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_publ_contact_author_email biswasd@mail.nih.gov
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Nitrogen-bound Diazeniumdiolated Amidines
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'Debanjan Biswas'
'Jeffrey Deschamps'
'Larry Keefer'
'Joseph Hrabie'
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'x+1/2, -y+1/2, -z'
'-x, -y, -z'
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'x-1/2, y, -z-1/2''x, -y-1/2, z-1/2' '-x-1/2, y-1/2, z' _cell_length a 9.8141(5) cell length b 11.4621(7)_cell_length c 17.6029(9)_cell_angle_alpha 90.00 _cell_angle_beta 90.00 _cell_angle gamma 90.00 _cell_volume 1980.15(19) cell formula units Z 8 cell measurement temperature 294(2) _cell_measurement_reflns_used 5886 cell measurement theta min 2.31 cell measurement theta max 25.82 _exptl_crystal_description prisim _exptl_crystal colour colourless _exptl_crystal_size_min 0.107 _exptl_crystal_size_mid 0.144 0.551 exptl crystal size max _exptl_crystal_density_meas ? exptl crystal density diffrn 1.303 exptl crystal density method 'not measured' _exptl_crystal_F_000 816 _exptl_absorpt_coefficient_mu 0.098 # # # NOTE on absorbtion correction with SADABS: # # # # (Semi)empirical correction methods for absorption correction are more of # # a problem in that they often specify only a relative correction range # # [Tmin(emp) & Tmax(emp)]. # # # # Acta Cryst. procedures call in such cases for the multiplication of both # # empirical values with Tmax(expected). # # # # THIS RECOMMENDATION IS CURRENTLY UNDER REVIEW! (George # # and Ton are agruing this point!) # # # exptl absorpt correction type multi-scan _exptl_absorpt_process_details 'SADABS v2.10 (Bruker, 2000c)' _exptl_absorpt_correction_T_min 0.9482 exptl absorpt correction T max 0.9896 exptl special details ; ? ; _diffrn_ambient_temperature 294(2) # SMART APEX II parameters _diffrn_radiation_wavelength 0.71073 _diffrn_radiation_type MoK\a _diffrn_radiation_source 'fine-focus sealed tube' diffrn radiation monochromator graphite _diffrn_measurement_device_type 'Bruker SMART APEX II CCD' diffrn measurement method '\w scans' diffrn detector area resol mean ? _diffrn_reflns_number 19608

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01 0 0.23757(10) 0.29498(10) 0.06832(6) 0.0714(3) Uani 1 1 d . . .
N2 N 0.20244(12) 0.16960(10) 0.16465(6) 0.0593(3) Uani 1 1 d . . .
N3 N 0.03072(10) 0.28617(9) 0.13396(5) 0.0516(3) Uani 1 1 d . . .
02 0 0.33715(10) 0.14482(10) 0.14812(6) 0.0712(3) Uani 1 1 d . . .
C3 C 0.3848(2) 0.05895(17) 0.20119(12) 0.1006(7) Uani 1 1 d . . .
H3A H 0.4734 0.0322 0.1860 0.151 Uiso 1 1 calc R . .
H3B H 0.3227 -0.0057 0.2021 0.151 Uiso 1 1 calc R . .
H3C H 0.3902 0.0930 0.2509 0.151 Uiso 1 1 calc R . .
C1' C -0.04200(12) 0.31006(9) 0.07380(6) 0.0468(3) Uani 1 1 d . . .
N1' N -0.00626(14) 0.30174(12) 0.00115(6) 0.0634(3) Uani 1 1 d . . .
H1'A H 0.078(2) 0.2831(17) -0.0098(11) 0.095 Uiso 1 1 d . . .
H2'B H -0.073(2) 0.2994(17) -0.0327(12) 0.095 Uiso 1 1 d . . .
C2' C -0.18176(12) 0.35294(10) 0.09034(6) 0.0489(3) Uani 1 1 d . . .
C3' C -0.25944(14) 0.30218(12) 0.14735(7) 0.0589(3) Uani 1 1 d . . .
H3'A H -0.2242 0.2405 0.1755 0.071 Uiso 1 1 calc R . .
C4' C -0.38923(15) 0.34327(15) 0.16238(8) 0.0710(4) Uani 1 1 d . . .
