

779 **Appendix A. Supplementary Materials**

780 **1. Isotopic measurements**

781 The aliquots for Os isotopic analysis were added into chilled Pyrex® Carius tubes, along with
782 5 ml of concentrated HNO₃ and 2.3 ml of concentrated HCl. The Carius tubes were sealed and
783 then heated for at least 24 h at 220 °C (Shirey and Walker, 1995). Osmium was extracted from the
784 solution using CCl₄ solvent-extraction methods (Cohen and Waters, 1996), and then further
785 purified using microdistillation from a dichromate solution (Birck et al., 1997). This procedure
786 resulted in ~70 % yield for Os. Between 70-300 ng of purified Os were loaded onto outgassed Pt
787 filaments in HBr, activated with Ba(OH)₂, and analyzed as OsO₃⁻ by a *Thermo-Fisher Triton*
788 thermal ionization mass spectrometer (TIMS) at the University of Maryland (UMd) (Walker,
789 2012). Osmium isotopic data were corrected for instrumental and natural mass fractionation by
790 normalizing ¹⁹²Os/¹⁸⁸Os to 3.08271 (Allègre and Luck, 1980). Isobaric interferences from OsO₃⁻
791 species with ¹⁷O or ¹⁸O were corrected using the O isotopic composition reported by Nier (1950).

792 Molybdenum aliquots were prepared following the methods described in Worsham et al.
793 (2016a). In brief, aliquots were dried, dissolved in 1 M HF, and loaded onto an anion column of
794 AG 1-X8 (200-400 mesh) resin. Molybdenum was eluted using 6 M HNO₃-3 M HF, dried, and
795 dissolved in 6 M HCl. The Mo solution was then added to a smaller anion column with ~0.3 mL
796 AG 1-X8 (200-400 mesh) resin and eluted with 1 M HCl. This elution was repeated a second time.
797 This procedure resulted in ~50 % yield for Mo. Purified Mo aliquots were treated with
798 concentrated HCl and HNO₃ multiple times in order to destroy organics. The samples were then
799 dissolved in 6 M HCl, about 500-1000 ng Mo were loaded onto outgassed Re filaments, and
800 activated with ~ 2 µL of a 5 µg/µL La(NO₃)₃ solution. A double filament assembly was used and
801 the same amount of La(NO₃)₃ was added to the ionization Re filament. Molybdenum was measured

802 as MoO_3^- by the *Thermo-Fisher Triton Plus* TIMS at UMd. The $^{100}\text{Mo}^{18}\text{O}^{16}\text{O}_2^-$ species was
803 measured using a $10^{13} \Omega$ resistor amplifier for O isotope interference corrections. Molybdenum
804 isotopic data were corrected for instrumental and natural mass fractionation by normalizing
805 $^{98}\text{Mo}/^{96}\text{Mo}$ to 1.453171 (Lu and Masuda, 1994).

806 Aliquots for Ru isotopic analysis were prepared following the procedure discussed by
807 Bermingham et al. (2016). In brief, aliquots of the primary dissolution were dried and dissolved in
808 0.15 M HCl and then processed through a cation column of AG50WX8 (200-400 mesh) resin.
809 Ruthenium was immediately eluted using 0.15 M HCl and dried to about 5 μL for microdistillation,
810 in which $\text{H}_2\text{Cr}_2\text{O}_7$ was used as the oxidant and 6 M HCl was used as the trap solution and reductant.
811 This procedure resulted in ~50 % yield for Ru. About 1000 ng of purified Ru were loaded onto
812 outgassed single Pt filaments in HBr, activated with $\text{Ba}(\text{OH})_2$, and analyzed as RuO_3^- by a *Thermo-*
813 *Fisher Triton Plus* TIMS. Ruthenium isotopic data were corrected for instrumental and natural
814 mass fractionation by normalizing $^{99}\text{Ru}/^{101}\text{Ru}$ to 0.745075 (Chen et al., 2010). The O isotopic
815 composition reported by Nier (1950) was used to determine and correct for in-run ^{17}O and ^{18}O
816 molecular interferences.

