

# Supporting Information

## **In-situ Infrared Spectroscopy Reveals Persistent Alkalinity Near Electrode Surfaces during CO<sub>2</sub> Electroreduction**

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## Mass transport simulations

The concentrations of the (electro)active molecules within the diffusion layer were modelled as a 1-D system which took into account diffusion and bubble induced mass transfer.<sup>1-3</sup> Bubble induced mass transfer was included to the model by approximating the change in the diffusion layer thickness as a function of the current density.<sup>1</sup> Evolution of gas bubbles from the electrode surface is considered to contribute to the mass transport of reactants and products during their growth, break-off and induced wake flow. These effects are thoroughly described by Vogt et al.<sup>4</sup> and recently applied to describe nanomorphology induced mass transport during CO<sub>2</sub> electroreduction.<sup>1</sup> Rousar correlation<sup>5</sup> was used to include the convective effect created during the departure of the bubbles (Sh1) while the Vogt relation<sup>4</sup> was used to describe the convective effect of bubble growth and wake flow (Sh2).

$$Sh1 = \sqrt{\frac{12}{\pi}} Re_g^{0.5} Sc^{0.34} \Theta^{0.5}$$
$$Sh2 = \sqrt{\frac{12}{\pi}} Re_g^{0.5} Sc^{0.34} \left(1 - \frac{\sqrt{8}}{3} \frac{R_a}{R} \Theta\right) (1 + \Theta)$$

where  $\Theta$  is the fraction of the electrode area covered by the bubbles and  $R_a/R$  is the ratio of the contact length of a single bubble to its diameter. The Reynolds number ( $Re_g$ ) and Schmidt number ( $Sc$ ) for gas evolution are given by the following:

$$Re_g = \frac{V_{gas} d_b}{A \nu}$$
$$Sc = \frac{\nu}{D}$$

where  $d_b$  is the average departure diameter of the bubbles and  $\nu$  is the kinematic viscosity. The departure diameter of the bubbles are commonly assumed to be 50  $\mu\text{m}$  for electrodes with horizontal planes facing upward.<sup>6</sup> Departure diameter of the bubbles ( $d_b$ ) was measured with imaging lenses (Edmund optics) to justify this assumption for different electrolyte concentrations (Figure S20). The coverage of the bubbles were taken as 0.05 based on the hydrogen evolution data on metal electrodes<sup>7</sup> and  $R_a/R$  is assumed to be 0.75.<sup>4</sup>

The Reynolds number and current density can be correlated by calculating the area normalized volume flux due to gas evolution by;

$$\frac{V_{gas}}{A} = \frac{J}{nF} \frac{RT}{P}$$

where P is pressure, T is temperature, R is the gas constant, n is average number of electrons transferred for gaseous products, F is the Faraday constant, J is the current density for gaseous products.

The mass transport number for bubble induced convection can be derived from the Sheerwood number ( $Sh_{bubble}$ ) which can be obtained by combining Sh1 and Sh2 in the following equations:

$$Sh_{bubble} = (Sh_1^2 + Sh_2^2)^{0.5}$$

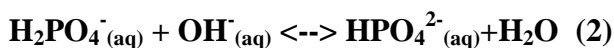
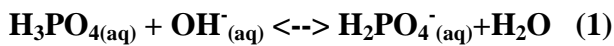
$$k_{bubble} = \frac{Sh_{bubble} D_i}{d_b}$$

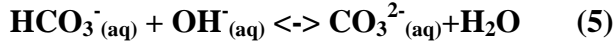
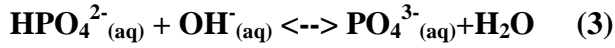
where  $D_i$  is the diffusivity of the molecule of interest and  $k_{bubble}$  is the mass transport number for bubble induced convection. This number can be correlated to the double layer thickness( $\sigma$ ) via the equation;

$$\sigma = \frac{D_i}{k_{bubble}}$$

The change in the double layer thickness as a function of current density is given in Figure S21.

By considering the change in the double layer thickness as a function of current density, the concentration of molecules within the boundary layer was calculated by using the Nernst-Planck equation.<sup>1-3, 8</sup> Due to high electrolyte concentration, the effect of migration on the transport of the molecules from the bulk to the surface was assumed to be negligible. In addition, the concentration of molecules in the bulk was considered to be at their equilibrium concentrations for reactions 1 to 6 given below. CO<sub>2</sub> and/or water molecules are consumed at the cathode to produce CO<sub>2</sub> reduction products and hydrogen, while the produced OH<sup>-</sup> is neutralized by the following equilibria and reactions.<sup>4</sup>





The equilibrium constant for these reactions are  $K_1 = 6.92 \times 10^{11} \text{ M}^{-1}$ ,  $K_3 = 4.79 \times 10^1 \text{ M}^{-1}$ ,  $K_4 = 4.44 \times 10^7 \text{ M}^{-1}$  and  $K_5 = 4.66 \times 10^3 \text{ M}^{-1}$ .<sup>2-3</sup> For the reaction 2, which is the parent buffer reaction, apparent  $K_2$  values are calculated based on activity coefficients<sup>9</sup> and used to estimate the initial pH of the solutions before  $\text{CO}_2$  purging with the following approach.

$$K_2 = \frac{a_{\text{HPO}_4^{2-}}}{a_{\text{OH}^-} a_{\text{H}_2\text{PO}_4^-}} = \frac{\gamma_{\text{HPO}_4^{2-}} [\text{HPO}_4^{2-}]}{\gamma_{\text{OH}^-} [\text{OH}^-] \gamma_{\text{H}_2\text{PO}_4^-} [\text{H}_2\text{PO}_4^-]} = \text{apparent } K_2 = \frac{[\text{HPO}_4^{2-}]}{[\text{OH}^-] [\text{H}_2\text{PO}_4^-]}$$

When the parent phosphate solution is purged with the  $\text{CO}_2$  the following reaction takes place to form bicarbonate.



The equilibrium concentrations of the respective ions for reaction 6 can be calculated by using the reactions 2 and 4 and equilibrium constants  $K_2$  and  $K_4$ .

The forward rate constants for phosphate buffer reactions (1-3) were assumed to be on the order of fast acid-base reactions and taken as  $1 \times 10^{10} \text{ M}^{-1} \text{ s}^{-1}$ ,<sup>10</sup> while the forward reaction rate for reaction (4) is  $5.93 \times 10^3 \text{ M}^{-1} \text{ s}^{-1}$ .<sup>2</sup> The forward reaction rate of reaction (5) is assumed to be  $1 \times 10^8 \text{ M}^{-1} \text{ s}^{-1}$ .<sup>2</sup> The corresponding backward reaction rates were calculated from equilibrium constants. Diffusion coefficients were corrected for viscosity by using Stokes-Einstein equation.<sup>11</sup>

The concentration of the molecules within the diffusion layer and at the surface can be extracted by solving the following coupled differential equations:

$$\frac{\delta[\text{H}_3\text{PO}_4]}{\delta x} = D_{\text{H}_3\text{PO}_4} \frac{\delta^2[\text{H}_3\text{PO}_4]}{\delta x^2} - k_{1f} [\text{H}_3\text{PO}_4] * [\text{OH}^-] + k_{1b} [\text{H}_2\text{PO}_4^-]$$

$$\frac{\delta[\text{H}_2\text{PO}_4^-]}{\delta x} = D_{\text{H}_2\text{PO}_4^-} \frac{\delta^2[\text{H}_2\text{PO}_4^-]}{\delta x^2} + k_{1f} [\text{H}_3\text{PO}_4] * [\text{OH}^-] - k_{1b} [\text{H}_2\text{PO}_4^-] - k_{2f} [\text{H}_2\text{PO}_4^-] [\text{OH}^-] + k_{2b} [\text{HPO}_4^{2-}]$$

$$\frac{\delta[\text{HPO}_4^{2-}]}{\delta x} = D_{\text{HPO}_4^{2-}} \frac{\delta^2[\text{HPO}_4^{2-}]}{\delta x^2} + k_{2f} [\text{H}_2\text{PO}_4^-] [\text{OH}^-] - k_{2b} [\text{HPO}_4^{2-}] - k_{3f} [\text{HPO}_4^{2-}] [\text{OH}^-] + k_{3b} [\text{PO}_4^{3-}]$$

$$\frac{\delta[\text{PO}_4^{3-}]}{\delta x} = D_{\text{PO}_4^{3-}} \frac{\delta^2[\text{PO}_4^{3-}]}{\delta x^2} + k_{3f} [\text{HPO}_4^{2-}] [\text{OH}^-] - k_{3b} [\text{PO}_4^{3-}]$$

$$\frac{\delta[CO_2]}{\delta x} = D_{CO_2} \frac{\delta^2[CO_2]}{\delta x^2} - k_{4f}[CO_2][OH^-] + k_{4b}[HCO_3^-]$$

$$\frac{\delta[HCO_3^-]}{\delta t} = D_{HCO_3^-} \frac{\delta^2[HCO_3^-]}{\delta x^2} + k_{4f}[CO_2][OH^-] - k_{4b}[HCO_3^-] - k_{5f}[HCO_3^-][OH^-] + k_{5b}[CO_3^{2-}]$$

$$\frac{\delta[CO_3^{2-}]}{\delta t} = D_{CO_3^{2-}} \frac{\delta^2[CO_3^{2-}]}{\delta x^2} + k_{5f}[HCO_3^-][OH^-] - k_{5b}[CO_3^{2-}]$$

$$\frac{\delta[OH^-]}{\delta t} = D_{OH^-} \frac{\delta^2[OH^-]}{\delta x^2} - k_{4f}[CO_2][OH^-] + k_{4b}[HCO_3^-] - k_{1f}[H_3PO_4][OH^-] + k_{1b}[H_2PO_4^-]$$

$$k_{2f}[H_2PO_4^-][OH^-] + k_{2b}[HPO_4^{2-}] - k_{3f}[HPO_4^{2-}][OH^-] + k_{3b}[PO_4^{3-}] - k_{5f}[HCO_3^-][OH^-] + k_{5b}[CO_3^{2-}]$$

