

Supplementary Information

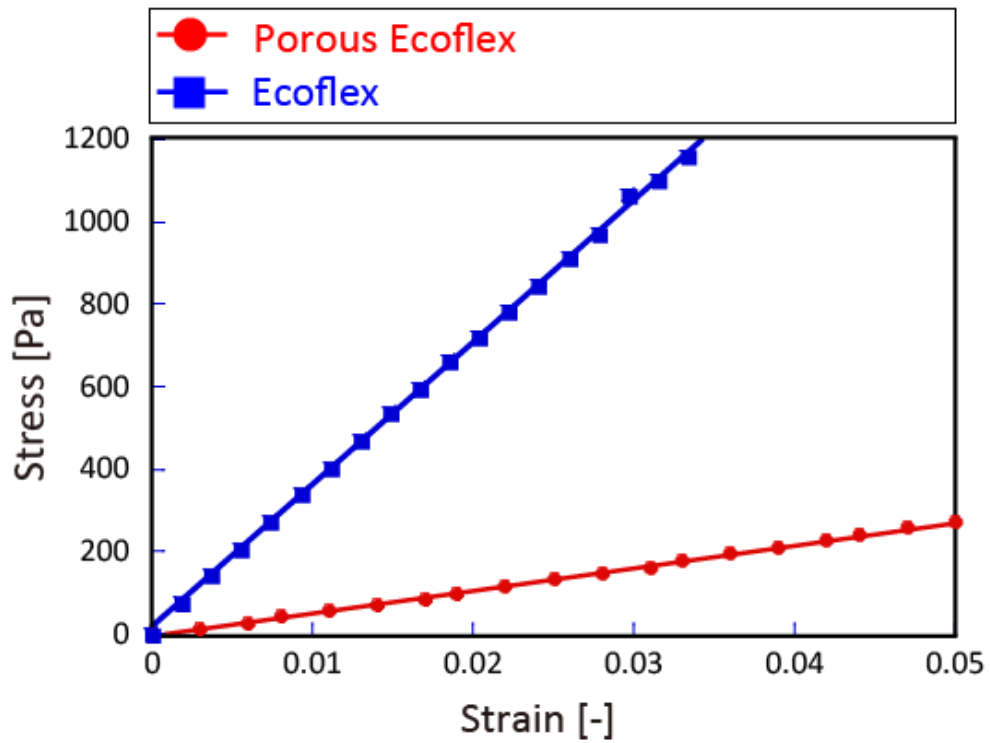
Highly Stretchable Sensing Array for Independent Detection of Pressure and Strain Exploiting Structural and Resistive Control