817 Tungsten aliquots from the primary dissolution were exposed to air for 1-2 weeks in order to
818 oxidize Fe in the solution from +2 to +3. Ferrous Fe was then removed using a diisopropyl ether
819 extraction procedure (Dodson et al., 1936). The resulting solution was dried, dissolved in 1 M
820 HCl-0.1 M HF, and eluted through a cation column of AG50-X8 (200-400 mesh) resin with 1 M
821 HCl-0.1 M HF. The solution was then dried, dissolved in 0.5 M HCl-0.5 M HF, loaded onto a
822 column of AG1-X8 (100-200 mesh) resin, and eluted with 6 M HCl-1 M HF. This elution was
823 repeated twice using progressively less resin and acid (Touboul and Walker, 2012). This procedure
824 resulted in ~60 % yield for W. Organics accrued during the column chemistry were removed by

825 drying the sample multiple times in concentrated HCl and HNO₃. About 300-1000 ng of purified
826 W were then dissolved in 1 M HCl- 0.01 M HF, loaded onto outgassed single Re filaments,
827 activated with 1 μL of a 5 μg/μL La-5 μg/μL Gd solution, and measured as WO₃⁻ using a *Thermo-*
828 *Fisher Triton* TIMS following the method of Archer et al. (2017). This method allowed
829 independent measurement of both ¹⁸²W/¹⁸⁴W and ¹⁸³W/¹⁸⁴W. Potential mass interference from
830 ReO₃⁻ species were also monitored and corrected for. Tungsten isotopic data were corrected for
831 instrumental and natural mass fractionation by normalizing ¹⁸⁶W/¹⁸⁴W to 0.92767 (Volkening et
832 al., 1991).

833 Some prior studies of terrestrial and cosmochemical materials have observed deviations in
834 ¹⁸³W/¹⁸⁴W ratios for reference standards and samples that were processed through certain column
835 chemistry procedures and analyzed by multi-collector inductively-coupled plasma mass
836 spectrometry (e.g., Kruijer et al., 2013; Cook and Schönbachler, 2016; Kruijer and Kleine, 2018).
837 Such deviations have been interpreted to be the result of nuclear field shift effects, requiring
838 corrections to be made to account for the observed deviations (Cook and Schönbachler, 2016).
839 However, no such effects have been observed for reference standards, terrestrial samples, or
840 meteorite samples using the column chemistry procedures described here, coupled with thermal
841 ionization mass spectrometry (Archer et al., 2017; Mundl et al., 2017; Mundl et al., 2018; Archer
842 et al., 2019). Consequently, no corrections to the measured ¹⁸³W/¹⁸⁴W ratios from this study have
843 been made.

844 Values of μ¹⁸²W for the SBT were corrected for nucleosynthetic variations using the method
845 reported by Kruijer et al. (2014a). In this correction, variation in the *r*-process component for irons
846 is subtracted from the μ¹⁸²W value using μ¹⁸³W as an *r*-process component proxy. This correction
847 is based on the ^{182/184}W vs. ^{183/184}W isotopic composition of fine- and coarse-grained CAI, which

848 give a $^{182/184}\text{W}$ vs. $^{183/184}\text{W}$ (186/184 normalized) correlation of $+1.41 \pm 0.06$. The ΔT_{CAI} ages were
849 then calculated using the CAI initial value $\mu^{182}\text{W}$ of -349 ± 7 (Kruijer et al., 2014b), the present-
850 day chondritic $\mu^{182}\text{W}$ value of -190 ± 10 (Kleine et al., 2004), and the decay constant for ^{182}Hf of
851 $0.078 \pm 0.002 \text{ Myr}^{-1}$ (Vockenhuber et al., 2004). The ΔT_{CAI} ages for Babb's Mill, South Byron,
852 and ILD 83500 were calculated from the $\mu^{182}\text{W}$ and $\mu^{183}\text{W}$ values determined by normalizing to
853 $^{186}\text{W}/^{184}\text{W}$. The uncertainties for the ΔT_{CAI} ages include the 2SD determined from the analysis of
854 standards run during an analytical campaign for $\mu^{182}\text{W}$ and $\mu^{183}\text{W}$ compositions, and the
855 uncertainty associated with the $\mu^{183}\text{W}$ *r*-process correction only (Kruijer et al., 2014a). Tungsten
856 isotopic data were not obtained for Milton because there was insufficient material to make this
857 measurement.

858

859 **2. Fractional crystallization modeling**

860 In this study, Eq. S1 is used to calculate the concentration of an element throughout the
861 evolution of a liquid melt, where F_n is the fraction of liquid ($n = 100$ is pure liquid), C_{L_n} is the
862 concentration of an element in the liquid phase at F_n , and D_n is the partition coefficient of an
863 element. The concentration of an element is calculated at each 0.1 % fraction of liquid with respect
864 to the concentration of the previous liquid fraction. For S, a constant partition coefficient of 0.001
865 is used (Walker et al., 2008). The partition coefficients for P and C are determined at each F_n by
866 considering the concentration of S and P or S and C, respectively, in the liquid at F_{n+1} . Equation
867 S2 is used to account for the effects of S on P and C partitioning behavior (Chabot and Jones,
868 2003).

