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2 **Supplementary Information for**

3 **Marine Ice Sheet Instability Amplifies and Skews Uncertainty in Projections of Future Sea** 4 **Level Rise**

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8 **This PDF file includes:**

9 Supplementary text

10 Figs. S1 to S5

11 Captions for Movies S1 to S4

12 References for SI reference citations

13 **Other supplementary materials for this manuscript include the following:**

14 Movies S1 to S4

15 Supporting Information Text

16 Stochastic Perturbation Theory

17 We take the stochastic perturbation approach outlined by Moon and Wettlaufer (1) and Fitzmaurice (2) for non-autonomous
18 dynamical systems. We consider a system of the form

$$19 \quad \frac{dL}{dt} = f(L, t) + \sigma_F \xi(t) \quad [1]$$

20 where $f(L, t)$ is the deterministic system dynamics, σ_F is the amplitude of stochastic forcing, and $\xi(t)$ is a Wiener process
21 which is continuous in time, but can be approximated (for our purposes) as white noise when the system is numerically solved
22 using the Euler-Maruyama method or similar. We assume the Martingale property wherein discrete increments of process $\xi(t)$
23 are uncorrelated in time.

24 The right hand side of equation 1 can be expanded in terms of a small perturbation, $\ell(t)$, about the solution to the
25 deterministic version of the system, $L_d(t)$

$$26 \quad \frac{d\ell}{dt} = [\omega\ell + \kappa\ell^2 + \dots] + \sigma_F \xi(t) \quad [2]$$

where $\omega(t) = \left. \frac{df}{dL} \right|_{L_d}$ and $\kappa(t) = \left. \frac{1}{2} \frac{d^2f}{dL^2} \right|_{L_d}$ are parameters that may be state- and time-dependent, and which define the
leading-order behavior of the system. For equation 1 in the main text, these parameters are given by

$$\omega = \lambda b_x [Ph_g^{-2}L + (\beta - 1)\gamma h_g^{\beta-2}] + Ph_g^{-1} \quad [3]$$

$$\kappa = (\lambda b_x)^2 h_g^{-2} \left[Ph_g^{-1}L + P(\lambda b_x)^{-1} - \frac{1}{2}(\beta - 1)(\beta - 2)\gamma h_g^{\beta-1} \right] \quad [4]$$

27 where $h_g = -\lambda b_g$ is the grounding line ice thickness, and $\lambda = \frac{\rho_w}{\rho_i}$.

28 We expand in terms of powers of the noise magnitude σ_F (where $\sigma_F \ll \ell$): $\ell = \ell_0 + \sigma_F \ell_1 + \frac{\sigma_F^2}{2} \ell_2$. The leading order terms
29 describe initial perturbation from the deterministic solution of the system, and in general $\ell_0 = 0$ if the system begins on the
30 deterministic trajectory (which we will take to be the case here, which greatly simplifies this analysis). The terms that are
31 first-order in σ_F are

$$32 \quad \frac{d\ell_1}{dt} = \omega(t)\ell_1 + \xi, \quad [5]$$

33 which can be written in the form of the Fokker-Planck equation

$$34 \quad \frac{\partial \rho}{\partial t} = -\omega(t) + \frac{\partial}{\partial \ell_1}(\ell_1 \rho) + \frac{1}{2} \frac{\partial^2 \rho}{\partial \ell_1^2}, \quad [6]$$

35 where ρ is the probability density function of the first-order stochastic solution. We solve the Fokker-Planck equation in the
36 typical fashion, by taking the Fourier transform in ℓ_1 , solving the characteristic equation, and then re-inverting the Fourier
37 transform. The result is a probability density function with second moment (variance)

$$38 \quad \sigma_L(t)^2 = \frac{\sigma_F^2}{\Delta t} e^{2\omega(t)} \int_0^t e^{-2\omega(s)} ds. \quad [7]$$

39 This is the general nonlinear evolution equation for the spread of the stochastic PDF, which will provide the most accurate
40 solution if ω is strongly time-dependent. However, we can solve for an approximate analytic form of the variance by assuming
41 constant ω , which gives

$$42 \quad \sigma_L(t)^2 = \frac{\sigma_F^2}{2\omega\Delta t} (e^{2\omega t} - 1), \quad [8]$$

43 which works fairly well soon after the onset of the instability and becomes a worse approximation over time (but captures the
44 approximate rate of variance growth). Thus, we conclude that variance grows approximately exponentially with rate 2ω .

