Supplementary Information

Analogue of dynamic Hall effect in cavity magnon polariton system and coherently controlled logic device

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Supplementary References

Supplementary Note 1. Theoretical description of magnon-photon coupling in x-cavity

Hamiltonian of X-CMP dynamics

The whole system can be viewed as a coupled cavity magnon system in a photon bath. The Hamiltonian of the whole system has the following form:

$$H = H_{sys} + H_{bath} + H_{int} \tag{1}$$

Here, H_{sys} is the Hamiltonian of the coupled cavity magnon system isolated with surroundings, and H_{bath} is the Hamiltonian of the photon bath. As for the H_{int} , it represents the interaction effect between the coupled cavity magnon system and the photon bath. The detailed expressions of these three parts are shown as following:

$$H_{sys} = \hbar\omega_c a_x^{\dagger} a_x + \hbar\omega_m m^{\dagger} m + \hbar\omega_c a_y^{\dagger} a_y + \hbar\Omega_0 (m^{\dagger} a_x + m a_x^{\dagger}) + \hbar\Omega_0 (m^{\dagger} a_y + m a_y^{\dagger})$$
(2)

$$H_{bath} = \int \hbar \omega_k \sum_{r=A}^{D} (p_{k,r}^{\dagger} p_{k,r} + \frac{1}{2}) dk \tag{3}$$

$$H_{int} = \int i\hbar\lambda [(p_{k,A}a_x^{\dagger} - p_{k,A}^{\dagger}a_x) + (p_{k,C}a_x^{\dagger} - p_{k,C}^{\dagger}a_x) + (p_{k,B}a_y^{\dagger} - p_{k,B}^{\dagger}a_y) + (p_{k,D}a_y^{\dagger} - p_{k,D}^{\dagger}a_y)]dk$$
(4)

 $a_x(a_x^{\dagger}), a_y(a_y^{\dagger})$ represent the annihilation (creation) operators of X-cavity modes in x- and y- directions. $m(m^{\dagger})$ is the annihilation (creation) operator of the magnon. $p_{k,r}(p_{k,r}^{\dagger})$ is the annihilation (creation) operator of the photon with wave vector k, while the subscript index r=A,B,C,D corresponds to the port A,B,C,D respectively.

The equation motion for the extra-cavity photon

The equation of motion for the extra-cavity photon operator in Heisenberg representation reads

$$\frac{dp_{k,A}}{dt} = -\frac{i}{\hbar}[p_{k,A}, H] = -i\omega_k p_{k,A} - \lambda a_x \tag{5}$$

The solution of this dynamic equation can be formally written as

$$p_{k,A}(t) = e^{-i\omega_k(t-t_0)} p_{k,A}(t_0) - \lambda \int_{t_0}^t e^{-i\omega_k(t-t')} a_x(t') dt'$$
(6)

Analogously, we can also get the expressions of the photon operators for the other three ports:

$$p_{k,C}(t) = e^{-i\omega_k(t-t_0)} p_{k,C}(t_0) - \lambda \int_{t_0}^t e^{-i\omega_k(t-t')} a_x(t') dt'$$
(7)

$$p_{k,B}(t) = e^{-i\omega_k(t-t_0)} p_{k,B}(t_0) - \lambda \int_{t_0}^t e^{-i\omega_k(t-t')} a_y(t') dt'$$
(8)

$$p_{k,D}(t) = e^{-i\omega_k(t-t_0)} p_{k,D}(t_0) - \lambda \int_{t_0}^t e^{-i\omega_k(t-t')} a_y(t') dt'$$
(9)

The equation motion for the intra-cavity photon

Similar to Supplementary equation (5), we can write the equations of motion for the two orthogonal X-cavity modes in the Heisenberg representation.

$$\frac{da_x}{dt} = -\frac{i}{\hbar}[a_x, H_{sys}] + \int_0^\infty \lambda p_{k,A} dk + \int_0^\infty \lambda p_{k,C} dk \tag{10}$$

$$\frac{da_y}{dt} = -\frac{i}{\hbar}[a_y, H_{sys}] + \int_0^\infty \lambda p_{k,B} dk + \int_0^\infty \lambda p_{k,D} dk \tag{11}$$

By substituting H_{sys} and Supplementary equation (6)-(9) into Supplementary equation (10) and (11), we obtain a new form of equations of motion for x- and y- directions, respectively.

$$-i\omega a_x = -i\omega_c a_x - i\Omega_0 m + \sqrt{2\kappa_p} (p_A^{in} + p_C^{in}) - 2\kappa_p a_x \tag{12}$$

$$-i\omega a_y = -i\omega_c a_y - i\Omega_0 m + \sqrt{2\kappa_p} (p_B^{in} + p_D^{in}) - 2\kappa_p a_y \tag{13}$$

where κ_p is the coupling strength between feedlines and X-cavity, which follows the relation $\sqrt{\kappa_p} = \sqrt{\pi}\lambda$.

