1			
2	Supplementary Information for		
3			
4	Satellite Observations Reveal Extreme Methane Leakage from a Natural Gas Well		
5	Blowout		
6			
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24 25	This PDF file includes:		
23 26	Supplementary Text		
20 27	Figs. S1 to S10		
28	Table S1 to S2		
28 29	Captions for Movie S1		
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## 31 Supplementary Text

- 32
- 33 <u>Section 1: Emission uncertainty quantification</u>

The total uncertainty ( $\sigma_{total}$ ) of the emissions rate  $Q_T$  estimated using the mass balance approach of *Methods* 3 is quantified as follows:

36

37 
$$\sigma_{\text{total}} = \sqrt{\sigma_{\text{meteo}}^2 + \sigma_{\text{sampling}}^2 + \sigma_{\text{precision}}^2 + \sigma_{\text{method}}^2}$$
 .....(S1)

38

39 Here,  $\sigma_{meteo}$  is the uncertainty of  $Q_T$  due to the error in WRF-simulated meteorology.  $\sigma_{sampling}$ 40 is the uncertainty of  $Q_T$  due to the spatial sampling of TROPOMI XCH<sub>4</sub> on 27 February 2018, 41 and  $\sigma_{precision}$  is the uncertainty due to precision of TROPOMI XCH<sub>4</sub> retrievals.  $\sigma_{method}$  is the 42 uncertainty of the emission quantification method.

43

44 To quantify  $\sigma_{meteo}$ , WRF XCH<sub>4</sub> is sampled at six hourly time instances before and after the 45 TROPOMI overpass time (17:35 UTC). The WRF XCH<sub>4</sub> output for each time instance is then 46 interpolated and re-gridded to the TROPOMI measurement pixels (see Fig. S3), which are then 47 used to generate multiple emission estimates (see Table S1) resulting in a  $\sigma_{meteo}$  of 14 t/hr. 48 Note that  $\sigma_{meteo}$  accounts for inaccuracies in the time interpolation as well as the temporal 49 representation of meteorological variations, including wind speed and direction, in the WRF simulations.  $\sigma_{sampling}$  was calculated by bootstrapping the emission-influenced and background 50 51 pixels. 10,000 instances of half the number of emission-influenced pixels (=15) and background 52 pixels (=5) were randomly selected and used to calculate 10,000  $Q_T$  values. The spread of these 53  $Q_w$  is  $\sigma_{\text{sampling}} = 25$  t/hr.  $\sigma_{\text{precision}}$  is the error on the  $Q_T$  due to precision error of individual 54 TROPOMI XCH<sub>4</sub> retrievals in the emission-influenced and background regions. Note that the 55 precision error represents the influence of the radiance measurement noise on TROPOMI XCH<sub>4</sub>. 56 (provided as XCH4 precision in TROPOMI data products, see Hu et al., 28). By propagating the 57 precision error of the measurements, we find  $\sigma_{\text{precision}} = 3.2 \text{ t/hr}$ .  $\sigma_{\text{method}}$  is taken as the 1 58 standard deviation of mean emission rate estimates from 4 different approaches: 1. mass balance 59 method with 1-band retrievals (see Methods 3); 2. cross-sectional flux (CSF) method with 1-band retrievals (SI Section 2); 3. slope method (SI Section 3) with 1-band retrievals; 3. mass balance 60 method with 2-band retrievals (SI Section 4). The  $\sigma_{method}$  is found to be 13 t/hr. Finally, using 61 62 Equation S1, we calculate  $\sigma_{total} = 32$  t/hr. 63

