

## Supplementary file

# Rapid synthesis of transition metal dichalcogenide–carbon aerogel composites for supercapacitor electrodes

Matthew J. Crane<sup>1,\*</sup>, Matthew B. Lim<sup>2,\*</sup>, Xuezhe Zhou<sup>2</sup> and Peter J. Pauzauskis<sup>2,3</sup>

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### 1. THEORETICAL SURFACE AREA CALCULATION

For each TMD, we calculated the theoretical surface area by extrapolating from the unit cell and neglecting edge effects. As an example calculation for WS<sub>2</sub>, the specific surface area is

$$\frac{a^2 N_a}{MW} \quad (1)$$

where  $a$  is the (100) lattice parameter ( $a=b=3.1532 \text{ \AA}$  and  $c=12.3230 \text{ \AA}$ ),  $MW$  is the molecular weight of the TMD unit cell, and  $N_a$  is Avogadro's number. For WS<sub>2</sub>, MoS<sub>2</sub>, and NbSe<sub>2</sub>, the theoretical specific surface areas are 482.77, 752.14, and 468.87 m<sup>2</sup>/g, respectively.

### 2. SCHERRER ANALYSIS OF TMD-LOADED AEROGELS

We quantified the size of the TMD crystals loaded into the aerogels using the Scherrer equation,

$$L_a = \frac{1.32\lambda_{Ka}}{\beta \cos\theta} \quad (2)$$

where the crystal thickness  $L_a$  in the (002) direction is a function of the x-ray wavelength  $\lambda_{Ka}$ , the position of the (002) diffraction peak  $\theta$ , and the full width at half maximum (FWHM) of the peak  $\beta$ , which we correct for instrument broadening with  $\beta = \sqrt{\beta_m^2 + \beta_{ref}^2}$ , where  $\beta_m$  and  $\beta_{ref}$  are the measured FWHM of the TMD (002) peak and the measured FWHM of a peak of a corundum standard that occurs at a similar Bragg angle to the TMD (002) peak<sup>1</sup>.

### 3. VOLUMETRIC CAPACITANCE CALCULATION FROM GALVANOSTATIC DISCHARGE

We calculated volumetric capacitance of a single electrode from galvanostatic discharge profiles using the equation adapted from gravimetric capacitance<sup>2</sup>:

$$C_{s,v,galv} = \frac{8\rho l \int_{t_1}^{t_2} V dt}{m_a (V_2 - V_1)^2} \quad (3)$$

where  $l$  is the constant discharge current,  $m_a$  is the total mass of active material in both electrodes,  $\rho$  is the bulk density of the active material, and  $(t_1, V_1)$ ,  $(t_2, V_2)$  are two chosen points on the voltage-time curve. Our reported values use the full potential window of our discharge tests (0.9–0.1 V).

We note that, while gravimetric capacitance is frequently used as a figure of merit for supercapacitors, volumetric capacitance represents a more pragmatic metric for high density energy

storage and a more reliable parameter in evaluating the charge-storage performance of low bulk density electrode materials, like aerogels<sup>3,4</sup>. Additionally, volumetric capacitance normalizes results for significant changes in density. Finally, many earlier studies on the supercapacitor applications of TMD-carbon composites employed thin film-like electrodes obtained through filtration<sup>5–8</sup>. Owing to the very small mass of active material, this can lead to artificially high values of gravimetric capacitance that do not translate to larger-scale devices.

### 4. VOLUMETRIC CAPACITANCE CALCULATION FROM EIS

Volumetric capacitance can also be calculated from electrochemical impedance spectroscopy (EIS) using the equation<sup>9</sup>:

$$C_{s,v,EIS} = \frac{\rho}{2\pi f Z'' m_a} \quad (4)$$

where  $f$  is the frequency and  $Z''$  is the imaginary component of impedance,  $m_a$  is the total mass of active material in both electrodes, and  $\rho$  is the bulk density of the active material.