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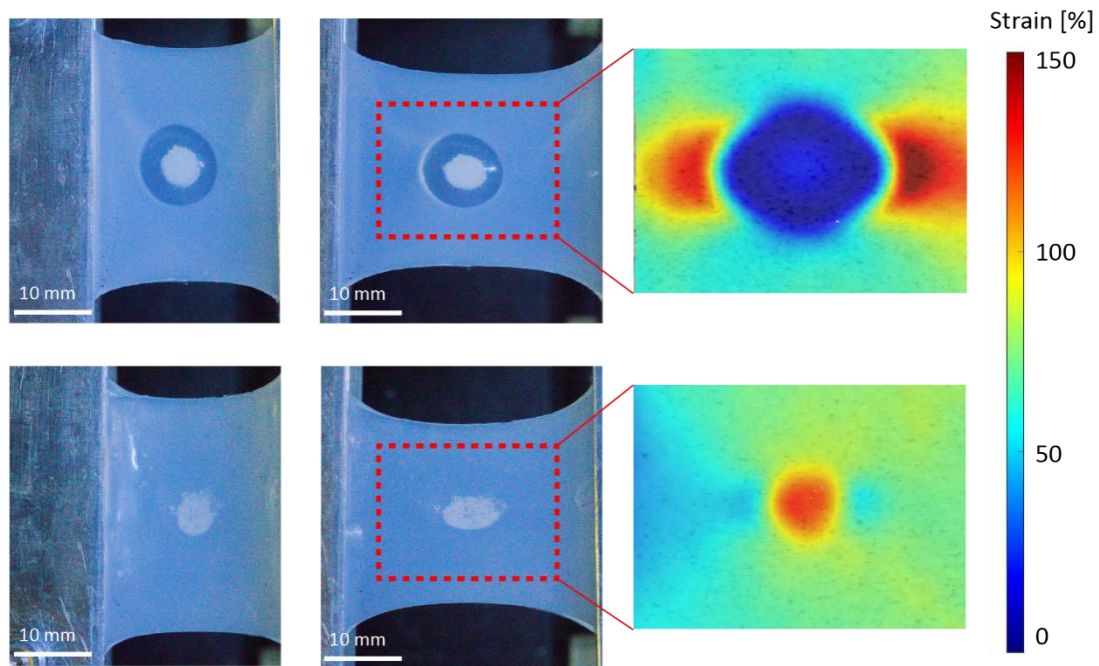
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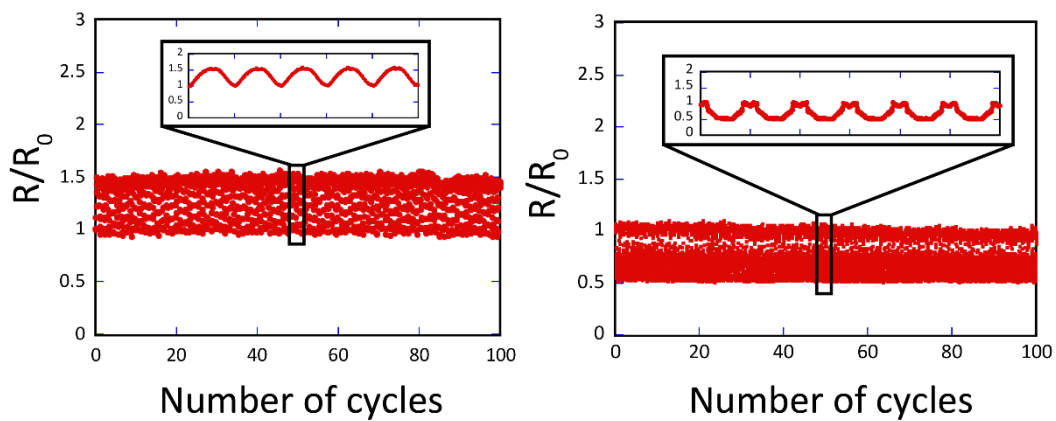
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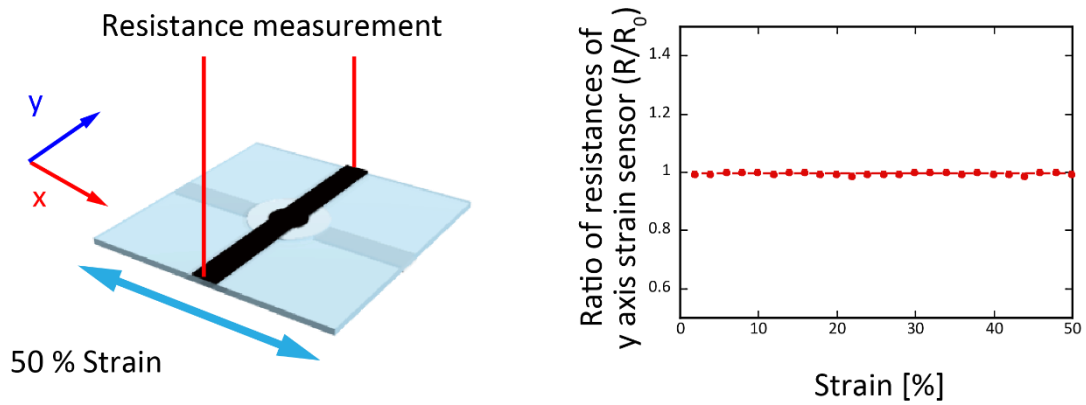
Supplementary Figure S1. Stress–strain relationship of porous silicone. The Young’s moduli of porous silicone and regular Ecoflex were 5.50 kPa and 34.5 kPa, respectively.



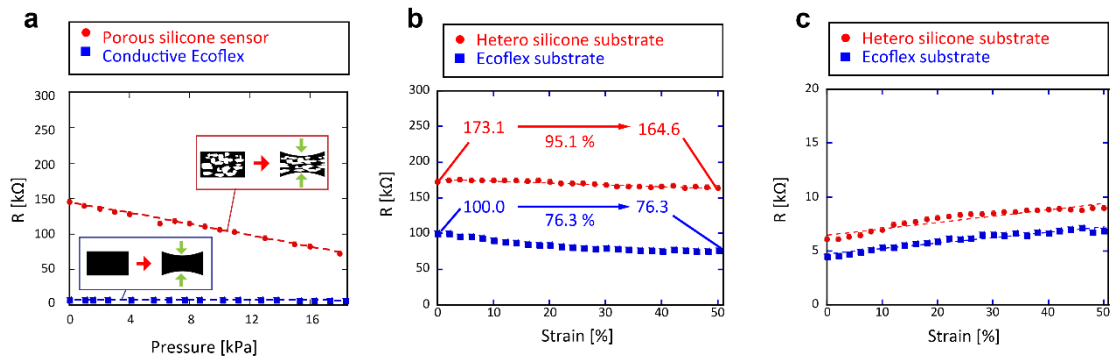
Supplementary Figure S2. Stability of pressure sensing elements during the application of 50% strain.



