

Modified simon's minimax and optimal two-stage designs for single-arm phase II cancer clinical trials

SUPPLEMENTARY MATERIALS

(a) $\alpha=0.1$ and $\beta=0.1$

| P_0 | P_1 | sample size in total (n) | | | | | | | | | | | | |
|-------|-------|--------------------------|------|-----|------|------|------|------|------|----|----|------|-----|-----|
| | | SM+0 | +1 | +2 | +3 | +4 | +5 | +6 | +7 | +8 | +9 | +10 | +11 | +12 |
| 0.05 | 0.25 | M=SM | A | A | | O=SO | | | | | | | | |
| 0.1 | 0.3 | M=SM | A | | | | | | | | | O=SO | | |
| 0.15 | 0.35 | M=SM | O=SO | | | | | | | | | | | |
| 0.2 | 0.4 | M=SM | O=SO | | | | | | | | | | | |
| 0.25 | 0.45 | M=SM | O=A | | | | SO | | | | | | | |
| 0.3 | 0.5 | M=SM | | | A | | | | O=SO | | | | | |
| 0.35 | 0.55 | SM | | M=A | | | O=SO | | | | | | | |
| 0.4 | 0.6 | M=SM | | | | | O=SO | | | | | | | |
| 0.45 | 0.65 | M=SM | | | | O=SO | | | | | | | | |
| 0.5 | 0.7 | M=SM | | A | | | | O=SO | | | | | | |
| 0.55 | 0.75 | SM | M=A | | O=SO | | | | | | | | | |
| 0.6 | 0.8 | SM | M=A | | SO | | | O | | | | | | |
| 0.65 | 0.85 | M=SM | | | O=SO | | | | | | | | | |
| 0.7 | 0.9 | M=SM | | | O=SO | | | | | | | | | |
| 0.75 | 0.95 | M=SM=SO=O | | | | | | | | | | | | |

(b) $\alpha=0.05$ and $\beta=0.2$

| P_0 | P_1 | sample size in total (n) | | | | | | | | | | | | |
|-------|-------|--------------------------|--------|-------|--------|--------|--------|--------|--------|--------|----|---------|-----|-----|
| | | SM+0 | +1 | +2 | +3 | +4 | +5 | +6 | +7 | +8 | +9 | +10 | +11 | +12 |
| 0.05 | 0.25 | SM | M=O=SO | | | | | | | | | | | |
| 0.1 | 0.3 | M=SM | O=A | A | | SO(+3) | | | | | | | | |
| 0.15 | 0.35 | M=O=SM | | | | | A | SO(+6) | | | | | | |
| 0.2 | 0.4 | M=O=SM | | | | | A | | | | | SO(+10) | | |
| 0.25 | 0.45 | M=SM | A | | O | | SO(+2) | | | | | | | |
| 0.3 | 0.5 | M=SM | | | O=A | | | | SO(+4) | | | | | |
| 0.35 | 0.55 | M=O=SM | | | | | SO(+5) | | | | | | | |
| 0.4 | 0.6 | SM | | M=O=A | | | | | SO(+5) | | | | | |
| 0.45 | 0.65 | SM | | M=O=A | | SO(+2) | | | | | | | | |
| 0.5 | 0.7 | M=SM | | O=A | | | | SO(+4) | | | | | | |
| 0.55 | 0.75 | SM | M | | O=A | | | | SO(+4) | | | | | |
| 0.6 | 0.8 | M=O=SM | | | | | | | | SO(+8) | | | | |
| 0.65 | 0.85 | SM | M=O=A | | SO(+2) | | | | | | | | | |
| 0.7 | 0.9 | SM | SO | M=O | | | | | | | | | | |
| 0.75 | 0.95 | SM | | SO | M=O | | | | | | | | | |

(c) $\alpha=0.05$ and $\beta=0.1$

| P_0 | P_1 | sample size in total (n) | | | | | | | | | | | | |
|-------|-------|--------------------------|-----|--------|-----|------|------|------|------|------|------|------|-----|------|
| | | SM+0 | +1 | +2 | +3 | +4 | +5 | +6 | +7 | +8 | +9 | +10 | +11 | +12 |
| 0.05 | 0.25 | M=SM | A | | O=A | | SO | | | | | | | |
| 0.1 | 0.3 | M=SM | A | O=SO | | | | | | | | | | |
| 0.15 | 0.35 | M=SM | | | | | | O=SO | | | | | | |
| 0.2 | 0.4 | M=SM | | | | A | | | | | O=SO | | | |
| 0.25 | 0.45 | M=SM | A | | | | | | | O=SO | | | | |
| 0.3 | 0.5 | M=SM | | | A | | | | | | | O=SO | | |
| 0.35 | 0.55 | M=SM | | | A | | | O=SO | | | | | | |
| 0.4 | 0.6 | M=SM | | | | | | | A | | | | | O=SO |
| 0.45 | 0.65 | M=SM | | A | | | | | O=SO | | | | | |
| 0.5 | 0.7 | M=SM | | | | A | | | | O=SO | | | | |
| 0.55 | 0.75 | SM | M | | A | | O=SO | | | | | | | |
| 0.6 | 0.8 | M=SM | | A | | | | | | O=SO | | | | |
| 0.65 | 0.85 | SM | M=A | | | O=SO | | | | | | | | |
| 0.7 | 0.9 | M=SM | | | | O=SO | | | | | | | | |
| 0.75 | 0.95 | SM | | M=O=SO | | | | | | | | | | |

1. Abbreviation: M, the modified minimax design, O, the modified optimal design, SM, Simon's minimax design, SO, Simon's optimal design, A, the admissible design.
 2. "=" indicates that they are identical but "≠" shows that they are not identical.
 3. SO(+XX) shows that Simon's optimal design has "XX" additional samples, compared to the modified optimal design.