Supplementary Figure S5 plots the EIS-derived volumetric capacitances of the aerogels as a function of frequency. Even at the lowest frequency of 10 mHz where volumetric capacitance is maximized, it is less than one-third of the maximum value obtained from galvanostatic testing. We note that the relatively low capacitance obtained from EIS versus other methods is well-documented for supercapacitors based on porous carbons<sup>9–12</sup>. For example, Lufrano *et al.* observed that the capacitance of carbon composite electrodes with H<sub>2</sub>SO<sub>4</sub> electrolyte was 20% lower when measured with EIS than with galvanostatic charge-discharge tests<sup>9</sup>. Various explanations have been proposed for the discrepancy—such as the increased hindrance for alternating current penetration into the bulk electrode<sup>10,11</sup>; or the presence of deeply trapped ions that are immobile under AC conditions but can be released at low potentials in DC methods<sup>13</sup>. However, nothing conclusive has emerged to date.

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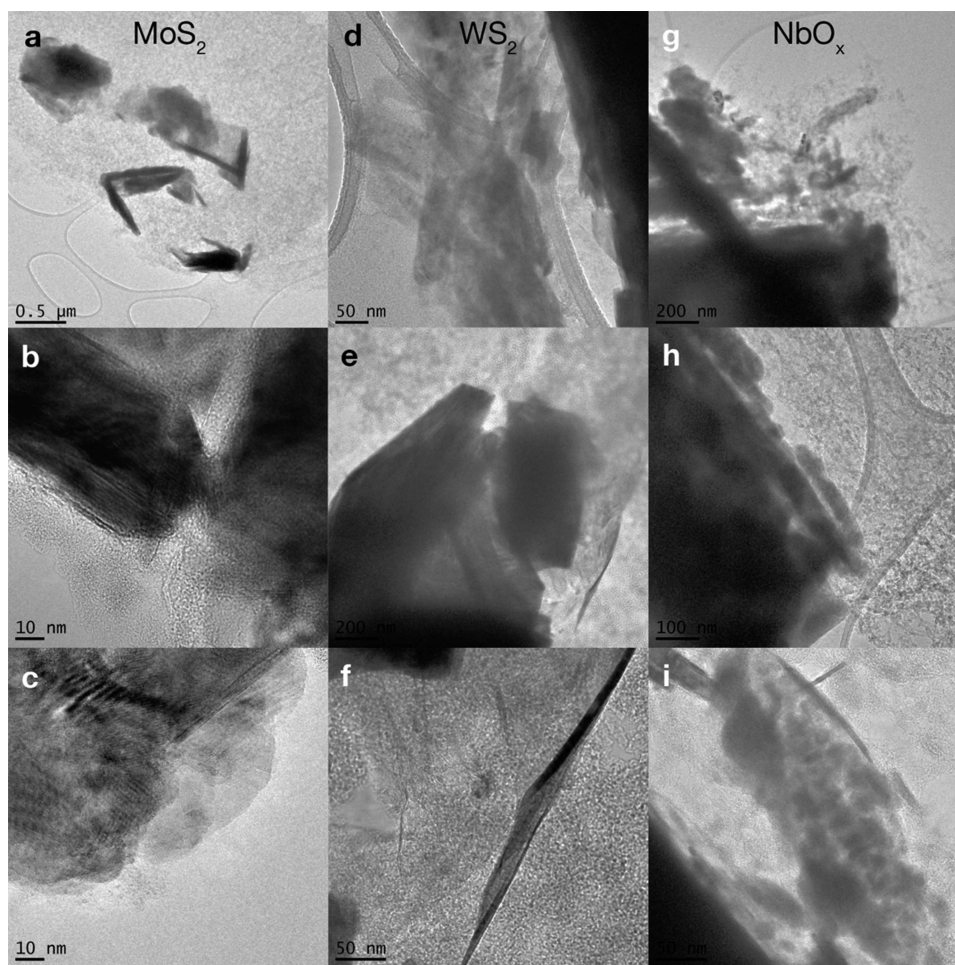
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<sup>1</sup>Department of Chemical Engineering, University of Washington, Seattle, WA 98195-1750, USA; <sup>2</sup>Department of Materials Science & Engineering, University of Washington, Seattle, WA 98195-2120, USA and <sup>3</sup>Fundamental & Computational Sciences Directorate, Pacific Northwest National Laboratory, Richland, WA 99352, USA.