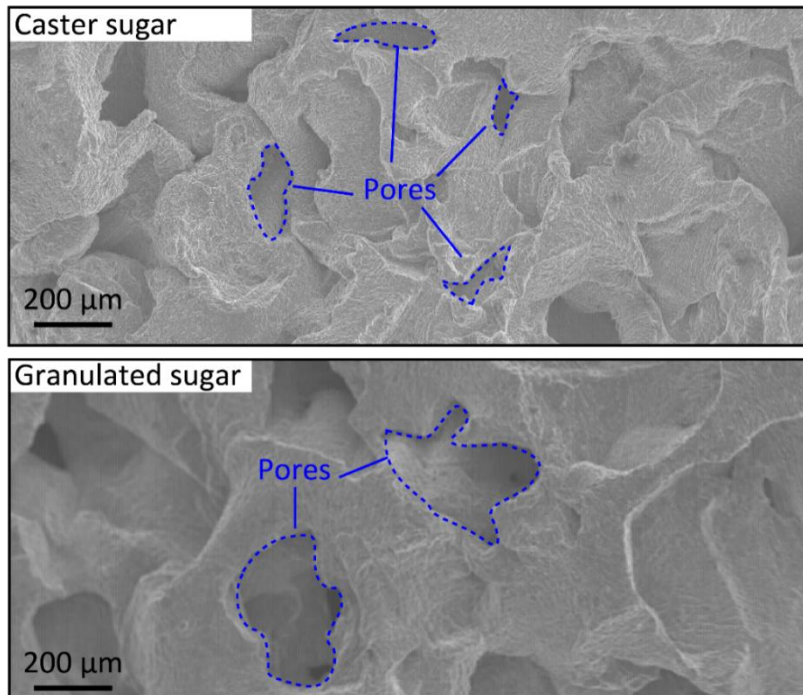
Supplementary Figure S3. Repeatability tests of pressure and strain sensors. In the strain tests, the device was stretched up to 50% strain 100 times, whereas in the pressure tests, a pressure of 15 kPa was applied on the device 100 times.



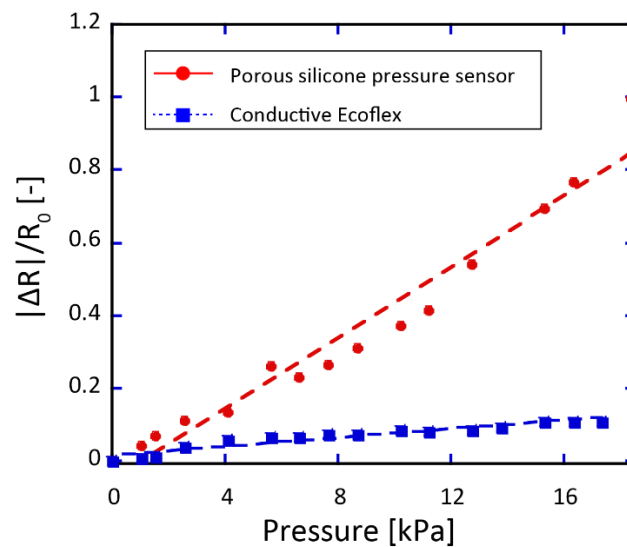
Supplementary Figure S4. Y-axis strain detection under x-axis tensile deformation.



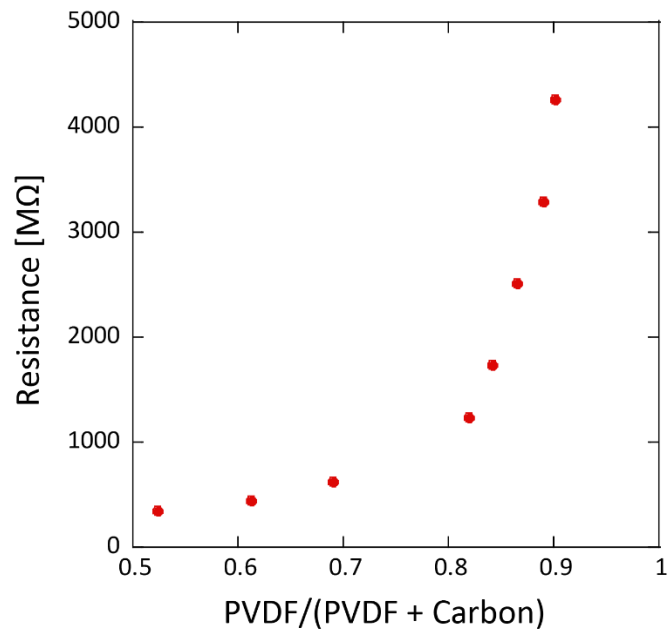
Supplementary Figure S5. Sensing characteristics of 1-pixel devices using the real resistance value.



