral leg. The pelvic roller was adjusted

58 depending on pelvic height and inclination angle of the base of the pelvis. Therefore, two translational  
 59 and one rotational degrees of freedom in the sagittal plane of the pelvis were adjustable. Degrees of  
 60 freedom for adjustment are shown in yellow in Figure 3 (C and E).

61 S2 Table Measured body posture and alignment.

	Target angles	H1391	H1406
<b>Impacted femur</b>			
Flexion angle [°]	37.6	37.3	37.1
Calf angle [°]	33.4	33.8	33.8
Knee angle [°]	109	108.9	109.1
Internal rotation [°]	15	14.8	14.65
Femur Anteversion angle [°]	13	10.8	12.3
<b>Contra femur</b>			
Flexion angle [°]	37.6	37.2	37.4
Calf angle [°]	33.4	32.5	32.2
Knee angle [°]	109	111.3	111.4
Internal rotation [°]	0	-1.1°	-1.2
Femur Anteversion angle [°]	13	7.0	7.9
<b>pelvis</b>			
Pelvic rotation about Z [°]	15	13.7	15.2
Pelvic tilt [°]	12	12.4	7.1

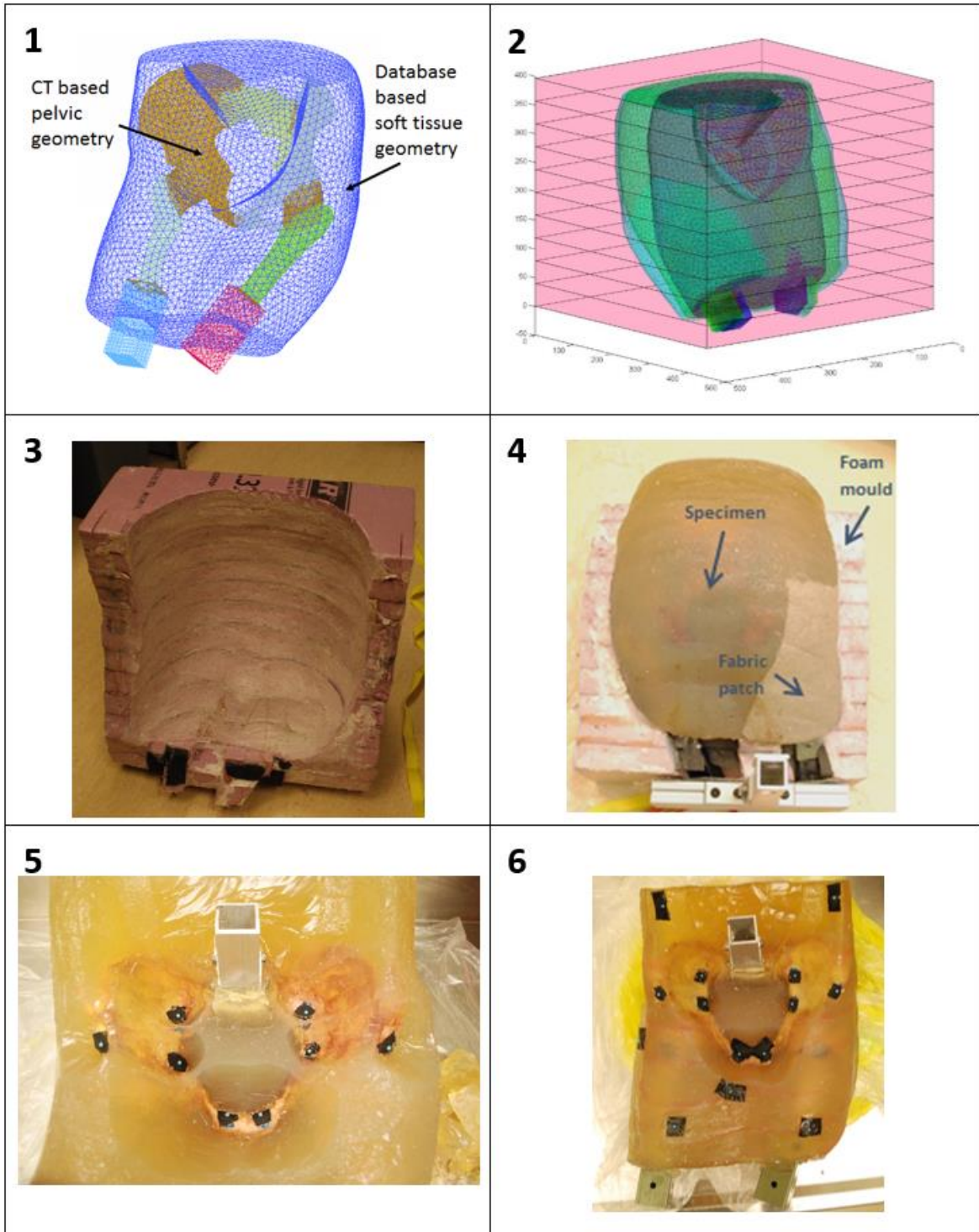
## 62 **Soft tissue surrogate**

63 During dissections the material over the greater trochanter was observed to be a combination of skin,  
 64 adipose tissue, fascia, and tendon attachments, which supported the choice of a surrogate material  
 65 with properties in between muscle and adipose tissue.

66 Custom mould shapes, based on a shapes database (SizeUSA, [TC]<sup>2</sup> Labs, Apex, NY, USA) were created  
 67 for each specimen to represent the desired soft tissue geometry, mass and inertia. The following steps  
 68 were performed to mould the soft tissue surrogate around the specimen:

- 69 1. CT segmentation of femur and pelvis geometries
- 70 2. Selection of a database shape based on the bone geometry, BMI, mass, height, and desired
- 71 soft tissue thickness for each subject.
- 72 3. Positioning of the segmented bones into fall alignment
- 73 4. Positioning the soft tissue shape around the specimen and morphing it into fall alignment (S5
- 74 Fig, image 1)
- 75 5. Fine tuning of the shape for target inertia and mouldability. E.g. The upper thighs were
- 76 connected.
- 77 6. Virtual mould shape creation (S5 Fig, image 2)
- 78 7. Physical mould shape creation in polystyrene foam (S5 Fig, image 3)
- 79 8. Ballistic gel mixing
- 80 9. Wrapping of ballistic gel soaked fabric patches around the distal femurs and the square tubes
- 81 10. Application of a ballistic gel soaked fabric patch on the right posterior side of the mould shape
- 82 11. Positioning of the specimen in the mould shape in fall alignment
- 83 12. Casting the gel around the specimen. The gel was at a temperature of 30 degrees Celsius when
- 84 cast around the specimen.
- 85 13. Storage of the mould and specimen in at 4 degrees for 38 hours
- 86 14. Demoulding and storage at room temperature for 30 hours (S5 Fig, image 4)
- 87 15. Preparation of fiducial markers on bone and soft tissue surrogate with dark backgrounds (S5
- 88 Fig, image 4 and 5)
- 89 16. Dynamic testing 68 hours after moulding the gel around the specimen





90

91 **S5 Fig Soft tissue surrogate moulding steps:** 1) database shape with CT-based bone geometry; 2) virtual model for mould  
 92 creation; 3) physical foam mould, posterior part; 4) specimen while demoulding, still in the anterior part of the mould. 5)  
 93 demoulded soft tissue with ballistic gel removed from marker sites for marker visibility; 6) demoulded specimen with  
 94 spherical markers attached. Black tape was added to improve contrast for fiducial markers.

95

96



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