Supporting Information

Seismic loading of fault-controlled fluid seepage systems by great subduction earthquakes

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I provide further information on the coseismic static stress changes and volumetric static strain produced by different source fault models available for the M_w~7.9-8.2 1944 Tonankai earthquake, the M_w7.7 1992 Nicaragua earthquake, the M_w~8.5-8.7 2005 Nias earthquake, and the M_w7.6 2012 Costa Rica earthquake. Normal ($\Delta\sigma_n$) and shear ($\Delta\tau$) stress changes compose the Coulomb Failure Function^{1,2,3,4,5,6}, Δ CFF, which is used to determine whether slip on a source fault promotes failure on surrounding receiver faults, and this happens when Δ CFF is positive (see section Methods in main text). Normal stress change patterns ($\Delta\sigma_n$) obtained for the Tonankai and Costa Rica earthquakes are shown in two figures (Figs. S1-S2) as supplement to the main article. Normal stress change ($\Delta\sigma_n$), shear stress change ($\Delta\tau$) and Coulomb stress changes (Δ CFF) have been calculated using different finite-fault rupture models (some of which available on the online SRCMOD database⁷). The values of static stress changes have been resolved on specific fault-controlled fluid pathways (thrust or normal faults), and are reported in three tables (Tables S1-S3) (see also main text).

Fig. S1



Figure S1. Normal stress changes ($\Delta \sigma_n$; bar, unclamping positive) produced by the M_w~7.9-8.2 1944 Tonankai earthquake considering different source fault models: (a) Satake⁸, (b) Kato & Ando⁹, (c) Tanioka & Satake¹⁰, (d) Ichinose *et al.*¹¹, (e) Kikuchi *et al.*¹² and (f) Baba *et al.*¹³. Normal stress changes in vertical cross sections are superposed onto the Nankai sedimentary wedge¹⁴, which is indicated by gray shading. A convenient range of stress change values (-5, 5 bar) has been arbitrarily chosen; note that in some models the calculated stresses may exceed this range. The thick white lines in sections indicate the seismogenic fault considered in the respective finite fault model. Note that the rupture fault is not captured in the cross section of panel (a), while in panel (b) it is intercepted only in the far lower right-hand side corner of the section. In horizontal sections stress is sampled at 7.5 km depth (dashed blue line in vertical cross sections). Symbols are as those in Fig. 2 of main text. This figure was generated using the Coulomb 3.4 software (https://earthquake.usgs.gov/research/software/coulomb) Adobe Illustrator CS3 and (https://www.adobe.com).



Figure S2. Normal stress changes ($\Delta \sigma_n$; bar, unclamping positive) produced by the M_w7.6 2012 Costa Rica earthquake considering different source fault models: (a) Hayes¹⁶, (b) Yue *et al.*¹⁷, and (c) Liu *et al.*¹⁸ (symbols are as those in Fig. 2 of main text). Small yellow circles indicate different types of seafloor methane seeps. Normal stress changes in vertical cross sections are superposed onto the Costa Rica sedimentary wedge^{19,20}, which is indicated by gray shading. A convenient range of stress change values (-5, 5 bar) has been arbitrarily chosen; note that in some models the calculated stresses may exceed this range. The thick white lines in sections indicate the seismogenic source considered in the respective finite fault model. In horizontal sections stress is sampled at 5 km depth (dashed blue line in vertical cross sections). This figure was generated using the Coulomb 3.4 software (https://earthquake.usgs.gov/research/software/coulomb) and Adobe Illustrator CS3 (https://www.adobe.com).

Fig. S2

Table S1. Static stress changes and static strain calculated from available source models of the 1944Tonankai earthquake, as well as the $M_w7.2$ and $M_w7.4$ earthquakes of 05 September 2004. Normalstress change $\Delta\sigma_n$ (plain text), shear stress change $\Delta\tau$ (in parenthesis) and Coulomb Failure Function ΔCFF (bold) are sampled at various depths on a thrust fault (strike 225°, dip 40°, rake 90°)connecting MV#5 to the basal thrust décollement. For static strain, + indicates volumetric expansion,and – volumetric contraction. Source faults of 2004 earthquakes are based on focal mechanismsolutionsusing using the transformUSGS(https://earthquake.usgs.gov/earthquakes/eventpage/usp000d3ka/executive;

https://earthquake.usgs.gov/earthquakes/eventpage/usp000d3mb/executive), with fault dimensions following the relationships of Wells and Coppersmith²¹.