45 We note some features about the variance growth rate, ω (equation 3). The first term, which is typically the larger term
46 (though not dominant) is proportional to the bed slope, b_x . Thus, the growth rate will generally increase with b_x , when it
47 is positive (reverse-sloping bed). When b_x is sufficiently negative (forward-sloping bed), ω will also be negative, and the
48 variance will remain bounded in time (though it won't necessarily go to zero). If we assume that the grounding line begins at
49 a steady-state, then $PL = \gamma(-\lambda b_g)^\beta$, and we can simplify to $\omega = Ph_g^{-1} (\beta\lambda b_x L h_g^{-1} + 1)$. It is important to note here that
50 $(\beta\lambda b_x L h_g^{-1} + 1) = S_T$ is the same stability parameter (S_T) which is derived in Robel et al. (2018)(3), and which determines
51 whether the slow time scale is stable or not (which is the only time scale in the model defined in equation 1 in the main text).
52 Ice sheet geometry also matters in determining this growth rate, though this is, in some sense, fixed by the bed topography.
53 Finally, β , the exponent for the grounding line flux also plays a role in determining the growth rate. Generally, the more
54 nonlinear the grounding line flux is (e.g. for Coulomb plastic beds near the grounding line (4)), the more rapidly the ensemble
55 variance will grow (see Figure S1). This should also be kept in mind when interpreting the results of the ISSM ensemble
56 simulations in this study, which assume power-law sliding at the bed.

57 We can follow a similar procedure to solve the Fokker-Planck form of the equation for the terms that are second-order in
 58 σ_F : ℓ_2 . This provides an analytical form of the third moment (skewness) of the probability density function (which was zero
 59 for the first-order terms):

$$60 \quad Sk_L = \frac{\sigma_F^2}{\sigma_L^3 \Delta t} [-6\kappa S + 6\kappa\sigma_L^2 M + \sigma_F^2 \kappa^3 M^3] \quad [9]$$

where

$$S(t) = \frac{\Delta t^2}{\sigma_F^4} e^{3\omega(t)} \int_0^t \sigma_L^4 e^{-3\omega(s)} ds \quad [10]$$

$$M(t) = \frac{\Delta t}{\sigma_F^2} e^{\omega(t)} \int_0^t \sigma_L^2 e^{-\omega(s)} ds. \quad [11]$$

61 This lengthy approximation is typically dominated by the second term in the minimal grounding line model, allowing us to
 62 drop the first and third terms to derive an expression for the skewness of the probability density function

$$63 \quad Sk_L(t) = \frac{6\kappa M(t) \sigma_F^2}{\sigma_L \Delta t}. \quad [12]$$

64 Again, assuming that ω and κ are constant in time, we can solve the corresponding linear problem to derive a simplified
 65 approximate analytic form of the skewness

$$66 \quad Sk_L(t) = 6\kappa\sigma_F [2\omega^3 \Delta t (e^{2\omega t} - 1)]^{-\frac{1}{2}} (e^{\omega t} - 1)^2 \quad [13]$$

67 The skewness is also dependent on ω through σ_L . However, critically, it is also proportional to κ . κ is proportional to
 68 b_x^2 meaning that skewness increases rapidly as the bed slope increases in magnitude, This is the case both for reverse- and
 69 forward-sloping beds, though as we showed above σ_L will remain sharply bounded for forward-sloping beds, and so will
 70 skewness. If we again make the assumption that the system begins at a steady-state ($PL = \gamma h_g^\beta$), then we can simplify the
 71 terms inside the brackets to: $PLh_g^{-1} [1 - \frac{1}{2}(\beta - 1)(\beta - 2)] + P(\lambda b_x)^{-1}$. This expression is dominated by the first term, in
 72 which the sign is set by $1 - \frac{1}{2}(\beta - 1)(\beta - 2)$. This is a quadratic expression which is positive for $0 < \beta < 3$ and negative for
 73 $\beta > 3$. In asymptotic analyses of the grounding line ice flux (4–6), this exact exponent is the target of considerable analysis. It
 74 is generally the case that $\beta > 3$, and often considerably so. Thus, we may conclude that the skewness of ensemble projections
 75 will generally be negative during the marine ice sheet instability, corresponding to ensemble projection distributions with a fat
 76 tail in the direction of more ice loss.

77 Figure S1 shows variation in ensemble statistics as a function of changing grounding line flux nonlinearity, β . This plot
 78 shows that the skewness is zero or positive (towards slower retreat) when $\beta \leq 3$ and that skewness becomes increasingly
 79 negative as β increases above 3.

80 **Autocorrelated Forcing.** Moon & Wettlaufer (1) invoke the Martingale property to simplify their approach to stochastic
 81 perturbation analysis, via an appeal to the Fokker-Planck equation (see ??). The Martingale property assumes that the forcing
 82 is white noise, thus disallowing any autocorrelation in the forcing function. However, in reality, forcing from the ocean and
 83 atmosphere may be expected to have persistence at time scales longer than the forcing time step.