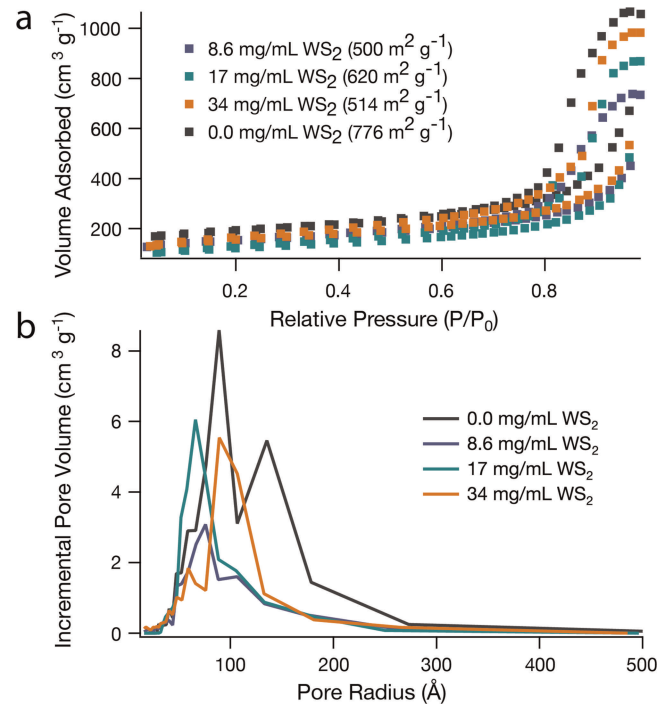
Correspondence: Peter J. Pauzauskis, (peterpz@uw.edu)

\*These authors contributed equally to this work.