869 Values of D_0 for P and C are taken from Chabot et al. (2017) and Worsham et al. (2016b),
870 respectively. The β_{SPC} variable is determined using Eq. S3 (Jones and Malvin, 1990), in which β_S

871 and β_P are taken from Chabot et al. (2017) and β_C is taken from Worsham et al. (2016b). For P, the
 872 effects of C are not considered and for C, the effects of P are not considered. The β_{SPC} and “Fe
 873 domains” (Eq. S4; Chabot et al., 2017) variables are calculated at each F_n , where X_i is the mole
 874 fraction of an element.

$$875 \quad \text{Eq. S1: } C_{Ln-1} = \frac{C_{Ln}}{(F_{n-1} + 1 - F_{n-1}D_{n-1})}$$

$$876 \quad \text{Eq. S2: } \frac{1}{D} = \frac{[\text{Fe domains}]^{\beta_{SPC}}}{D_o}$$

$$877 \quad \text{Eq. S3: } \beta_{SPC} = \left[\frac{2X_S}{2X_S + 4X_P + 4X_C} \right] \beta_S + \left[\frac{4X_P}{2X_S + 4X_P + 4X_C} \right] \beta_P + \left[\frac{4X_C}{2X_S + 4X_P + 4X_C} \right] \beta_C$$

$$878 \quad \text{Eq. S4: Fe domains} = \frac{1 - 2X_S - 4X_P - 4X_C}{1 - X_S - 3X_P - 3X_C}$$

$$879 \quad \text{Eq. S5: } C_{Sn} = C_{Ln}D_n$$

880 After determining the concentration of S, P, and C at each F_n , the D values for the HSE are
 881 calculated at each F_n using Eq. S2-S4 by collectively considering the changes in S, P, and C content
 882 in the liquid (Jones and Malvin, 1990; Chabot and Jones, 2003; Worsham et al., 2016b; Chabot et
 883 al., 2017). The concentration of HSE in the liquid at each F_n is then determined using Eq. S1 and
 884 the solid composition (C_{Sn}) at each F_n is determined using Eq. S5.

885

886 **3. Thermal accretion model**

887 This study uses a thermal accretion model (Eq. S6) that describes a solid sphere, which gains
 888 heat through ^{26}Al decay and loses heat by conduction (Carslaw and Jaeger, 1959). The model
 889 solves for the temperature at a certain depth within the sphere at any time (t) after accretion and
 890 we assume that differentiation occurred instantaneously when the temperature halfway to the

891 center of the body from the surface reached 1600 K (Kruijer et al., 2017). This assumption is made
 892 since ~50 % of silicate melt fractions may be necessary for core formation (Taylor, 1992). In order
 893 to be consistent with past studies, we assume a radius of $R = 40$ km for the parent body and the
 894 temperature is evaluated at a depth of $r = 20$ km (Kruijer et al., 2017). The background nebular
 895 temperature is represented as T_0 , thermal conductivity is represented as K , thermal diffusivity is
 896 represented as k , and a ^{26}Al decay constant of $\lambda = 9.83 \times 10^{-7} \text{ yr}^{-1}$ is used with a Solar System initial
 897 $^{26}\text{Al}/^{27}\text{Al}$ ratio of 5.23×10^{-5} (Norris et al., 1983; Jacobsen et al., 2008). All values used in this
 898 model are listed in Table S1.

899 Eq. S6:
$$T = T_0 + \frac{kA}{K\lambda} e^{-\lambda t} \left(\frac{R \sin\left(r * \left(\frac{\lambda}{k}\right)^{\frac{1}{2}}\right)}{r \sin\left(R * \left(\frac{\lambda}{k}\right)^{\frac{1}{2}}\right)} - 1 \right) + \frac{2R^3 A}{r\pi^3 K} \sum_{n=1}^{\infty} \frac{(-1)^n}{n(n^2 - \frac{\lambda R^2}{k\pi^2})} \sin\left(\frac{n\pi r}{R}\right) e^{-kn^2\pi^2 t/R^2}$$

