Supplementary Information

## Training high-strength aluminum alloys to withstand fatigue

Qi Zhang, Yuman Zhu, Xiang Gao, Yuxiang Wu, Christopher Hutchinson\*

Department of Materials Science and Engineering, Monash University, Clayton, 3800, VIC,

AUSTRALIA.

\*Correspondence to: christopher.hutchinson@monash.edu

| Alloy  | Compositions (wt.%)                   | Solution treatment      | Aging treatment |           |
|--------|---------------------------------------|-------------------------|-----------------|-----------|
|        |                                       |                         | UA              | PA        |
| AA2024 | Al-4.6Cu-1.3Mg-(Zn-Mn-Si-Fe-Cr-Ti)    | 493°C 1h, air quenching | 191°C 30min     | 191°C 7h  |
| AA6061 | Al-1Mg-0.67Si-(Cu- Zn-Mn-Fe-Cr-Ti)    | 530°C 1h, air quenching | 177°C 20min     | 177°C 20h |
| AA7050 | Al-2.2Cu-2.3Mg-6.2Zn-(Mn-Si-Fe-Cr-Ti) | 480°C 1h, air quenching | 150°C 10min     | 150°C 10h |

Table S1. Alloys compositions and heat treatment conditions for AA2024, AA6061 and AA7050.



Fig. S1. Fatigue strength versus tensile strength for alloy steel, carbon steel, stainless steel and cast iron <sup>10</sup>.



**Fig. S2.** Bright field TEM images showing initial precipitation microstructure in grains for the under aged (UA) AA2024 (**a**), AA6061 (**b**) and AA7050 (**c**), the peak aged (PA) AA2024 (**d**), AA6061 (**e**) and AA7050 (**f**), and the cyclically trained UA AA2024 (**g**), AA6061 (**h**) and AA7050 (**i**) alloys. The electron beam is closely parallel to <100<sub>Al</sub> for AA2024 and AA6061, and is closely parallel to <110<sub>Al</sub> for AA7050.



**Fig. S3**. Engineering stress strain curves for UA, PA and trained AA2024 (**a**), AA6061 (**b**) and AA7050 (**c**) alloys.



**Fig. S4.** The fatigue crack growth (FCG) da/dN- $\Delta$ K curves in log scale for PA and UA AA2024 (**a**), AA6061 (**b**) and AA7050 (**c**) alloys. Tests were performed with pre-cracks both parallel (//) and perpendicular ( $\perp$ ) to the rolling direction (RD).



**Fig. S5.** Summary of the surface relief size evolution for UA and PA samples during fatigue. The stress amplitudes applied are 200 MPa for AA2024 (**a**), 120 MPa for AA6061 (**b**) and 195 MPa for AA7050 (**c**).



**Fig. S6.** Bright field TEM images showing the microstructure in PFZ's for PA and HCF treated AA2024 (a), AA6061 (b) and AA7050 (c) alloys. The electron beam is closely parallel to  $<001>_{A1}$  for AA2024 and AA6061, and is closely parallel to  $<110>_{A1}$  for AA7050. AA2024 was fatigued at 185 MPa for  $1\times10^6$  cycles, AA6061 was fatigued at 120 MPa for  $2\times10^6$  cycles and AA7050 was fatigued at 175 MPa for  $2\times10^6$  cycles.



**Fig. S7.** Cyclic training profiles showing the stress amplitude evolution as a function of cycle number for UA AA2024 (**a**), AA6061 (**b**) and AA7050 (**c**) alloys.



**Fig. S8.** LAADF-STEM images showing the precipitation microstructure in grains for the cyclically trained UA AA2024 (**a**, **d**), AA6061 (**b**, **e**) and AA7050 (**c**, **f**) alloys. The electron beam direction was parallel to  $<100>_{AI}$  for AA2024 and AA6061 and parallel to  $<110>_{AI}$  for 7050.



Fig. S9. Comparisons between the microstrains in original UA samples, samples after cyclical training and samples after tensile to the same final training stress ( $\sigma_f$ ) for AA2024, AA6061 and AA7050 alloys.