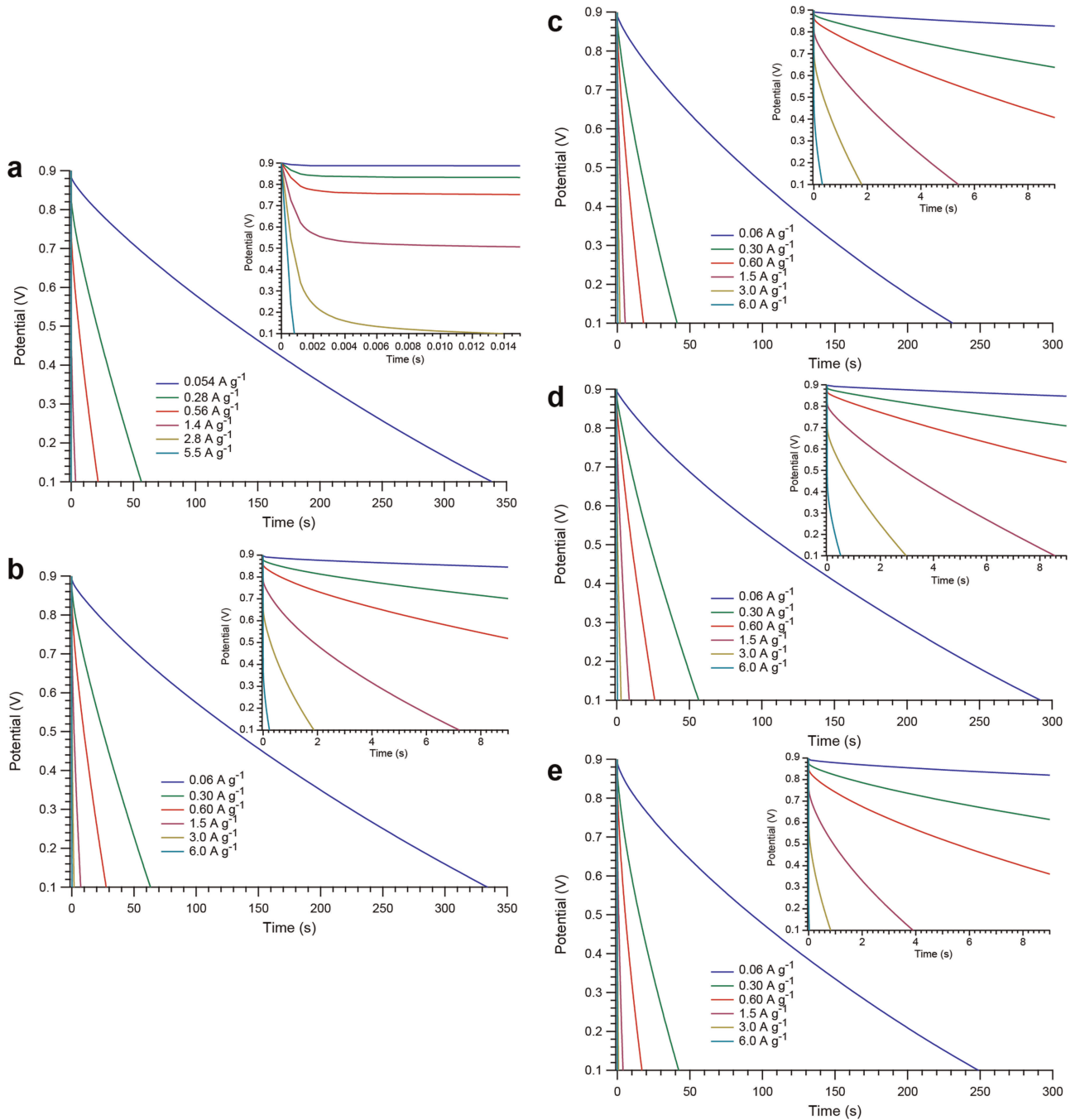
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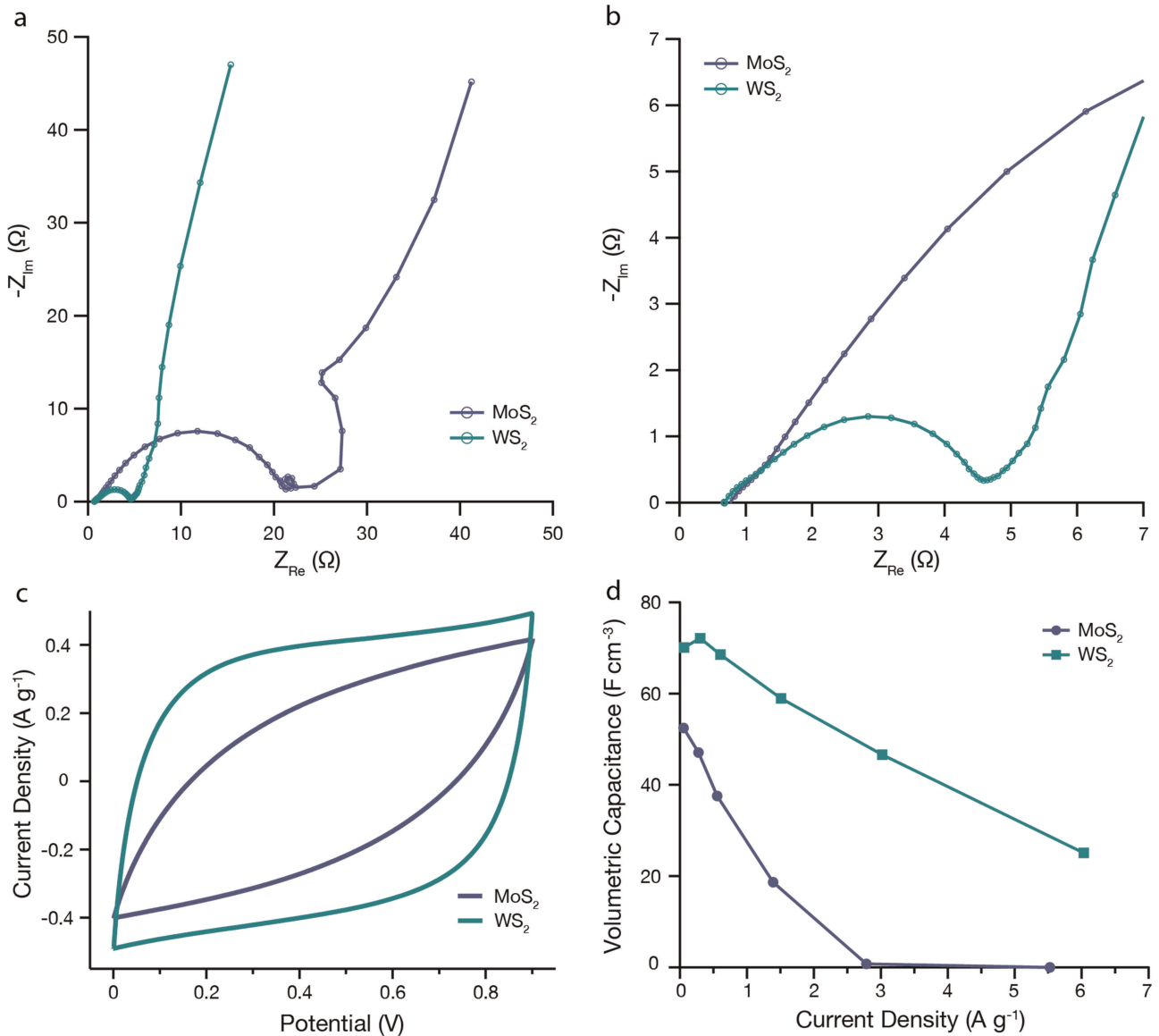
**Figure S1** Additional TEM images of pyrolyzed MoS<sub>2</sub> (a–c), WS<sub>2</sub> (d–f), and NbO<sub>x</sub> (g–i) loaded aerogels showing exfoliation and morphology of TMD sheets within the RF support matrix. Samples pictured were synthesized from 17 mg ml<sup>-1</sup> TMD dispersions.