H4'A H -0.4417 0.3085 0.2001 0.085 Uiso 1 1 calc R . .
C5' C -0.44078(16) 0.43565(15) 0.12151(10) 0.0770(5) Uani 1 1 d . . .
H5'A H -0.5280 0.4632 0.1317 0.092 Uiso 1 1 calc R . .
C6' C -0.36325(17) 0.48747(14) 0.06544(10) 0.0736(4) Uani 1 1 d . . .
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C7' C -0.23470(15) 0.44597(11) 0.04926(8) 0.0613(3) Uani 1 1 d . . .
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N1 0.0501(6) 0.0551(5) 0.0443(5) -0.0007(4) -0.0019(4) 0.0018(4)
01 \ 0.0521(5) \ 0.0906(7) \ 0.0715(6) \ 0.0250(5) \ 0.0068(4) \ 0.0017(5)
N2 0.0618(7) 0.0630(6) 0.0530(6) 0.0036(5) -0.0011(5) 0.0108(5)
N3 0.0491(6) 0.0601(6) 0.0455(5) 0.0002(4) -0.0004(4) 0.0052(4)
02 \ 0.0647(6) \ 0.0845(7) \ 0.0644(6) \ 0.0047(5) \ -0.0041(4) \ 0.0248(5)
C3 0.1171(16) 0.0898(12) 0.0949(13) 0.0083(10) -0.0112(11) 0.0518(11)
C1' 0.0497(6) 0.0449(6) 0.0457(6) -0.0012(4) -0.0004(5) -0.0037(5)
N1' 0.0524(6) 0.0925(9) 0.0452(6) -0.0025(5) -0.0018(5) 0.0025(6)
C2' 0.0503(6) 0.0488(6) 0.0476(6) -0.0050(5) -0.0035(5) 0.0010(5)
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\texttt{C4' 0.0587(8) 0.0919(11) 0.0624(8) -0.0144(7) 0.0090(6) 0.0022(7)}
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C6' 0.0737(10) 0.0606(8) 0.0864(10) -0.0091(7) -0.0194(8) 0.0175(7)
C7' 0.0643(8) 0.0522(7) 0.0672(8) 0.0020(6) -0.0083(6) 0.0022(6)
_geom_special details
All esds (except the esd in the dihedral angle between two l.s. planes)
```

are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes. ;

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N3 C1' 1.3060(15) . ?
O2 C3 1.4354(19) . ?
C3 H3A 0.9600 . ?
C3 H3B 0.9600 . ?
C3 H3C 0.9600 . ?
C1' N1' 1.3294(16) . ?
C1' C2' 1.4858(17) . ?
N1' H1'A 0.88(2) . ?
N1' H2'B 0.89(2) . ?
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C3' H3'A 0.9300 . ?
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C4' H4'A 0.9300 . ?
C5' C6' 1.381(2) . ?
C5' H5'A 0.9300 . ?
C6' C7' 1.378(2) . ?
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geom angle publ flag
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O2 C3 H3B 109.5 . . ?
H3A C3 H3B 109.5 . . ?
O2 C3 H3C 109.5 . . ?
H3A C3 H3C 109.5 . . ?
H3B C3 H3C 109.5 . . ?
N3 C1' N1' 128.37(12) . . ?
N3 C1' C2' 114.51(10) . . ?
N1' C1' C2' 117.12(11) . . ?
C1' N1' H1'A 118.5(13) . . ?
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H1'A N1' H2'B 123.0(18) . . ?
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C3' C2' C1' 120.66(11) . . ?
C7' C2' C1' 119.81(11) . . ?
C4' C3' C2' 120.07(13) . . ?
C4' C3' H3'A 120.0 . .
C2' C3' H3'A 120.0 . . ?
C5' C4' C3' 120.02(15) . . ?
C5' C4' H4'A 120.0 . . ?
C3' C4' H4'A 120.0 . . ?
C4' C5' C6' 120.13(14) .
                        . ?
C4' C5' H5'A 119.9 . . ?
C6' C5' H5'A 119.9 . . ?
C7' C6' C5' 120.25(14) .
                        . ?
C7' C6' H6'A 119.9 . .
                       ?
C5' C6' H6'A 119.9 . .
                       ?
C6' C7' C2' 119.98(14) . . ?
C6' C7' H7'A 120.0 . . ?
C2' C7' H7'A 120.0 . . ?