Supplementary Figure 1: Comparisons of the modified designs with $\gamma_1 = 1/3$, $\gamma_2 = 2/3$, and $\epsilon = 0.1$ to Simon's and the admissible designs for $p_1 - p_0 = 0.2$.

(a) $\alpha=0.1$ and $\beta=0.1$

| P_0 | P_1 | sample size in total (n) | | | | | | | | | | | | | | | | | | | | | | |
|-------|-------|------------------------------|-----|------|------|------|------|----|------|------|------|-----|------|------|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|
| | | SM+0 | +1 | +2 | +3 | +4 | +5 | +6 | +7 | +8 | +9 | +10 | +11 | +12 | +13 | +14 | +15 | +16 | +17 | +18 | +19 | +20 | +21 | +22 |
| 0.05 | 0.2 | M=SM | A | | A | | SO | O | | | | | | | | | | | | | | | | |
| 0.1 | 0.25 | M≠SM | | | | | | | | | O=SO | | | | | | | | | | | | | |
| 0.15 | 0.3 | M=SM | A | O=SO | | | | | | | | | | | | | | | | | | | | |
| 0.2 | 0.35 | M=SM | | | | | O=SO | | | | | | | | | | | | | | | | | |
| 0.25 | 0.4 | M=SM | | | | A | | | | O=SO | | | | | | | | | | | | | | |
| 0.3 | 0.45 | SM | | M | A | | | | | | | | | O=SO | | | | | | | | | | |
| 0.35 | 0.5 | M=SM | | | A | | | A | | | O=SO | | | | | | | | | | | | | |
| 0.4 | 0.55 | M=SM | | | | | | | | | | | | | | | O=SO | | | | | | | |
| 0.45 | 0.6 | SM | M=A | A | | O=SO | | | | | | | | | | | | | | | | | | |
| 0.5 | 0.65 | M=SM | | A | | | A | | | | | | O=SO | | | | | | | | | | | |
| 0.55 | 0.7 | SM | M=A | | A | | O=SO | | | | | | | | | | | | | | | | | |
| 0.6 | 0.75 | M≠SM | | A | | | | | O=SO | | | | | | | | | | | | | | | |
| 0.65 | 0.8 | M=SM | | | O=SO | | | | | | | | | | | | | | | | | | | |
| 0.7 | 0.85 | M=SM | | | | | | | O=SO | | | | | | | | | | | | | | | |
| 0.75 | 0.9 | M≠SM | | | | A | | | | O=SO | | | | | | | | | | | | | | |
| 0.8 | 0.95 | SM=SO≠ M=O | | | | | | | | | | | | | | | | | | | | | | |

(b) $\alpha=0.05$ and $\beta=0.2$

| P_0 | P_1 | sample size in total (n) | | | | | | | | | | | | | | | | | | | | | | |
|-------|-------|------------------------------|-----|---------|---------|----|------|----|---------|-----|---------|-----|---------|-----|-----|-----|-----|-----|-----|-----|-----|----------|----------|-----|
| | | SM+0 | +1 | +2 | +3 | +4 | +5 | +6 | +7 | +8 | +9 | +10 | +11 | +12 | +13 | +14 | +15 | +16 | +17 | +18 | +19 | +20 | +21 | +22 |
| 0.05 | 0.2 | M=SM | O=A | SO (+1) | | | | | | | | | | | | | | | | | | | | |
| 0.1 | 0.25 | M=SM | O=A | A | SO (+2) | | | | | | | | | | | | | | | | | | | |
| 0.15 | 0.3 | M=SM | O=A | | | | | | SO (+6) | | | | | | | | | | | | | | | |
| 0.2 | 0.35 | M=SM | | | | | A | | | O | A | | | | | | | | | | | | SO (+11) | |
| 0.25 | 0.4 | SM | | M | A | | | | O≠A | | | | SO (+4) | | | | | | | | | | | |
| 0.3 | 0.45 | SM | | M | O=A | | | A | | | | | | | | | | | | | | SO (+13) | | |
| 0.35 | 0.5 | SM | | M | | | A | | | O≠A | | | SO (+3) | | | | | | | | | | | |
| 0.4 | 0.55 | SM | M | A | | | | | | | O | | | | | | | | | | | SO (+5) | | |
| 0.45 | 0.6 | M=SM | | | A | | A | | SO | | | O | | | | | | | | | | | | |
| 0.5 | 0.65 | SM | M=A | | A | | A | | O | | A | | | | | | | | | | | SO (+8) | | |
| 0.55 | 0.7 | M=SM | | A | | | | | O | | SO (+2) | | | | | | | | | | | | | |
| 0.6 | 0.75 | M=SM | | | | | O=SO | | | | | | | | | | | | | | | | | |
| 0.65 | 0.8 | M=SM | | | A | | | | O≠A | | | | | | | | | | | | | SO (+6) | | |
| 0.7 | 0.85 | M=SM | | | O≠A | | | | | | | | | | | | | | | | | SO (+7) | | |
| 0.75 | 0.9 | M=SM | | | | A | O | | | | | | | | | | | | | | | SO (+4) | | |
| 0.8 | 0.95 | SM=SO | M=O | | | | | | | | | | | | | | | | | | | | | |