Sixteen boundary conditions were given in the Table S11 to solve eight second order time dependent partial differential equations for concentration of the species of  $H_3PO_4$ ,  $H_2PO_4^-$ ,  $HPO_4^{2-}$ ,  $PO_4^{3-}$ ,  $CO_2$ ,  $OH^-$ ,  $HCO_3^-$  and  $CO_3^{2-}$  at the surface and boundary layer. Bulk solution is where the distance from the electrode surface is larger than the boundary layer thickness. It is assumed to have infinite supply of molecules from the bulk.

The first boundary condition is based on the flux of the reactants and products which can be related to the partial current density of the reactants and products for an electrochemical reaction.

$$D_{CO_2} \frac{\delta[CO_2]}{\delta x} = CO_2 \text{ consumption}$$

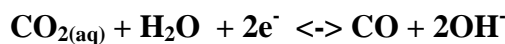
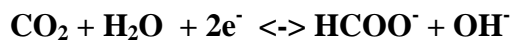
$$D_{OH^-} \frac{\delta[OH^-]}{\delta x} = OH^- \text{ production}$$

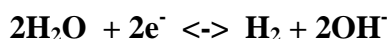
$CO_2$  consumption and  $OH^-$  production can be related to current density by the following equations.

$$CO_2 \text{ consumption} = \frac{J}{F} \left( \sum_i a_i \frac{x_i}{n_i} \right)$$

$$OH^- \text{ production} = \frac{J}{F} \left( \sum_i x_i \right)$$

Where  $a_i$  is the number of moles  $CO_2$  molecules consumed per moles of product.  $x_i$  is the current efficiency and  $n_i$  is the number of electrons transferred for the following reactions. These values are given in Table SI 3. ( pls note that the deprotonation of formic acid to formate must to be excluded).





The second boundary condition is that at the solution edge of the boundary layer the concentration of the molecules are equal to the equilibrium concentrations (i.e. bulk) when a constant current is applied ( $t > 0$ ). The initial values of the concentrations, before a galvanostatic step is applied, are assumed to be the same as the bulk concentrations ( $t = 0$ )

and are listed in Table 4 for different electrolyte

concentrations.

To account for solubility of  $\text{CO}_2$  in different electrolyte concentrations, the following Sechenov Equation was used;<sup>12</sup>

$$\text{Log} \left( \frac{CO_2^{\text{water}}}{CO_2^{\text{electrolyte}}} \right) = \sum (h_G + h_{ion}) C_i$$

where  $h_G$  can be approximated by and all parameters are given Table 2;

$$h_G = h_{G,0} + h_T(T - 298.15)$$

All the parameters are given in Table SI2.

**Formation of oxygenates on nanowires:** Drawing structure-activity relationships requires very careful designed set of experiments on well-defined surfaces, e.g single crystals, shape controlled nanoparticles, by using in-situ and/or online techniques addressing structural changes on catalyst surface and reaction intermediates. Poorly defined surfaces, such as randomly grown nanowires, are very vulnerable to not only mass transport effects but also structural changes during the electroreduction experiments which are not straightforward to identify. Therefore, we don't find it convenient to draw structure activity relationships purely based on catalytic activity and selectivity studies on ill-defined surfaces. The FE and partial current density of ethanol, acetate and propanol are given for nanowire electrodes as a function of electrolyte concentration in Figure S8 and Figure S10, respectively. Acetaldehyde is considered to be intermediate for ethanol and acetate formation during  $\text{CO}_2$  electroreduction.<sup>13-14</sup> Both electrochemical and non-electrochemical pathways were proposed. Non-electrochemical pathway was suggested to take place via disproportionation of aldehydes by high local pH (or bulk pH for CO reduction).<sup>15</sup> Therefore, local alkaline conditions as a result of poor mass transport might favour the formation of these two product. This partially explains formation of ethanol and acetate on copper surfaces. However, the higher production rates of ethanol compared to acetate, in agreement with literature for different copper surfaces, implies existence of another pathway for the formation of ethanol. Single crystal studies suggested that this pathway is structure sensitive and ethylene vs ethanol selectivity should be able to tuned by catalyst structure.<sup>14</sup> We think dissolution, re-deposition and surface reconstruction under OCP and/or cathodic potentials challenges both fundamental and

practical studies. Propanol is one of the least studied compounds among the detected products. Different pathways proposed.<sup>16</sup> First of all, interestingly, no propionic acid is detected to the best of our knowledge in most of the studies. This partially rules out the effect of Cannizzaro type of reactions on the mechanism. We believe propanol is formed via insertion of CO to an C<sub>2</sub> intermediate which is improved most likely by re-adsorption effects in porous structures. Production of propanol therefore most likely be influenced by formation C<sub>2</sub> compounds, CO formation and/or coverage. Recently, mesoscale and morphological effects was identified as key parameter for the enhanced formation of propanol.<sup>17</sup> However, smooth copper electrodes are also capable of making minor amount of propanol.<sup>18</sup>

C<sub>2</sub> products were considered to be formed via an early CO coupling.<sup>19</sup> Propanol is the only C<sub>3</sub> product observed in appreciable amount and the pathway towards propanol is not clear yet. Considering the fact that propanol is nearly always accompany the C<sub>2</sub> products, we think it is formed by a CO insertion to an C<sub>2</sub> intermediate. Therefore C<sub>2</sub> and C<sub>3</sub> products are considered to be formed via common rate determining step while the individual selectivity's are determined by the catalyst structure<sup>20</sup>, kinetic barriers,<sup>21</sup> mesoscale effects,<sup>22</sup> and possibly CO coverage.<sup>23</sup> We think the total production rate of these products are important rather than only ethylene and the summation of partial current density for C<sub>2</sub> and C<sub>3</sub> products is very similar for different electrolyte concentrations. The increase in the formation of methane at high electrolyte concentration takes places “mostly” at the expense of ethanol and propanol rather than ethylene (Figure 3 main text and FigureSI 10). Pls note that at low electrolyte concentration(0.1M) mass transfer limited current density is slightly lower which also partially explains the lower production of ethylene.



$t > 0$ at the electrode surface	$t > 0$ in the bulk solution
$D_{H_3PO_4} \frac{\delta[H_3PO_4]}{\delta x^2} = 0$	$H_3PO_4 = [H_3PO_4]_i$
$D_{H_2PO_4^-} \frac{\delta[H_2PO_4^-]}{\delta x^2} = 0$	$H_2PO_4^- = [H_2PO_4^-]_i$
$D_{HPO_4^{2-}} \frac{\delta[HPO_4^{2-}]}{\delta x^2} = 0$	$HPO_4^{2-} = [HPO_4^{2-}]_i$
$D_{PO_4^{3-}} \frac{\delta[PO_4^{3-}]}{\delta x} = 0$	$PO_4^{3-} = [PO_4^{3-}]_i$
$D_{CO_2} \frac{\delta[CO_2]}{\delta x} = CO_2 \text{ consumption}$	$CO_2 = [CO_2]_i$
$D_{OH^-} \frac{\delta[OH^-]}{\delta x} = OH^- \text{ production}$	$OH^- = [OH^-]_i$
$D_{HCO_3^-} \frac{\delta[HCO_3^-]}{\delta x^2} = 0$	$HCO_3^- = [HCO_3^-]_i$
$D_{CO_3^{2-}} \frac{\delta[CO_3^{2-}]}{\delta x^2} = 0$	$CO_3^{2-} = [CO_3^{2-}]_i$