- 64 Our WRF simulation is nudged to NCEP meteorological fields. To ensure that we are not
- 65 underestimating  $\sigma_{\text{meteo}}$  by sampling output of a single meteorological model at multiple time 66 steps, we consider the instantaneous wind speed at 10-meter height  $U_{10}$  in the blowout region
- 67 from two additional meteorological models (see Table S2). Varon et al. (1) derived the empirical
- relation between  $U_{10}$  and effective wind speed  $U_{eff}$  for the integrated mass enhancement (IME) method ( $U_{eff} = a \log U_{10} + 0.6$ ,  $a = 1.0 \pm 0.1 \text{ ms}^{-1}$ ) and CSF method ( $U_{eff} = b U_{10}$ , b =
- 70 1.4  $\pm$  0.1). Note that the IME method of Varon et al. (1) is similar to mass balance method
- 71 used in this study. In both CSF and IME methods, the emission estimate Q is directly
- 72 proportional to the  $U_{eff}$ . The  $U_{10}$  of NCEP, ERA-5 and ERA-interim have a 1 standard deviation
- 73 of 0.2 ms<sup>-1</sup>. This 7% error on  $U_{10}$  translates to 10 % error on CSF's  $U_{eff}$ , and 6% error on mass

balance's  $U_{eff}$ . These errors are lower than  $\sigma_{meteo}$  (= 12%) providing further confidence that we are not underestimating the meteorological error.

76 77

78 Section 2: Emission quantification using the CSF method

As an alternative to the area-integral-based mass balance approach (see *Methods* 3), we also use

80 the cross-sectional flux (CSF) method as described in Varon et al. (1) to quantity the blowout

81 emission rate. In this method, the measurement-derived emission rate Q of an isolated point

source is quantified using the line-integral mass balance technique along a transect across the
 plume:

84 85

86  $C = \int_{-\infty}^{+\infty} \Delta \Omega (x, y) dy$  .....(S2)

87

88  $Q = CU_{eff}$  ..... (S3) 89

90 where *C* is the tracer enhancement integrated along the transect line (in the *y* direction),

91 perpendicular to the wind direction (blowing in the *x* direction), over the detectable width of the 92 plume.  $U_{eff}$  is the effective wind speed at which column averaged CH<sub>4</sub> is transported at the

93 location of the transect line.  $\Delta\Omega$  is the XCH<sub>4</sub> enhancement relative to an upwind background for 94 a given measurement along the transect. This method can be applied to multiple transect lines at 95 different distances downwind of the source resulting in multiple estimates of Q. These estimates 96 can be used to derive error characteristics of Q

97

98 We made 20 transect lines downwind of the blowout location and perpendicular to the local wind 99 direction (see Fig. S4). The upwind background is the same as used for the mass balance method. For each pixel intersecting a transect line, the product of  $\Delta\Omega$ , and the length of intersection of the 100 transect lines and the pixel was calculated. These numbers were added and multiplied by the U101 102 which was calculated from the WRF XCH<sub>4</sub> output: for the blowout tracer, emission rate  $Q_w$  is 103 known and the line integrals  $C_w$  for each transect line can be calculated from the corresponding XCH<sub>4</sub> output. The ratio between  $Q_w$  and the error weighted average of  $C_w$  gives  $U_{eff} = 5.2 \text{ m s}^{-1}$ . 104 105 Using the empirically derived relation ( $U_{eff} = bU_{10}$ ,  $b = 1.4 \pm 0.1$ ) given in Varon et al. (1) 106 and  $U_{10}$  from NCEP-FNL (see Table S2), which is used as meteorological boundary condition in 107 WRF, we calculate  $U_{eff} = 4.4 \pm 0.5$  m s<sup>-1</sup>. This  $U_{eff}$  is slightly smaller than WRF-derived  $U_{eff}$ . In line with Varon et al. (1), we assume a 40% uncertainty on  $U_{eff}$ . Note that calculating  $C_w$  on the 108 109 WRF XCH<sub>4</sub> regridded TROPOMI pixels also accounts for the bias introduced applying the 110 mass-balance method to coarse resolution TROPOMI measurements.