(c) $\alpha=0.05$ and $\beta=0.1$

| P_0 | P_1 | sample size in total (n) | | | | | | | | | | | | | | | | | | | | | | |
|-------|-------|------------------------------|-----|-----|--------|----|----|------|----|----|----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|
| | | SM+0 | +1 | +2 | +3 | +4 | +5 | +6 | +7 | +8 | +9 | +10 | +11 | +12 | +13 | +14 | +15 | +16 | +17 | +18 | +19 | +20 | +21 | +22 |
| 0.05 | 0.2 | M≠SM | A | A | O=SO | | | | | | | | | | | | | | | | | | | |
| 0.1 | 0.25 | M=SM | A | O=A | | | | | | | | | SO | | | | | | | | | | | |
| 0.15 | 0.3 | M=SM | | | | | | A | | | | | | A | | | | | | | | O=SO | | |
| 0.2 | 0.35 | M=SM | A | | | | | O=SO | | | | | | | | | | | | | | | | |
| 0.25 | 0.4 | M≠SM | A | | | A | | | | A | | | | | | | | | | | | O=SO | | |
| 0.3 | 0.45 | SM | | | M=A | | | | A | | | | | | A | | | | | | | | O=SO | |
| 0.35 | 0.5 | M=SM | | | A | | | | | | | | | O=SO | | | | | | | | | | |
| 0.4 | 0.55 | M=SM | | | | | A | | | | | | O=SO | | | | | | | | | | | |
| 0.45 | 0.6 | SM | | A | M | A | | A | | | | | | | | | | | | | | | O=SO | |
| 0.5 | 0.65 | M=SM | | A | | A | | | | | | | | O=SO | | | | | | | | | | |
| 0.55 | 0.7 | SM | | | M=A | | A | | A | | | | | | | | | | | | | | O=SO | |
| 0.6 | 0.75 | SM | M=A | | A | | | | | | | | | O=SO | | | | | | | | | | |
| 0.65 | 0.8 | M≠SM | | | A | | | A | | | | | | | A | | | | | | | O=SO | | |
| 0.7 | 0.85 | M=SM | A | | | A | | | | | | | | SO | | | O | | | | | | | |
| 0.75 | 0.9 | M=SM | | | | | A | | | | | | | O=SO | | | | | | | | | | |
| 0.8 | 0.95 | SM | | | M=O=SO | | | | | | | | | | | | | | | | | | | |

1. Abbreviation: M, the modified minimax design, O, the modified optimal design, SM, Simon's minimax design, SO, Simon's optimal design, A, the admissible design.
2. "=" indicates that they are identical but "≠" shows that they are not identical.
3. SO(+XX) shows that Simon's optimal design has "XX" additional samples, compared to the modified optimal design.

Supplementary Figure 2: Comparisons of the modified designs with $\gamma_1 = 1/3$, $\gamma_2 = 2/3$, and $\varepsilon = 0.1$ to Simon's and the admissible designs for $p_1 - p_0 = 0.15$.

Supplementary Table 1: The characteristics of the modified minimax and optimal designs for $\Delta = p_1 - p_0 = 0.2$ and $(\alpha, \beta) = (0.1, 0.1)$

| p_0 | p_1 | α | β | Design method | r_1 | n_1 | r | n | EN_0 | PET_0 | PET_1 | n_1/n (%) |
|-------|-------|----------|---------|------------------|-------|-------|-----|-----|--------|---------|---------|-------------|
| 0.05 | 0.25 | 0.1 | 0.1 | Modified Minimax | 0 | 13 | 2 | 20 | 16.4 | 0.513 | 0.024 | 65.0% |
| | | | | Modified Optimal | 0 | 9 | 2 | 24 | 14.5 | 0.630 | 0.075 | 37.5% |
| 0.1 | 0.3 | 0.1 | 0.1 | Modified Minimax | 1 | 16 | 4 | 25 | 20.4 | 0.515 | 0.026 | 64.0% |
| | | | | Modified Optimal | 1 | 12 | 5 | 35 | 19.8 | 0.659 | 0.085 | 34.3% |
| 0.15 | 0.35 | 0.1 | 0.1 | Modified Minimax | 2 | 17 | 7 | 32 | 24.2 | 0.520 | 0.033 | 53.1% |
| | | | | Modified Optimal | 3 | 19 | 7 | 33 | 23.4 | 0.684 | 0.059 | 57.6% |
| 0.2 | 0.4 | 0.1 | 0.1 | Modified Minimax | 3 | 19 | 10 | 36 | 28.3 | 0.455 | 0.023 | 52.8% |
| | | | | Modified Optimal | 3 | 17 | 10 | 37 | 26.0 | 0.549 | 0.046 | 45.9% |
| 0.25 | 0.45 | 0.1 | 0.1 | Modified Minimax | 5 | 23 | 13 | 39 | 31.5 | 0.468 | 0.019 | 59.0% |
| | | | | Modified Optimal | 3 | 15 | 13 | 40 | 28.5 | 0.461 | 0.042 | 37.5% |
| 0.3 | 0.5 | 0.1 | 0.1 | Modified Minimax | 6 | 26 | 15 | 39 | 35.1 | 0.297 | 0.005 | 66.7% |
| | | | | Modified Optimal | 7 | 22 | 17 | 46 | 29.9 | 0.671 | 0.067 | 47.8% |
| 0.35 | 0.55 | 0.1 | 0.1 | Modified Minimax | 7 | 21 | 19 | 44 | 31.7 | 0.536 | 0.038 | 47.7% |
| | | | | Modified Optimal | 7 | 20 | 20 | 47 | 30.8 | 0.601 | 0.058 | 42.6% |
| 0.4 | 0.6 | 0.1 | 0.1 | Modified Minimax | 7 | 21 | 20 | 41 | 34.0 | 0.350 | 0.012 | 51.2% |
| | | | | Modified Optimal | 7 | 18 | 22 | 46 | 30.2 | 0.563 | 0.058 | 39.1% |
| 0.45 | 0.65 | 0.1 | 0.1 | Modified Minimax | 9 | 21 | 22 | 41 | 30.8 | 0.512 | 0.031 | 51.2% |
| | | | | Modified Optimal | 9 | 20 | 24 | 45 | 30.2 | 0.591 | 0.053 | 44.4% |
| 0.5 | 0.7 | 0.1 | 0.1 | Modified Minimax | 11 | 23 | 23 | 39 | 31.0 | 0.500 | 0.021 | 59.0% |
| | | | | Modified Optimal | 11 | 21 | 26 | 45 | 29.0 | 0.668 | 0.068 | 46.7% |
| 0.55 | 0.75 | 0.1 | 0.1 | Modified Minimax | 13 | 23 | 25 | 39 | 28.8 | 0.636 | 0.041 | 59.0% |
| | | | | Modified Optimal | 10 | 18 | 26 | 41 | 27.0 | 0.609 | 0.057 | 43.9% |
| 0.6 | 0.8 | 0.1 | 0.1 | Modified Minimax | 9 | 16 | 25 | 36 | 26.5 | 0.473 | 0.027 | 44.4% |
| | | | | Modified Optimal | 9 | 15 | 28 | 41 | 25.5 | 0.597 | 0.061 | 36.6% |
| 0.65 | 0.85 | 0.1 | 0.1 | Modified Minimax | 8 | 13 | 23 | 31 | 22.0 | 0.499 | 0.034 | 41.9% |
| | | | | Modified Optimal | 10 | 15 | 25 | 34 | 21.7 | 0.648 | 0.062 | 44.1% |
| 0.7 | 0.9 | 0.1 | 0.1 | Modified Minimax | 11 | 16 | 20 | 25 | 20.0 | 0.550 | 0.017 | 64.0% |
| | | | | Modified Optimal | 11 | 15 | 22 | 28 | 18.9 | 0.703 | 0.056 | 53.6% |
| 0.75 | 0.95 | 0.1 | 0.1 | Modified Minimax | 6 | 8 | 16 | 19 | 12.0 | 0.633 | 0.057 | 42.1% |
| | | | | Modified Optimal | 6 | 8 | 16 | 19 | 12.0 | 0.633 | 0.057 | 42.1% |