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O1 N1 N3 C1' 41.94(15) . . . ?
N2 N1 N3 C1' -142.94(11) . . . .
                                 ?
N1 N2 O2 C3 177.92(12) . . . ?
N1 N3 C1' N1' 0.89(18) . . . ?
N1 N3 C1' C2' -178.47(9) . . . ?
N3 C1' C2' C3' -41.56(16) . . . ?
N1' C1' C2' C3' 139.00(13) . . . .
N3 C1' C2' C7' 137.40(12) . . . ?
N1' C1' C2' C7' -42.04(16) . . . ?
C7' C2' C3' C4' 0.77(19) . . . ?
C1' C2' C3' C4' 179.73(12) . . . ?
C2' C3' C4' C5' -0.9(2) . . . ?
C3' C4' C5' C6' 0.0(2) . . . ?
C4' C5' C6' C7' 1.0(2) . . . ?
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C5' C6' C7' C2' -1.1(2) . . . ?C3' C2' C7' C6' 0.25(19) . . . ? C1' C2' C7' C6' -178.73(12) . . . ?

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?

N1' H2'B O1 0.89(2) 2.24(2) 3.0075(17) 144.8(17) 4 455 N1' H2'B O2 0.89(2) 2.30(2) 3.1051(16) 150.0(17) 4_455 _diffrn_measured_fraction_theta max 0.997 _diffrn_reflns_theta_full 25.00 _diffrn_measured_fraction_theta full 1.000 _refine_diff_density_max 0.149 _refine_diff_density_min -0.146_refine_diff_density_rms 0.028 #_____ data 9 database code depnum ccdc archive 'CCDC 761562' #TrackingRef 'Amidine-Crystal-Data.cif.txt' audit creation method SHELXL-97 _chemical_name_systematic ? ; _chemical_name_common ? _chemical_melting_point ? 'C16 H18 N4 O2' 'C16 H18 N4 O2' _chemical_formula_moiety chemical formula sum chemical formula weight 298.34 loop_ _atom_type_symbol _atom_type_description _atom_type_scat_dispersion_real _atom_type_scat_dispersion imag _atom_type_scat_source C C 0.0033 0.0016 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4' H H 0.0000 0.0000 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4' N N 0.0061 0.0033 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4' 0 0 0.0106 0.0060 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4' _symmetry_cell_setting orthorhombic Pbca _symmetry_space_group_name_H-M loop_ _symmetry_equiv_pos_as_xyz 'x, y, z' 'x+1/2, -y+1/2, -z' '-x, y+1/2, -z+1/2' '-x+1/2, -y, z+1/2' '-x, -y, -z' '-x-1/2, y-1/2, z' 'x, -y-1/2, z-1/2' 'x-1/2, y, -z-1/2' _cell_length a 9.9137(7) _cell_length_b 13.7220(10) _cell_length_c 22.4918(16) _cell_angle alpha 90.00 _cell_angle_beta 90.00 _cell_angle_gamma 90.00 cell volume 3059.7(4) _cell_formula_units Z 8 cell measurement temperature 100(2)cell measurement reflns used 8050 _cell_measurement_theta_min 2.69

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cell measurement theta max
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_exptl_crystal_size max
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_exptl_crystal_density_meas
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_exptl_crystal_density method
                               'not measured'
_exptl_crystal_F_000
                               1264
exptl absorpt coefficient mu
                               0.089
# #
# NOTE on absorbtion correction with SADABS: #
# #
# (Semi)empirical correction methods for absorption correction are more of #
# a problem in that they often specify only a relative correction range #
# [ Tmin(emp) & Tmax(emp)]. #
# #
# Acta Cryst. procedures call in such cases for the multiplication of both #
# empirical values with Tmax(expected). #
# #
# THIS RECOMMENDATION IS CURRENTLY UNDER REVIEW! (George #
# and Ton are agruing this point!) #
# #
multi-scan
exptl absorpt correction type
_exptl_absorpt_process_details
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;
?