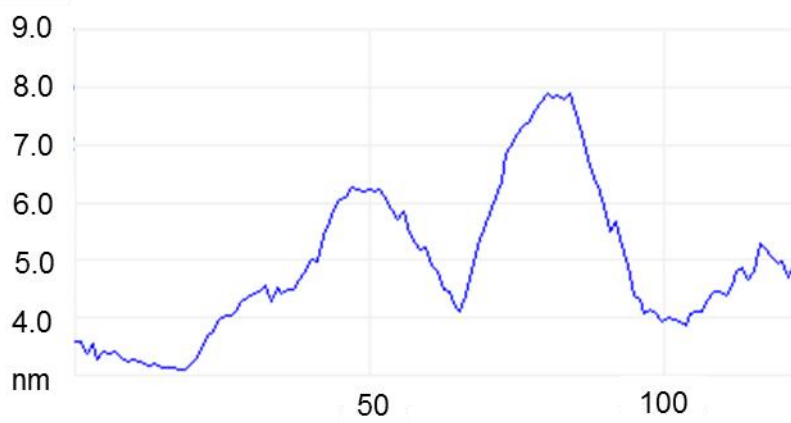
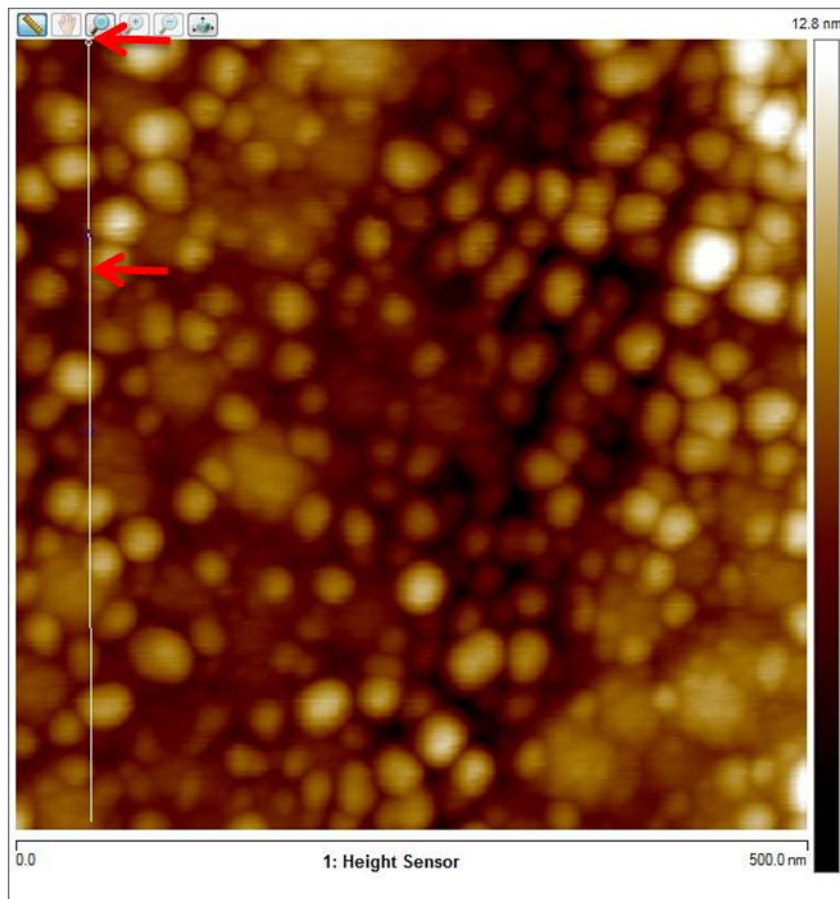
**Table SI 1:** Boundary conditions to solve time dependent differential equations.

Parameter	value
$D_{\text{H}_3\text{PO}_4}$	$8.7 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$
$D_{\text{H}_2\text{PO}_4^-}$	$8.46 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$
$D_{\text{HPO}_4^{2-}}$	$6.9 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$
$D_{\text{PO}_4^{3-}}$	$6.12 \times 10^{-10} \text{ m}^2 \text{ s}^{-1}$
$D_{\text{OH}^-}$	$5.27 \times 10^{-9} \text{ m}^2 \text{ s}^{-1}$
$D_{\text{CO}_2}$	$1.91 \times 10^{-9} \text{ m}^2 \text{ s}^{-1}$
$\text{CO}_2 h_{G,0}$	$-0.0172 \text{ m}^3 \text{ kmol}^{-1}$
$\text{CO}_2 h_T$	$-0.000338 \text{ m}^3 \text{ kmol}^{-1}$
$\text{H}_2\text{PO}_4^- h_{ion}$	$0.1009 \text{ m}^3 \text{ kmol}^{-1}$
$\text{HPO}_4^{2-} h_{ion}$	$0.1559 \text{ m}^3 \text{ kmol}^{-1}$
$\text{K}^+ h_{ion}$	$0.0929 \text{ m}^3 \text{ kmol}^{-1}$

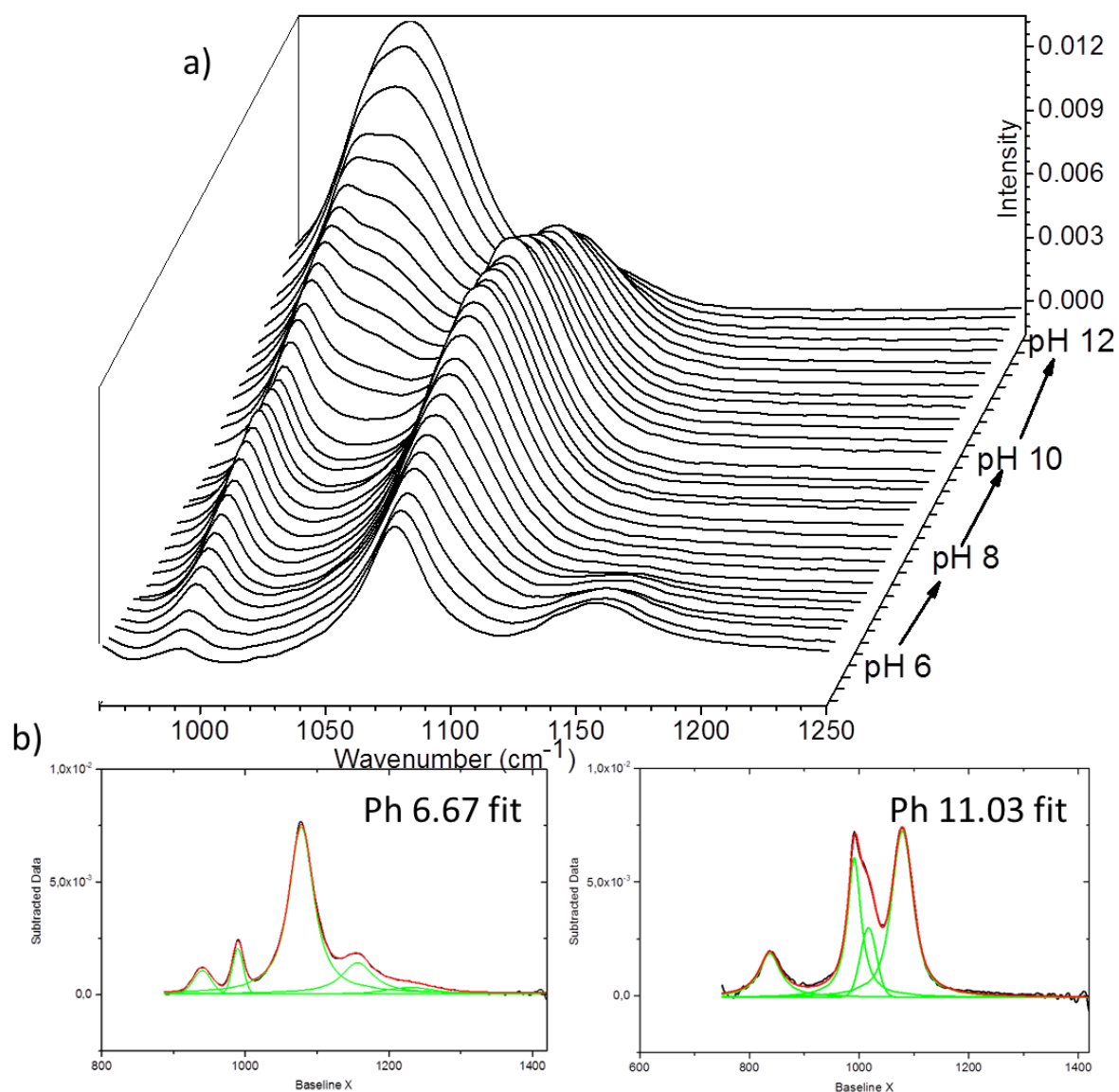
**Table SI 2:** Simulation parameters. Pls not that diffusion coefficients were corrected for each electrolyte concentration by using Stokes-Einstein relation.