Supplementary Table 2: The characteristics of the modified minimax and optimal designs for $\Delta = p_1 - p_0 = 0.2$ and $(\alpha, \beta) = (0.05, 0.2)$

| p_0 | p_1 | α | β | Design method | r_1 | n_1 | r | n | EN_0 | PET_0 | PET_1 | n_1/n (%) |
|-------|-------|----------|---------|------------------|-------|-------|-----|-----|--------|---------|---------|-------------|
| 0.05 | 0.25 | 0.05 | 0.2 | Modified Minimax | 0 | 9 | 2 | 17 | 12.0 | 0.630 | 0.075 | 52.9% |
| | | | | Modified Optimal | 0 | 9 | 2 | 17 | 12.0 | 0.630 | 0.075 | 52.9% |
| 0.1 | 0.3 | 0.05 | 0.2 | Modified Minimax | 1 | 15 | 5 | 25 | 19.5 | 0.549 | 0.035 | 60.0% |
| | | | | Modified Optimal | 1 | 12 | 5 | 26 | 16.8 | 0.659 | 0.085 | 46.2% |
| 0.15 | 0.35 | 0.05 | 0.2 | Modified Minimax | 2 | 15 | 7 | 28 | 20.1 | 0.604 | 0.062 | 53.6% |
| | | | | Modified Optimal | 2 | 15 | 7 | 28 | 20.1 | 0.604 | 0.062 | 53.6% |
| 0.2 | 0.4 | 0.05 | 0.2 | Modified Minimax | 4 | 18 | 10 | 33 | 22.3 | 0.716 | 0.094 | 54.5% |
| | | | | Modified Optimal | 4 | 18 | 10 | 33 | 22.3 | 0.716 | 0.094 | 54.5% |
| 0.25 | 0.45 | 0.05 | 0.2 | Modified Minimax | 4 | 17 | 13 | 36 | 25.1 | 0.574 | 0.060 | 47.2% |
| | | | | Modified Optimal | 4 | 16 | 14 | 39 | 24.5 | 0.630 | 0.085 | 41.0% |
| 0.3 | 0.5 | 0.05 | 0.2 | Modified Minimax | 6 | 19 | 16 | 39 | 25.7 | 0.666 | 0.084 | 48.7% |
| | | | | Modified Optimal | 4 | 14 | 17 | 42 | 25.6 | 0.584 | 0.090 | 33.3% |
| 0.35 | 0.55 | 0.05 | 0.2 | Modified Minimax | 8 | 21 | 18 | 39 | 26.3 | 0.706 | 0.091 | 53.8% |
| | | | | Modified Optimal | 8 | 21 | 18 | 39 | 26.3 | 0.706 | 0.091 | 53.8% |
| 0.4 | 0.6 | 0.05 | 0.2 | Modified Minimax | 7 | 17 | 21 | 41 | 25.6 | 0.641 | 0.092 | 41.5% |
| | | | | Modified Optimal | 7 | 17 | 21 | 41 | 25.6 | 0.641 | 0.092 | 41.5% |
| 0.45 | 0.65 | 0.05 | 0.2 | Modified Minimax | 8 | 17 | 23 | 41 | 25.1 | 0.663 | 0.099 | 41.5% |
| | | | | Modified Optimal | 8 | 17 | 23 | 41 | 25.1 | 0.663 | 0.099 | 41.5% |
| 0.5 | 0.7 | 0.05 | 0.2 | Modified Minimax | 12 | 23 | 23 | 37 | 27.7 | 0.661 | 0.055 | 62.2% |
| | | | | Modified Optimal | 8 | 16 | 24 | 39 | 25.2 | 0.598 | 0.074 | 41.0% |
| 0.55 | 0.75 | 0.05 | 0.2 | Modified Minimax | 11 | 20 | 25 | 37 | 27.0 | 0.586 | 0.041 | 54.1% |
| | | | | Modified Optimal | 7 | 13 | 26 | 39 | 24.1 | 0.573 | 0.080 | 33.3% |
| 0.6 | 0.8 | 0.05 | 0.2 | Modified Minimax | 8 | 13 | 25 | 35 | 20.8 | 0.647 | 0.099 | 37.1% |
| | | | | Modified Optimal | 8 | 13 | 25 | 35 | 20.8 | 0.647 | 0.099 | 37.1% |
| 0.65 | 0.85 | 0.05 | 0.2 | Modified Minimax | 7 | 11 | 24 | 31 | 19.5 | 0.574 | 0.069 | 35.5% |
| | | | | Modified Optimal | 7 | 11 | 24 | 31 | 19.5 | 0.574 | 0.069 | 35.5% |
| 0.7 | 0.9 | 0.05 | 0.2 | Modified Minimax | 8 | 11 | 23 | 28 | 16.3 | 0.687 | 0.090 | 39.3% |
| | | | | Modified Optimal | 8 | 11 | 23 | 28 | 16.3 | 0.687 | 0.090 | 39.3% |
| 0.75 | 0.95 | 0.05 | 0.2 | Modified Minimax | 8 | 10 | 20 | 23 | 13.2 | 0.756 | 0.086 | 43.5% |
| | | | | Modified Optimal | 8 | 10 | 20 | 23 | 13.2 | 0.756 | 0.086 | 43.5% |