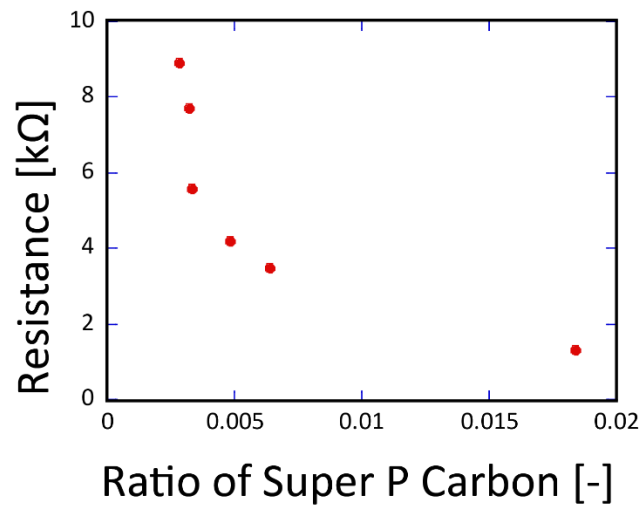
Supplementary Figure S6. Differences in pore size of caster and granulated sugar based on scanning electron microscopy images.



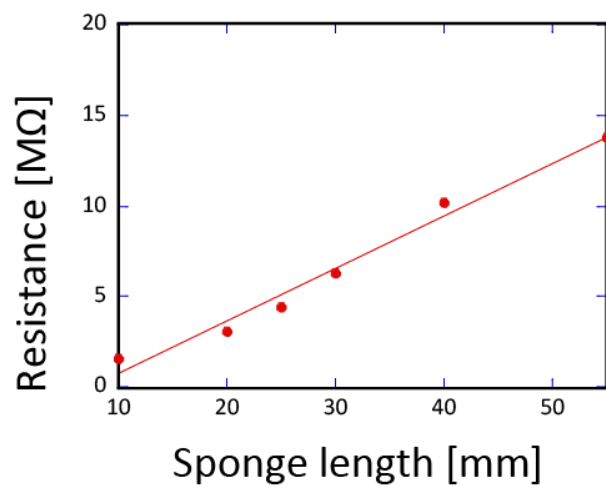
Supplementary Figure S7. Resistance variations of pressure sensors with respect to pressure. The sensitivity of the pressure sensor that used porous silicone (red) was $4.6\% \text{ kPa}^{-1}$, and that of the pressure sensor that used regular Ecoflex and carbon particle mixture elastomer (blue) was $0.6\% \text{ kPa}^{-1}$.



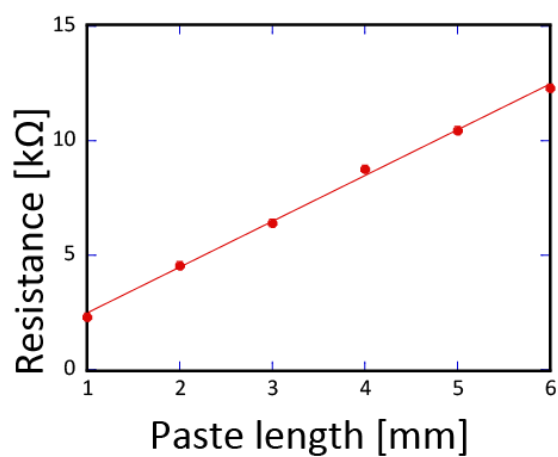
Supplementary Figure S8. Resistance variations with respect to the ratio of PVDF in the PVDF and carbon mixture. The resistance increases as a function of the amount of PVDF.