	$\text{H}_2$	$\text{CO}$	$\text{C}_2\text{H}_4$	$\text{CH}_4$	Formate
$x_i$	0.5	0.01	0.1	0.25	0.1
$n_i$	2	2	12	8	2
$a_i$	0	1	2	1	1

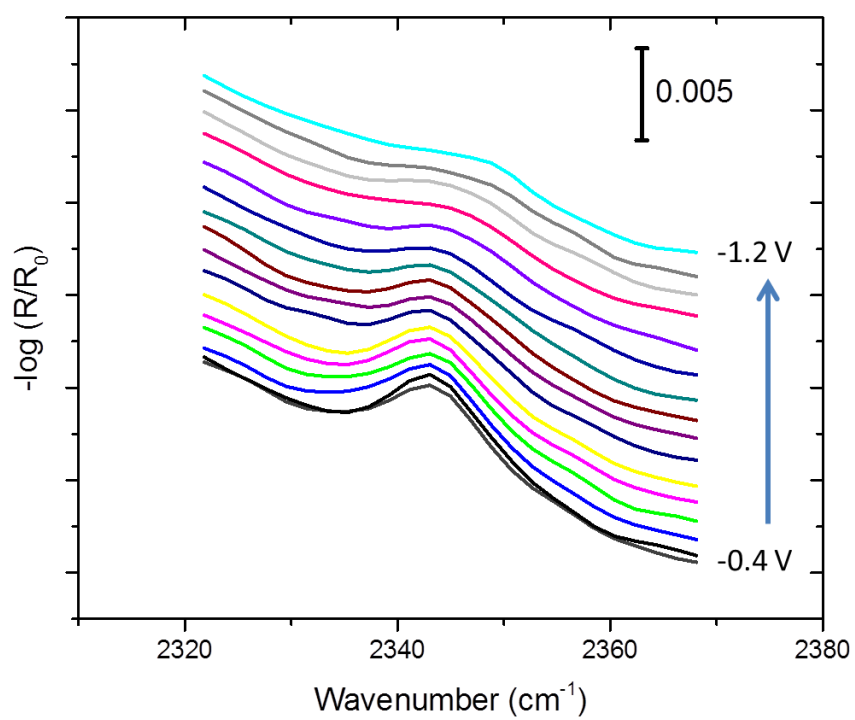
**Table SI 3:**  $a_i$  is the number of moles  $\text{CO}_2$  molecules consumed per moles of product.  $x_i$  is the current efficiency and  $n_i$  is the number of electrons transferred for the following reactions.



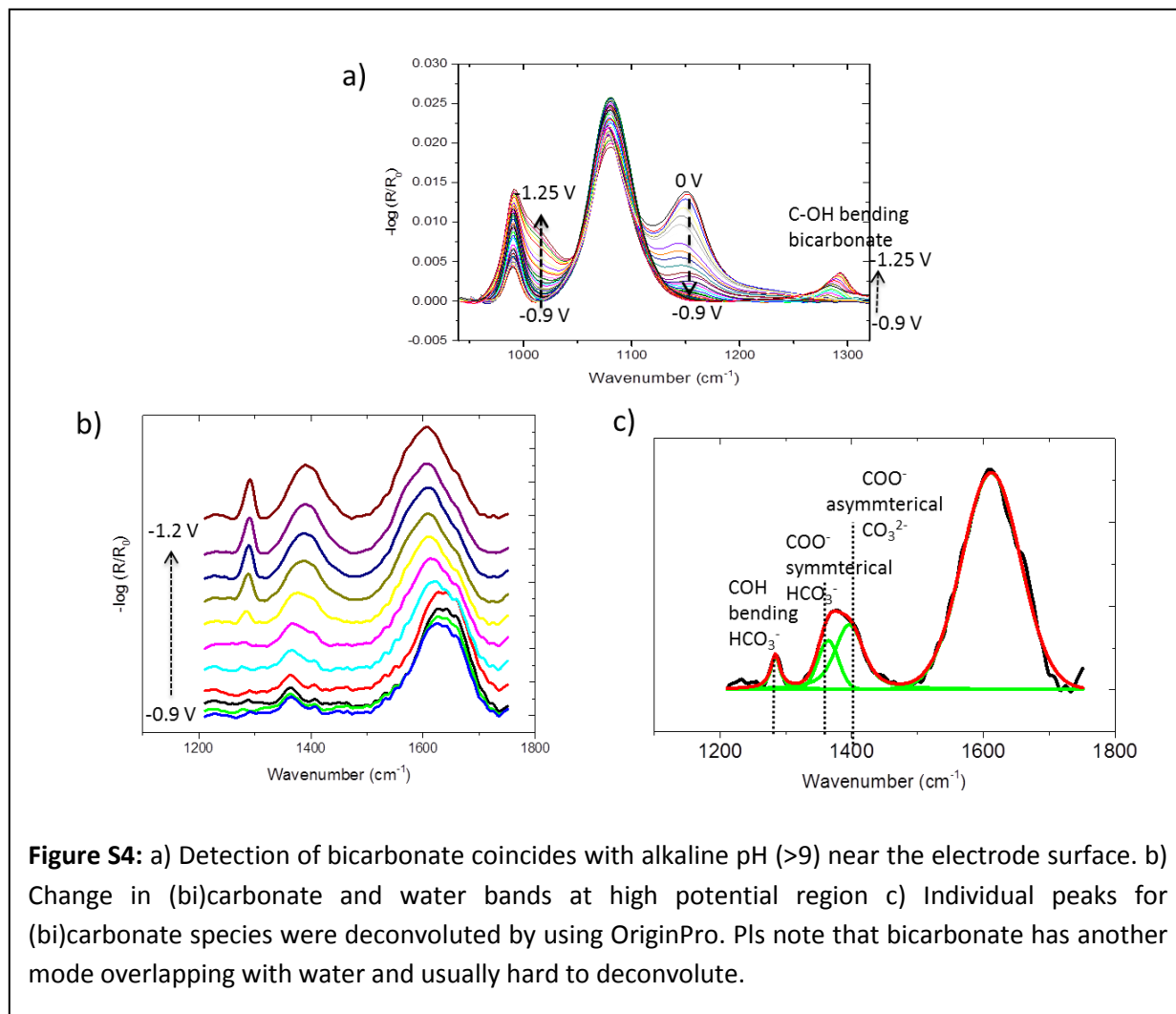
**Figure S1:** AFM image and height profile of Cu film on Ge along (red) marked direction

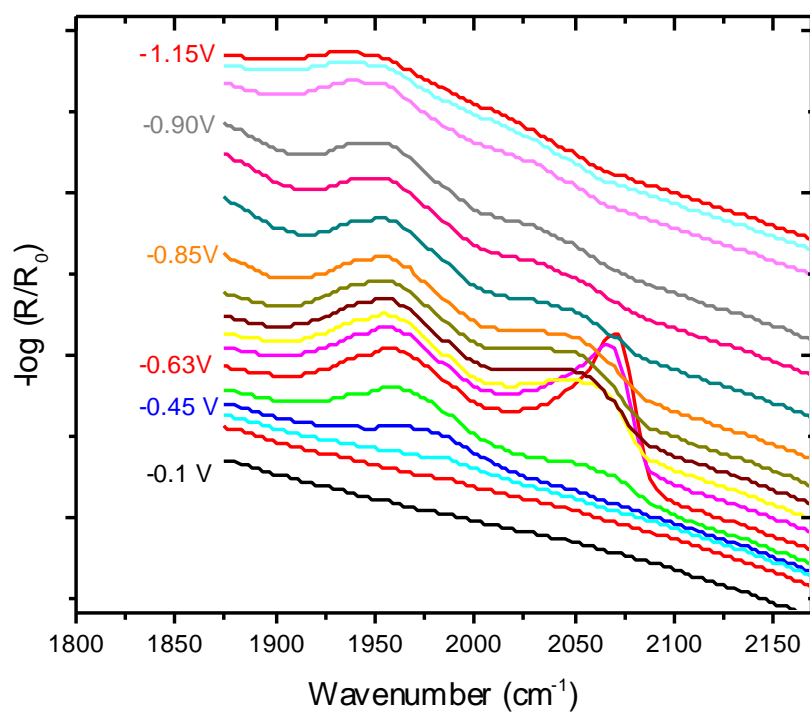


**Figure S2:** a) SEIRA spectra of phosphate species for different pH values between 6 and 12 under an applied potential of +0.1 V vs RHE. The spectra were obtained by addition of KOH to parent  $\text{KH}_2\text{PO}_4$  solution. b) Individual peaks for each phosphate species were deconvoluted by using OriginPro



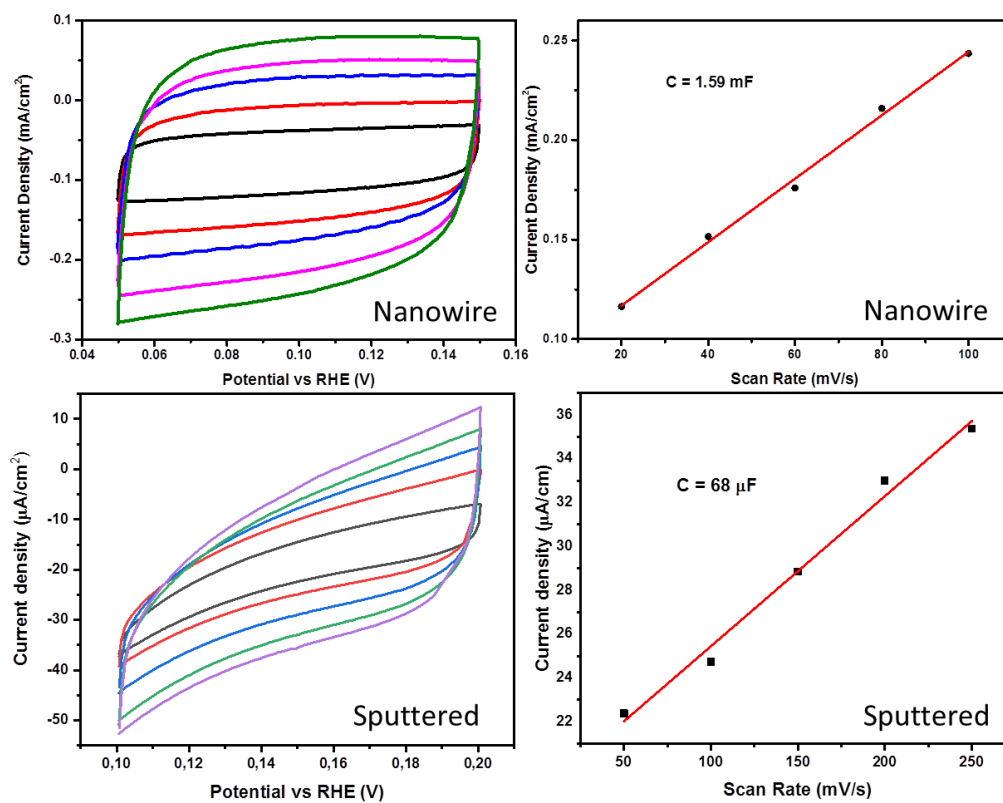
**Figure S3:** Potential dependent changes in the asymmetrical stretching of  $\text{CO}_2(\text{aq})$