Supplementary Table 3: The characteristics of the modified minimax and optimal designs for $\Delta = p_1 - p_0 = 0.2$ and $(\alpha, \beta) = (0.05, 0.1)$

| p_0 | p_1 | α | β | Design method | r_1 | n_1 | r | n | EN_0 | PET_0 | PET_1 | n_1/n (%) |
|-------|-------|----------|---------|------------------|-------|-------|-----|-----|--------|---------|---------|-------------|
| 0.05 | 0.25 | 0.05 | 0.1 | Modified Minimax | 0 | 15 | 3 | 25 | 20.4 | 0.463 | 0.013 | 60.0% |
| | | | | Modified Optimal | 0 | 10 | 3 | 28 | 17.2 | 0.599 | 0.056 | 35.7% |
| 0.1 | 0.3 | 0.05 | 0.1 | Modified Minimax | 2 | 22 | 6 | 33 | 26.2 | 0.620 | 0.021 | 66.7% |
| | | | | Modified Optimal | 2 | 18 | 6 | 35 | 22.5 | 0.734 | 0.060 | 51.4% |
| 0.15 | 0.35 | 0.05 | 0.1 | Modified Minimax | 3 | 23 | 9 | 38 | 29.9 | 0.540 | 0.018 | 60.5% |
| | | | | Modified Optimal | 3 | 19 | 10 | 44 | 26.9 | 0.684 | 0.059 | 43.2% |
| 0.2 | 0.4 | 0.05 | 0.1 | Modified Minimax | 5 | 24 | 13 | 45 | 31.2 | 0.656 | 0.040 | 53.3% |
| | | | | Modified Optimal | 4 | 19 | 15 | 54 | 30.4 | 0.673 | 0.070 | 35.2% |
| 0.25 | 0.45 | 0.05 | 0.1 | Modified Minimax | 6 | 26 | 17 | 49 | 37.1 | 0.515 | 0.018 | 53.1% |
| | | | | Modified Optimal | 6 | 22 | 19 | 57 | 32.5 | 0.699 | 0.071 | 38.6% |
| 0.3 | 0.5 | 0.05 | 0.1 | Modified Minimax | 7 | 24 | 21 | 53 | 36.6 | 0.565 | 0.032 | 45.3% |
| | | | | Modified Optimal | 8 | 24 | 24 | 63 | 34.7 | 0.725 | 0.076 | 38.1% |
| 0.35 | 0.55 | 0.05 | 0.1 | Modified Minimax | 10 | 34 | 24 | 53 | 47.1 | 0.313 | 0.002 | 64.2% |
| | | | | Modified Optimal | 7 | 20 | 26 | 59 | 35.6 | 0.601 | 0.058 | 33.9% |
| 0.4 | 0.6 | 0.05 | 0.1 | Modified Minimax | 12 | 29 | 27 | 54 | 38.1 | 0.637 | 0.033 | 53.7% |
| | | | | Modified Optimal | 11 | 25 | 32 | 66 | 36.0 | 0.732 | 0.078 | 37.9% |
| 0.45 | 0.65 | 0.05 | 0.1 | Modified Minimax | 14 | 31 | 30 | 54 | 40.6 | 0.581 | 0.019 | 57.4% |
| | | | | Modified Optimal | 11 | 23 | 33 | 61 | 34.9 | 0.687 | 0.068 | 37.7% |
| 0.5 | 0.7 | 0.05 | 0.1 | Modified Minimax | 14 | 27 | 32 | 53 | 36.1 | 0.649 | 0.036 | 50.9% |
| | | | | Modified Optimal | 13 | 24 | 36 | 61 | 34.0 | 0.729 | 0.074 | 39.3% |
| 0.55 | 0.75 | 0.05 | 0.1 | Modified Minimax | 15 | 28 | 33 | 50 | 38.7 | 0.513 | 0.011 | 56.0% |
| | | | | Modified Optimal | 10 | 18 | 35 | 54 | 32.1 | 0.609 | 0.057 | 33.3% |
| 0.6 | 0.8 | 0.05 | 0.1 | Modified Minimax | 15 | 26 | 32 | 45 | 35.9 | 0.479 | 0.008 | 57.8% |
| | | | | Modified Optimal | 12 | 19 | 37 | 53 | 29.5 | 0.692 | 0.068 | 35.8% |
| 0.65 | 0.85 | 0.05 | 0.1 | Modified Minimax | 12 | 18 | 31 | 41 | 26.2 | 0.645 | 0.042 | 43.9% |
| | | | | Modified Optimal | 10 | 15 | 33 | 44 | 25.2 | 0.648 | 0.062 | 34.1% |
| 0.7 | 0.9 | 0.05 | 0.1 | Modified Minimax | 13 | 18 | 26 | 32 | 22.7 | 0.667 | 0.028 | 56.3% |
| | | | | Modified Optimal | 11 | 15 | 29 | 36 | 21.2 | 0.703 | 0.056 | 41.7% |
| 0.75 | 0.95 | 0.05 | 0.1 | Modified Minimax | 12 | 15 | 24 | 28 | 18.1 | 0.764 | 0.036 | 53.6% |
| | | | | Modified Optimal | 12 | 15 | 24 | 28 | 18.1 | 0.764 | 0.036 | 53.6% |