;
_diffrn_ambient_temperature
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                               '\w scans'
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_diffrn_reflns_number
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diffrn reflns av sigmaI/netI
                               0.0178
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_diffrn_reflns_limit_h_max
                               13
diffrn reflns limit k min
                               -18
_diffrn_reflns_limit_k_max
                               18
_diffrn_reflns_limit_l_min
                               -27
_diffrn_reflns_limit l max
                               30
_diffrn_reflns_theta_min
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_diffrn_reflns_theta_max
                               29.17
reflns number total
                               4131
_reflns_number_gt
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reflns threshold expression
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_computing_data_collection
                               'Bruker SMART v5.631 (Bruker, 2001)'
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computing cell refinement
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_computing_data_reduction
Bruker SAINT v6.45A (Bruker, 2002), Bruker XPREP v6.14 (Bruker, 2001)
;
_computing_structure solution
                                  'Bruker SHELXTL v6.14 (Bruker, 2000b)'
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                                 'Bruker SHELXTL v6.14 (Bruker, 2000b)'
_refine_special_details
;
Refinement of F<sup>2</sup> against ALL reflections. The weighted R-factor wR and
goodness of fit S are based on F^2^, conventional R-factors R are based
on F, with F set to zero for negative F^2^-. The threshold expression of
F^2 > 2sigma(F^2) is used only for calculating R-factors(gt) etc. and is
not relevant to the choice of reflections for refinement. R-factors based
on F<sup>2</sup> are statistically about twice as large as those based on F, and R-
factors based on ALL data will be even larger.
refine ls structure factor coef Fsqd
_refine_ls_matrix type
                                  full
refine 1s weighting scheme
                                  calc
refine 1s weighting details
'calc w=1/[\s^2^(Fo^2^)+(0.0596P)^2^+0.7787P] where P=(Fo^2^+2Fc^2^)/3'
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                                 direct
atom sites solution secondary
                                  difmap
_atom_sites_solution_hydrogens
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                                  ?
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_refine_ls_number_restraints
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refine ls R factor all
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refine ls R factor gt
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refine ls wR factor gt
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_refine_ls_restrained S all
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_refine_ls_shift/su mean
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loop_
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_atom_site_type_symbol
atom site fract x
atom site fract y
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atom site disorder group
N1 N 0.53139(8) -0.09689(5) 0.36447(4) 0.01579(17) Uani 1 1 d . . .
01 0 0.63318(7) -0.09296(5) 0.39774(3) 0.02145(16) Uani 1 1 d . . .
N2 N 0.52967(8) -0.10581(6) 0.30791(4) 0.01739(18) Uani 1 1 d . . .
02 0 0.66272(7) -0.10869(5) 0.28834(3) 0.01998(16) Uani 1 1 d . . .
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N3 N 0.39993(8) -0.09989(6) 0.38856(4) 0.01741(17) Uani 1 1 d . . .
C3 C 0.65802(11) -0.10615(7) 0.22374(5) 0.0215(2) Uani 1 1 d . . .
H3B H 0.6102 -0.1648 0.2091 0.026 Uiso 1 1 calc R . .
H3A H 0.7512 -0.1079 0.2079 0.026 Uiso 1 1 calc R . .
C4 C 0.58771(10) -0.01639(7) 0.20066(4) 0.0191(2) Uani 1 1 d . . .
C5 C 0.64892(11) 0.07509(7) 0.20554(5) 0.0224(2) Uani 1 1 d . . .
H5 H 0.7360 0.0806 0.2229 0.027 Uiso 1 1 calc R . .
C6 C 0.58278(11) 0.15818(8) 0.18511(5) 0.0262(2) Uani 1 1 d . . .
H6 H 0.6251 0.2201 0.1883 0.031 Uiso 1 1 calc R . .
C7 C 0.45481(12) 0.15079(8) 0.16006(5) 0.0268(2) Uani 1 1 d . . .
H7 H 0.4097 0.2076 0.1463 0.032 Uiso 1 1 calc R . .
C8 C 0.39306(11) 0.06016(8) 0.15524(5) 0.0252(2) Uani 1 1 d . . .
H8 H 0.3058 0.0548 0.1381 0.030 Uiso 1 1 calc R . .
C9 C 0.45972(11) -0.02272(7) 0.17565(5) 0.0218(2) Uani 1 1 d . . .
H9 H 0.4171 -0.0845 0.1724 0.026 Uiso 1 1 calc R .
C10 C 0.36309(10) -0.01622(7) 0.41256(4) 0.01572(18) Uani 1 1 d . . .
N11 N 0.24625(9) -0.01521(6) 0.44263(4) 0.02009(18) Uani 1 1 d . . .