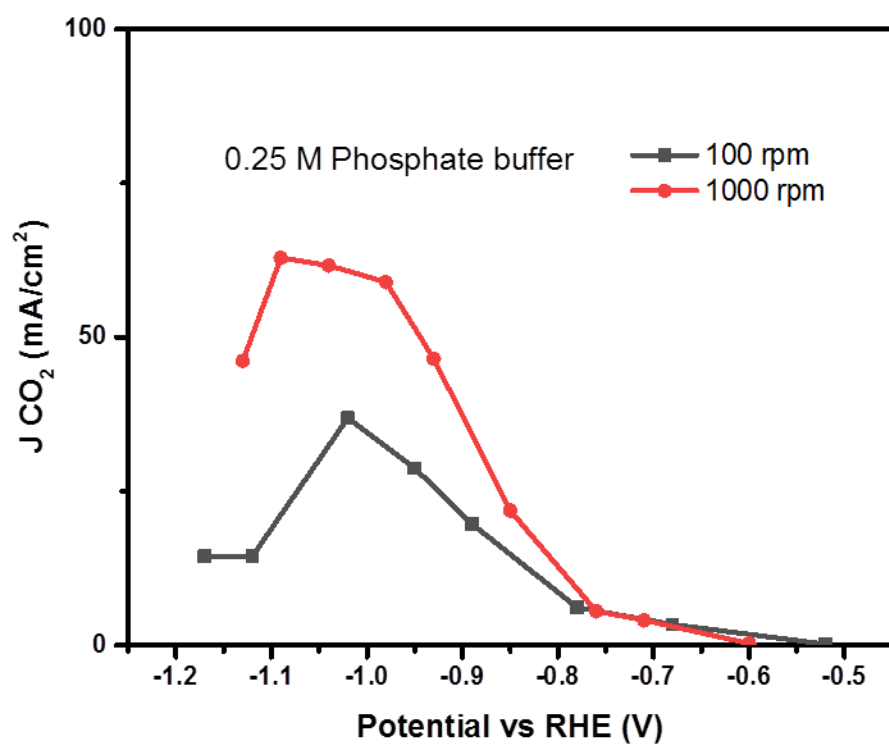


**Figure S5:** Adsorption of CO as a function of potential given for 0.5 M phosphate buffer.

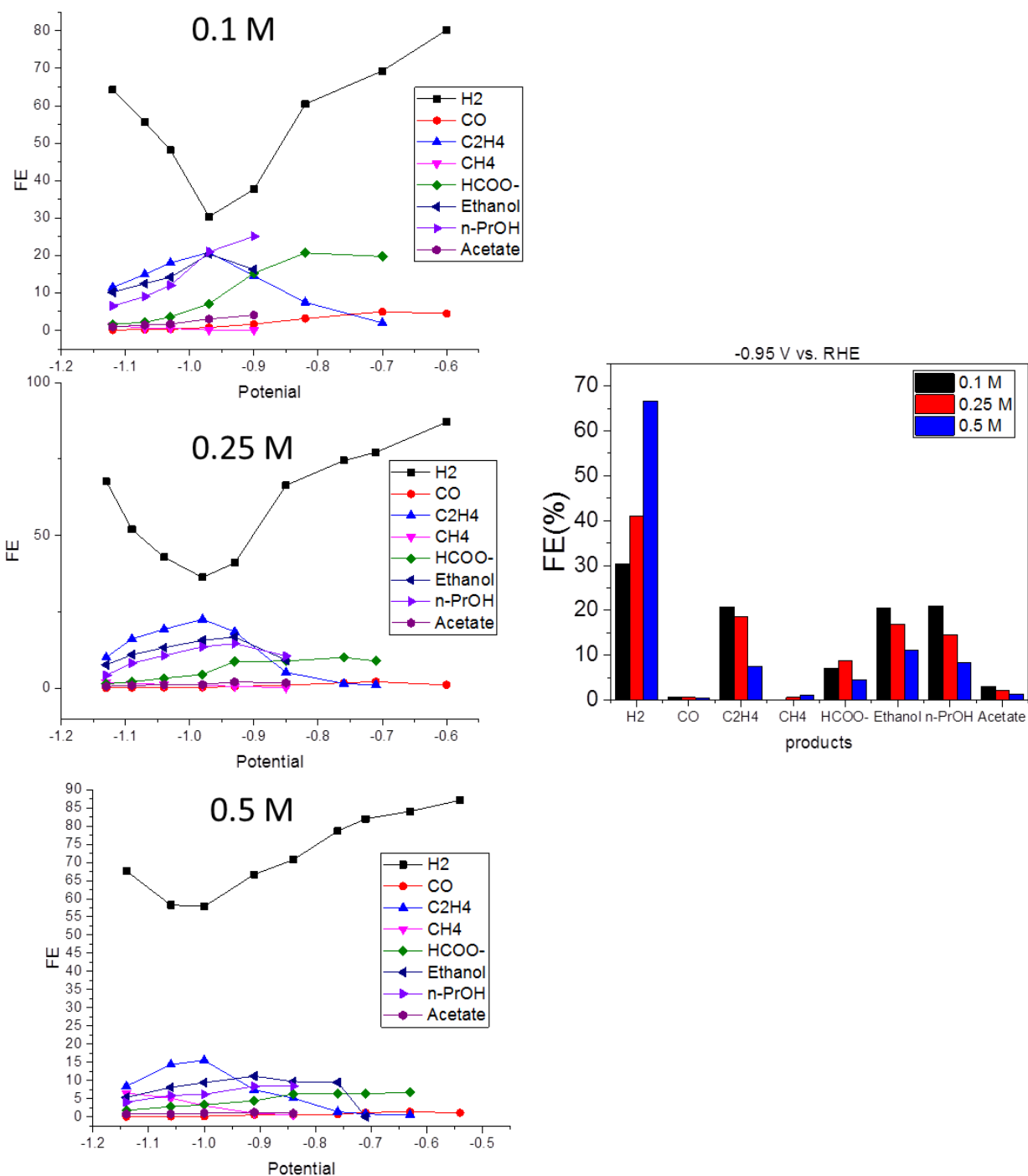




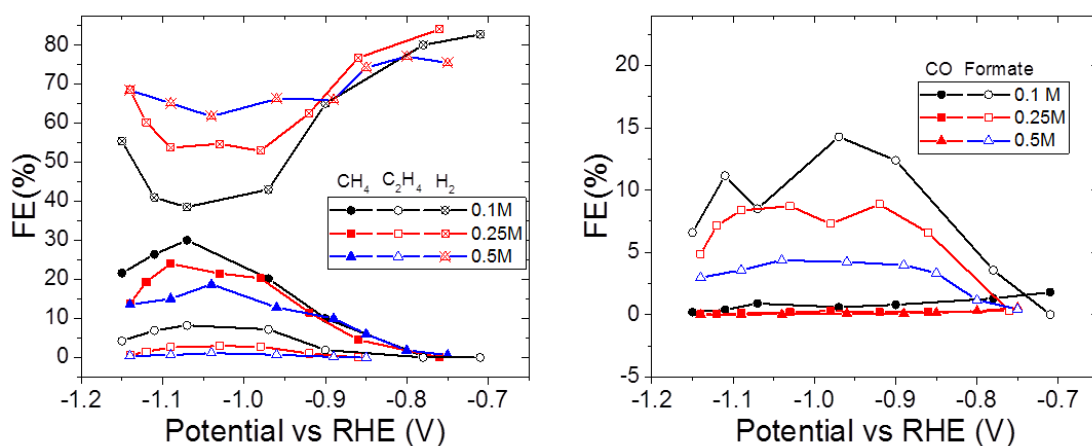
**Figure S6** Determination of double layer capacitance and roughness factor in 0.1 M NaClO<sub>4</sub> for Nanowire and sputtered copper electrodes.