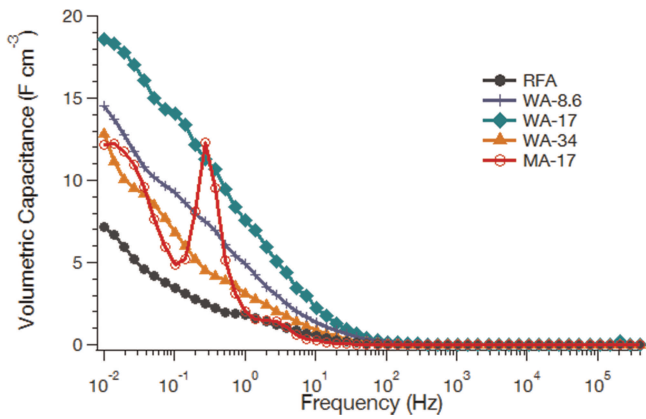
**Figure S2** Nitrogen sorption isotherms with BET surface area (a) and BJH pore size distribution (b) of pyrolyzed aerogel with different mass loadings of WS<sub>2</sub>.



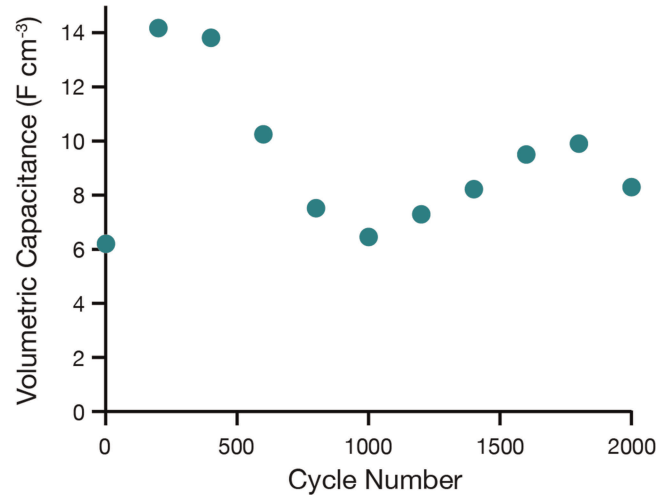
**Figure S3** Galvanostatic discharge curves, used to calculate specific capacitance values, for supercapacitors containing MA-17 (a), RFA (b), WA-8.6 (c), WA-17 (d), and WA-34 (e) aerogel electrodes. Insets show same curves at shorter timescales.