$M_{w} \sim 7.9-8.2$ 1944 Tonankai earthquake							
Along thrust depth	Satake ⁸	Kato & Ando ⁹	Tanioka &	Ichinose et al. ¹¹	Kikuchi et al. ¹²	Baba <i>et al</i> . ¹³	
depth; Lat; Long			Satake ¹⁰				
1.9 km; N33.676;	0.65 (-0.88) bar	1.51 (-1.92) bar	3.36 (-5.23) bar	1.53 (-1.92) bar	1.37 (-1.16) bar	2.97 (-0.48) bar	
E136.563	-0.62 bar	-1.31 bar	-3.88 bar	-1.31 bar	-0.61 bar	0.71 bar	
5 km; N33.702;	0.76 (-0.97) bar	1.40 (-1.70) bar	3.31 (-3.31) bar	1.27 (-1.77) bar	2.26 (-1.37) bar	10.98 (-4.02) bar	
E136.538	-0.67 bar	-1.14 bar	-1.98 bar	-1.26 bar	-0.47 bar	0.19 bar	
12 km; N33.755;	1.79 (-1.18) bar	1.65 (-0.99) bar	11.94 (-4.69) bar	0.82 (-1.12) bar	3.17 (-4.74) bar	26.26 (-18.1) bar	
E136.475	-0.46 bar	-0.33 bar	0.08 bar	-0.79 bar	-3.48 bar	-7.58 bar	
15 km; N33.781;	2.37 (-1.31) bar	1.69 (-0.73) bar	5.84 (-9.37) bar	0.92 (-0.78) bar	4.29 (-6.61) bar	38.52 (20.18) bar	
E136.452	-0.36 bar	-0.06 bar	-7.03 bar	-0.41 bar	-4.90 bar	35.59 bar	
Static strain	$+0.5\ 10^{-5}$	$+0.5\ 10^{-5}$	$+10^{-5}$	$+0.5\ 10^{-5}$	-10^{-5}	$+10^{-5}$	
$M_w7.2$ and $M_w7.4$ 2004 earthquakes							
Along thrust depth	M _w 7.2 - USGS	M _w 7.4 - USGS	Cumulated	—	—	-	
depth; Lat; Long	2004.09.05	2004.09.05	sources				
	10:07:07 UTC	14:57:18 UTC					
1.9 km; N33.676;	0.02 (0.02) bar	0.15 (-0.09) bar	0.16 (-0.04) bar	—	—	-	
E136.563	0.02 bar	-0.03 bar	0.02 bar				
5 km; N33.702;	0.08 (-0.04) bar	0.33 (-0.24) bar	0.42 (-0.26) bar	—	—	-	
E136.538	0.00 bar	-0.11 bar	-0.10 bar				
12 km; N33.755;	0.14 (-0.12) bar	0.39 (-0.39) bar	0.55 (-0.53) bar	—	—	-	
E136.475	-0.07 bar	-0.24 bar	-0.31 bar				
15 km; N33.781;	0.13 (-0.14) bar	0.35 (-0.40) bar	0.50 (-0.56) bar	-	-	-	
E136.452	-0.09 bar	-0.26 bar	-0.36ar				

Table S2. Static stress changes and static strain imparted by the $M_w7.6$ Costa Rica and $M_w7.7$ 1992 Nicaragua earthquakes. Normal stress change $\Delta\sigma_n$ (plain text), shear stress change $\Delta\tau$ (in parenthesis) and Coulomb Failure Function Δ CFF (bold) are sampled on normal faults controlling specific mound structures located along section AB (Fig. 3b of main text) and CD (Fig. 3c of main text), respectively. Stress changes are calculated from available source models, and sampled at the sea bottom, 5 km depth, and near the basal thrust décollement considering a fault with strike 132°, dip 60°, and rake - 90°. Shear stress change and Coulomb Failure Function are indicated in parenthesis and in bold, respectively. For static strain, + indicates volumetric expansion, and – volumetric contraction.

