Science Advances NAAAS

advances.sciencemag.org/cgi/content/full/6/36/eabc3296/DC1

Supplementary Materials for

On-site identification of ozone damage in fruiting plants using vapor-deposited conducting polymer tattoos

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Published 4 September 2020, *Sci. Adv.* **6**, eabc3296 (2020) DOI: 10.1126/sciadv.abc3296

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Additional Methods Figs. S1 to S9 Table S1 References

Additional Methods

Relative Water Content

The relative water content (RWC) of a leaf was calculated using equation 1:

$$
RWC \left(% \right) = \frac{Fresh \; Weight - Dry \; Weight}{rurgid \; Weight - Dry \; Weight} \times 100 \left(% \right) \tag{1}
$$

The dry weight was determined after each leaf was heated at 50 °C for 5 days, when the mass became constant. The turgid weight was measured after immersing fresh leaves in distilled water for 5 hours in the dark and removing extra water on the surface with Texwipes.

Fig. S1. **Effects of ozone exposure**. Images of underside (abaxial side) of a grape leaf after exposure to increasing doses of ozone. The scale bars are 10 mm. The vapor-deposited PEDOT-Cl electrode ("tattoo") is clearly visible in the 0 ppmh image. Photo Credit: Dr. Jae Joon Kim, University of Massachusetts Amherst.

Fig. S2. **Comparison of electrode materials**. **a**, Images of electrodes on grape leaves. The scale bars are 10 mm. The expansion shows a picture of the as-deposited PEDOT:PSS droplet on the hydrophobic surface of grape leaf. **b**, Picture of the PEDOT-Cl tattoo before and after exposure to ozone. **c**-**f**, Magnified images of the electrodes on the leaf after bending and rinsing treatment. The scale bars are 5 mm (top row) and 1 mm (bottom row). **g**-**i**, Comparison of relative conductivity change after water, saline water and ozone exposure. Photo Credit: Dr. Jae Joon Kim, University of Massachusetts Amherst.

Fig. S3. Investigating the surface of a grape leaf. SEM images of the surface of a grape leaf.

Fig. S4. Measurement setup. Picture and scheme of a typical impedance measurement on an electrode decorated grape leaf. The scale bar is 10 mm. Photo Credit: Dr. Jae Joon Kim, University of Massachusetts Amherst.

Fig. S5. **Conduction pathways in a representative leaf**. Scheme of the conduction pathways operating at different bias frequencies during an impedance measurement.

Fig. S6. **Effect of electrode dimensions on impedance spectra of a grape leaf**. **a**, Image of electrodes on the grape leaf. The scale bar is 10 mm. Photo Credit: Dr. Jae Joon Kim, University of Massachusetts Amherst. **b**, impedance and **c**, phase as a function of frequency.

Fig. S7. **Calibrating ozone dose**. Calibration curve for obtaining ozone dose (ppmh) as a function of exposure time inside an ozone generation chamber.

Fig. S8. **The equivalent electrical circuit used to model impedance data**. The equivalent circuit contains components arising from the electrode and leaf tissue.