C12 C 0.16817(11) -0.10441(8) 0.45102(5) 0.0249(2) Uani 1 1 d . . .
H12C H 0.0821 -0.0988 0.4299 0.037 Uiso 1 1 calc R . .
H12B H 0.1511 -0.1143 0.4935 0.037 Uiso 1 1 calc R . .
H12A H 0.2189 -0.1600 0.4353 0.037 Uiso 1 1 calc R . .
C13 C 0.17976(11) 0.07325(8) 0.46367(5) 0.0262(2) Uani 1 1 d . . .
H13C H 0.1833 0.0755 0.5072 0.039 Uiso 1 1 calc R . .
H13B H 0.0854 0.0732 0.4506 0.039 Uiso 1 1 calc R . .
H13A H 0.2259 0.1304 0.4473 0.039 Uiso 1 1 calc R . .
C14 C 0.44555(10) 0.07503(6) 0.40979(4) 0.01575(19) Uani 1 1 d . . .
C15 C 0.48967(10) 0.11261(7) 0.35529(4) 0.01779(19) Uani 1 1 d . . .
H15 H 0.4622 0.0830 0.3191 0.021 Uiso 1 1 calc R . .
C16 C 0.57415(10) 0.19376(7) 0.35446(5) 0.0214(2) Uani 1 1 d . . .
H16 H 0.6048 0.2191 0.3176 0.026 Uiso 1 1 calc R . .
C17 C 0.61386(11) 0.23791(7) 0.40734(5) 0.0239(2) Uani 1 1 d . . .
H17 H 0.6721 0.2929 0.4066 0.029 Uiso 1 1 calc R . .
C18 C 0.56808(11) 0.20134(7) 0.46122(5) 0.0237(2) Uani 1 1 d . . .
H18 H 0.5942 0.2320 0.4973 0.028 Uiso 1 1 calc R . .
C19 C 0.48423(10) 0.12015(7) 0.46280(5) 0.0197(2) Uani 1 1 d . . .
H19 H 0.4533 0.0954 0.4998 0.024 Uiso 1 1 calc R . .
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_atom_site_aniso U 33
_atom_site_aniso_U_23
_atom_site_aniso_U_13
_atom_site_aniso_U_12
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01 \ 0.0163(3) \ 0.0256(4) \ 0.0225(4) \ -0.0007(3) \ -0.0028(3) \ 0.0019(3)
N2 0.0149(4) 0.0175(4) 0.0197(4) -0.0010(3) 0.0034(3) -0.0004(3)
02 \ 0.0151(3) \ 0.0229(3) \ 0.0219(4) \ -0.0005(3) \ 0.0047(3) \ 0.0013(3)
N3 0.0143(4) 0.0182(4) 0.0198(4) -0.0012(3) 0.0032(3) -0.0020(3)
C3 0.0232(5) 0.0203(4) 0.0211(5) -0.0013(3) 0.0072(4) 0.0033(4)
C4 \quad 0.0210(5) \quad 0.0181(4) \quad 0.0183(4) \quad -0.0012(3) \quad 0.0070(4) \quad 0.0007(3)
C5 0.0190(5) 0.0228(5) 0.0254(5) -0.0011(4) 0.0026(4) -0.0034(4)
C6 \ 0.0270(6) \ 0.0187(5) \ 0.0329(6) \ -0.0006(4) \ 0.0009(4) \ -0.0048(4)
C7 0.0272(6) 0.0195(5) 0.0338(6) 0.0007(4) 0.0010(4) 0.0009(4)
\texttt{C8} \ \texttt{0.0205(5)} \ \texttt{0.0231(5)} \ \texttt{0.0319(6)} \ -\texttt{0.0026(4)} \ \texttt{0.0004(4)} \ -\texttt{0.0003(4)}
C9 0.0217(5) 0.0179(4) 0.0258(5) -0.0029(4) 0.0055(4) -0.0028(4)
C10 \ 0.0141(4) \ 0.0186(4) \ 0.0145(4) \ 0.0004(3) \ -0.0016(3) \ -0.0001(3)
N11 0.0155(4) 0.0223(4) 0.0225(4) -0.0017(3) 0.0037(3) 0.0003(3)
C12 \ 0.0177(5) \ 0.0287(5) \ 0.0284(6) \ 0.0032(4) \ 0.0046(4) \ -0.0042(4)
C13 \ 0.0192(5) \ 0.0308(5) \ 0.0285(6) \ -0.0055(4) \ 0.0045(4) \ 0.0061(4)
C14 0.0130(4) 0.0142(4) 0.0200(5) -0.0008(3) -0.0009(3) 0.0016(3)