M_w 7.6 2012 Costa Rica earthquake					
Mound	Haves ¹⁶	Yue <i>et al.</i> ¹⁷	Liu <i>et al</i> . ¹⁸		
Lat; Long; depth	5				
M#1					
N9.708: W86.074: 3.2 km	-4.50 (-0.97) bar	6.77 (19.20) bar	0.55 (-1.01) bar		
	-2.77 bar	21 91 har	-0 79 har		
N9 703: W86 073: 5 km	0.41(2.00) bar	3358(517) bar	1.43(0.01) bar		
119.705, W00.075, 5 Km	2 16 har	18 60 bar	0.58 bar		
M#2	2.10 Dai	18.00 Dai	0.38 Dai		
101#2	0.18(0.42) has	1.15(1.12) here	10.01(2.66) here		
N9.785; W80.074; 2.7 Km	0.18 (0.43) bar	1.15 (1.15) bar	10.01 (2.00) bar		
NO 554 MICC 001 51	-0.50 bar	1.59 bar	6.66 bar		
N9.774; W86.081; 5 km	1.4/(-4.41) bar	4.46 (-1.21) bar	4.15(3.51) bar		
	-3.83 bar	0.58 bar	5.17 bar		
N9.765; W86.084; 7 km	6.61 (1.55) bar	-0.56 (-6.81) bar	2.79 (2.82) bar		
	4.19 bar	-7.04 bar	3.93 bar		
M#3					
N9.967; W86.012; 1.2 km	1.39 (1.09) bar	-1.94 (-1.36) bar	-1.21 (-0.87) bar		
	1.64 bar	-2.13 bar	-1.35 bar		
N9.953; W86.023; 5 km	-0.67 (-0.15) bar	-1.51 (-1.84) bar	-1.62 (-0.32) bar		
	-0.42 bar	-2.45 bar	-1.35 bar		
N9.934: W86.039: 10 km	3.68(-2.07) bar	2.10(-1.93) bar	2.62(-0.41) bar		
10.000 i, 000.000, 10 km	-0.60 bar	-1.09 bar	0.64 bar		
Static strain	$+10^{-5}$	$+10^{-6}$	$-0.5 \ 10^{-5}$		
	M 7 7 1002 Missurger	+10	0.5 10		
Manual	M _w /./ 1992 Nicaragua	и еантариаке			
Mound	Hayes	—	—		
Lat; Long; depth					
M#4		—	—		
N11.185; W87.200; 1.5 km	15.87 (8.26) bar				
	14.60 bar				
N11.172; W87.212; 5 km	19.87 (7.73) bar	—	—		
	15.68 bar				
N11.160; W87.223; 8 km	32.03 (52.04) bar				
	64.86 bar				
M#5		_	_		
N11.203: W87.156: 1.2 km	11.16 (5.42) bar				
	9.88 har				
N11 189 W87 168 5 km	1946(652) bar				
	14 30 bar				
N11 176: W87 175: 0 km	7.00(9.50) bar				
N11.170, W07.175, 7 Km	12 30 hav				
<u>М#(</u>	12.30 Dai				
N11 220, XV97 122, 0.01	7.02 (4.97) 1	_	_		
N11.239; W87.133; 0.9 km	/.93 (4.8/) bar				
	8.04 bar				
N11.223; W87.144; 5 km	11.44 (3.63) bar				
	8.51 bar				
N11.203; W87.163; 10 km	42.84 (44.78) bar	-	—		
	61.92 bar				
Static strain	$+10^{-5}$	-	-		

