# Supporting Information: Mixed-Matrix Membranes Formed from Imide-Functionalized UiO-66-NH<sup>2</sup> for Improved Interfacial Compatibility

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**Section A: Supporting characterization results for the Pure MOF and PSM-MOF**

Figure S1. TEM images of oligomer-coated UiO-66-NH<sup>2</sup> under different magnifications. MOF core and oligomer shell are labeled in the left top image. Different surface structures can be observed between these PSM-MOF structures and the pure-MOF structures, as shown in Figure 2.



Figure S2. Pore size distribution and  $N_2$  adsorption isotherms for Pure MOF and PSM-MOF. Pore size distribution was calculated using the built-in function of Micromeritics 3Flex Share software based on N2@Tarazona NLDFT Model.



Figure S3. <sup>1</sup>H NMR spectra change upon 6FDA-Durene oligomer PSM of UiO-66-NH2. Peaks were assigned according to the literature<sup>10</sup>. Unassigned peaks may result from coupling and exchange effects from HF and 6FDA-Durene oligomer.

**Section B: Supporting characterization results for the MMMs and upper bound plots**



Figure S4. Cross-sectional FESEM (left) and FIB-SEM (right) images of 10% Pure MOF MMM. Both images show more serious particle aggregation than for the PSM-MOF MMMs.



Figure S5.  $H_2/CH_4$  and  $H_2/O_2$  upper bound plots (blue circles: experimental data; pink stars: Maxwell Model predictions)

<b>MOF</b>	<b>Loading</b> $(wt\%)$	<b>Polymer</b>	<b>Pressure</b> (bar)	$CO2$ permeability (Barrer)	<b>Selectivity</b> CO <sub>2</sub> /CH <sub>4</sub>	Ref.
6FDA-Durene/ UiO- $66-NH2$	40	6FDA-Durene		1890	17.7	This work
$NH2-UiO-66-ABA$	30	Matrimid <sup>®</sup>	9	37.9	47.7	Vankelecom. 2015 <sup>1</sup>
$UiO-66-NH2$	30	PAO-PIM-1	N.A.	8126	18.4	Jin, $2017^2$
$UiO-66-NH2$	20	PIM-1 (in-situ crosslinking)	$\overline{2}$	15815	19.1	Kaliaguine, $2018^3$
PEG@UiO-66-NH <sub>2</sub>	40	$PEBAX^{\circledR}$	3	425	56	Qiao, $20174$

Table S1. CO<sub>2</sub>/CH<sub>4</sub> separation data for MOF-based MMMs from the literature



Figure S6. Derivative Thermal Gravimetric Analysis of the oligomer, Pure-MOF and PSM-MOF. Different stages of weight loss can be observed for the oligomer and the Pure-MOF.



Figure S7. CO<sub>2</sub>/CH<sub>4</sub> upper bound plot with comparative literature data for 6FDA-Durene (black circle: experimental data for 6FDA-Durene; blue circles: experimental data for PSM-MOF MMM; pink stars: Maxwell Model predictions; red circles: experimental data for Pure MOF MMM; black squares: literature data for 6FDA-Durene<sup>6-9</sup>). The difference in reported transport properties for 6FDA-Durene relates to differences in casting conditions and the temperature/pressure at which data were obtained.



Figure S8. Cross-sectional SEM images of 40% PSM-MOF MMM taken near the top surface (left) and bottom surface (right).



Table S2. Permeation results for independently prepared samples of 6FDA-Durene and corresponding MMMs to evaluate reproducibility.

Table S3. Permeation results for Pure MOF MMMs

<b>Loading</b>	<b>Permeability (Barrer)</b>	<b>Selectivity</b>	
$(wt\%)$	CH <sub>4</sub>	CO <sub>2</sub>	CO <sub>2</sub> /CH <sub>4</sub>
15%	132	1990	15.1
30%	226	3260	14.4



Figure S9. CO<sub>2</sub> and CH<sub>4</sub> sorption isotherms for 6FDA-Durene and corresponding MMMs.



Figure S10. Physical aging of 6FDA-Durene and corresponding MMMs shown in CO<sub>2</sub>/CH<sub>4</sub> upper bound plot (left) and normalized helium permeability plot (right). The number indicates the week number of a specific test. PIM-1 aging data was added as a reference.

# **Section C: Using the Maxwell model to predict transport in MMMs and volume fraction calculation**

#### *C1. Gas transport prediction using the Maxwell Model*

Experimental data  $(P_{MMM})$  at low loadings (below 20 wt%) were first used to calculate pure MOF permeability  $(P_f)$  for each gas. These values  $(P_{MMM}$  at loadings below 20 wt% and  $P_f$ ) were then used together with the pure polymer permeability  $(P_p)$  to predict MMM permeabilities at all loadings. Volume fractions of MOF loading were calculated as described in section C2.

## *C2. Volume fraction calculation*

TGA with an air sweep flow was used to determine the weight fraction of MOF fillers in MMMs. TGA profiles show that 6FDA-Durene decomposes completely under air flow at 700 °C (weight loss  $= 100\%$ ). Therefore, equation (1) was used to calculate the weight fraction of the MOF in the MMM:

$$
MOF loading (wt\%) = \frac{wt\% remained of MMM at 700 °C}{wt\% remained of pure MOF at 700 °C}
$$
 (1)

To convert weight fraction to volume fraction, densities of the pure MOF and MMM are required. A crystal density of 1.36 g cm<sup>−</sup><sup>3</sup> for the pure UiO-66-NH<sup>2</sup> was taken from Mason *et al.*<sup>5</sup> Density of MMMs can be measured using a density kit attached to a Mettler Toledo mass balance (30029886). Equation (2) was then used to convert weight fraction to volume fraction:

$$
MOF loading (vol\%) = \frac{MOF loading (wt\%)}{\rho_{MOF}} \rho_{MMM}
$$
 (2)

where,  $\rho_{MOF}$  and  $\rho_{MMM}$  are the densities of the MOF and MMM, respectively.

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