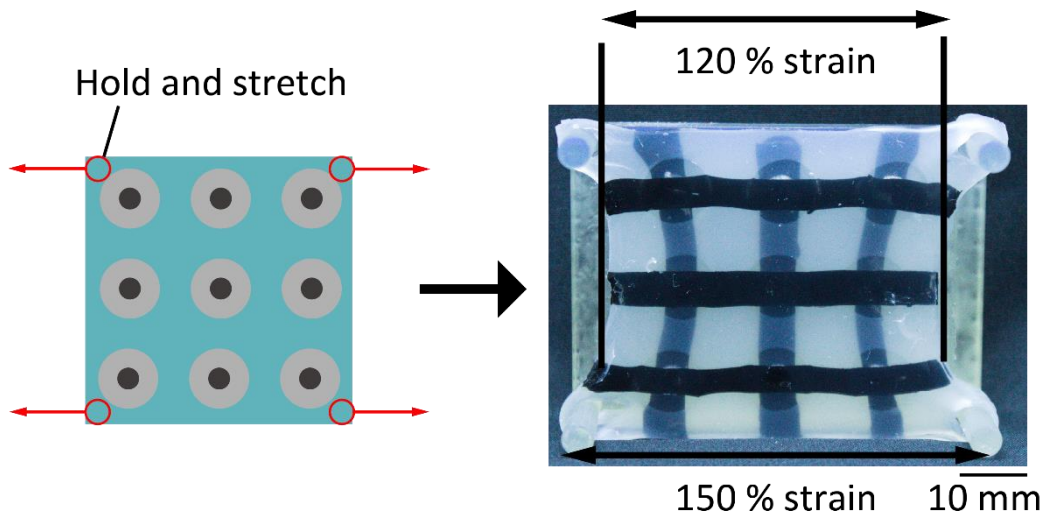
Supplementary Figure S9. Resistance variations with respect to the ratio of Super P carbon in porous silicone. The thickness of the porous silicone in this test device was 1.5 mm. The width and length were 5 mm and 30 mm, respectively.



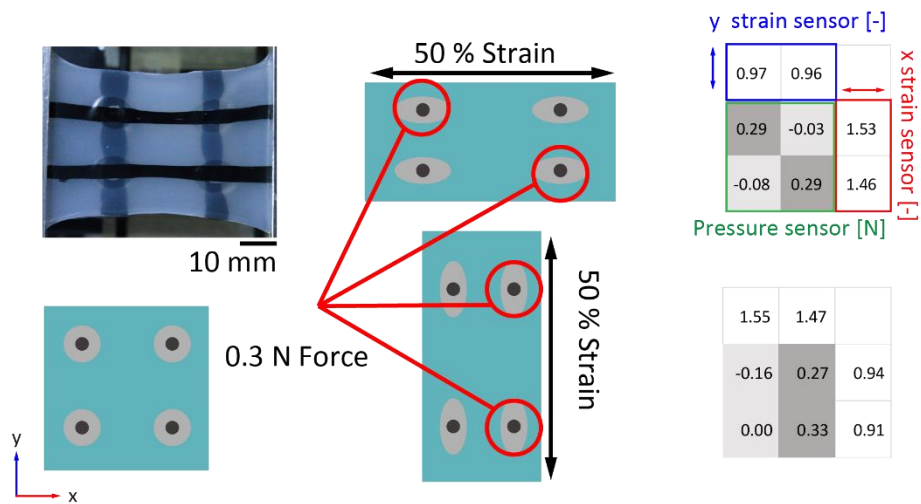
Supplementary Figure S10. Resistance variations with respect to the length of porous silicone electrodes coated with Super P carbon.



Supplementary Figure S11. Resistance variations with respect to the length of conductive silicone paste electrode.



Supplementary Figure S12. Holding points of the 9-pixel strain test.

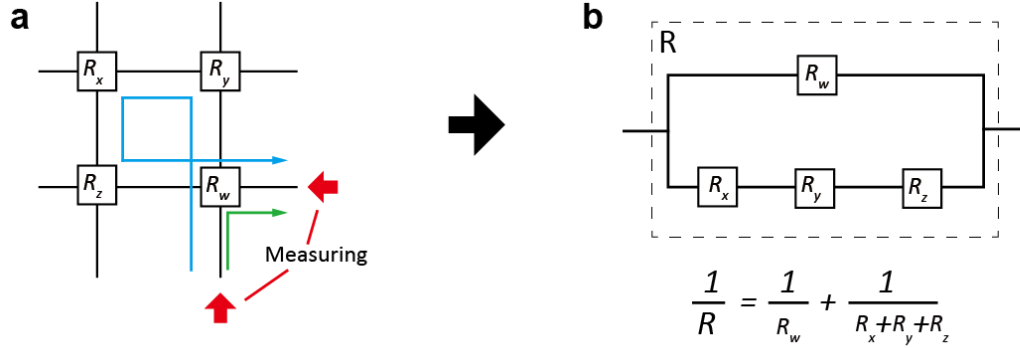


Supplementary Figure S13. Demonstration of the 4-pixel device.