111

112 The *Q* values calculated for the transect lines in Fig. S4 are shown in Fig. S5. The error-weighted 113 average of these *Q* values is  $130\pm 28$  t/hr. The uncertainty  $\sigma_{total}$  of *Q* is calculated as follows 114

115 
$$\sigma_{\text{total}} = \sqrt{\sigma_{\text{meteo-sampling}}^2 + \sigma_{\text{precision}}^2 + \sigma_{\text{method}}^2}$$
 .....(S4)

- 117  $\sigma_{\text{meteo-sampling}}$  is the combined error due to meteorology and TROPOMI XCH<sub>4</sub> sampling. It is
- 118 calculated by first estimating Q values for each transect line on WRF XCH<sub>4</sub> using  $U_{eff} = 5.2 \text{ ms}^{-1}$ .
- 119 The 1 standard deviation of the difference between the *Q* values of WRF and TROPOMI for all
- 120 transect lines (red curve in Fig. S5) gives  $\sigma_{\text{meteo-sampling}}$ .  $\sigma_{\text{precision}}$  is the TROPOMI XCH<sub>4</sub>
- 121 retrieval precision (as in Section 1).  $\sigma_{method} = 13 \text{ t/hr}$  is the uncertainty due to use of CSF
- 122 method on 1-band data (as in Section 1). Overall, this method leads to  $\sigma_{total} = 28$  t/hr.
- 123
- 124 The variability in *Q* is in large part due to the TROPOMI sampling and meteorological
- 125 variability as a similar variability is found for WRF *Q* values. This is shown in Fig. S5. To
- 126 facilitate comparison, the WRF Q values shown in Fig. S5 are multiplied with 1.625 so that their
- 127 mean matches the mean of TROPOMI *Q* values. The Pearson correlation coefficient between
- 128 WRF and TROPOMI-derived Q values is 0.77, indicating that 60% of the variability in the
- 129 TROPOMI *Q* values can be explained by the TROPOMI sampling, and meteorological effects
- such as wind variability and changes in boundary layer height, which are simulated in WRF. The
- rest of the variability could be caused by errors in TROPOMI measurements and/or errors in the
- 132 WRF-simulated transport.
- 133 134
- 135 <u>Section 3: Emission quantification using the slope method</u>
- 136 The blowout Emission rate can be estimated using the slope method as in Kort et al. (2). By
- 137 performing linear regression between TROPOMI and WRF XCH<sub>4</sub> (see Fig. S6), we find a slope
- 138 of  $1.23 \pm 0.14$ . By multiplying this slope with the emission rate of 80 t/hr used in the WRF
- 139 simulation, emission rate of  $98 \pm 22$  t/hr is calculated. This compares well with our mass balance
- estimate of  $120 \pm 32$  t/hr. The two methods are not expected to yield the same answer, since the
- slope method uses WRF and TROPOMI XCH<sub>4</sub> values for each pixel, whereas, the mass balance
- 142 method uses the difference between averages of background and blowout-influenced pixels
- 143 resulting in a different weighing.
- 144
- 145
- 146 <u>Section 4: Emission quantification using 2-band retrievals</u>
- 147 Here we quantify the emission rate for the blowout using data from the operational 2-band
- 148 TROPOMI XCH<sub>4</sub> retrievals. We find XCH<sub>4</sub> enhancement in the 2-band retrievals that are similar
- to the 1-band retrievals during the Ohio blowout. The emission quantification with the 2-band
- retrievals (*Methods* 3) yields  $100 \pm 32$  t/hr, which is in close agreement with the emission rate
- estimate from the 1-band retrievals of  $120 \pm 32$ . The 1-band and 2-band XCH<sub>4</sub> product differ in
- 152 the spectral information used to constrain the retrieval (only the 2-band retrieval uses NIR data).
- 153 Both the 1-band and 2-band TROPOMI XCH<sub>4</sub> products show small striping effects. In this study,
- 154 neither of the products is corrected for striping effect as the available methods may introduce
- 155 new errors. We have checked and found that the striping effect in XCH<sub>4</sub> is significantly smaller
- 156 than the signal associated with the Ohio blowout event. In addition, the sampling error
- 157  $(\sigma_{sampling})$  derived using the bootstrapping method should account for the error due to the
- 158 striping effect (Section 1).
- 159
- 160
- 161
- 162