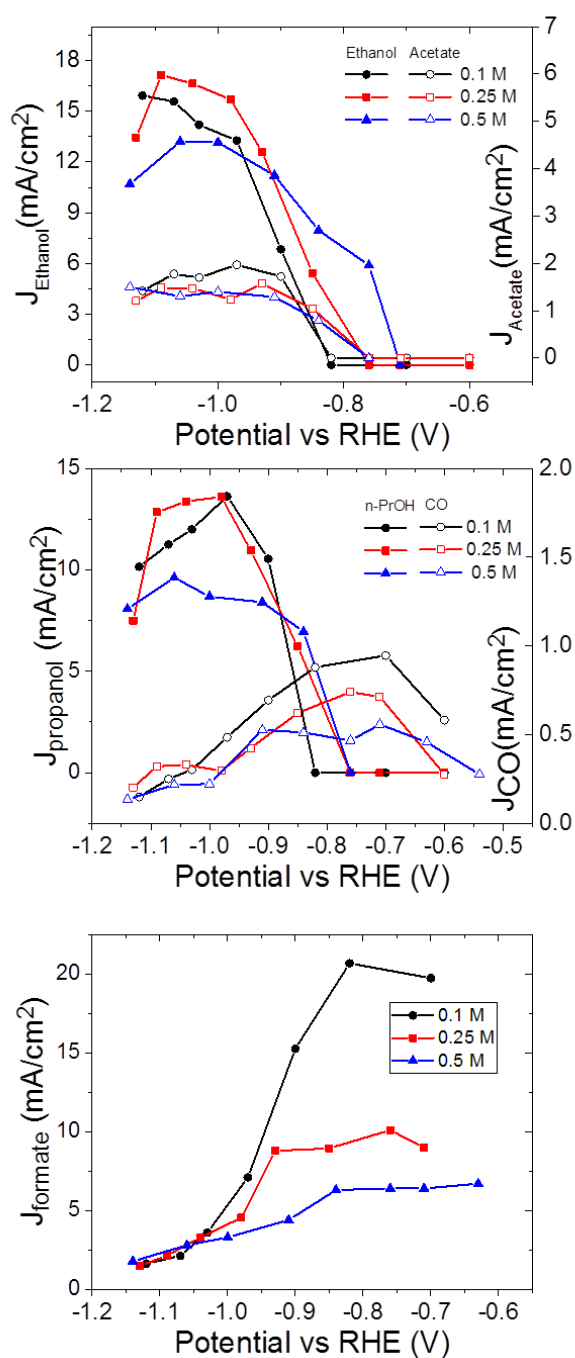
**Figure S7:** Effect of stirring on the partial current density of CO<sub>2</sub> reduction.



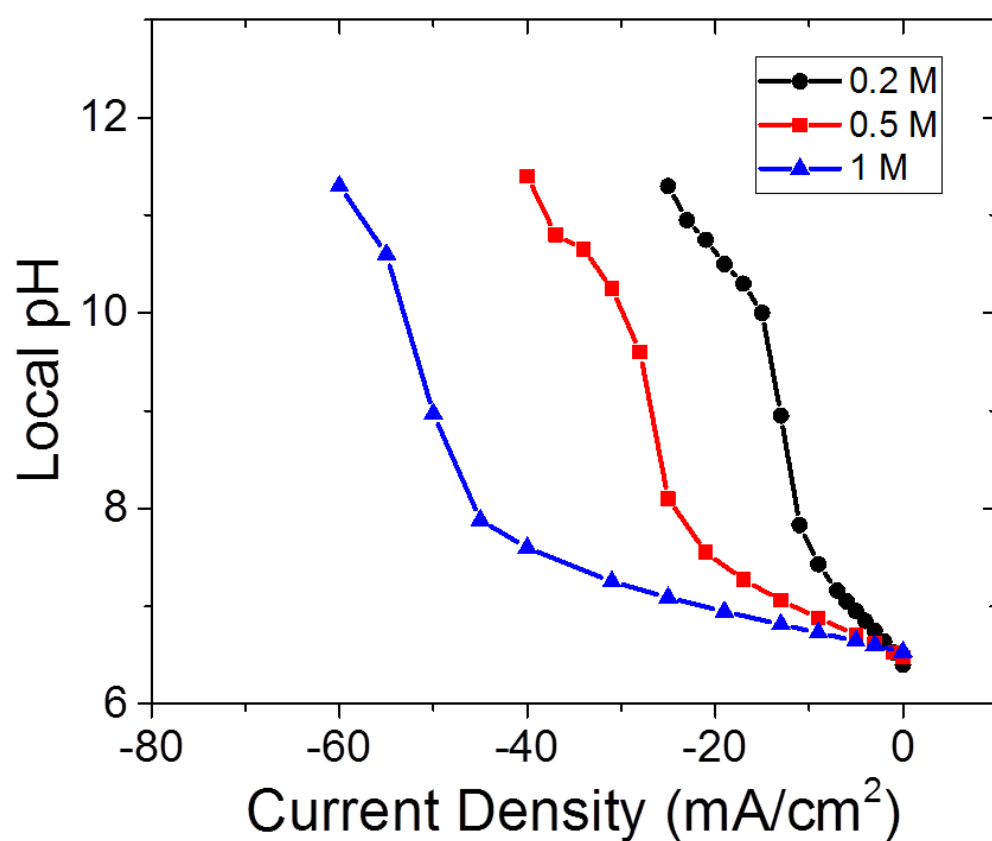
**Figure S8:** Faradaic efficiency of gaseous and liquid products as a function of electrolyte concentration for nanowire copper electrodes.. The electrolytes are composed of equimolar amounts of  $\text{H}_2\text{PO}_4^-$  and  $\text{HPO}_4^{2-}$ . FE of hydrogen increased notably at higher electrolyte concentrations and the selectivity towards C<sub>2</sub> and C<sub>3</sub> products decreased at potentials between -0.7 V vs RHE to -1 V vs RHE as a function of electrolyte concentration. The decrease in the selectivity of CO<sub>2</sub> reduction products are mostly result of increase in the hydrogen production (see main text).



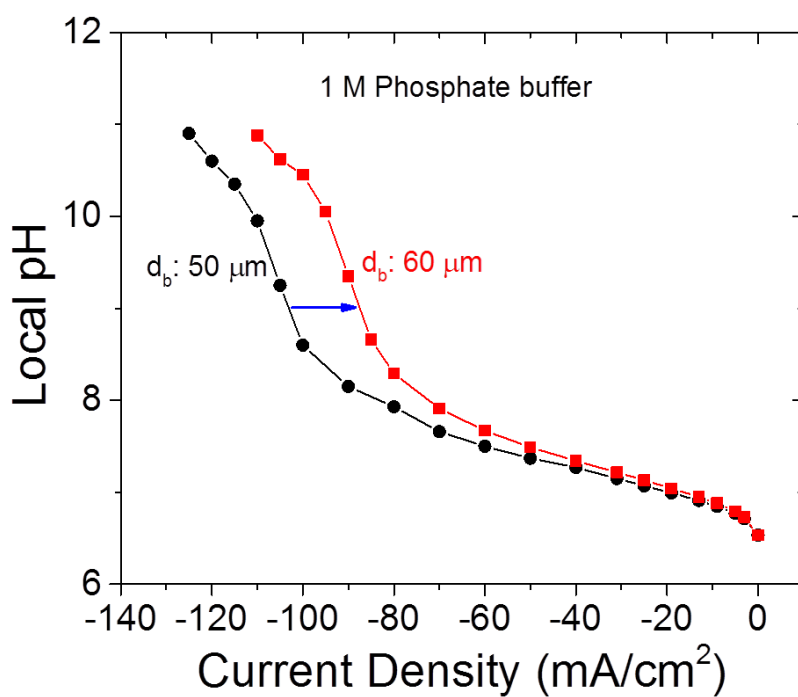
**Figure S9:** Faradaic efficiency of gaseous and liquid products as a function of electrolyte concentration for sputtered copper electrodes.. The electrolytes are composed of equimolar amounts of  $\text{H}_2\text{PO}_4^-$  and  $\text{HPO}_4^{2-}$ . FE of hydrogen increased notably at higher electrolyte concentrations and the selectivity towards  $\text{C}_1$  and  $\text{C}_2$  products decreased at potentials between -0.8 V vs RHE to -1.1 V vs RHE as a function of electrolyte concentration. The decrease in the selectivity of  $\text{CO}_2$  reduction products are mostly result of increase in the hydrogen production (see main text).