Table S3. Static stress changes and static strain imparted by the $M_w 8.5$ -8.7 2005 Nias earthquake. Normal stress change $\Delta \sigma_n$ (plain text), shear stress change $\Delta \tau$ (in parenthesis) and Coulomb Failure Function ΔCFF (bold) are sampled on thrust faults controlling specific seepage structures. Seepage structures consist of mud volcanoes (MV) and mud diapirs (MD) exposed on Nias and Simeulue islands^{23,24}, as well as an offshore methane cold seep systems exhibiting extensive buildups of authigenic carbonate deposits²⁵ (MS). Stress changes are calculated from available source models, and sampled at surface (or at sea floor) and at depth near the basal subduction thrust considering a fault with strike 325°, dip 40°, and rake 90°. The basal subduction thrust has been speculatively assumed as that of Singh *et al.*²⁶. The latter shows, however, some difference with the geometry of source faults used in the different finite fault models (see Fig. 4 of main text). For this reason, stress changes have also been calculated near the intersection with the source fault of each finite fault model. Static strain (+ indicates volumetric expansion, and – volumetric contraction) is estimated beneath the seepage structures situated along section AB in Figure 4 of main text.

$M_w 8.5 - 8.7 2005$ Nias earthquake						
Mud volcano/diapir/seep	Shao & Ji ²⁷	Konca <i>et al.</i> ²⁸	Yatimantoro &	Hayes ³⁰		
Lat; Long; depth			Tanioka ²⁹			
MV#1 Nias Island						
N1.435; E97.456; 0 km	6.59 (-7.85) bar	1.56 (-1.86) bar	4.65 (-5.54) bar	1.52 (-1.81) bar		
	-5.22 bar	-1.24 bar	-3.68 bar	-1.20 bar		
N1.478; E97.488; 5 km	10.73 (-12.38) bar	6.21 (-5.86) bar	7.98 (-8.66) bar	0.65 (-1.21) bar		
	-8.08 bar	-3.38 bar	-5.47 bar	-0.95 bar		
N1.524; E97.518; 10 km	9.03 (-15.80) bar	13.43 (-10.50) bar	17.12(-13.80) bar	1.99 (-2.48) bar		
	-12.19 bar	-5.13 bar	-6.95 bar	-1.69 bar		
N1.565; E97.548; 15 km	4.40 (-10.85) bar	19.29 (-15.57) bar	36.71 (-13.13) bar	1.38 (-4.41) bar		
	-9.09 bar	-7.85 bar	1.55 bar	-3.86 bar		
N1.610; E97.579; 20 km	7.89 (-8.97) bar	22.04 (-17.21) bar	79.10 (-25.21) bar	-0.92 (-3.56) bar		
	-5.81 bar	-8.39 bar	6.42 bar	-3.93 bar		
Near model source fault	-29.20 (12.05) bar	13.54 (-15.84) bar	-4.72 (0.44) bar	-16.02 (5.06) bar		
	0.36 bar	-10.43 bar	-1.45 bar	-1.35 bar		
MV#2 Nias Island						
N1.357; E97.542; 0 km	8.17 (-9.74) bar	0.41 (-0.49) bar	6.32 (-7.53) bar	0.35 (-0.42) bar		
	-6.47 bar	-0.33 bar	-5.00 bar	-0.28 bar		
N1.401; E97.574; 5 km	11.51 (-14.46) bar	3.52 (-4.05) bar	7.38 (-8.43) bar	-0.13 (-0.36) bar		
	-9.85 bar	-2.65 bar	-5.48 bar	-0.41 bar		
N1.445; E97.605; 10 km	11.97 (-16.30) bar	6.97 (-8.04) bar	20.86 (-10.40) bar	4.09 (-2.00)bar		
	-11.51 bar	-5.25 bar	-2.05 bar	-0.36 bar		
N1.488; E97.635; 15 km	16.18 (-12.09) bar	9.58 (-11.36) bar	49.76 (-11.84) bar	8.25 (-4.13) bar		
	-5.61 bar	-7.53 bar	8.06 bar	-0.83 bar		
N1.531; E97.665; 20 km	6.22 (-17.64) bar	13.37 (-12.91) bar	52.14 (-38.54) bar	11.30 (-4.92) bar		
	-15.15 bar	-7.56 bar	-17.68 bar	-0.40 bar		
Near model source fault	-40.97 (25.04) bar	6.76 (-12.74) bar	6.11 (-5.73) bar	-18.10 (0.88) bar		
	8.65 bar	-10.03 bar	-3.29 bar	-6.37 bar		
MD#1 Nias Island						
N1.236; E97.389; 0 km	10.91 (-13.00) bar	4.83 (-5.75) bar	5.30 (-6.31) bar	8.94 (-10.66) bar		
	-8.64 bar	-3.82 bar	-4.19 bar	-7.08 bar		
N1.262; E97.436; 5 km	13.22 (-16.17) bar	0.89 (-2.80) bar	8.57 (-3.872) bar	0.59 (-4.42) bar		
	-10.88 bar	-2.44 bar	-0.44 bar	-4.18 bar		
N1.299; E97.472; 10 km	14.95 (-20.22) bar	3.07 (-3.53) bar	20.46 (-8.16) bar	-2.90 (-1.18) bar		
	-14.24 bar	-2.31 bar	0.02 bar	-2.34 bar		
N1.338; E97.511; 15 km	34.01 (-20.26) bar	6.92 (-8.51) bar	35.48 (-18.65) bar	2.22 (-0.77) bar		
	-6.65 bar	-5.74 bar	-4.46 bar	0.12 bar		
N1.376; E97.549; 20 km	30.72 (-47.30) bar	8.58 (-12.37) bar	52.55 (-34.24) bar	11.75 (-5.14) bar		
	-35.01 bar	-8.94 bar	-13.22 bar	-0.44 bar		
Near model source fault	-120.17 (67.78) bar	11.05 (-28.24) bar	111.04 (-41.03) bar	24.46 (-16.63) bar		
	19.71 bar	-23.82 bar	3.38 bar	-6.85 bar		
MD#2 Nias Island						
N1.052; E97.572; 0 km	9.26 (-11.03) bar	-1.73 (2.07) bar	3.77 (-4.49) bar	9.25 (-11.03) bar		
	-7.33 bar	1.37 bar	-2.98 bar	-7.33 bar		