- 163 <u>Section 5: Influence of regular emissions</u>
- 164 In our emission quantification method (*Methods* 3), the TROPOMI XCH<sub>4</sub> enhancement ( $X_T$ )
- also includes enhancements due to regular emissions in the blowout-influenced region (see Fig.
- 166 S7). These emissions are accounted for since the WRF XCH<sub>4</sub> enhancement  $(X_w)$  is calculated by
- taking the sum of the EPA, blowout and boundary tracers. The effect of the regular emission will
- 168 cancel out in  $\frac{X_T}{X_W}$  if the EPA emissions are a good estimate of the anthropogenic emissions. We
- assess the impact of EPA emissions being an underestimate of the regular emissions in the
- 170 downwind enhancement region. The XCH<sub>4</sub> enhancement of the EPA tracer ( $X_W^{epa}$ ) is 1.5 ppb,
- 171 which is ~5% of  $X_W$  (= 27 ppb) for sum of all WRF tracers. If the EPA underestimates the
- 172 emissions in the blowout-influenced region by a factor of 5,  $X_w$  would be 33 ppb ( $X_w$  +
- 173 4  $\times X_w^{epa}$  ), resulting in  $Q_T = 97$  t/hr. This estimate is still in statistical agreement with the
- 174 original emission estimate of 120±32 t/hr, indicating that our results are robust to EPA inventory 175 uncertainties.
- 176
- 177 Further, we also do a CSF quantification for the same transects lines and background area used
- 178 for 27 February 2018 (SI Section 2) but for measurements on 28 November 2017, i.e., before the
- blowout when wind conditions were similar. Then we find a Q of 2 (-2/+7) t/hr, which is well
- 180 within the estimated uncertainty of Q of 28 t/hr during the blowout. This further supports our

181 finding that the large downwind XCH<sub>4</sub> enhancements along the transects are caused primarily by

- 182 the blowout CH<sub>4</sub> emissions and are not due to regular emissions in the region.
- 183

184 During all overpasses –albeit somewhat less pronounced on 20 April 2018–a secondary

- 185 enhanced region around the city of Pittsburgh is visible, likely caused by sustained emissions due
- to O&G and coal mining operations in that area as suggested by EPA inventory (Fig. S8). It
- 187 should be noted that the local Pittsburgh area emissions is not expected to contribute to the
- 188 blowout enhancement due to the orientation of wind fields and use of *influence* mask (see Fig. 2c
- 189 of main text).
- 190 191
- 192 <u>Section 6: Source pixel enhancement</u>
- In Fig. 2c of the main text, we observe that the pixel containing the blowout, as well as the one immediately downwind of it, show a less pronounced  $XCH_4$  enhancement than the pixels further
- immediately downwind of it, show a less pronounced XCH<sub>4</sub> enhancement than the pixels further downwind. This could be for a number of reasons. First, in the pixel containing the well blowout,
- 195 downwind. This could be for a number of reasons. First, in the pixel containing the well blowout,
- the location of the well is half-way in the downwind direction, (see Fig. S9b) and this would cause only a partial enhancement. It is noteworthy that this low XCH<sub>4</sub> enhancement would not be
- cause only a partial emiancement. It is noteworthy that this low  $ACH_4$  emiancement would not be captured by the WRF simulation as the "point source" is an evenly distributed CH<sub>4</sub> emission
- source over a WRF grid pixel of 5 km  $\times$  5 km, causing a local representation error. The
- 200 TROPOMI pixel size is  $7 \text{ km} \times 7 \text{ km}$  at nadir. However, the pixels shown in the analysis region
- 201 are 25 km wide because they are near the edge of the swath, and are thus stretched due to the
- 202 large viewing zenith angle. Second, there can be a bias in the XCH<sub>4</sub> measurements caused by
- 203 scattering of light due to simultaneously emitted liquid droplets and fine particles such as water
- and hydraulic fracturing fluids which can also be seen in the video of the blowout (see Movie
- 205 S1). Third, the logarithmic dependence of XCH<sub>4</sub> on the absorption line depth would also result in
- an underestimate of average XCH<sub>4</sub> in the partially enhanced pixels. The partial pixel
- 207 enhancement effect would be less significant further downwind of the source once the plume
- 208 widths increases and becomes comparable to the pixel width. This is evident in the large