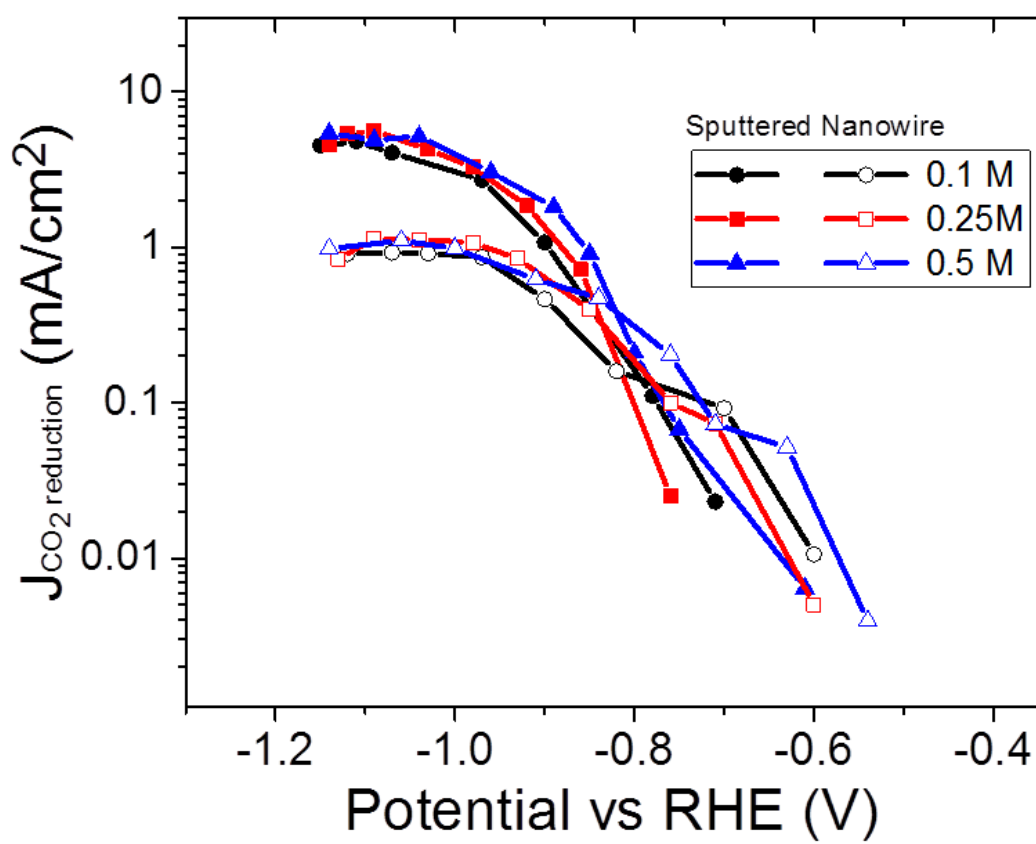
**Figure S10:** Partial current density of of gaseous and liquid products as a function of electrolyte concentration for nanowire electrodes. Partial current density of Methane, Ethylene and Hydrogen are given in main text.



**Figure S11:** Local pH as a function of current density calculated by including diffusion and convection via stirring (without bubble induced convection). Double layer thickness is taken as 100  $\mu\text{m}$  which is a typical thickness that can be achieved with extensive magnetic stirring. This value is used commonly for calculating near surface concentration of molecules during  $\text{CO}_2$  electroreduction.<sup>2-3</sup> This graph indicates the model dramatically underestimates the buffer capacity without bubble induced mass transport term at high currents ( $> 20 \text{ mA/cm}^2$ ).

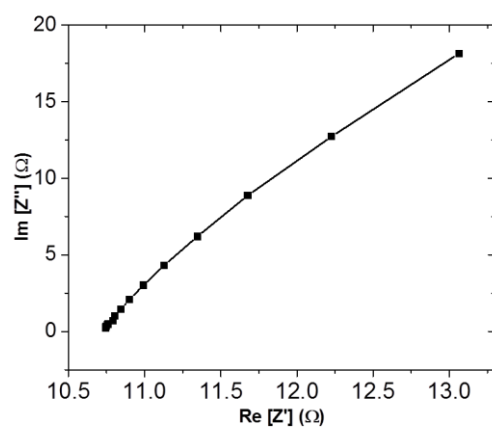


**Figure S12:** Local pH as a function of current density calculated by bubble induced mass transport model for two different bubble departure diameters ( $d_b$ ). The difference after breakdown of the buffer is notably high compared to buffered region.

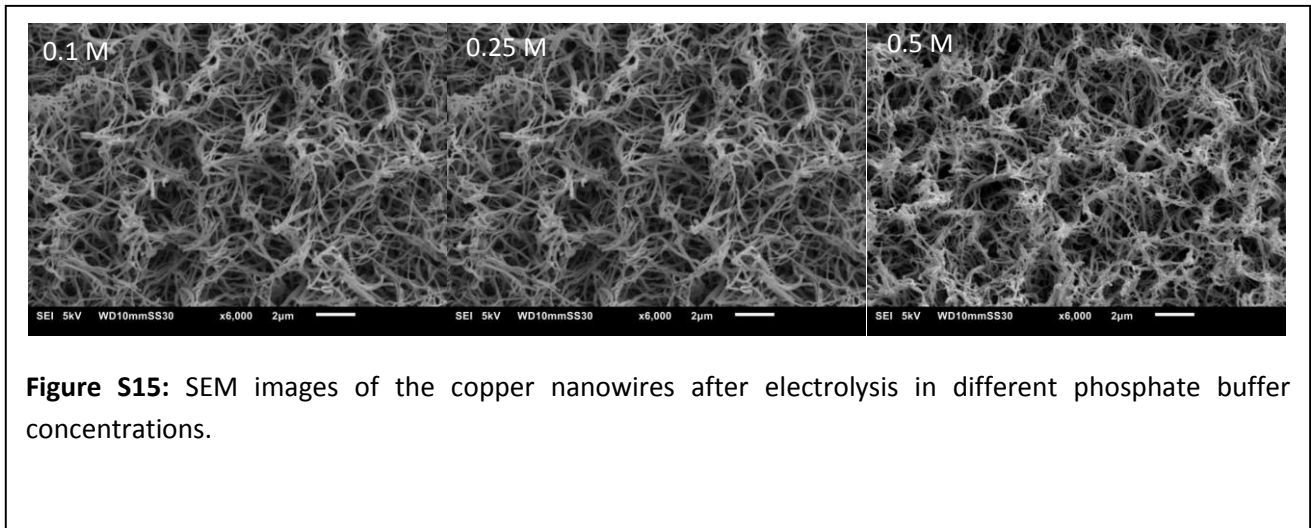


**Figure S13:** Electrochemically active surface area normalized partial current density for CO<sub>2</sub> reduction.

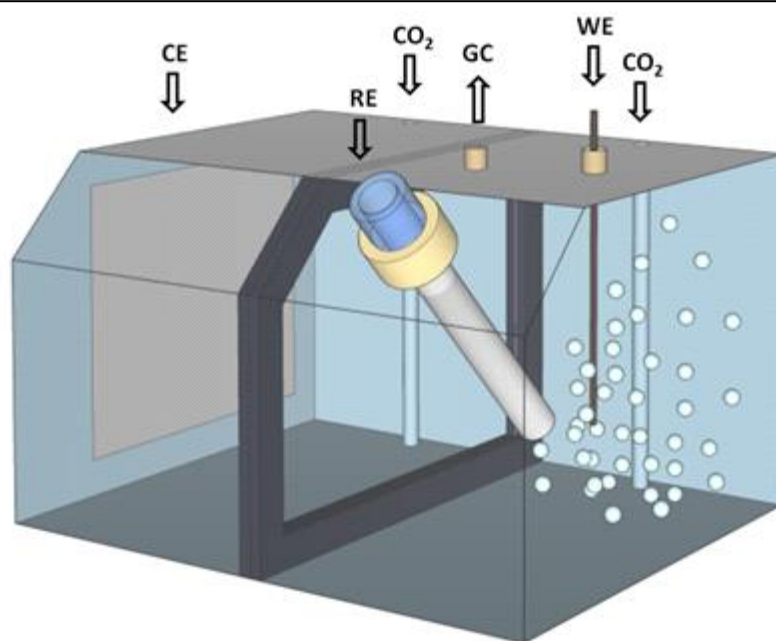




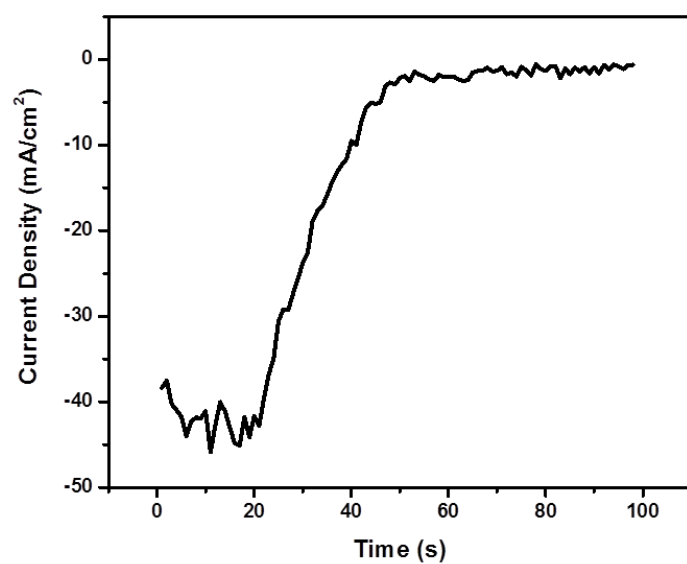
**Figure S14:** Electrochemical impedance spectroscopy of Cu film on Ge before SEIRAS measurements in 0.5 M phosphate buffer.



