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Supplementary Materials for

Designing hierarchical nanoporous membranes for highly efficient gas adsorption and storage

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Effect of the reaction temperature on the morphology of carbon spheres

Figure S1 shows the microscopic morphology of the cellulose hydrothermal carbonization product at a cellulose concentration of 0.04 g ml-1 after 5 h at different reaction temperatures. **Figure 2C** shows the microscopic morphology of uncarbonized cellulose, and with a hydrothermal temperature of 200 °C (**Fig. S1A**), the morphology of the carbon spheres clearly remains nanofibrous. However, small carbon spheres already appear on the surface of the fiber, indicating that cellulose begins to undergo carbonization into spheres at 200 °C. When the temperature increases to 220 °C, the extent of the reaction is still relatively small (**Fig. S1B**). **Figure S1B** shows that with the increased hydrothermal reaction temperature, most of the original fibrous morphology disappears. However, the carbon spheres clearly show evidence of fusion phenomena. Most of the reaction products do not form a complete spherical morphology, and the carbon spheres are unevenly distributed. The particle sizes of the carbon spheres are distributed over a wide range, with both µm-sized and nm-sized spheres. **Figure 2, (D and E)** reveals that when the hydrothermal temperature reaches 240 °C, the fusion phenomena do not occur, and the hydrothermal products have a high degree of sphericity, uniform distribution, narrow distribution of particle size, and an average diameter of 2-3 µm. The surfaces of the carbon spheres are smooth and separated from each other. **Figure S1C** shows the aggregation phenomenon among carbon spheres when the temperature increases to 260 °C.

Figure S1 | SEM micrographs of cellulose and carbon spheres at various temperatures. SEM of carbon spheres obtained by hydrothermal treatment of cellulose at 200 $^{\circ}C$ (A), 220 $^{\circ}C$ (B), and 260 °C (C).

Effect of the reaction time on the morphology of the carbon spheres

Figure S2 shows the change in the SEM micrographs when the carbonization time was extended from 3 h to 7 h at a carbonization temperature of 240 **°**C and a cellulose reaction concentration of 0.04 g ml-1 . As shown in **Figure S2A**, when the carbonization time is 3 h, very few carbon spheres reach a particle size of 2 μm, and the majority of the carbon spheres are amorphous. As the carbonization time increases to 5 h, the particle size of the carbon spheres increases from 1.5 μm in **Fig. S2A** to 2 μm in **Fig. 2E**. When the time is further increased to 7 h, the particle size of the carbon spheres increases from 2.0 μm (in **Fig. 2E**) to 2.5 μm (in **Fig. S2B**). The longer reaction time is responsible for the larger particle size of the carbon spheres. However, an aggregation phenomenon occurs to some extent, and the high temperature is related to the severity of aggregation. The formation of aggregates of deformed carbon spheres may be attributed to the fact that mechanical stirring does not ensure complete uniformity of cellulose in the system. With the high concentrations of carbon spheres, aggregation is prone to occur when the carbon spheres increase in size, leading to deformed carbon spheres. With a reaction time of 7 h, cellulose is deposited at the bottom of the reaction vessel, resulting in a relatively large concentration of carbon spheres at the bottom. It can be concluded that the optimal hydrothermal reaction temperature and time for preparing cellulose-based carbon spheres are 240 **°**C and 5 h, respectively.

Figure S2 | SEM micrographs of carbon spheres obtained by hydrothermal treatment of cellulose at various times: 3 h (A) and 7 h (B) (the carbonization temperature and concentration were 240 $^{\circ}$ C and 0.04 g ml⁻¹, respectively).

Effect of the reaction concentration on the morphology of carbon spheres

Figure S3 shows the microscopic morphology of cellulose products at different concentrations undergoing hydrothermal carbonization for 5 h at 240 **°**C. When the cellulose concentration is increased from 0.02 g ml⁻¹ to 0.03 g ml⁻¹, the diameter of the carbon spheres increases to 2 μ m (**Fig. S3B**), but the diameter decreases to 1.5 μm at 0.04 g ml-1 (**Fig. 2E**). When the concentration increases from 0.04 g ml⁻¹ (**Fig. 2E**) to 0.05 g ml⁻¹ (**Fig. S3C**), the diameter of some carbon spheres increases, but the diameter of a few individual carbon spheres continues to decrease. Aggregation of carbon spheres also occurs. It is clear that although the particle size of the resulting carbon spheres reaches a maximum at a cellulose concentration of 0.05 g ml⁻¹, the sphericity of the carbon spheres is not uniform, and aggregation occurs. Therefore, the optimal cellulose concentration for the preparation of cellulose-based carbon spheres is 0.04 g ml⁻¹.

Figure S3 | SEM micrographs of carbon spheres obtained by hydrothermal treatment of cellulose at various concentrations: 0.02 g ml⁻¹ (A), 0.03 g ml⁻¹ (B), and 0.05 g ml⁻¹ (C); the carbonization temperature and time were 240 °C and 5 h, respectively.

Figure S4 | Photographs of the hierarchical nanoporous membranes created using a doctor blade coating method. A, Photograph of large-area HNM $(10 \times 10 \text{ cm}^2)$ fabricated by a doctor-blade method. **B,** Photograph of free-standing and flexible HNM without absence of cracks. Photo credit: J.T., Stanford University. Permission granted.

Dubinin-Radushkevich fitting of VOC adsorption isotherms

In the actual adsorption process, the adsorption is not at equilibrium, and both adsorption and desorption processes occur at the same time. In order to investigate the mechanism of adsorption equilibrium for toluene/acetone, the Dubinin-Radushkevich model (*36*) was employed to fit the adsorption isotherm experimental data. Major parameters that may affect the adsorption process include the surface performance of the GO/HCS composite membranes, concentration of toluene/acetone, and temperature.

The Dubinin-Radushkevich (DR) equation is expressed as (*36*):

$$
q = W_0 \exp\left[-\left(\frac{(RT \ln(p_0/p)}{E}\right)^2\right]
$$
 Equation S1

Where q is the adsorption capacity (%, mass) of the adsorbate, p/p_0 is the relative pressure (the ratio of adsorbate vapor pressure to saturated vapor pressure), and E and W_0 are constants that depend only on the adsorbate properties of the pore volume and surface area. In this study, *k* and W_0 can be calculated from the adsorption isotherm data.

Table S2. Dubinin-Radushkevich model fit parameters for toluene and acetone adsorption on HNM.

Adsorbate	E (kJ/mol)	W_0 (cc/g)	Mean relative	\mathbb{R}^2	ΔH (kJ/mol)
			error $(\%)$		
Acetone	24.5	0.754	6.5	0.936	24
Toluene	48.2	0.792	3.5	0.985	49

Table S3. VOC adsorption capacity and yields of HNM regenerated over five cycles.

Cycles	Adsorption capacity (mg/g)		Yield $(\%)$	
	Toluene	Acetone	Toluene	Acetone
$_{0}$	372.0	248.3		
	369.1	245.1	99.8	99.4
2	371.5	246.6	99.5	98.9
3	366.2	247.3	98.4	98.8
4	369.3	244.1	98.3	98.5
5	366.5	246.0	98.3	98.4

Figure S5 | VOC adsorption-desorption onto HNM over five cycles.

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