



Article

## Supplementary Materials: A Facile Synthesis of (PIM-Polyimide)-(6FDA-Durene-Polyimide) Copolymer as Novel Polymer Membranes for CO<sub>2</sub> Separation

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## S-1. Materials

4,4'-(Hexafluoroisopropylidene) di-phthalic anhydride (6FDA), 2,3,5,6-tetramethyl benzene-1,4-diamine (durene), and 4,5-dichloro phthalonitrile (98%), were purchased from Tokyo Chemical Industry (TCI) Co. Ltd. (Tokyo, Japan) and were used as obtained. 5,5',6,6'-Tetrahydroxy-3,3,3',3'-tetramethyl-1,10-spirobisindane (97%) was obtained from Alfa Aesar. Acetic anhydride, toluene, and triethylamine were obtained from Sigma Aldrich. Methanol, ethanol, dimethylformamide, dimethylacetamide, potassium carbonate, and potassium hydroxide were purchased from DaeJung Chemicals & Metals Co. Ltd. in South Korea. 6FDA, durene, and K<sub>2</sub>CO<sub>3</sub> were dried under a vacuum at 60 °C for 24 h prior to use. Anhydride monomer of PIM (An) was synthesized following the literature method [22]. All chemicals, unless otherwise noted, were obtained from commercial sources and were used as received.

## S-2. Characterization and Measurements

The <sup>1</sup>H NMR spectra were obtained on an Agilent 400-MR (400 MHz) instrument using  $d_6$ -DMSO or CDCl<sub>3</sub> as a reference or an internal deuterium lock.

The attenuated total reflection Fourier transform infrared (ATR-FTIR) spectra were recorded using a Bruker Vertex 80v Hyperion 2000 ATR-FTIR spectrometer.

Molar masses were determined by gel permeation chromatography (GPC) using two PL Gel 30 cm  $\times$  5  $\mu$ m mixed C columns at 30 °C running in DMF and calibrated against polystyrene ( $M_n$  = 600×106 gmol<sup>-1</sup>) standards using a Knauer refractive index detector.

The thermal stability of the membranes was analyzed by thermogravimetric analysis (TGA) measurements conducted on a Shimadzu TGA-2950 instrument at a heating rate of 10  $^{\circ}$ C min<sup>-1</sup> under a nitrogen flow.

The tensile properties were measured on a Shimadzu EZ-TEST E2-L instrument benchtop tensile tester using a crosshead speed of 5 mm.min $^{-1}$  at 25  $^{\circ}$ C under 50% relative humidity. The engineering stress was calculated from the initial cross-sectional area of the sample and Young's modulus (E) was determined from the initial slope of the stress-strain curve. The membrane samples were cut into rectangular shapes 40 mm  $\times$  10 mm (total) and 20 mm  $\times$  10 mm (test area) in size.

The densities of the membranes (g.cm<sup>-3</sup>) were determined experimentally using a top-loading electronic Mettler Toledo balance (XP205, Mettler-Toledo, Switzerland) coupled with a density kit based on the Archimedes principle. The samples were weighed in air and in a known-density liquid, high-purity heptane. The measurements were performed at room temperature using the buoyancy method, and the density was calculated as follows:

$$\rho_{polymer} = \frac{W_0}{W_0 - W_1} \cdot \rho_{liquid} \tag{S1}$$

where  $W_0$  and  $W_1$  are the membrane weights in air and in heptane respectively. Heptane sorption of the membranes was not considered due to their extremely low absorption properties.

The X-ray diffraction patterns of the membranes were measured using a Rigaku DMAX-2200H diffractometer operated at a scanning rate of  $4^{\circ}$  min<sup>-1</sup> in a  $2\theta$  range from  $5^{\circ}$  to  $30^{\circ}$  with Cu K $\alpha$ 1 X-ray radiation ( $\lambda$  = 0.1540598). The d-spacings were calculated using Bragg's law (d =  $\lambda$ /2sin $\theta$ ).