900

901 The background temperature is assumed to be 250 K, consistent with models by Hevey and
 902 Sanders (2006), Kruijer et al. (2014b), and Kruijer et al. (2017), which is the average temperature
 903 estimated for a circumsolar disk at 2.5 AU and 1 Myr after T-Tauri star formation (Woolum and
 904 Cassen, 1999). The power per unit volume A (W m^{-3}) = $H * \rho$, where H is the power per unit mass
 905 (W kg^{-1}) and ρ is the density of the planetesimal (kg m^{-3}). The power per unit mass, H , is equal to
 906 (total Al atoms/kg) * ($^{26}\text{Al}/^{27}\text{Al}$) * ($2.0 \times 10^{-26} \text{ W/atom}$), where ($^{26}\text{Al}/^{27}\text{Al}$) is a function of time, the
 907 parent body concentration of Al is based off of the range observed in carbonaceous chondrites
 908 (0.86-1.68 wt. %; Lodders and Fegley, 1998), and the decay power of ^{26}Al is calculated from a
 909 decay energy of ^{26}Al of $6.4 \times 10^{-13} \text{ J/atom}$ with its half-life of $9.83 \times 10^{-7} \text{ yr}^{-1}$ (Hevey and Sanders,
 910 2006). We note that this calculation of heat production differs from that reported by Kruijer et al.
 911 (2017). Kruijer et al. (2017) report using a range of Al concentration from 8.65-16.8 wt. %, which
 912 is an order of magnitude greater than used here. In addition, Kruijer et al. (2017) report calculating

913 heat production as $A = \text{Al concentration} * (^{26}\text{Al}/^{27}\text{Al})$ and it is calculated in this study as $A = (\text{total}$
914 $\text{Al atoms/kg}) * (^{26}\text{Al}/^{27}\text{Al}) * (2.0 \times 10^{-26} \text{ W/atom}) * (\rho)$, where $(^{26}\text{Al}/^{27}\text{Al})$ is a function of time in both
915 models. Despite these differences between the model inputs, the results of both models differ by
916 less than 0.2 Myr. For this study, 0.86 wt. % Al relates to $A = 12.3 * (^{26}\text{Al}/^{27}\text{Al})$, 1.20 wt. % Al
917 relates to $A = 17.1 * (^{26}\text{Al}/^{27}\text{Al})$ and 1.68 wt. % Al relates to $A = 23.9 * (^{26}\text{Al}/^{27}\text{Al})$. Therefore, the
918 results in this study for 0.86 wt. % Al and 1.20 wt. % Al are similar to the results by Kruijer et al.
919 (2017) for 12 wt. % Al and 16.8 wt. % Al, respectively.

920 **Supplementary Tables**

921 **Table S1**

922 Osmium isotopic composition data for Milton and the SBT.

Sample	n ^a	$\mu^{189}\text{Os}$	2SD	$\mu^{190}\text{Os}$	2SD
Milton	1	-4	8	25	18
Babb's Mill	2	1	6	-4	7
Babb's Mill (<i>rep</i>)	1	8	7	-1	4
South Byron	3	8	7	-4	7
ILD 83500	1	3	6	-3	7

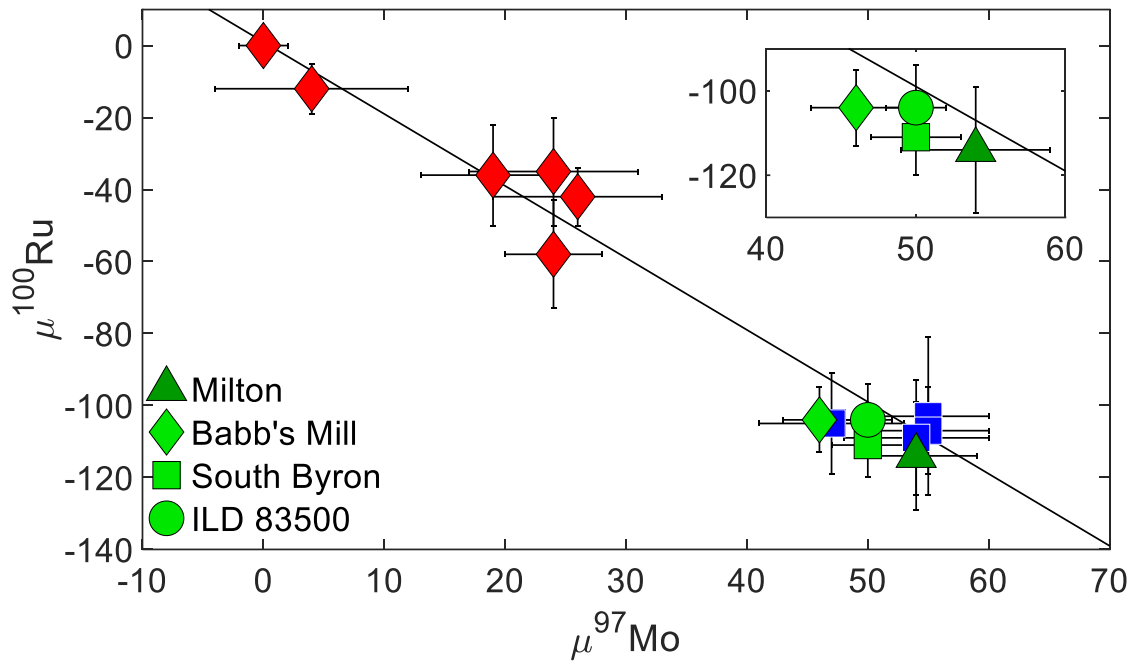
923 ^a n is the number of analyses. The reported $\mu^{189}\text{Os}$ and $\mu^{190}\text{Os}$ values
 924 reflect the average values obtained for each meteorite piece. Uncertainties
 925 reflect the largest (of n analyses) 2SD of the standards run during an
 926 analytical campaign.