Supplementary Table 4: The characteristics of the modified minimax and optimal designs for $\Delta = p_1 - p_0 = 0.15$ and $(\alpha, \beta) = (0.1, 0.1)$

| p_0 | p_1 | α | β | Design method | r_1 | n_1 | r | n | EN_0 | PET_0 | PET_1 | n_1/n (%) |
|-------|-------|----------|---------|------------------|-------|-------|-----|-----|--------|---------|---------|-------------|
| 0.05 | 0.2 | 0.1 | 0.1 | Modified Minimax | 0 | 18 | 3 | 32 | 26.4 | 0.397 | 0.018 | 56.3% |
| | | | | Modified Optimal | 1 | 19 | 3 | 38 | 23.7 | 0.755 | 0.083 | 50.0% |
| 0.1 | 0.25 | 0.1 | 0.1 | Modified Minimax | 1 | 23 | 6 | 40 | 34.6 | 0.315 | 0.012 | 57.5% |
| | | | | Modified Optimal | 2 | 21 | 7 | 50 | 31.2 | 0.648 | 0.075 | 42.0% |
| 0.15 | 0.3 | 0.1 | 0.1 | Modified Minimax | 5 | 34 | 11 | 53 | 41.7 | 0.597 | 0.033 | 64.2% |
| | | | | Modified Optimal | 3 | 23 | 11 | 55 | 37.7 | 0.54 | 0.054 | 41.8% |
| 0.2 | 0.35 | 0.1 | 0.1 | Modified Minimax | 6 | 33 | 15 | 58 | 45.5 | 0.5 | 0.028 | 56.9% |
| | | | | Modified Optimal | 5 | 27 | 16 | 63 | 43.6 | 0.539 | 0.051 | 42.9% |
| 0.25 | 0.4 | 0.1 | 0.1 | Modified Minimax | 9 | 39 | 20 | 64 | 52.1 | 0.476 | 0.02 | 60.9% |
| | | | | Modified Optimal | 7 | 29 | 22 | 72 | 48.1 | 0.557 | 0.057 | 40.3% |
| 0.3 | 0.45 | 0.1 | 0.1 | Modified Minimax | 13 | 45 | 26 | 71 | 57.8 | 0.509 | 0.02 | 63.4% |
| | | | | Modified Optimal | 9 | 30 | 29 | 82 | 51.4 | 0.589 | 0.069 | 36.6% |
| 0.35 | 0.5 | 0.1 | 0.1 | Modified Minimax | 14 | 43 | 30 | 72 | 59.3 | 0.437 | 0.016 | 59.7% |
| | | | | Modified Optimal | 12 | 34 | 33 | 81 | 53.2 | 0.592 | 0.061 | 42.0% |
| 0.4 | 0.55 | 0.1 | 0.1 | Modified Minimax | 18 | 45 | 34 | 73 | 57.2 | 0.564 | 0.031 | 61.6% |
| | | | | Modified Optimal | 16 | 38 | 40 | 88 | 54.5 | 0.67 | 0.076 | 43.2% |
| 0.45 | 0.6 | 0.1 | 0.1 | Modified Minimax | 22 | 50 | 39 | 75 | 62.5 | 0.502 | 0.016 | 66.7% |
| | | | | Modified Optimal | 14 | 32 | 40 | 78 | 54.2 | 0.517 | 0.046 | 41.0% |
| 0.5 | 0.65 | 0.1 | 0.1 | Modified Minimax | 19 | 40 | 41 | 72 | 58.0 | 0.437 | 0.017 | 55.6% |
| | | | | Modified Optimal | 18 | 35 | 47 | 84 | 53.0 | 0.632 | 0.068 | 41.7% |
| 0.55 | 0.7 | 0.1 | 0.1 | Modified Minimax | 16 | 31 | 44 | 71 | 54.2 | 0.419 | 0.024 | 43.7% |
| | | | | Modified Optimal | 19 | 34 | 46 | 75 | 50.1 | 0.606 | 0.057 | 45.3% |
| 0.6 | 0.75 | 0.1 | 0.1 | Modified Minimax | 22 | 39 | 43 | 64 | 54.5 | 0.381 | 0.009 | 60.9% |
| | | | | Modified Optimal | 21 | 34 | 47 | 71 | 47.1 | 0.646 | 0.061 | 47.9% |
| 0.65 | 0.8 | 0.1 | 0.1 | Modified Minimax | 22 | 33 | 43 | 60 | 42.6 | 0.643 | 0.051 | 55.0% |
| | | | | Modified Optimal | 20 | 30 | 45 | 63 | 41.8 | 0.642 | 0.061 | 47.6% |
| 0.7 | 0.85 | 0.1 | 0.1 | Modified Minimax | 15 | 22 | 40 | 52 | 36.8 | 0.506 | 0.037 | 42.3% |
| | | | | Modified Optimal | 14 | 20 | 45 | 59 | 36.2 | 0.584 | 0.067 | 33.9% |
| 0.75 | 0.9 | 0.1 | 0.1 | Modified Minimax | 19 | 26 | 33 | 40 | 33.2 | 0.485 | 0.012 | 65.0% |
| | | | | Modified Optimal | 12 | 16 | 39 | 48 | 29.0 | 0.595 | 0.068 | 33.3% |
| 0.8 | 0.95 | 0.1 | 0.1 | Modified Minimax | 13 | 16 | 27 | 31 | 21.3 | 0.648 | 0.043 | 51.6% |
| | | | | Modified Optimal | 13 | 16 | 27 | 31 | 21.3 | 0.648 | 0.043 | 51.6% |