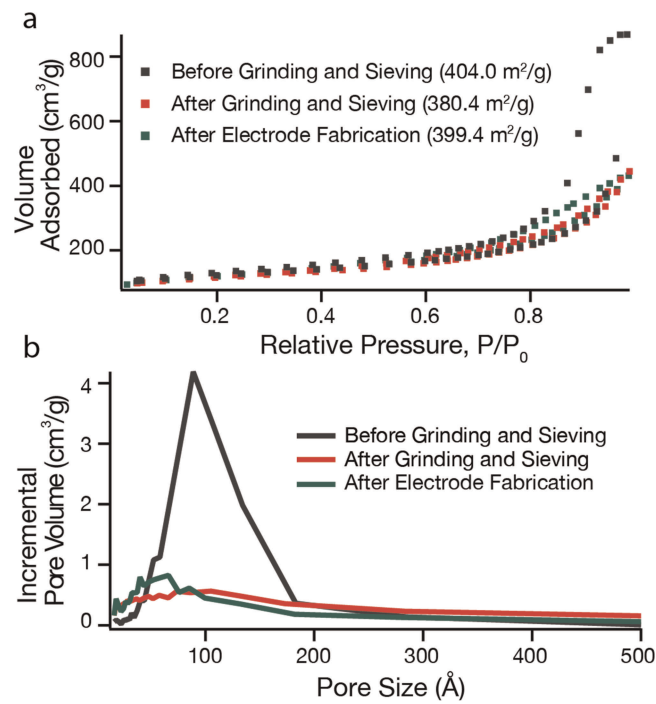
**Figure S4** Electrochemical characterization of MA-17 and WA-17 supercapacitors. This includes Nyquist plots from EIS (**a**: full range, **b**: detail of high to mid frequency), cyclic voltammetry at a sweep rate of  $20\text{ mV s}^{-1}$  (**c**), and the specific volumetric capacitance (**d**) as a function of applied current density from galvanostatic tests. *Note on Figure S4.* The Nyquist plot of MA-17 exhibits unusual characteristics at lower frequencies that are difficult to interpret. Between the semicircular RIC region and the steeply sloped constant phase region, there is a small loop followed by a larger arc that curves back on the real impedance axis, instead of the expected  $45^\circ$  Warburg line. These features indicate low-frequency inductive behavior in the system, which is not typically observed in supercapacitors. We note, however, that these features also appeared for duplicate coin cells made with the same active material. One possible explanation is offered by Bisquert *et al.*, who extensively studied inductive phenomena in the context of a porous, heterogeneous electroactive material composed of two different solids in contact with electrolyte<sup>14</sup>—a good model for our TMD/carbon aerogel composite electrodes. They found that inductive behavior resulted from the coupled dielectric relaxation in the two solid phases, with the relaxation being driven by changes in the electrochemical potential of the phases due to charge transfer between them.



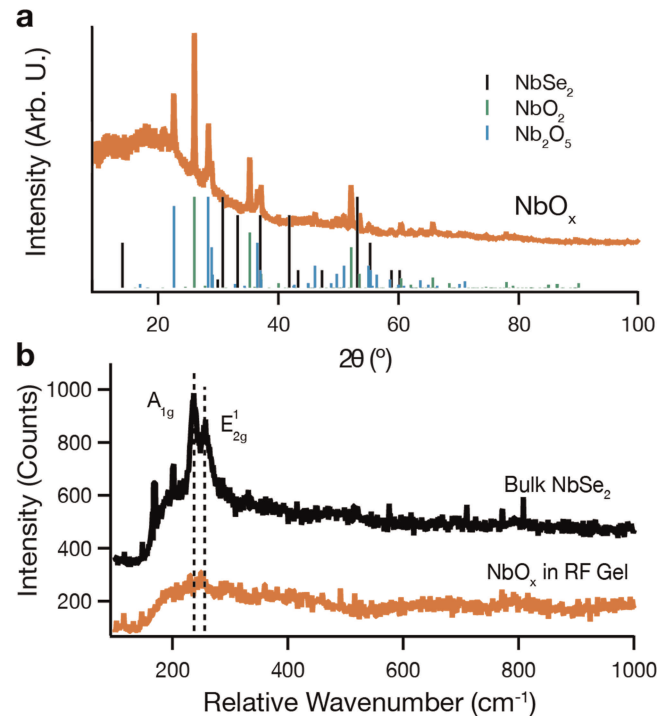
**Figure 55** Specific volumetric capacitance, derived from electrochemical impedance spectroscopy, as a function of frequency for the different aerogel supercapacitors.