Supplementary Note 2. Input-output relations

The extra-cavity asymptotic output operators at $t = +\infty$ can be related to the input operators at $t_0 = -\infty$ and the cavity photon ones through a linear relationship^{1,2}. The standard definitions of the input and output photons are $p_{k,r}^{in} = p_{k,r}(t_0)e^{i\omega_k(t_0)}$ and $p_{k,r}^{out} = p_{k,r}(t)e^{i\omega_k(t)}$. By substituting them into Supplementary equation (6)-(9), we can get the response formula of the photon with wave vector k at each port, shown below

$$p_{k,r}^{out} = p_{k,r}^{in} - \sqrt{2\pi}\lambda a(\omega_k) \tag{14}$$

Here, the $a(\omega_k)$ is the Fourier Transformation of $a_x(t')$ or $a_y(t')$ depending on the port number, r.

$$a(\omega_k) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} e^{i\omega_k t'} a(t') dt'$$
(15)

The input and output signals are the sum of photons with different wave vectors i.e. the wave packets. Therefore, we define the input and output wave packets as

$$p_r^{in} = \frac{1}{\sqrt{2\pi}} \int_0^\infty e^{-i\omega_k t} p_{k,r}^{in} dk \tag{16}$$

$$p_r^{out} = \frac{1}{\sqrt{2\pi}} \int_0^\infty e^{-i\omega_k t} p_{k,r}^{out} dk \tag{17}$$

Substituting these two definitions into the Supplementary equation (14) and transferring $a_r(\omega_k)$ from the frequency domain back to the time domain a(t), we can obtain the input-output relation as

$$p_r^{out} = p_r^{in} - \sqrt{2\pi}\lambda a(t) \tag{18}$$

Supplementary Note 3. Transmission of X-CMP dynamics

Start from the dynamic equation of magnon in Heisenberg representation

$$\frac{dm}{dt} = -\frac{i}{\hbar} [m, H_{sys}] = -i\omega_m m - i\Omega_0 (a_x + a_y)$$
(19)

If we assume the solution of this equation follows the general form as $m = |m|e^{-i\omega t}$, then Supplementary equation (19) should be:

$$(\omega - \omega_m)m = \Omega_0(a_x + a_y) \tag{20}$$

Now, we put the intrinsic damping of the magnon into this equation i.e. $\omega_m \to \omega_m - i\alpha\omega_m$, then Supplementary equation (20) becomes

$$(\omega - \omega_m + i\alpha\omega_m)m = \Omega_0(a_x + a_y) \tag{21}$$

In experiment, for general assumption, the port A and port C are the input ports, and the port B and port D are output ports. Under this condition, we can set p_C^{in} and p_D^{in} as zero and obtain the equations of motion of the coupled cavity magnon system in the cross cavity as following:

$$[\omega - \omega_c + i(\beta_{in}\omega_c + 2\kappa_p)]a_x - \Omega_0 m = i\sqrt{2\kappa_p}p_A^{in}$$
$$[\omega - \omega_c + i(\beta_{in}\omega_c + 2\kappa_p)]a_y - \Omega_0 m = i\sqrt{2\kappa_p}p_B^{in}$$
$$(\omega - \omega_m + i\alpha\omega_m)m - \Omega_0(a_x + a_y) = 0$$
(22)

Here, $\beta_{in}\omega_c$ is the intrinsic damping of the cavity. We can also use a lumped damping factor β to represent the loaded damping of the cavities, i.e. $\beta\omega_c = \beta_{in}\omega_c + 2\kappa_p$.

Dynamics hall effect in X-CMP

Firstly, if we only input microwave power at port A. As a result, input condition can be simplified as $p_A^{in} = \tilde{V}_x^{in}$ and $p_B^{in} = 0$, using Supplementary equation (22), we get the expressions of a_x and a_y in the frequency domain as:

$$a_x = -\frac{\sqrt{2\kappa_p V_x^{in}}}{i(\omega - \omega_c) - \beta\omega_c + \frac{\Omega_0^2}{i(\omega - \omega_m) - \alpha\omega_m + \frac{\Omega_0^2}{i(\omega - \omega_c) - \beta\omega_c}}}$$
$$a_y = a_x + \frac{\sqrt{2\kappa_p} \widetilde{V}_x^{in}}{i(\omega - \omega_c) - \beta\omega_c}$$
(23)

Substituting these two expressions into Supplementary equation (18), we get the output signals from the port C and port D, respectively, i.e. $p_C^{out} = \tilde{V}_x^{out} = -\sqrt{2\kappa_p}a_x$ and $p_D^{out} = \tilde{V}_y^{out} = -\sqrt{2\kappa_p}a_y$:

$$\widetilde{V}_{x}^{out} = \frac{2\kappa_{p}\widetilde{V}_{x}^{in}}{i(\omega - \omega_{c}) - \beta\omega_{c} + \frac{\Omega_{0}^{2}}{i(\omega - \omega_{m}) - \alpha\omega_{m} + \frac{\Omega_{0}^{2}}{i(\omega - \omega_{c}) - \beta\omega_{c}}}}{\widetilde{V}_{y}^{out} = \frac{2\kappa_{p}\widetilde{V}_{x}^{in}}{i(\omega - \omega_{c}) - \beta\omega_{c} + \frac{\Omega_{0}^{2}}{i(\omega - \omega_{m}) - \alpha\omega_{m} + \frac{\Omega_{0}^{2}}{i(\omega - \omega_{c}) - \beta\omega_{c}}}}{-\frac{2\kappa_{p}\widetilde{V}_{x}^{in}}{i(\omega - \omega_{c}) - \beta\omega_{c}}}$$
(24)