N1.090; E97.609; 5 km	13.60 (-13.97) bar	-2.55 (2.25) bar	1.84 (-3.11) bar	-0.86 (-3.61) bar
	-8.53 bar	1.23 bar	-2.38 bar	-3.96 bar
N1.129; E97.645; 10 km	25.93 (-19.99) bar	2.91 (-0.63) bar	-1.62 (-2.13) bar	-2.79 (-0.61) bar
	-9.62 bar	0.54 bar	-2.78 bar	-1.72 bar
N1.167: E 97.685: 15 km	38.52 (-38.57) bar	8.24 (-4.24) bar	-4.86 (-2.83) bar	4.52 (-1.95) bar
	-23.17 bar	-0.95 har	-4.77 har	-0.15 har
N1 207 · E97 720 · 20 km	30.91(-52.94) bar	1452(-735) bar	-7.09(-5.65) bar	17.03(-8.52) bar
111.207, E97.720, 20 Mil	-40 58 bar	-1 54 bar	-8 49 har	-1 71 har
Near model source fault	-160.41(-7.74) bar	0.58 (-10.08) bar	39.24(-51.88) har	107.96(-82.14) bar
ited model source hunt	-71 90 bar	-9 85 har	-36 19 har	-38 96 har
MS#1 offshore	-71.70 Dai	-7.05 Dai	-50.17 Dai	-50.70 bai
N2 562: E06 757: 1.4 $l_{\rm rm}$	1.22(1.20) her	212(256) her	0.27 (0.78) have	1.72(1.28) her
N2.303, E90.757, 1.4 KIII	-1.25 (1.59) bai	5.12 (-2.50) Dai	0.27 (0.78) bai	-1.72 (1.20) Dai
NO 590, EOC 799, 5 1	0.90 Dar	-1.51 Dar	0.09 Dar	0.59 Dar
N2.389; E90.788; 5 KIII	-0.10 (2.14) bar	0.38 (-3.00) bar	4.2/(-0.75) bar	0.02(0.23) bar
NO (10 EQ(022 101	2.10 bar	-2.51 Dar	0.98 Dar	U.20Dar
N2.018; E90.833; 10 km	2.65 (2.05) bar	0.08 (-0.40) bar	8.10(-1.58) bar	0.30 (-2.85) bar
NO (4(FO(970 151	3.11 Dar	-4.03 bar	1.68 Dar	-0.20 bar
N2.646; E96.879; 15 Km	2.07 (1.22) bar	2.37(-5.94) bar	9.22 (-2.20) bar	12.91 (-6.99) bar
	2.05 bar	-4.99 bar	1.49 bar	-1.83 bar
N2.679; E96.922; 20 km	11.72 (3.18) bar	-1.49 (-3.70) bar	4.90 (-2.92) bar	15.09 (-11.13) bar
	7.87 bar	-4.30 bar	-0.96 bar	-5.10 bar
Near model source fault	-24.91 (34.15) bar	-4.33 (1.26) bar	13.11 (-5.93) bar	-0.37 (-0 .91) bar
	24.19 bar	-0.47 bar	-0.69 bar	-1.06 bar
MV#3 Simeulue Island				
N2.370; E96.403; 0 km	-0.89 (1.06) bar	11.45 (-13.65) bar	-7.88 (9.39) bar	-2.50 (2.98) bar