Ozone	Element		Electrode part					Tissue part					Chi-
exposure			$\mathsf{R}_{\mathsf{poly}}(\Omega)$	$A_{W}(\Omega)$	B_{W} (s)	D	C_{eni} (F)	$R_{ex}(\Omega)$	$R_{in}(\Omega)$	Y_{0}	D	$C_m(F)$	square
Ω ppmh	Value			(Ω, F) 1.1.E+04 1.4.E+05 1.1.E-03 3.2.E-01 1.7.E-10 3.3.E+04 4.2.E+03 4.2.E-09							6.6.E-01 4.6.E-11		$1.8E - 06$
	Error	(%)	$2.0.E+00$ 8.9.E-01						1.8.E+00 5.1.E-01 1.7.E+00 1.4.E+00 5.2.E-01 2.2.E+00 2.0.E-01				
6.5 ppmh	Value			(Ω, F) 1.2.E+04 1.1.E+05 1.1.E-03 3.4.E-01 2.0.E-10 3.3.E+04 4.7.E+03 5.3.E-09							6.4.E-01 4.5.E-11		$1.4.E-06$
	Error	(%)		9.2.E-01 7.0.E-01 1.4.E+00 3.8.E-01 1.3.E+00 1.1.E+00 4.7.E-01 2.3.E+00 2.1.E-01									
10.9 ppmh	Value			(Ω, F) 9.9.5+03 9.2.5+04 7.4.5-03 3.4.5-01 2.2.5-10 3.8.5+04 5.8.5+03 7.8.5-09							6.1.E-01 4.7.E-11		$1.7E-06$
	Error	(%)		1.4.E+00 8.5.E-01 1.3.E+00 4.4.E-01 1.8.E+00 1.3.E+00 5.8.E-01 3.1.E+00 3.0.E-01									
15.0 ppmh	Value			(Ω, F) 6.2.E+03 8.6.E+04 6.4.E-04 3.6.E-01 2.5.E-10 4.7.E+04 8.5.E+03 1.3.E-08							5.5.E-01 3.6.E-11		$1.7.E-06$
	Error	(%)		2.9.E+00 9.7.E-01 1.2.E+00 4.5.E-01 2.2.E+00 1.5.E+00 7.8.E-01 4.5.E+00 4.8.E-01									
18.9 ppmh	Value			(Ω, F) 2.7.E+03 7.0.E+04 5.4.E-04 3.8.E-01 2.5.E-10 7.1.E+04 1.1.E+04 4.9.E-08							4.4.E-01 4.3.E-11		$2.3.E-06$
	Error	(%)		4.1.E+00 2.1.E+00 1.5.E+00 7.8.E-01 2.2.E+00 2.0.E+00 1.6.E+00 7.8.E+00 1.1.E+00									
22.7 ppmh	Value			(Ω, F) 5.2.E+03 1.5.E+05 8.9.E-04 3.8.E-01 8.5.E-11 6.2.E+04 7.9.E+03 6.7.E-08							3.6.E-01 4.8.E-12		$5.0.E-06$
	Error	(%)		1.9.E+00 1.6.E+00 2.1.E+00 6.9.E-01 2.0.E+00 2.8.E+00 1.5.E+01 2.3.E+01 4.0.E+00									
26.5 ppmh	Value			(Ω, F) 7.0.E+03 1.6.E+05 8.0.E-04 3.8.E-01 7.9.E-11					5.4.E+04 2.0.E+04 9.6.E-09		4.7.E-01 2.7.E-12		$4.8 - 06$
	Error	(%)		$3.2.E+00$ $8.5.E-01$					1.4. E+00 4.2. E-01 1.8. E+00 1.7. E+00 6.0. E+00 2.3. E+01 2.9. E+00				

Table S1. **Extracted values from circuit modelling**. Extracted values, percent error for each circuit component and the corresponding fitting accuracy (chi-square).

The equivalent electrical circuit model is comprised of an electrode part and tissue components, as previously reported by our research group (49). Electrode parts include a resistor, R_{poly}, that represents the intrinsic conductivity of the PEDOT-Cl electrode, a capacitor, Cepi, that accounts for the capacitance introduced at the interface between the electrode and the insulating leaf epidermis, and a transmissive Warburg component, W_s, that stands for ion diffusion between the polymer coating and leaf cells. The Warburg component is further comprised of three subparts: a diffusion impedance constant, AW, a Warburg exponent, p, and a characteristic ion diffusion time, B_W. Additional circuit components for the saline droplet were not necessary to accurately fit the recorded data in the frequency range used in this study. The Hayden model (6) ; was used to translate three principal cellular components of a grape leaf into discrete circuit elements: extracellular fluid was represented by a resistor, R_{ex} ; intracellular fluid was represented by a resistor, R_{in} ; and the cell membrane was represented by capacitor, C_M . The cell membrane capacitance was represented in the circuit as a constant phase element (CPE) instead of a simple capacitor because leaf tissue is composed of an ensemble of cells that result in electronic dispersity. The value for C_M was calculated using Equation 2 (4*:*,50):

$$
C_M = Y_p^{\frac{1}{p}} (R_{in} + R_{ex})^{\frac{1-p}{p}}
$$
 (2)

where Y_0 is the CPE constant and p is the CPE exponent.

Fig. S9. **A**. **Comparison of the impedance-frequency relationship between the measured data and the fitting curve**. The measured data is plotted with a solid black line and the fitting curve based on the equivalent model circuit is plotted as a dotted line. **B.** Comparison of the phase-frequency relationship between the measured data and the fitting curve. The measured data is plotted with a solid black line and the fitting curve based on the equivalent model circuit is plotted as a dotted line.

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