84 We can get a sense for the influence of autocorrelation in the time-dependent forcing function, by following the approach of
 85 Roe & Baker (7). For a first-order autoregressive discrete forcing process with autocorrelation coefficient $r = 1 - \Delta t/\tau_F$ (where
 86 τ_F is the decorrelation time scale), they derive a scaling for the expected spread of the prognostic variable (L in our case)

$$87 \quad \sigma_L = \sigma_L^{r=0} \left[\frac{1 - r^2}{(1 - r)^2} \right]^{\frac{1}{2}} \quad [14]$$

88 where $\sigma_L^{r=0}$ is the ensemble spread for white noise forcing, derived in the section above. Thus, in terms of τ_F , the ensemble
 89 spread is

$$90 \quad \sigma_L = \sigma_L^{r=0} \left[2 \frac{\tau}{\Delta t} - 1 \right]^{\frac{1}{2}}. \quad [15]$$

91 Strictly speaking, this added factor is derived for a stable auto-regressive model. However, it turns out to match numerically
 92 calculated values of σ_L for autocorrelated forcing (see Fig. 2 in the main text) sufficiently close to the initial steady-state
 93 condition, similarly to the linearized approximations for $\sigma_L^{r=0}$ calculated in section ?? which are good for some time after the
 94 onset of instability, and degrade after a sufficiently long period of unstable growth of the ensemble spread. However, it does not
 95 provide an analytical estimate for the skewness in the presence of autocorrelated forcing.