```

```
C15 \ 0.0174(4) \ 0.0165(4) \ 0.0194(4) \ -0.0008(3) \ 0.0000(4) \ 0.0024(3)
C16 0.0196(5) 0.0167(4) 0.0279(5) 0.0029(4) 0.0040(4) 0.0017(3)
C17 \ 0.0203(5) \ 0.0149(4) \ 0.0364(6) \ -0.0012(4) \ -0.0015(4) \ -0.0003(4)
C18 \ 0.0243(5) \ 0.0176(4) \ 0.0293(5) \ -0.0043(4) \ -0.0071(4) \ 0.0010(4)
C19 \ 0.0206(5) \ 0.0179(4) \ 0.0205(5) \ -0.0012(3) \ -0.0026(4) \ 0.0027(4)
_geom_special details
All esds (except the esd in the dihedral angle between two l.s. planes)
are estimated using the full covariance matrix. The cell esds are taken
into account individually in the estimation of esds in distances, angles
and torsion angles; correlations between esds in cell parameters are only
used when they are defined by crystal symmetry. An approximate (isotropic)
treatment of cell esds is used for estimating esds involving l.s. planes.
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_geom_bond_site_symmetry_2
geom bond publ flag
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N1 N2 1.2782(12) . ?
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N2 O2 1.3911(10) . ?
O2 C3 1.4542(12) . ?
N3 C10 1.3202(12) . ?
C3 C4 1.5073(14) . ?
C3 H3B 0.9900 . ?
C3 H3A 0.9900 . ?
C4 C9 1.3908(15) . ?
C4 C5 1.3986(13) . ?
C5 C6 1.3931(15) . ?
C5 H5 0.9500 . ?
C6 C7 1.3919(16) . ?
C6 H6 0.9500 . ?
C7 C8 1.3903(15) . ?
C7 H7 0.9500 . ?
C8 C9 1.3931(15) . ?
C8 H8 0.9500 . ?
С9 Н9 0.9500 . ?
C10 N11 1.3414(12) . ?
C10 C14 1.4967(13) . ?
N11 C12 1.4603(13) . ?
N11 C13 1.4602(13) . ?
C12 H12C 0.9800 . ?
C12 H12B 0.9800 . ?
C12 H12A 0.9800 . ?
C13 H13C 0.9800 . ?
C13 H13B 0.9800 . ?
C13 H13A 0.9800 . ?
C14 C19 1.3970(13) . ?
C14 C15 1.3999(14) . ?
C15 C16 1.3935(13) . ?
C15 H15 0.9500 . ?
C16 C17 1.3916(15) . ?
C16 H16 0.9500 . ?
C17 C18 1.3879(16) . ?
C17 H17 0.9500 . ?
C18 C19 1.3905(14) . ?
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C18 H18 0.9500 . ?

C19 H19 0.9500 . ?

loop_									
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_geom	_angl	.e_a	atc	m_	si	te_	_1a	ibe	1_2
_geom	_angl	.e_a	atc	om_	sı	te_	_1a	ibe	T_3
_geom	_angi	.e	. : .	_	~		- - -		1
_geom	_angi	.e_s	51t	.е_	sy	mme	etr	:У_	1
_geom	_angi	.e_s	51t	.e_	_sy 	mme	ετr	:У_	3
_geom	_angi	.e_p		Σ_{-}	<u> </u>	ag	_	,	
OI NI	NZ 1	20	/د. 10	(0		•	• •	5	
N2 N1	113 1	11	53			•	•••	, >	
N1 N2	02 1	07	76	(0)	·) ')	•	• •	, ,	
N2 02	C3 1	06	56	. 7	, ``	•		, ,	
C10 N	3 N1	112	2.7	61	י 8 ו	•	•••	?	
02 C3	$C4^{-1}$	12.	.24	. (8	۰, ۱		. 7		
02 C3	нзв	109	9.2		· .	?			
C4 C3	H3B	109	9.2			?			