927 **Table S2**

928 Terms and values used in the thermal accretion model.

Term	Symbol	Units	Value	Source
Al concentration	Al	Wt. %	0.86-1.68	Lodders and Fegley (1998)
Ambient temperature	T_o	K	250	Woolum and Cassen (1999)
Decay constant	λ	yr ⁻¹	9.83×10^{-7}	Norris et al. (1983)
Decay energy	E	J atom ⁻¹	6.4×10^{-13}	Hevey and Sanders (2006)
Density	ρ	kg m ⁻³	3200	Kruijer et al. (2017)
Diffusivity	k	m ² s ⁻¹	5×10^{-7}	Kruijer et al. (2017)
Initial ²⁶ Al/ ²⁷ Al	²⁶ Al/ ²⁷ Al _i	atom/atom	5.23×10^{-5}	Jacobsen et al. (2008)
Power per unit mass	H	W kg ⁻¹	^a	
Power per unit volume	A	W m ⁻³	H x ρ	
Depth assessed for temperature	r	km	20	Kruijer et al. (2017)
Radius of body	R	km	40	Kruijer et al. (2017)
Thermal conductivity	K	W m ⁻¹ K ⁻¹	2.1	LaTourrette and Wasserburg (1998)

929 ^a $H = (\text{Al atoms/kg}) * (^{26}\text{Al}/^{27}\text{Al}) * (E * \lambda_{\text{sec}})$, where (²⁶Al/²⁷Al) is a function of time and λ is in units of s⁻¹.



931

932 **Fig. S1.** Compilation of CRE-corrected $\mu^{97}\text{Mo}$ vs. $\mu^{100}\text{Ru}$ data for iron meteorites from

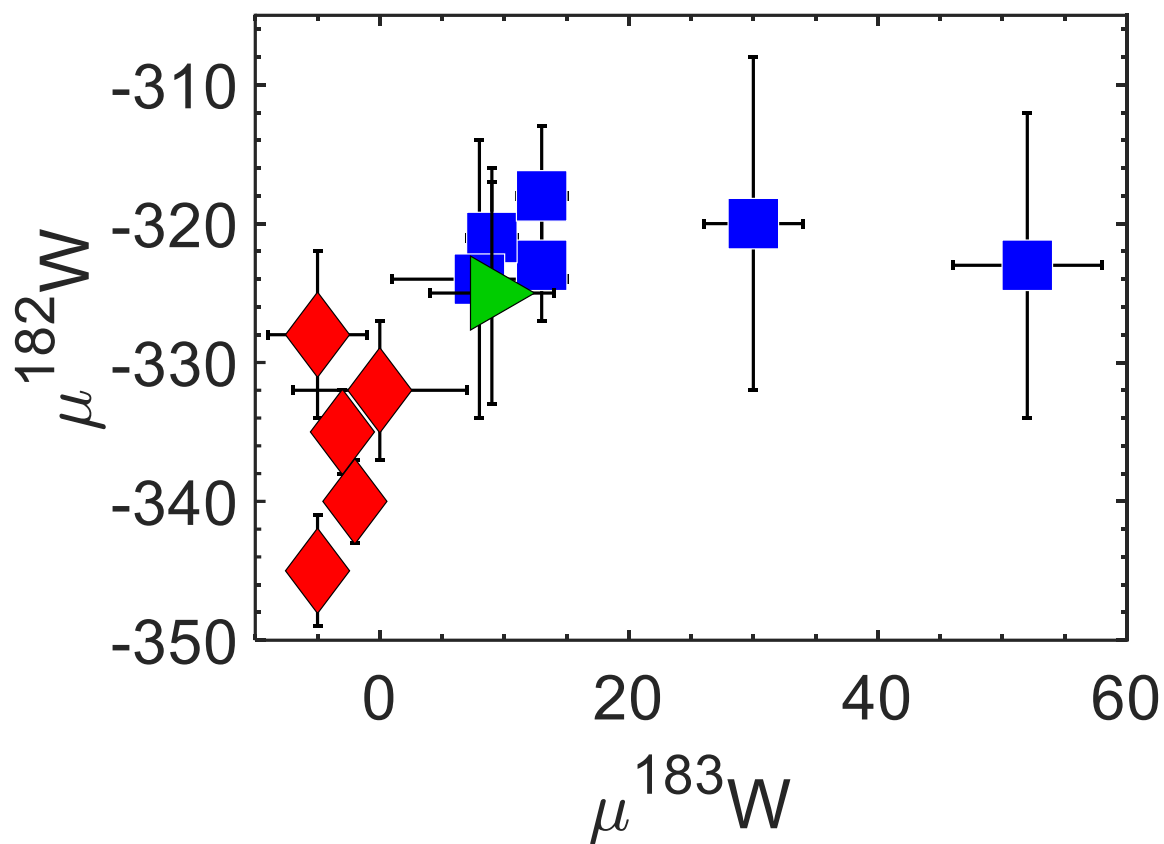
933 Birmingham et al. (2018). Blue squares represent meteorites classified as CC type and red