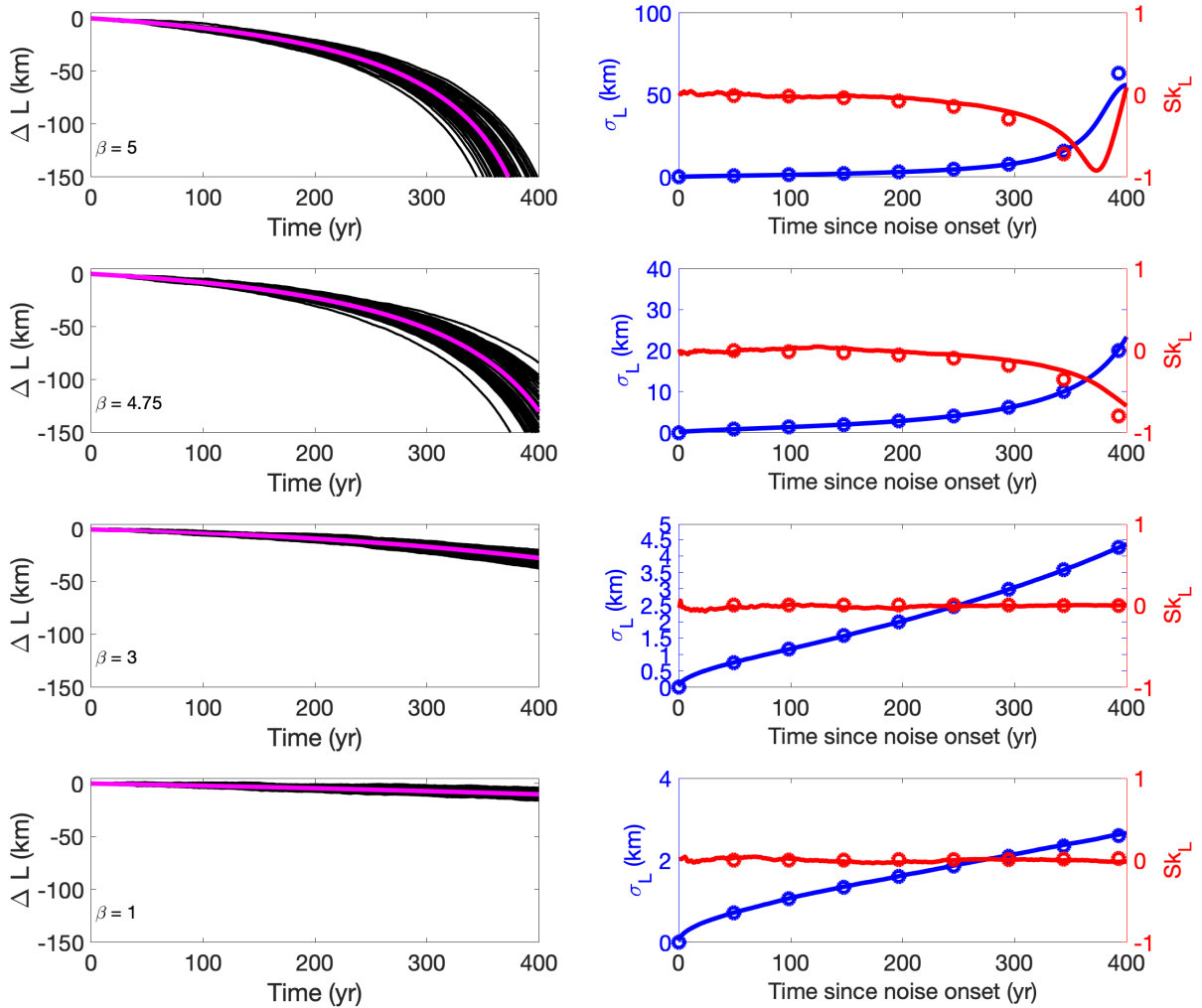


Fig. S1. Ensembles of grounding line retreat simulated with minimal prognostic model of grounding line migration (equation 1 in main text). In all simulations: $P = 0.35$ m/yr, $b_x = 3 \times 10^{-3}$. β and γ varied in each row to keep initial value of γh_g^β constant. (Left-side) Grounding line migration over different bed slopes. Black lines are 50 randomly-chosen ensemble members (out of 10000 used to calculate ensemble statistics). Magenta lines are simulations with $\eta = 0$. (Right-side) Ensemble statistics: standard deviation (blue), skewness (red, with more retreat being negative skew).

96 **Ocean Model Simulation.** The Massachusetts Institute of Technology general circulation model (MITgcm; (8)) was used to
97 simulate the evolution of oceanic conditions in the Amundsen Sea over the 1992-2007 period. The simulation includes a
98 thermodynamic sea ice model (9) and a representation of ocean induced melting and freezing parameterized as a diffusive flux
99 of temperature and salinity (10, 11). The model relies on a global configuration that is part of the Estimating the Circulation
100 and Climate of the Ocean, Phase II (ECCO2) project (12, 13). The model domain covers the Amundsen Sea Embayment,
101 from Abbott to Getz ice shelves, and extends at least 100 km beyond the outer edge of the continental shelf, similar to the
102 configuration in Seroussi et al. (14). The model grid is extracted from the 18 km Cube Sphere of Menemenlis et al. (12),
103 downscaled to a 2 km horizontal grid spacing, and includes 46 uneven vertical levels, which constrains the time steps to 115
104 s. The initial and boundary conditions are interpolated from the ECCO2 integration (15), and the atmospheric forcing is
105 constrained with the Japan Meteorological Agency and Central Research Institute of Electric Power Industry 25 year reanalysis
106 (16) over the 1992-2007 period. A constant turbulent exchange and friction velocity coefficients is applied for the exchange of
107 fresh water and heat at the ice shelf base (17), similar to Dinniman et al. (18), and Schodlok et al. (19, 20). Ice shelf cavities
108 do not evolve during the simulation as the objective of this simulation is to assess the variability in oceanic conditions in ice
109 shelf cavities, independently of changes happening over the ice sheet.

110 The dominant time scale of variability in the ocean model simulation is almost exactly one year, likely due to the dominance
111 of the annual cycle in the forcing. Longer time scales are not present due to the absence of ocean-atmosphere coupling which
112 tends to produce low-frequency modes of variability in fully coupled climate models in this region (21). We show the ensemble
113 statistics for Thwaites Glacier with ocean forcing persistent at $\tau_F = 13$ months in supplemental Fig. 2. The interannual
114 standard deviation of the maximum melt rate at depth is $\sigma_M = 1.4$ m/yr. However, it should be noted that calculations of
115 standard deviation from time series depend on the time step under consideration. The inter-monthly standard deviation is 5
116 m/yr.