209 enhancements (106±2 ppb, Fig. 1b) seen at 36 km downwind of the source. The development of

- a spatially dispersed plume is also evident in WRF XCH<sub>4</sub> (see Fig. 2a of main text).
- 211 212
- 213 Section 7: Total emission quantification

The uncertainty of extrapolating the blowout emission rate to the full 20-day period is difficult to 214 215 assess from only a single instantaneous emission estimate derived from TROPOMI, without 216 knowing the time dependence of the emissions. However, a range of total emission can be 217 derived by considering a range of plausible emission rate time dependences. The gas well can be 218 described as a pressurized chamber of finite volume leaking gas from a small orifice. For such a 219 well, an exponentially declining emission rate during the blowout period is expected, with e-220 folding time equal to the ratio of the reservoir capacity and the instantaneous leakage rate. An approximately constant emission rate occurs if the leakage during the blowout period is small 221 222 compared with the well capacity, i.e., e-folding time is very large compared to the blowout 223 period. An exponential reduction has been observed in previous studies measuring emission rates 224 from gas well blowout episodes: Conley et al. (3) observed exponentially decreasing emissions 225 from the Aliso Canyon storage tank during the major portion of the  $\sim$ 3.5 month leakage period. 226 Lee at al. (4) observed a decreasing emission rate from the uncontrolled Elgin platform gas 227 release over a period of a month and a half, in the North Sea. Although not mentioned explicitly 228 by Lee at al. (4), their measurements point to exponentially decreasing emissions.

229

For the Ohio blowout gas well, the pressure inside the chamber is proportional to the N moles of gas that are present as determined by the ideal gas law. Everything else kept constant, the emission rate Q is proportional to the pressure difference across the orifice. Assuming the pressure inside the well is many times larger than the atmospheric pressure outside and negligible changes in temperature, Q is given by

- 235
- $\begin{array}{ll} 236 \\ 237 \end{array} \qquad Q(t) = \frac{dN}{dt} \approx -\lambda N \end{array}$

238 Where  $\lambda$  is a constant. Using this equation, we derive the total emission *E* until a given time  $(t_c)$ 239 of the blowout as a function of the ratio between initial emission rate  $Q_0$  and the emission rate  $Q_t$ 240 at measurement time  $t_m$  as 241

- 242  $E = \frac{Q_t (1 e^{-\lambda t_c})}{-\lambda e^{\lambda t_m}}$
- 243
- 244  $\lambda = \frac{\log\left(Q_t/Q_0\right)}{t_m}$

Using these equations, the *E* for the Ohio blowout is shown in Fig. S10 with  $t_c = 20$  days,  $t_m =$ 13 days and  $Q_t = 120$  t/hr for  $0.1 < \frac{Q_t}{Q_0} < 1$ . Assuming a near-constant emission rate, we get a total emission of 57 kt CH<sub>4</sub> (or  $60 \pm 15$  after accounting for uncertainties in the blowout emission rate). Any sustained exponential decrease in the emission rate leads to E > 57 kt CH<sub>4</sub>, which means that we are likely underestimating our total emission estimate and its uncertainty.