Supplementary Table S1. Comparison of stretchable pressure sensors used in this study and other studies.

| Reference | Method | Material | Pressure limit [kPa] | Sensitivity [% kPa ⁻¹] | Strain limit [%] |
|------------------------------------|------------|--------------------|-------------------------|---------------------------------------|---------------------|
| i) Zhu et al. ¹⁸ | Resistive | Graphene | 0 - 0.1 | 553 | Not independent |
| | | | 0.1 – 1.4 | 1 | Not independent |
| ii) Choong et al. ³⁴ | Resistive | Conductive polymer | 0 - 3 | 1000 | Not independent |
| | | | 3 - 8 | 200 | Not independent |
| iii) Gao et al. ²⁷ | Resistive | Liquid metal | 50 | 2 | Not independent |
| iv) Lipomi et al. ²³ | Capacitive | CNT + Ecoflex | 800 | 0.023 | Not independent |
| v) S. Yao and Y. Zhu ²⁴ | Capacitive | Ag nano wire | 0-400 | 0.162 | Not independent |
| | | | 400-1300 | 0.057 | Not independent |
| vi) Y. Pang et al. ²⁵ | Resistive | Graphene | 1000 | 0.09 | Not independent |
| vii) Park et al. ³⁵ | Resistive | Gold film | 1 | 200 | 15 |
| viii) This study | Resistive | Carbon mixture | 18 | 4.8 | 50 |

Supplementary Information 1
Measurements of 9-pixel pressure maps



Supplementary Figure S14. Schematic diagram illustrating the measurement method with a 4-pixel device. a. Measurement points and electrical paths b. Combined resistance.

Supplementary Fig. S10 shows two electrical paths in the case of pressure sensing at point w using the 4-pixel device. All electrodes and sensor elements in the developed device are conductive. In addition, the sensing mechanism of the developed device was piezoresistive effect. This is the reason the actual resistance at point R_w is equivalent to the combined resistance (Equations 1 and 2):

$$\frac{1}{R} = \frac{1}{R_w} + \frac{1}{R_x + R_y + R_z} \quad (1)$$

$$R = \frac{R_w(R_x + R_y + R_z)}{R_x + R_y + R_z + R_w} \quad (2)$$

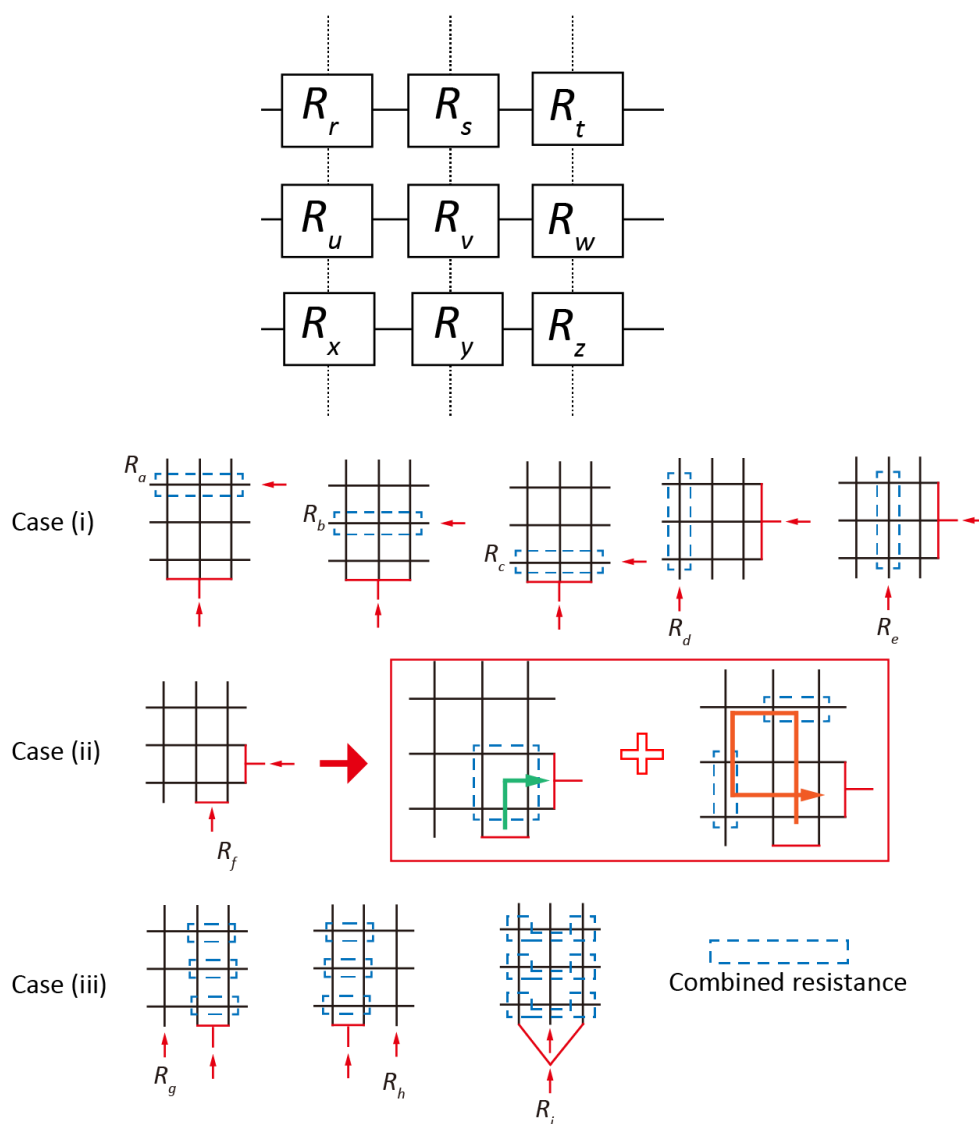
It is assumed that three resistance values, except the resistance of point w, decreased to 1/2 when pressure was applied at points x, y, and z. The combined resistance R' obtained using the same two-point measurement method is as follows (Equations 3 and 4):