117 Ice Sheet System Model (ISSM) Configuration

118 ISSM is a finite element software package which is used to solve the two-dimensional shelfy-stream approximation for this
119 study (22). It is publicly available for download from: <https://issm.jpl.nasa.gov/>. The model solves for ice velocity, surface and
120 base elevation, and grounding line position at each time step. In our simulations, basal friction follows a linear viscous law and
121 ice rigidity is a function of ice temperature, both are inverted on the basis of modern velocities (23) using data assimilation
122 (24). Ice temperature, basal friction and basin boundaries (covering the Thwaites Glacier catchment) are held fixed throughout
123 the simulation to reduce computational load and facilitate the large ensemble simulations. The horizontal resolution is 1 km
124 over the entire catchment basin. Grounding line position is determined by a floatation criterion: ice is floating if its thickness is
125 smaller than the floatation height and grounded otherwise. A minimum ice thickness is imposed to be 1 m everywhere, which
126 contributes negligibly to buttressing. We use a subelement parameterization in order to accurately capture the position of
127 the grounding line and integrate basal friction accurately over the grounded part of the domain(25). Sub-ice shelf basal melt
128 follows a simple function of depth: $M(z) = M_{max} - M_{max}(z_{max} - z)$, where M_{max} is the maximum melt rate that occurs at a
129 depth z_{max} . Melt is applied only to elements which are completely floating, which produces slower, but more rapidly-converged
130 (to a benchmark solution) retreat rates (26). Two week time steps are used for all simulations, though perturbations in M_{max}
131 are varied every month and renormalized to ensure that the standard deviation of monthly M_{max} is always 5 m/yr, regardless
132 of the long-term persistence. Bedrock elevation and initial surface elevation for the ice streams and ice shelves are derived
133 from a combination of Bedmap2 (27) and a mass conservation method (28). Surface mass balance and surface temperatures
134 averaged over the 1979-2010 period from RACMO2 (29) are applied at the surface of the domain, and the geothermal flux used
135 to compute the ice steady state temperature comes from Shapiro and Ritzwoller (30). Surface mass balance is held constant
136 during all simulations.

137 Extended Results of ISSM Ensembles

138 In this section, we provide full diagnostic results for each ISSM ensemble of Thwaites Glacier simulation in the same format as
139 Figure 3 in the main text. Each of these plots corresponds to one of the lines in Figure 4 of the main text, exploring how
140 ensemble statistics change as a function of forcing persistence and uncertainty in the time-average forcing.

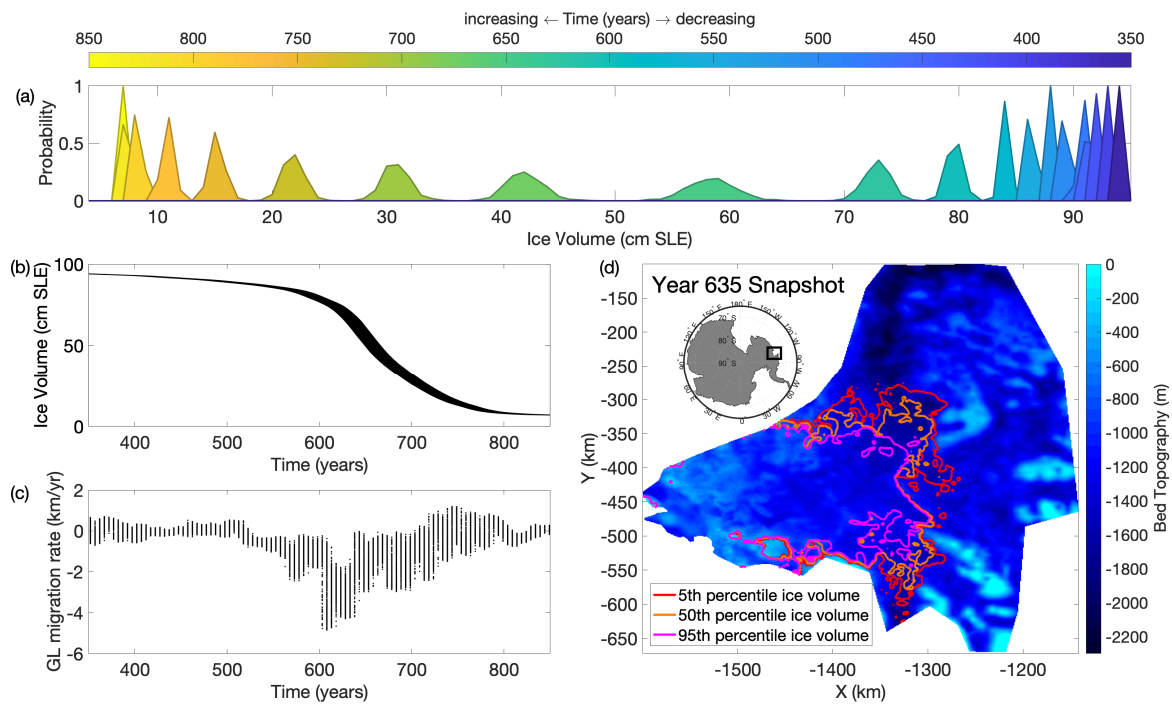


Fig. S2. Evolution of a 500-member ensemble of Ice Sheet System Model (ISSM) simulations of Thwaites glacier evolution over 500 years (where year zero in model time is the modern glacier state) in response to interannual variability ($\tau_F = 1.1$ yr) and constant average in maximum sub-ice shelf melt rate. (a) Evolution of ensemble probability distribution function (PDF) over time, plotted every 25 years, with probability on y-axis and Thwaites Glacier ice volume (in cm sea level equivalent; SLE) on x-axis. (b) Black lines are simulated ice volume contained in Thwaites Glacier catchment in cm SLE for all ensemble members. (c) Black dots are evolving grounding line migration rates for all ensemble members (based on the centroid of the 2D grounding line). (d) Snapshots (red, orange and pink lines) of grounding line positions at year 635 in model time, from 5th percentile, 50th percentile and 95th percentile ice volume ensemble members.