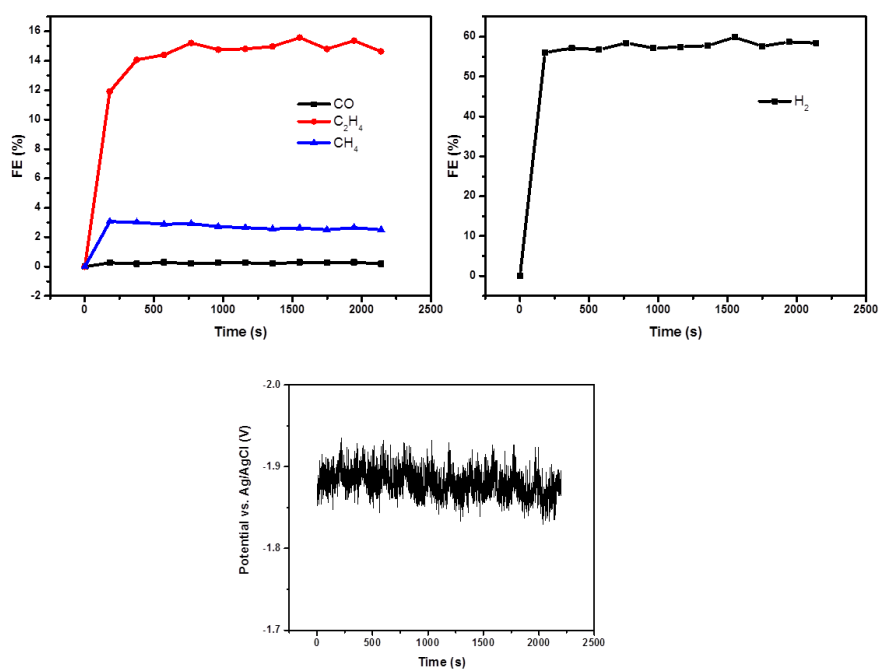
**Figure S15:** SEM images of the copper nanowires after electrolysis in different phosphate buffer concentrations.



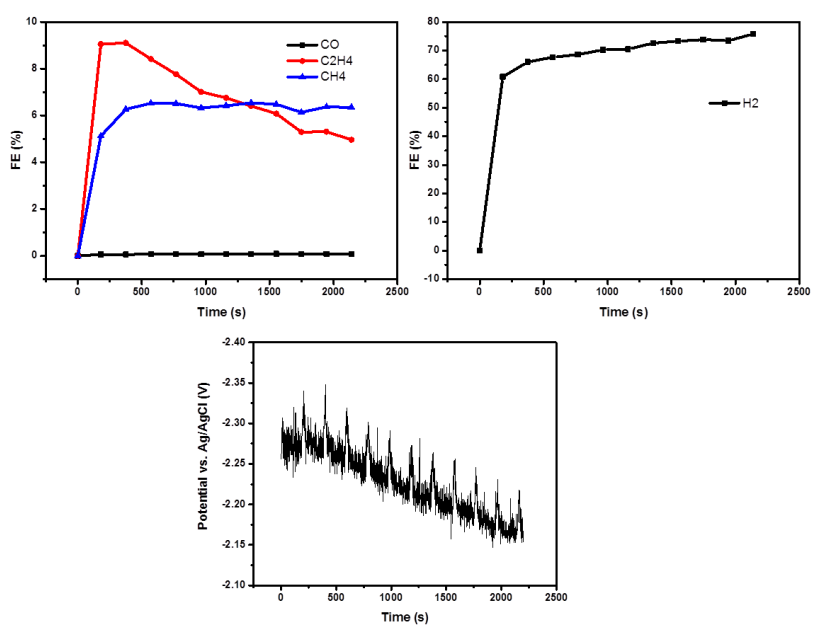
**Figure S16:** Illustration of the electrochemical cell used for CO<sub>2</sub> reduction



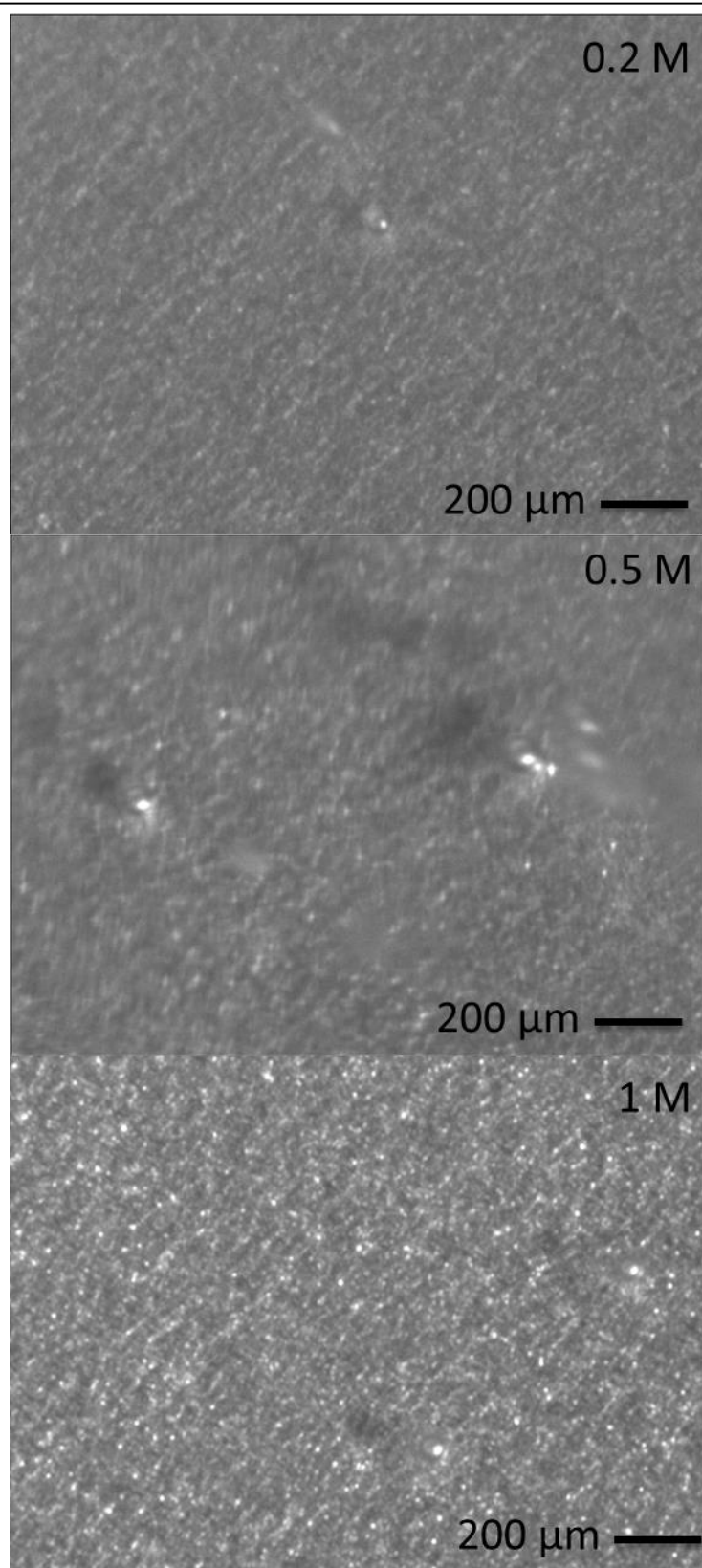
**Figure S17:** CuO reduction current transient at -0.8 V vs. Ag/AgCl in 0.25 M phosphate buffer.



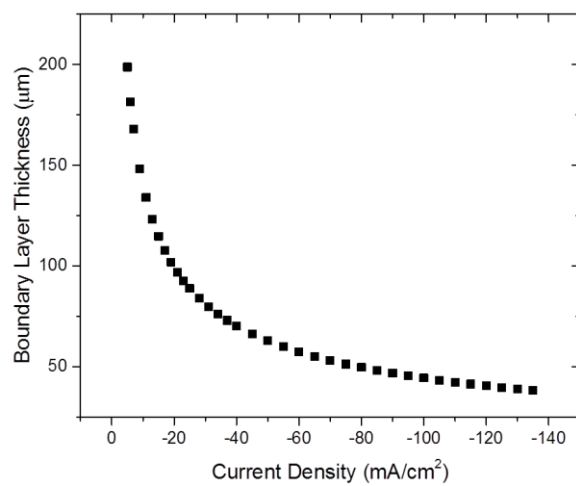
**Figure S18:** Change in the FE and potential as a function of time at current density of 125 mA/cm<sup>2</sup> in 0.5 M phosphate buffer.



**Figure S19:** Change in the FE and potential as a function of time at current density of 200 mA/cm<sup>2</sup> in 0.5 M phosphate buffer.



**Figure S20:** Bubble departure diameters as a function of electrolyte concentration were similar. The diameters were found to change between 40-70  $\mu\text{m}$  in different nucleation sites as a function of current density. ( 25 nm thick sputtered copper films on titanium foils at 5  $\text{mA}/\text{cm}^2$ ).



**Figure S21:** Effect of current density on diffusion layer thickness.



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