934 diamonds represent meteorites classified as NC type. Data from this study for the SBT and Milton

935 are also plotted. The black line represents the regression of the Mo-Ru cosmic correlation from

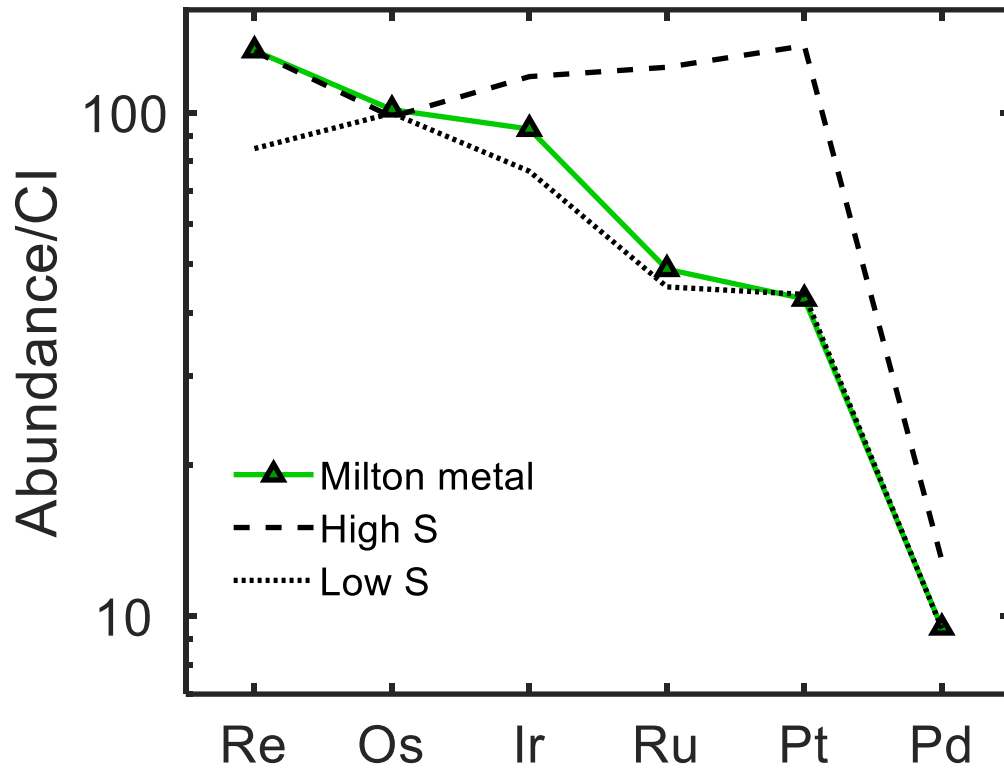
936 Birmingham et al. (2018). The inset shows the Mo and Ru isotopic composition of the SBT and

937 Milton without other meteorites.



938

939 **Fig. S2.** Compilation of $\mu^{183}\text{W}$ vs. $\mu^{182}\text{W}$ data for iron meteorites from Kruijer et al. (2017). Blue
 940 squares represent meteorites classified as CC type and red diamonds represent meteorites classified
 941 as NC type. The average SBT W isotopic composition is also plotted (green triangle). The average
 942 $\mu^{183}\text{W}$ value for the SBT ($+9 \pm 5$, 2SE, $n = 4$) is resolved from the W standard value obtained
 943 during the analytical campaigns for this work (0 ± 2 , 2SE, $n = 16$).