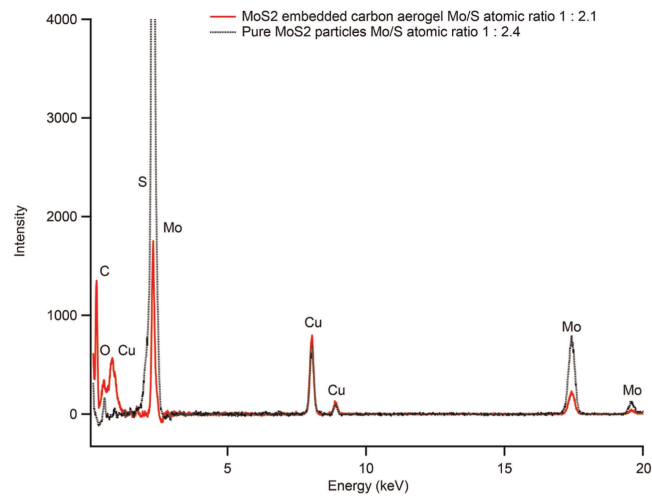
**Figure 56** Specific volumetric capacitance of WA-17 during galvanostatic cycling at 0.25 A g<sup>-1</sup>, derived from discharge curves at selected cycles.



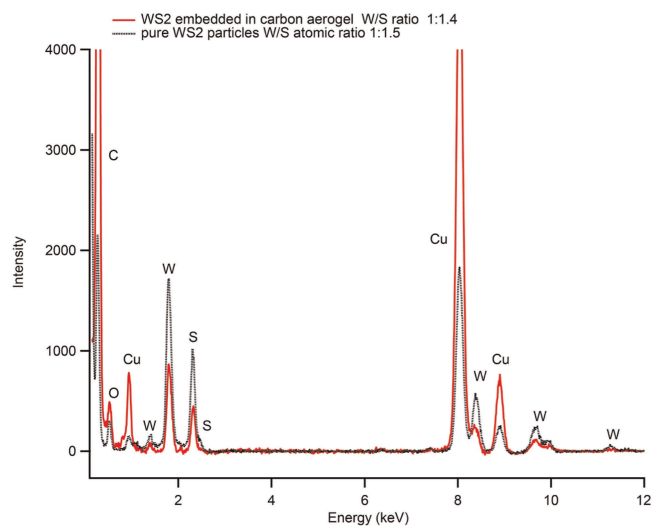
**Figure 57** Nitrogen sorption isotherms with BET surface area (a) and BJH pore size distribution (b) of pyrolyzed WS<sub>2</sub>-loaded aerogel before processing, after grinding and sieving, and after forming into a supercapacitor electrode with PTFE binder and carbon black.



**Figure S8** Raman (a) and XRD (b) characterization of the  $\text{NbSe}_2$ -loaded aerogel after pyrolysis at  $800^\circ\text{C}$ .



**Figure S9** Energy dispersive x-ray spectroscopy of  $\text{MoS}_2$  powder and  $\text{MoS}_2$ -loaded aerogel after pyrolysis.



**Figure S10** Energy dispersive x-ray spectroscopy of  $WS_2$  powder and  $WS_2$ -loaded aerogel after pyrolysis.