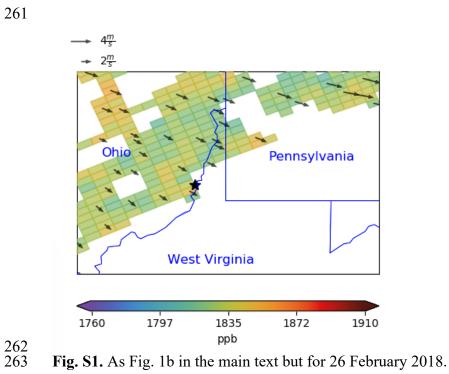
- **Table S1**: Uncertainty estimation due to meteorological errors derived as the sensitivity of the emission estimate to the temporal sampling of WRF.

Hour (UTC)	Q (t/hr)
15:00	135
16:00	93
17:00	96
18:00*	116
19:00	112
20:00	110
Standard deviation $(\sigma , \cdot)$	14

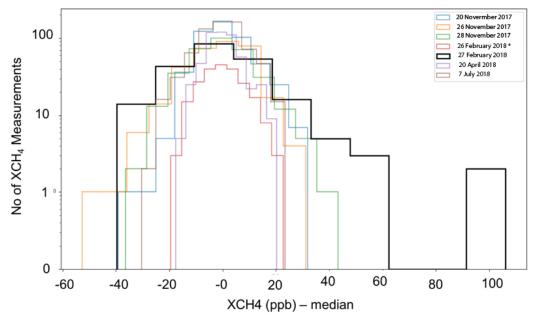
**Standard deviation** ( $\sigma_{meteo}$ ) **14** \*Hour of WRF output used to quantify the blowout emission. 

- **Table S2.** 10-meter wind speed averaged over the Ohio blowout region at 18:00 UTC on 27 February 2018, closest to the TROPOMI overpass time.
- 259

Meteorological Model	wind speed ± standard error (ms <sup>-1</sup> )
NCEP-FNL (5)	$3.1 \pm 0.3$
ECMWF ERA-5 (6)	$2.8 \pm 0.1$
ECMWF ERA-interim (7)	$3.3\pm0.1$



263 264



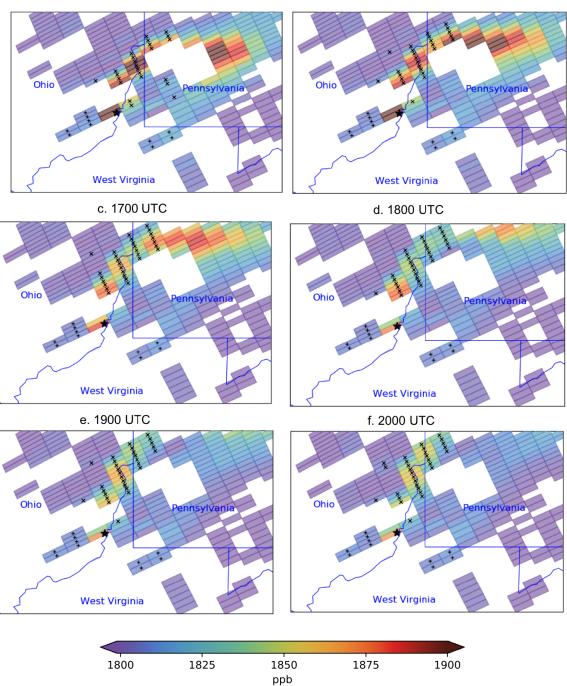


**Fig. S2.** Distribution of TROPOMI measurements for days with sufficient coverage in the

blowout region, as shown in Fig. 1 of main text, after subtracting the median of all measurements
on the respective day. Notice that the distribution of XCH<sub>4</sub> on 27 February 2018 (during blowout
period), is positive-skewed in comparison to other days due to the large CH<sub>4</sub> emission from the
blowout.