Supplementary Table 5: The characteristics of the modified minimax and optimal designs for $\Delta = p_1 - p_0 = 0.15$ and $(\alpha, \beta) = (0.05, 0.2)$

| p_0 | p_1 | α | β | Design method | r_1 | n_1 | r | n | EN_0 | PET_0 | PET_1 | n_1/n (%) |
|-------|-------|----------|---------|------------------|-------|-------|-----|-----|--------|---------|---------|-------------|
| 0.05 | 0.2 | 0.05 | 0.2 | Modified Minimax | 0 | 13 | 3 | 27 | 19.8 | 0.513 | 0.055 | 48.1% |
| | | | | Modified Optimal | 0 | 11 | 3 | 28 | 18.3 | 0.569 | 0.086 | 39.3% |
| 0.1 | 0.25 | 0.05 | 0.2 | Modified Minimax | 2 | 22 | 7 | 40 | 28.8 | 0.62 | 0.061 | 55.0% |
| | | | | Modified Optimal | 1 | 15 | 7 | 41 | 26.7 | 0.549 | 0.08 | 36.6% |
| 0.15 | 0.3 | 0.05 | 0.2 | Modified Minimax | 3 | 23 | 11 | 48 | 34.5 | 0.54 | 0.054 | 47.9% |
| | | | | Modified Optimal | 3 | 21 | 11 | 49 | 31.9 | 0.611 | 0.086 | 42.9% |
| 0.2 | 0.35 | 0.05 | 0.2 | Modified Minimax | 6 | 31 | 15 | 53 | 40.4 | 0.571 | 0.046 | 58.5% |
| | | | | Modified Optimal | 4 | 21 | 17 | 61 | 37.6 | 0.586 | 0.092 | 34.4% |
| 0.25 | 0.4 | 0.05 | 0.2 | Modified Minimax | 10 | 40 | 21 | 62 | 49.2 | 0.584 | 0.035 | 64.5% |
| | | | | Modified Optimal | 6 | 24 | 22 | 67 | 40.9 | 0.607 | 0.096 | 35.8% |
| 0.3 | 0.45 | 0.05 | 0.2 | Modified Minimax | 9 | 31 | 26 | 67 | 47.5 | 0.542 | 0.052 | 46.3% |
| | | | | Modified Optimal | 7 | 24 | 26 | 68 | 43.2 | 0.565 | 0.086 | 35.3% |
| 0.35 | 0.5 | 0.05 | 0.2 | Modified Minimax | 14 | 42 | 30 | 68 | 55.5 | 0.481 | 0.022 | 61.8% |
| | | | | Modified Optimal | 10 | 28 | 32 | 74 | 45.7 | 0.616 | 0.092 | 37.8% |
| 0.4 | 0.55 | 0.05 | 0.2 | Modified Minimax | 15 | 40 | 35 | 71 | 57.4 | 0.44 | 0.02 | 56.3% |
| | | | | Modified Optimal | 12 | 29 | 38 | 79 | 47.1 | 0.637 | 0.099 | 36.7% |
| 0.45 | 0.6 | 0.05 | 0.2 | Modified Minimax | 19 | 42 | 38 | 70 | 53.9 | 0.576 | 0.038 | 60.0% |
| | | | | Modified Optimal | 14 | 30 | 43 | 80 | 47.8 | 0.645 | 0.097 | 37.5% |
| 0.5 | 0.65 | 0.05 | 0.2 | Modified Minimax | 20 | 41 | 41 | 69 | 55.0 | 0.5 | 0.024 | 59.4% |
| | | | | Modified Optimal | 15 | 29 | 44 | 75 | 45.4 | 0.644 | 0.098 | 38.7% |
| 0.55 | 0.7 | 0.05 | 0.2 | Modified Minimax | 20 | 35 | 43 | 67 | 45.8 | 0.662 | 0.073 | 52.2% |
| | | | | Modified Optimal | 14 | 25 | 47 | 74 | 43.8 | 0.616 | 0.098 | 33.8% |
| 0.6 | 0.75 | 0.05 | 0.2 | Modified Minimax | 18 | 30 | 43 | 62 | 43.8 | 0.569 | 0.051 | 48.4% |
| | | | | Modified Optimal | 14 | 23 | 46 | 67 | 40.1 | 0.612 | 0.096 | 34.3% |
| 0.65 | 0.8 | 0.05 | 0.2 | Modified Minimax | 20 | 31 | 41 | 55 | 41.9 | 0.545 | 0.033 | 56.4% |
| | | | | Modified Optimal | 16 | 24 | 45 | 61 | 37.2 | 0.642 | 0.089 | 39.3% |
| 0.7 | 0.85 | 0.05 | 0.2 | Modified Minimax | 16 | 23 | 39 | 49 | 34.4 | 0.56 | 0.046 | 46.9% |
| | | | | Modified Optimal | 16 | 22 | 41 | 52 | 31.4 | 0.687 | 0.1 | 42.3% |
| 0.75 | 0.9 | 0.05 | 0.2 | Modified Minimax | 17 | 22 | 33 | 39 | 27.5 | 0.677 | 0.062 | 56.4% |
| | | | | Modified Optimal | 14 | 18 | 37 | 44 | 25.9 | 0.694 | 0.098 | 40.9% |
| 0.8 | 0.95 | 0.05 | 0.2 | Modified Minimax | 13 | 16 | 27 | 30 | 20.9 | 0.648 | 0.043 | 53.3% |
| | | | | Modified Optimal | 13 | 16 | 27 | 30 | 20.9 | 0.648 | 0.043 | 53.3% |