Because of the geometric symmetry of our device, it's straightforward to draw a conclusion that if signal was input from port B i.e. $p_A^{in} = 0$ and $p_B^{in} = \tilde{V}_y^{in}$, we can also observe the normal transmission signal and the dynamic Hall signal from the port C and port D, respectively. By means of this symmetric property, we have transformed supplementary equation (24) into a matrix equation which is shown as:

$$\frac{1}{2\kappa_p} \begin{bmatrix} i(\omega - \omega_c) - \beta\omega_c + \frac{\Omega_0^2}{i(\omega - \omega_m) - \alpha\omega_m} & \frac{\Omega_0^2}{i(\omega - \omega_m) - \alpha\omega_m} \\ \frac{\Omega_0^2}{i(\omega - \omega_m) - \alpha\omega_m} & i(\omega - \omega_c) - \beta\omega_c + \frac{\Omega_0^2}{i(\omega - \omega_m) - \alpha\omega_m} \end{bmatrix} \begin{bmatrix} \widetilde{V}_x^{out} \\ \widetilde{V}_y^{out} \end{bmatrix} = \begin{bmatrix} \widetilde{V}_x^{in} \\ \widetilde{V}_y^{in} \end{bmatrix}$$
(25)

To better describe the dynamic Hall effect, this matrix equation has been transformed into a much more straightforward form:

$$\begin{pmatrix} \tilde{V}_x^{out} \\ \tilde{V}_y^{out} \end{pmatrix} = 2\kappa_p \frac{\hat{T}}{det(\hat{T})} \begin{pmatrix} \tilde{V}_x^{in} \\ \tilde{V}_y^{in} \end{pmatrix}$$
(26)

Here, \hat{T} is the dynamic Hall tensor in X-CMP system, which plays an important role in controlling the direction of polariton flow. The detail of \hat{T} is shown below as

$$\hat{T} = \begin{bmatrix} i(\omega - \omega_c) - \beta\omega_c + \frac{\Omega_0^2}{i(\omega - \omega_m) - \alpha\omega_m} & -\frac{\Omega_0^2}{i(\omega - \omega_m) - \alpha\omega_m} \\ -\frac{\Omega_0^2}{i(\omega - \omega_m) - \alpha\omega_m} & i(\omega - \omega_c) - \beta\omega_c + \frac{\Omega_0^2}{i(\omega - \omega_m) - \alpha\omega_m} \end{bmatrix}$$
(27)

with the denominator $det(\hat{T})$ as,

$$\det(\hat{T}) = [i(\omega - \omega_c) - \beta\omega_c]^2$$

$$+ \frac{2\Omega_0^2[i(\omega - \omega_c) - \beta\omega_c]}{i(\omega - \omega_m) - \alpha\omega_m}$$
(28)

Because of the non-zero off-diagonal terms of the transfer matrix, the Hall signal is generated in the experiment. And since these off-diagonal terms exhibit a resonance response of the external magnetic field, the dynamic Hall signal can be modulated by the external field. We have shown a detailed description of the dynamic Hall signal in the manuscript.

Two-port input experiment

The second step of our experiment is the Two-port input experiment. The input signal is \tilde{V}^{in} , and we split it into two branches with same amplitude. A mechanical phase shifter was added into one branch to induce a phase difference between the two coherent signals (Φ). Then, these two signals were injected into the cross cavity from port A and port B, simultaneously. In theory, they can be described as:

$$p_A^{in} = \widetilde{V}_x^{in} = \widetilde{V}^{in} / \sqrt{2}$$

$$p_B^{in} = \widetilde{V}_y^{in} = i e^{i\Phi} \widetilde{V}^{in} / \sqrt{2}$$
(29)

By substituting these two input signals into Supplementary equation (26), it's straightforward to obtain the output signal from port C:

$$\widetilde{V}_C = \sqrt{2}\kappa_p (T_{xx} + ie^{i\Phi}T_{xy})\widetilde{V}^{in}/det(\hat{T})$$
(30)

And the spectra of the output signal in frequency domain is:

$$\widetilde{V}_C = \frac{\sqrt{2\kappa_p V^{in}}}{i(\omega - \omega_c) - \beta\omega_c + \frac{(1 + ie^{i\Phi})\Omega_0^2}{i(\omega - \omega_m) - \alpha\omega_m + \frac{(1 - ie^{i\Phi})\Omega_0^2}{i(\omega - \omega_c) - \beta\omega_c}}}$$
(31)

Supplementary References

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