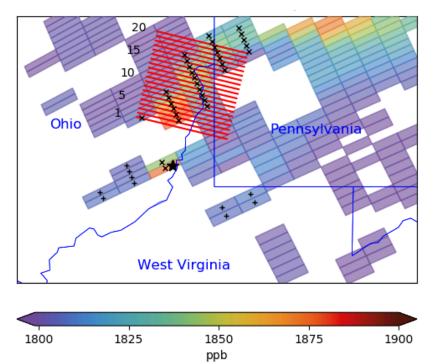


b. 1600 UTC



272 273

Fig. S3: WRF XCH<sub>4</sub> as in Fig. 2b in the main text for different hours adjacent to the TROPOMI overpass time on 27 February 2018 and the corresponding blowout-influenced (crosses) and 274 275 background pixels (pluses). Note that the influence mask is different for each hour as it is 276 calculated using the corresponding blowout tracer output.

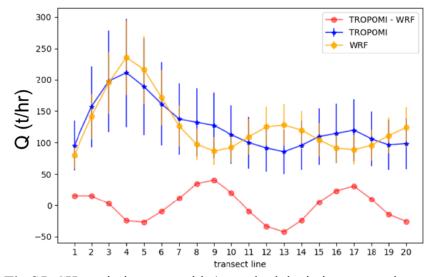


278 279

**Fig. S4**. As Fig. 2c of the main text, for CH<sub>4</sub> emission quantification using the CSF method. The

red lines are the transect lines perpendicular to the wind direction at the blowout location.

281 Emission estimates obtained per transect line are shown in Fig. S5.

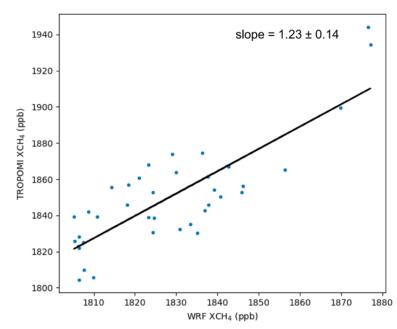


283 284 Fig S5. CH<sub>4</sub> emission rate, with 1 standard deviation uncertainty, calculated from TROPOMI

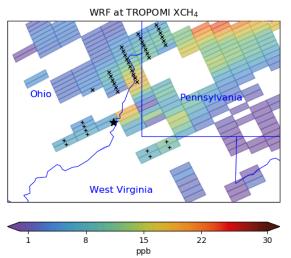
XCH<sub>4</sub> along the different transect lines shown in Fig. S4 using the CSF method. WRF-derived 285 286 emission rates are also plotted. Note that, to facilitate visual comparison, the WRF emission rates

are multiplied by 1.62 such that their mean is equal to the mean of the TROPOM- derived 287

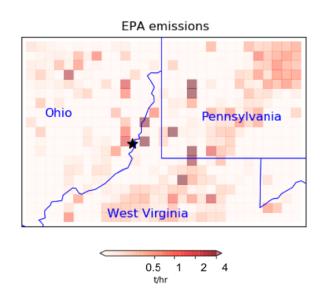
- 288 emission rates.
- 289



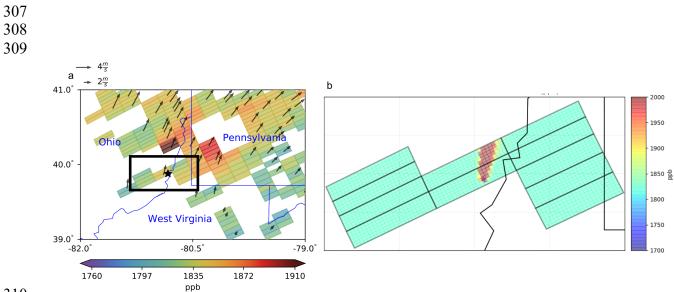
292
 293 Fig. S6 TROPOMI measurements vs WRF-simulated XCH<sub>4</sub>. Only the blowout-influenced
 294 and background pixels, marked with crosses and pluses in Figure 2c, are plotted.
 295



**Fig. S7.** WRF XCH<sub>4</sub> for the EPA tracer. The crosses and pluses mark the blowout-influenced and background pixels, respectively. 298 299 300



**Fig. S8**. Anthropogenic  $CH_4$  emission in the blowout region for 2012 according to EPA 2012 inventory. The blowout location is marked with a black star. 