$$\frac{1}{R'} = \frac{1}{R_w} + \frac{1}{\frac{R_x}{2} + \frac{R_y}{2} + \frac{R_z}{2}} \quad (3)$$

$$R' = \frac{R_w(R_x + R_y + R_z)}{R_x + R_y + R_z + 2R_w} \quad (4)$$

Therefore, the combined resistance decreases even though point w was not pressed. Therefore, it is difficult to measure pressure values precisely using only the resistances of the column and row.

In this study, the following method was adopted for mapping measurements. The 9-pixel device in Supplementary Fig. S11 yields nine resistance values ($R_r, R_s, R_t, R_u, R_v, R_w, R_x, R_y,$ and R_z) from the calculation of nine simultaneous equations based on nine combined resistance values ($R_a, R_b, R_c, R_d, R_e, R_f, R_g, R_h,$ and R_j) (Supplementary Fig. S11 and Equations 5–13).



Supplementary Figure S15. Measurement method used in the 9-pixel device.

First, given that the three electrodes are connected (red line) and the resistances are measured in

accordance with the red arrows (case (i)), R_r can be measured. Using the same method, R_s , R_t , R_u , R_v , R_w , R_x , R_y , and R_z can be measured. Second, given that the two electrodes are connected and the resistances are measured in accordance with the red arrows (case (ii)), the combined resistance R_f can be measured. Finally, given that the two electrodes are connected (red lines) and the resistances are measured in accordance with the red arrows (case (iii)), the combined resistance R_g can be measured. Using the same method, R_h and R_j can be measured. According to the basic theories of electric circuit, the combined resistances are as follows (Equations 5–13):

$$\frac{1}{R_r} + \frac{1}{R_s} + \frac{1}{R_t} = \frac{1}{R_a} \quad (5)$$

$$\frac{1}{R_u} + \frac{1}{R_v} + \frac{1}{R_w} = \frac{1}{R_b} \quad (6)$$

$$\frac{1}{R_x} + \frac{1}{R_y} + \frac{1}{R_z} = \frac{1}{R_c} \quad (7)$$

$$\frac{1}{R_r} + \frac{1}{R_u} + \frac{1}{R_x} = \frac{1}{R_d} \quad (8)$$

$$\frac{1}{R_s} + \frac{1}{R_v} + \frac{1}{R_y} = \frac{1}{R_e} \quad (9)$$

$$\frac{1}{\frac{1}{R_v} + \frac{1}{R_w} + \frac{1}{R_y} + \frac{1}{R_z}} + \frac{1}{\frac{1}{R_u} + \frac{1}{R_x} + R_r + \frac{1}{R_s} + \frac{1}{R_t}} = \frac{1}{R_f} \quad (10)$$