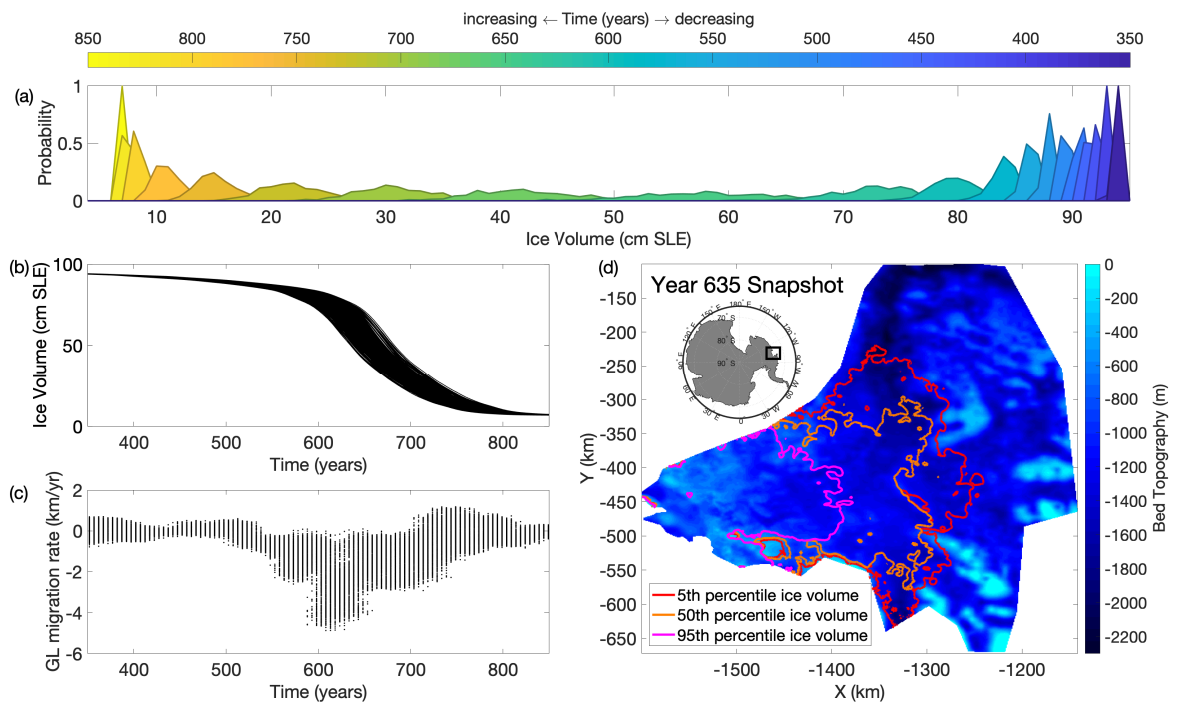


Fig. S3. Evolution of a 500-member ensemble of Ice Sheet System Model (ISSM) simulations of Thwaites glacier evolution over 500 years (where year zero in model time is the modern glacier state) in response to decadal variability ($\tau_F = 10$ yr) and constant average in maximum sub-ice shelf melt rate. (a) Evolution of ensemble probability distribution function (PDF) over time, plotted every 25 years, with probability on y-axis and Thwaites Glacier ice volume (in cm sea level equivalent; SLE) on x-axis. (b) Black lines are simulated ice volume contained in Thwaites Glacier catchment in cm SLE for all ensemble members. (c) Black dots are evolving grounding line migration rates for all ensemble members (based on the centroid of the 2D grounding line). (d) Snapshots (red, orange and pink lines) of grounding line positions at year 635 in model time, from 5th percentile, 50th percentile and 95th percentile ice volume ensemble members.