Supplementary Table 6: The characteristics of the modified minimax and optimal designs for $\Delta = p_1 - p_0 = 0.15$ and $(\alpha, \beta) = (0.05, 0.1)$

| p_0 | p_1 | α | β | Design method | r_1 | n_1 | r | n | EN_0 | PET_0 | PET_1 | n_1/n (%) |
|-------|-------|----------|---------|------------------|-------|-------|-----|-----|--------|---------|---------|-------------|
| 0.05 | 0.2 | 0.05 | 0.1 | Modified Minimax | 0 | 23 | 4 | 38 | 33.4 | 0.307 | 0.006 | 60.5% |
| | | | | Modified Optimal | 1 | 21 | 4 | 41 | 26.7 | 0.717 | 0.058 | 51.2% |
| 0.1 | 0.25 | 0.05 | 0.1 | Modified Minimax | 3 | 31 | 9 | 55 | 40.0 | 0.624 | 0.031 | 56.4% |
| | | | | Modified Optimal | 3 | 28 | 9 | 57 | 36.9 | 0.695 | 0.055 | 49.1% |
| 0.15 | 0.3 | 0.05 | 0.1 | Modified Minimax | 6 | 42 | 14 | 64 | 51.8 | 0.555 | 0.015 | 65.6% |
| | | | | Modified Optimal | 5 | 30 | 17 | 82 | 45.1 | 0.711 | 0.077 | 36.6% |
| 0.2 | 0.35 | 0.05 | 0.1 | Modified Minimax | 8 | 42 | 21 | 77 | 58.4 | 0.531 | 0.019 | 54.5% |
| | | | | Modified Optimal | 8 | 37 | 22 | 83 | 51.4 | 0.686 | 0.059 | 44.6% |
| 0.25 | 0.4 | 0.05 | 0.1 | Modified Minimax | 11 | 52 | 27 | 83 | 73.0 | 0.323 | 0.003 | 62.7% |
| | | | | Modified Optimal | 10 | 37 | 31 | 99 | 56.2 | 0.691 | 0.072 | 37.4% |
| 0.3 | 0.45 | 0.05 | 0.1 | Modified Minimax | 14 | 46 | 34 | 91 | 64.1 | 0.597 | 0.032 | 50.5% |
| | | | | Modified Optimal | 13 | 40 | 40 | 110 | 60.8 | 0.703 | 0.075 | 36.4% |
| 0.35 | 0.5 | 0.05 | 0.1 | Modified Minimax | 16 | 46 | 40 | 94 | 67.4 | 0.555 | 0.027 | 48.9% |
| | | | | Modified Optimal | 16 | 43 | 44 | 105 | 62.7 | 0.683 | 0.063 | 41.0% |
| 0.4 | 0.55 | 0.05 | 0.1 | Modified Minimax | 24 | 62 | 45 | 94 | 78.9 | 0.472 | 0.007 | 66.0% |
| | | | | Modified Optimal | 19 | 45 | 49 | 104 | 64.0 | 0.679 | 0.058 | 43.3% |
| 0.45 | 0.6 | 0.05 | 0.1 | Modified Minimax | 26 | 58 | 52 | 98 | 76.3 | 0.544 | 0.014 | 59.2% |
| | | | | Modified Optimal | 19 | 40 | 60 | 116 | 64.0 | 0.684 | 0.074 | 34.5% |
| 0.5 | 0.65 | 0.05 | 0.1 | Modified Minimax | 28 | 57 | 54 | 93 | 75.0 | 0.5 | 0.01 | 61.3% |
| | | | | Modified Optimal | 22 | 42 | 60 | 105 | 62.3 | 0.678 | 0.062 | 40.0% |
| 0.55 | 0.7 | 0.05 | 0.1 | Modified Minimax | 26 | 47 | 58 | 92 | 66.2 | 0.574 | 0.023 | 51.1% |
| | | | | Modified Optimal | 22 | 38 | 68 | 110 | 59.8 | 0.697 | 0.076 | 34.5% |
| 0.6 | 0.75 | 0.05 | 0.1 | Modified Minimax | 29 | 48 | 58 | 85 | 63.6 | 0.578 | 0.018 | 56.5% |
| | | | | Modified Optimal | 21 | 34 | 64 | 95 | 55.6 | 0.646 | 0.061 | 35.8% |
| 0.65 | 0.8 | 0.05 | 0.1 | Modified Minimax | 29 | 46 | 55 | 75 | 62.1 | 0.445 | 0.006 | 61.3% |
| | | | | Modified Optimal | 21 | 31 | 67 | 93 | 50.3 | 0.689 | 0.075 | 33.3% |
| 0.7 | 0.85 | 0.05 | 0.1 | Modified Minimax | 33 | 44 | 53 | 68 | 48.5 | 0.811 | 0.057 | 64.7% |
| | | | | Modified Optimal | 23 | 31 | 63 | 82 | 43.5 | 0.755 | 0.082 | 37.8% |
| 0.75 | 0.9 | 0.05 | 0.1 | Modified Minimax | 19 | 25 | 45 | 54 | 36.0 | 0.622 | 0.033 | 46.3% |
| | | | | Modified Optimal | 18 | 23 | 52 | 63 | 34.3 | 0.717 | 0.073 | 36.5% |
| 0.8 | 0.95 | 0.05 | 0.1 | Modified Minimax | 16 | 19 | 37 | 42 | 24.4 | 0.763 | 0.067 | 45.2% |
| | | | | Modified Optimal | 16 | 19 | 37 | 42 | 24.4 | 0.763 | 0.067 | 45.2% |