Tapping-mode AFM was conducted using a Bruker MultiMode instrument. A silicone cantilever with an end radius of <10 nm and a force constant of 40 Nm<sup>-1</sup> (NCHR, nanosensors, f=300 kHz) was used to image the samples at an ambient temperature.

## S-3. Gas Permeation Procedure

Permeation measurements of pure gas were taken using a high-vacuum time-lag measurement unit based on a constant-volume/variable-pressure method. All of the experiments were performed at a feed pressure of 2 bar (except for the pressure effect experiments which were carried out in the range of 100 mbar to 2 bar feed pressure) and a feed temperature of 30 °C. Before taking these measurements, both the feed and the permeate sides were thoroughly evacuated to below  $10^{-5}$  Torr  $(1.33\times10^{-8} \text{ bar})$  until the readout showed zero values for the removal of any residual gases. The downstream volume was calibrated using a Kapton membrane and was found to be 50 cm³. The upstream and downstream pressures were measured using a Baraton transducer (MKS; Model No. 626B02TBE) with a full scale of 10,000 and 2 Torr (13.3 and  $2.7\times10^{-3}$  bar), respectively. The pressure on the permeate side was recorded as a function of time using a pressure transducer and passed to a desktop computer through a shielded data cable. The permeability coefficient was determined from the linear slope of the downstream pressure versus a time plot (dp/dt) according to the following equation:

$$P = \frac{273}{76} \times \frac{Vl}{ATp_0} \times \frac{dp}{dt}$$
 (S2)

where, P is the permeability expressed in Barrer (1 Barrer =  $10^{-10}$  [cm³ (STP) cm.cm-².s-¹.cm-¹.Hg-¹], V (cm³) is the downstream volume, l (cm) is the membrane thickness, A (cm²) is the effective area of the membrane, T (K) is the measurement temperature,  $p_0$  (Torr) is the pressure of the feed gas in the upstream chamber, and dp/dt is the rate of the pressure change under a steady state. For each gas, the permeation tests were repeated more than three times, and the standard deviation from the mean values of the permeabilities was within ca.  $\pm$  3%. Sample-to-sample reproducibility was high and within  $\pm$  3%. The effective membrane areas were 15.9 cm². The ideal permselectivity,  $\alpha_{A/B}$ , of the membrane for a pair of gases (A and B) is defined as the ratio of the individual gas permeability coefficients:

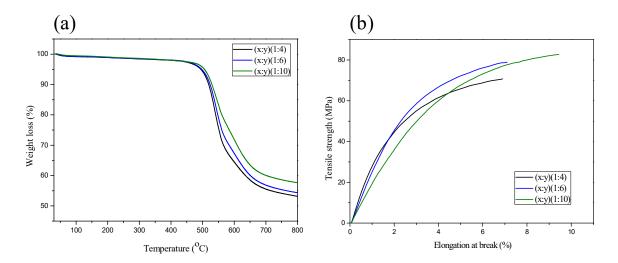
$$\alpha_{A/B} = \frac{P_A}{P_B} \tag{S3}$$

The diffusivity and solubility were obtained from the time-lag  $(\theta)$  value according to the equations:

$$D = \frac{l^2}{6\theta} \tag{S4}$$

$$S = \frac{P}{D} \tag{S5}$$

where, D (cm² s<sup>-1</sup>) is the diffusivity coefficient, l is the membrane thickness (cm) and  $\theta$  is the time lag (s), as obtained from the intercept of the linear steady-state part of the downstream pressure versus a time plot. The solubility, S, was calculated from Equation. (S5) with the permeability and diffusivity obtained from Equation. (S3) and (S4).



**Figure S1.** TGA graph (a) and S-S curve (b) of the copolymer [(PIM-PI)x-(6FDA-durene-PI)y] membranes.



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