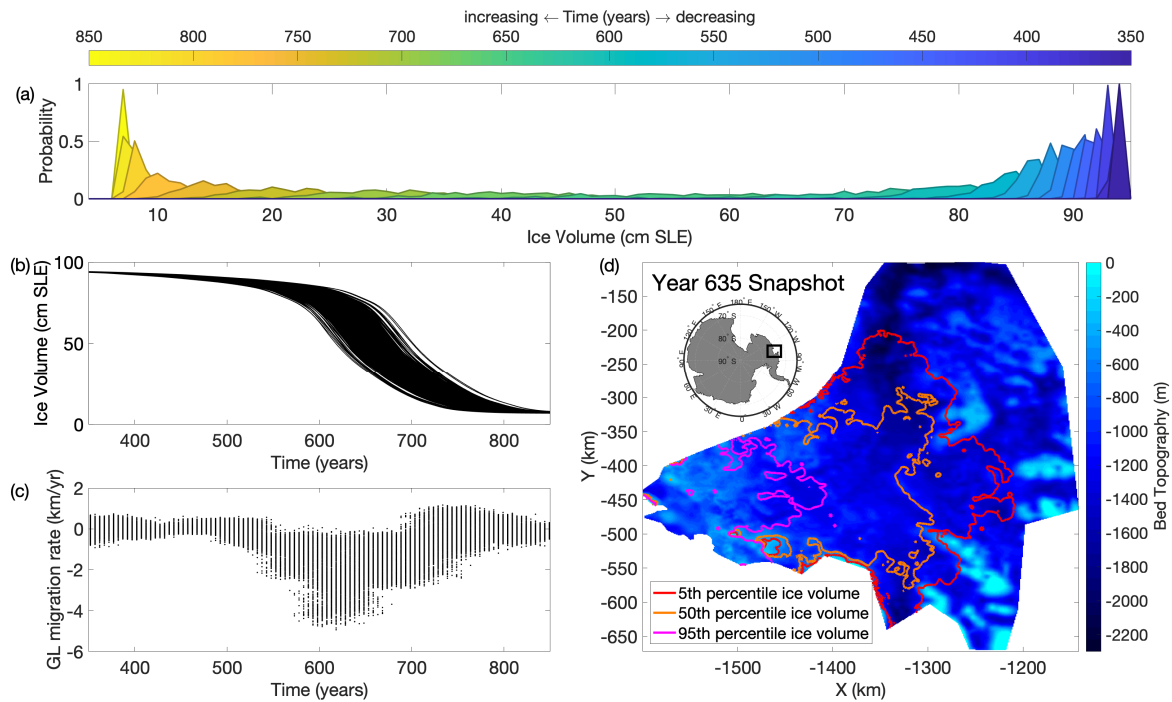


Fig. S4. Evolution of a 500-member ensemble of Ice Sheet System Model (ISSM) simulations of Thwaites glacier evolution over 500 years (where year zero in model time is the modern glacier state) in response to multidecadal variability ($\tau_F = 30$ yr) and constant average in maximum sub-ice shelf melt rate. (a) Evolution of ensemble probability distribution function (PDF) over time, plotted every 25 years, with probability on y-axis and Thwaites Glacier ice volume (in cm sea level equivalent; SLE) on x-axis. (b) Black lines are simulated ice volume contained in Thwaites Glacier catchment in cm SLE for all ensemble members. (c) Black dots are evolving grounding line migration rates for all ensemble members (based on the centroid of the 2D grounding line). (d) Snapshots (red, orange and pink lines) of grounding line positions at year 635 in model time, from 5th percentile, 50th percentile and 95th percentile ice volume ensemble members.