	0.71 bar	-9.01 bar	6.24 bar	1.98 bar
N2.413; E96.434; 5 km	0.15 (-1.15) bar	0.25 (-6.34) bar	0.12 (5.98) bar	9.07 (-2.31) bar
	-1.09 bar	-6.24 bar	6.03 bar	1.32 bar
N2.458; E96.467; 10 km	-4.14 (-2.01) bar	6.26 (-5.94) bar	2.15 (4.40)bar	6.23 (-3.32) bar
	-3.67 bar	-3.44 bar	5.26 bar	-0.83 bar
N2.500; E96.497; 15 km	-6.56 (2.49) bar	23.04 (-21.13) bar	-10.84 (0.83) bar	-4.82 (-1.70) bar
	-0.13 bar	-11.91 bar	-3.50 bar	-3.63 bar
N2.546; E96.529; 20 km	-12.62 (3.63) bar	16.97 (-33.75) bar	18.61 (2.21) bar	-12.46 (5.66) bar
	-1.42 bar	-26.96 bar	9.65 bar	0.67 bar
Near model source fault	-7.56 (-0.45) bar	-15.79 (-37.71) bar	13.07 (-7.10) bar	34.54 (-3.98) bar
	-3.47 bar	-44.03 bar	-1.88 bar	9.84 bar
MV#4 Simeulue Island				
N2.397; E96.371; 0 km	-0.96 (1.14) bar	13.27 (-15.68) bar	-8.37 (9.98) bar	-4.15 (4.95) bar
	0.76 bar	-10.51 bar	6.63 bar	3.29 bar
N2.447: E96.389: 5 km	3.01 (-1.78) bar	-0.91 (-7.59) bar	-0.97 (6.57) bar	8.92 (-0.68) bar
	-0.58 bar	-7.96 bar	6.19 bar	2.89 har
N2.495: E96.406: 10 km	0.95(-4.63) bar	1.94(-4.84) bar	2.29(6.34) bar	9.61 (-1.57) bar
1.2.1.90, 1.901100, 10 1111	-4 25 har	-4 07 har	7 26 har	2 27 har
N2 548· F96 425· 15 km	-5 51 (-1 86) bar	38.76(-16.11) bar	0.14(7.61) bar	-0.04(2.34) bar
1.2.0 10, 1200 120, 10 km	-4 06 har	-0 61 har	7 67 har	2.32 har
N 2 588 · F96 438 · 20 km	-6.08(-0.02) bar	57 36 (-56 51) her	-9254(015) bar	-12.92 (9.93) her
1, 2.500, 190, 490, 20 Kill	-0.00 (-0.02) bar	-33 56 har	-36 87 har	4 76 har
Near model source fault	-2.70 Dai _7 35 (_0 21) bar	-33.30 Dai _9 54 (_53 40) hor	-50.07 Dai 11 59 (_7 67) har	35 03 (-17 50) bor
itea model source fault	-7.55 (-0.21) 0d1	-5.57 (-55.77) Dai	-3 03 hor	_3 10 hor
Static strain	-5.15 Dal +10 ⁻⁵	$\pm 0.5 \ 10^{-5}$	$+0.5 10^{-5}$	$\pm 0.5 \ 10^{-5}$
	110	10.0 10	10.3 10	10.5 10

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