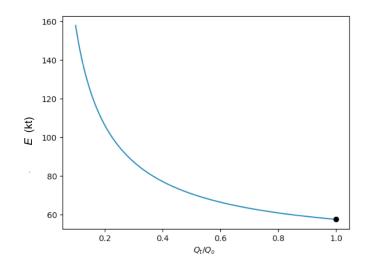
311 Fig S9. Illustration of partial pixel enhancement based in a high resolution WRF run.

312 XCH<sub>4</sub> measurements (left panel; as in Fig. 1b of main text) and high resolution (1x1 km<sup>2</sup>) WRF

313 XCH<sub>4</sub> (right panel) within the TROPOMI pixels over the blowout location. The star marks the

314 location of blowout well. The black box in the left panel shows the region that is enlarged in the 315 right panel. The color scale of the right panel has been adjusted to facilitate the visualization of

- right panel. The color scale of the right panel has been adjusted to facilitate the visualizationthe plume.
- 310 u 317
- 318





321 Fig. S10. Total emissions *E* from the Ohio blowout in 20 days as function of ratio between initial

322  $(\boldsymbol{q}_0)$  and measured emission rate  $(\boldsymbol{q}_t)$ . If the ratio between emission rates is 1 (black dot), E = 57323 kt.

326	Movie	S1.
327		of the leakage from the blowout on 3 March 2018 taken with FLIR (Forward Looking
328		ed) optical gas imaging cameras by Earthworks.
329	mmur	ed) optical gas inaging canteras by Darthworks.
330		
331		
332		
333		
334		
335		
336	Refere	ences
337	1.	D. J. Varon et al., Quantifying methane point sources from fine-scale satellite
338		observations of atmospheric methane plumes. Atmospheric Measurement
339		<i>Techniques</i> <b>11</b> (10), 5673-5686 (2018).
340	2.	E. A. Kort et al., Four corners: The largest US methane anomaly viewed from space.
341		Geophysical Research Letters <b>41</b> , 6898–6903 (2014).
342		https://doi.org/10.1002/2014GL061503
343	З.	S. Conley et al., Methane emissions from the 2015 Aliso Canyon blowout in Los Angeles,
344		CA. Science, <b>351</b> , 1317–1321 (2016).
345	4.	J. D. Lee et al., Flow rate and source reservoir identification from airborne chemical
346		sampling of the uncontrolled Elgin platform gas release. Atmos. Meas. Tech 11, 1725–
347		1739 (2018). <u>https://doi.org/10.5194/amt-11-1725-2018</u>
348	5.	National Centers for Environmental Prediction/National Weather Service/NOAA/U.S.
349		Department of Commerce. 2000, updated daily. NCEP FNL Operational Model Global
350		Tropospheric Analyses, continuing from July 1999. Research Data Archive at the National
351		Center for Atmospheric Research, Computational and Information Systems Laboratory.
352		https://doi.org/10.5065/D6M043C6. Accessed on 05-08-2019.
353	6.	Copernicus Climate Change Service (C3S), "ERA5: Fifth generation of ECMWF
354		atmospheric reanalyses of the global climate" (Copernicus Climate Change Service
355		Climate Data Store (CDS), 2019; <u>https://cds.climate.copernicus.eu/cdsapp#!/home</u> )
356		Accessed on 05-08-2019.
357	7.	D. P. Dee et al., The ERA-Interim reanalysis: Configuration and performance of the data
358		assimilation system. Quarterly Journal of the Royal Meteorological Society 137:656,
359		553–597 (2011).
360		