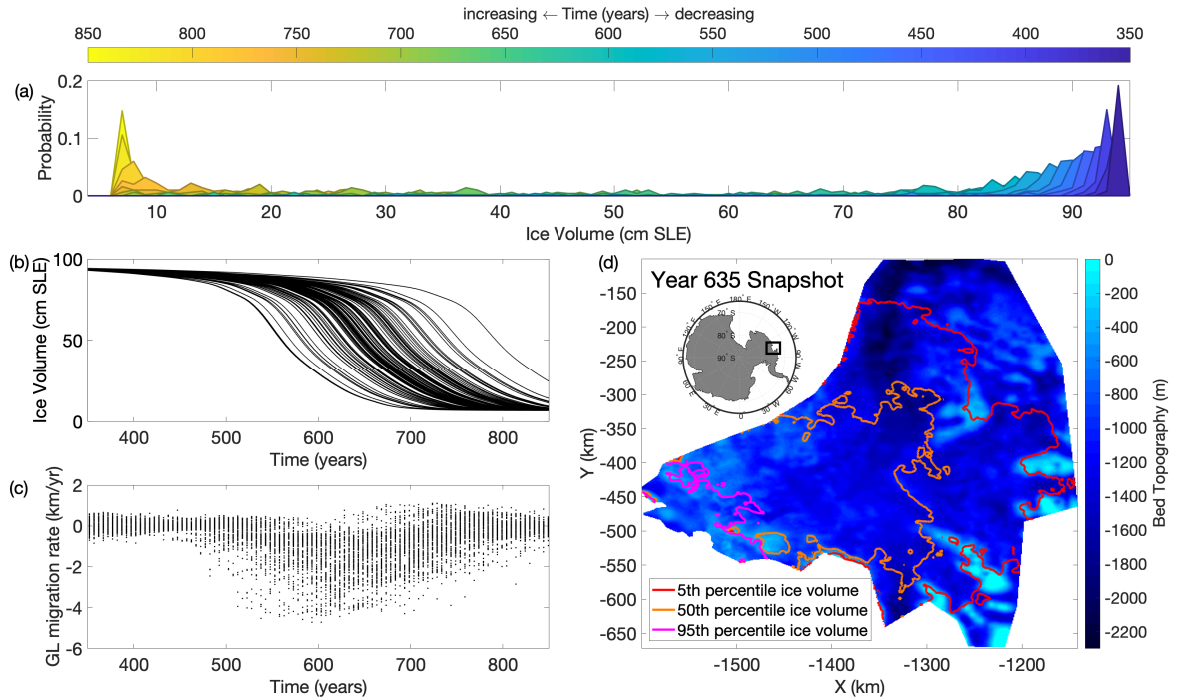


Fig. S5. Evolution of a 500-member ensemble of Ice Sheet System Model (ISSM) simulations of Thwaites glacier evolution over 500 years (where year zero in model time is the modern glacier state) in response to ocean forcing that is constant in time, but drawn from a Gaussian distribution for each individual ensemble member (mean 90 m/yr, standard deviation 5 m/yr). (a) Evolution of ensemble probability distribution function (PDF) over time, plotted every 25 years, with probability on y-axis and Thwaites Glacier ice volume (in cm sea level equivalent; SLE) on x-axis. (b) Black lines are simulated ice volume contained in Thwaites Glacier catchment in cm SLE for all ensemble members. (c) Black dots are evolving grounding line migration rates for all ensemble members (based on the centroid of the 2D grounding line). (d) Snapshots (red, orange and pink lines) of grounding line positions at year 635 in model time, from 5th percentile, 50th percentile and 95th percentile ice volume ensemble members.

141 Animations of ISSM Thwaites Glacier ensembles

142 **Movie S1.** Evolution of a 500-member ensemble of Ice Sheet System Model (ISSM) simulations of Thwaites
 143 glacier evolution over 500 years (where year zero in model time is the modern glacier state) in response to
 144 interannual variability ($\tau_F = 1.1$ yr) and constant average in maximum sub-ice shelf melt rate. Top left panel
 145 shows maximum melt rate (M_{max}) for a sample of 20 ensemble members. Top right panels shows evolving
 146 grounding line position for a sample of 20 ensemble members. Bottom panel shows the evolving probability
 147 distribution calculated from all ensemble members.

148 **Movie S2.** Evolution of a 500-member ensemble of Ice Sheet System Model (ISSM) simulations of Thwaites
 149 glacier evolution over 500 years (where year zero in model time is the modern glacier state) in response to
 150 interdecadal variability ($\tau_F = 10$ yr) and constant average in maximum sub-ice shelf melt rate. Top left panel
 151 shows maximum melt rate (M_{max}) for a sample of 20 ensemble members. Top right panels shows evolving
 152 grounding line position for a sample of 20 ensemble members. Bottom panel shows the evolving probability
 153 distribution calculated from all ensemble members.

154 **Movie S3.** Evolution of a 500-member ensemble of Ice Sheet System Model (ISSM) simulations of Thwaites
 155 glacier evolution over 500 years (where year zero in model time is the modern glacier state) in response to
 156 multidecadal variability ($\tau_F = 30$ yr) and constant average in maximum sub-ice shelf melt rate. Top left panel
 157 shows maximum melt rate (M_{max}) for a sample of 20 ensemble members. Top right panels shows evolving
 158 grounding line position for a sample of 20 ensemble members. Bottom panel shows the evolving probability
 159 distribution calculated from all ensemble members.

160 **Movie S4.** Evolution of a 500-member ensemble of Ice Sheet System Model (ISSM) simulations of Thwaites
 161 glacier evolution over 500 years (where year zero in model time is the modern glacier state) in response to
 162 ocean forcing that is constant in time, but drawn from a Gaussian distribution for each individual ensemble
 163 member (mean 90 m/yr, standard deviation 5 m/yr). Top left panel shows maximum melt rate (M_{max}) for a
 164 sample of 20 ensemble members. Top right panels shows evolving grounding line position for a sample of 20

165 ensemble members. Bottom panel shows the evolving probability distribution calculated from all ensemble
166 members.

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