02 C3	H3A	109	9.2			?			
C4 C3	нза	109	9.2	•		?			
НЗВ С	3 H3A	10)7.	9	•	. 3	?		
C9 C4	C5 1	.18	.92	(9)	•	. 7	Ş	
C9 C4	C3 1	20	.67	(9)	•	. 3	2	
C5 C4	C3 1	20	. 39	(9)	•	. 7	2	
C6 C5	C4 1	20	. 30	(1	0)	•	•	?	
C6 C5	H5 1	.19	. 8	•	•	?			
C4 C5	H5 1	.19	. 8	•	•	?			
C7 C6	C5 1	.20	.19	(9)	•	. 7)	
C7 C6	H6 1	.19	.9	•	•	?			
C5 C6	H6 I	.19.	.9	•	•	?		~	
	С6 I 117 1	.19.	. 8 / 1	(1	.0)	•	•	?	
	п/ 1 17 1	20	• ⊥ 1	•	•	f D			
C7 C8	C9 1	19	• ± 72	•	•	÷		2	
C7 C8	H8 1	20	. 1	. (1	,	?	•	•	
C9 C8	H8 1	20	.1			?			
C4 C9	C8 1	.21	. 00	(9)	•	. 7	2	
C4 C9	Н9 1	.19	5	·		?			
C8 C9	Н9 1	.19	. 5	•	•	?			
N3 C1	0 N11	. 11	17.	00	(8) .		?	
N3 C1	0 C14	12	24.	02	(8) .		?	
N11 C	10 C1	.4 1	118	.9	5 (8)	•	•	?
C10 N	11 C1	.2 1	L 2 0	• 9	4 (8)	•	•	?
C10 N	11 C1	.3 1	124	.1	8 (8)	•	•	?
C12 N	11 C1	.3 1	114	• 5	6 (8)	•	•	?
N11 C	12 H1	.2C	10	9.	5	•	. 3	2	
NII C	12 HI	.2B	10	9.	5	•	•	, 	
HIZC (1121	1 6	.09	- 5	•	•_	?	
	12 HI 012 H	. ZA 1 1 2 7	10	00	С Б	•	• •	, 2	
	СІ <u></u> Г. С12 г.	1121	1 1 1	09	• 5 • 5	•	•	f D	
N11 C	сіс п 13 ц1	30	10	09	5	•	•	•	
N11 C	13 H1	3B	10	9.	5	•		5	
H13C	C13 F	1131	3 1	.09	.5			?	
N11 C	13 H1	.3A	10	9.	5		. 7	, -	
H13C	C13 H	1137	¥ 1	.09	.5	•	•	?	
Н13В	C13 H	1137	A 1	09	.5			?	
C19 C	14 C1	.5 1	L19	.8	8 (9)			?
C19 C	14 C1	.0 1	L19	.0	2 (8)	•	•	?
C15 C	14 C1	.0 1	121	• 0	2 (8)	•	•	?
C16 C	15 C1	.4 1	119	.6	0(9)	•	•	?

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C16 C15 H15 120.2 . . ?
C14 C15 H15 120.2 . . ?
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С15 С16 Н16 119.8 . . ?
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C18 C17 C16 119.76(9) . . ?
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C17 C18 C19 120.50(10) . . ?
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C14 C19 H19 120.1 . . ?
loop
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N3 N1 N2 O2 -176.07(7) . . . ?
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                              ?
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N2 O2 C3 C4 58.72(10) . . . ?
02 C3 C4 C9 -107.47(11) . . . ?
O2 C3 C4 C5 70.84(12) . . . ?
C9 C4 C5 C6 -0.56(15) . . . ?
C3 C4 C5 C6 -178.89(10) . . . .
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C4 C5 C6 C7 0.44(17) . . . ?
C5 C6 C7 C8 -0.21(17) . . . ?
C6 C7 C8 C9 0.11(17) . . . ?
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C10 C14 C15 C16 -175.50(9) . . . ?
C14 C15 C16 C17 -0.51(14) . . . ?
C15 C16 C17 C18 -0.53(15) . . . ?
C16 C17 C18 C19 0.83(16) . . . ?
C17 C18 C19 C14 -0.07(15) . . . ?
C15 C14 C19 C18 -0.98(14) . . . ?
C10 C14 C19 C18 175.85(9) . . . ?
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