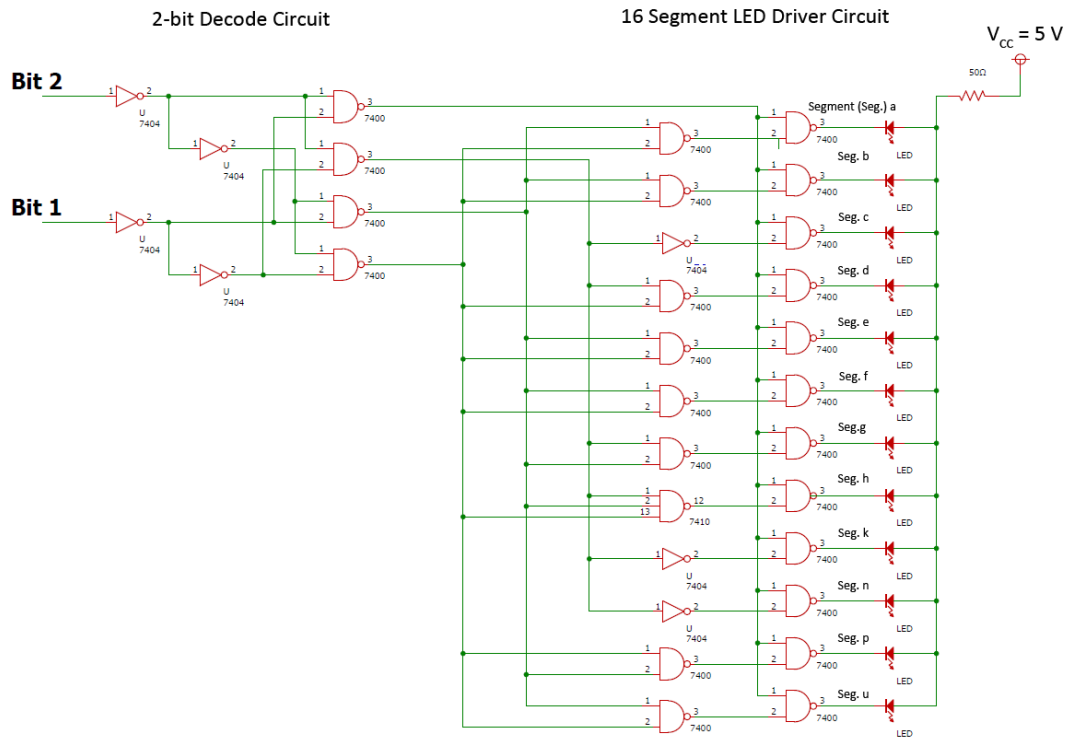
$$\frac{1}{\frac{1}{R_x} + \frac{1}{R_y} + R_z} + \frac{1}{\frac{1}{R_u} + \frac{1}{R_v} + R_w} + \frac{1}{\frac{1}{R_r} + \frac{1}{R_s} + R_t} = \frac{1}{R_g} \quad (11)$$

$$\frac{1}{\frac{1}{R_y} + \frac{1}{R_z} + R_x} + \frac{1}{\frac{1}{R_v} + \frac{1}{R_w} + R_u} + \frac{1}{\frac{1}{R_s} + \frac{1}{R_t} + R_r} = \frac{1}{R_h} \quad (12)$$

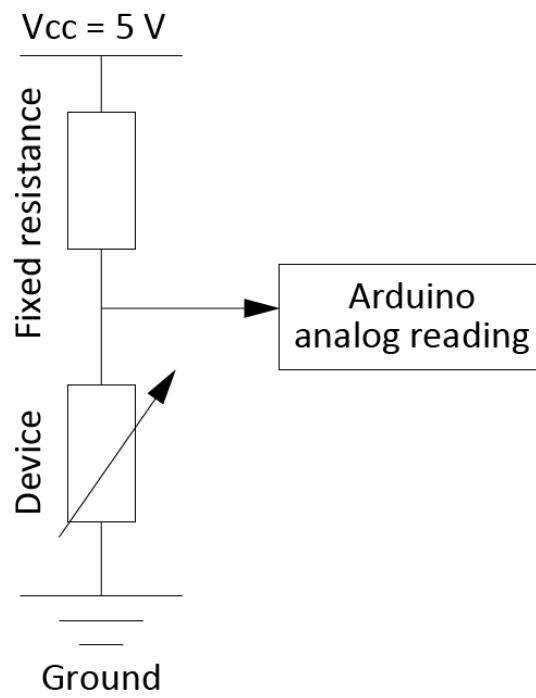
$$\frac{1}{\frac{1}{R_x} + \frac{1}{R_z} + R_y} + \frac{1}{\frac{1}{R_u} + \frac{1}{R_w} + R_v} + \frac{1}{\frac{1}{R_r} + \frac{1}{R_t} + R_s} = \frac{1}{R_j} \quad (13)$$

Each resistance (R_r , R_s , R_t , R_u , R_v , R_w , R_x , R_y , and R_z) in the array pressure sensor can be calculated

by solving these simultaneous equations numerically using the Newton method.



Supplementary Figure S16. Circuit diagram of a 2-pixel keyboard device.



Supplementary Figure S17. Circuit diagram of the strain indicator.

Supplementary Video S1 demonstrates the display control with indicative strains of the device.