944

945 **Fig. S3.** CI-normalized HSE patterns calculated from a constant HSE initial concentration from
 946 Table 4 and varying S and P parental melt compositions. Assuming Milton metal crystallized in
 947 the first ~10% of solid, the Re/Os of Milton metal resembles a high S system with 17 wt. % S, 1.5
 948 wt. % P, and <0.05 wt. % C. However, the Pt/Os of Milton metal resembles a lower S system with
 949 8 wt. % S, 1 wt. % P, and <0.05 wt. % C.

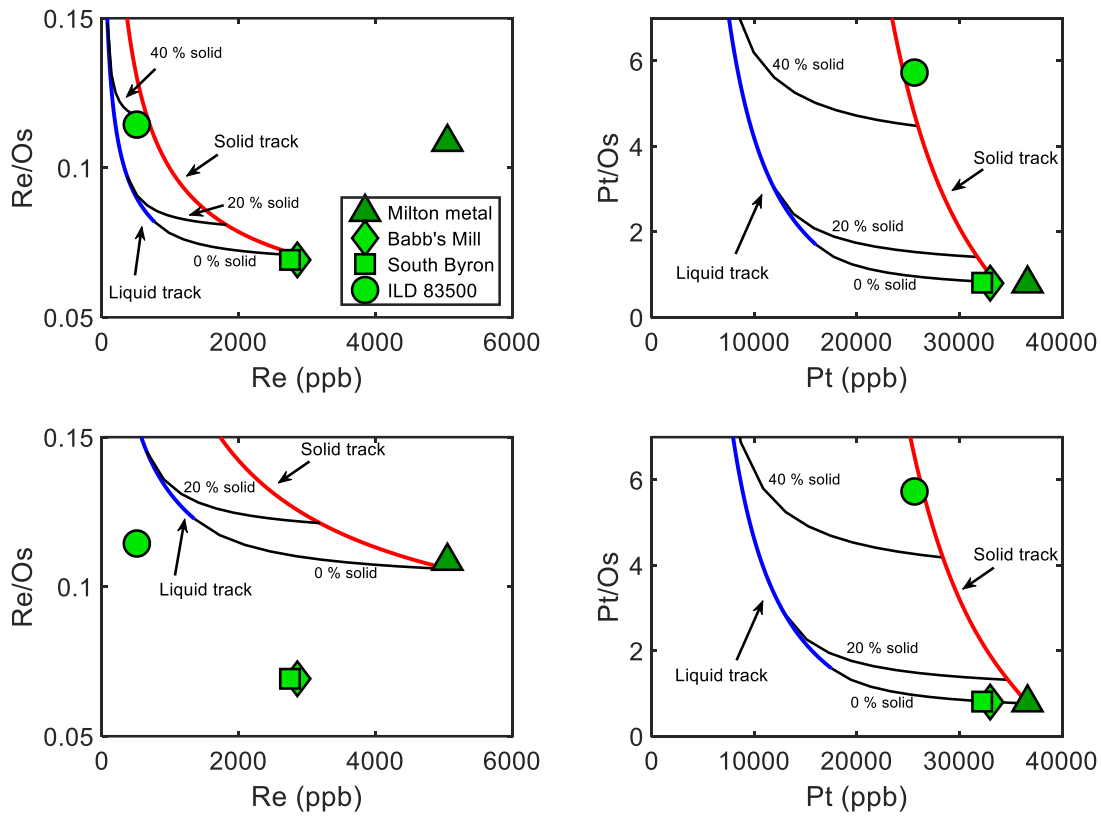
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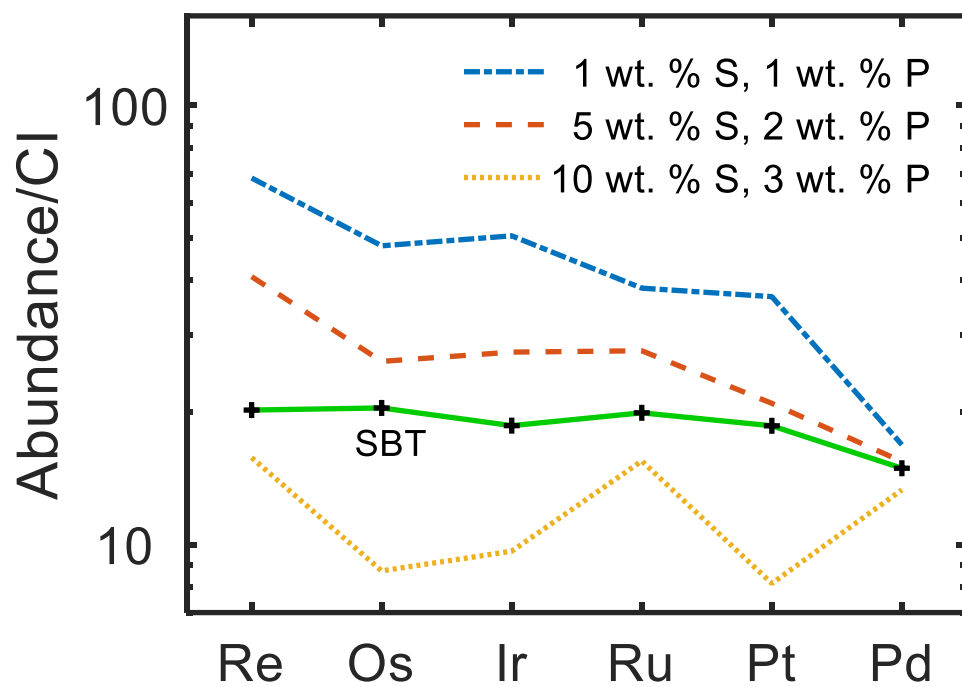
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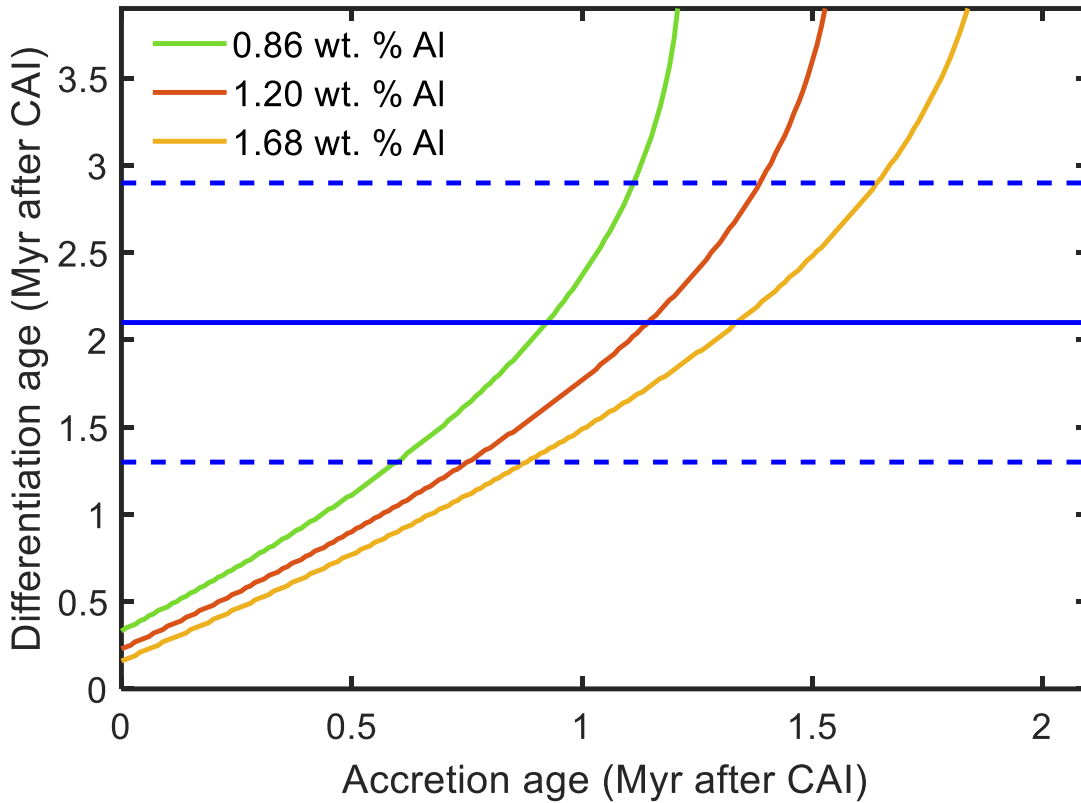
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956 **Fig. S4.** Fractional crystallization models for Re (ppb) vs. Re/Os and Pt (ppb) vs. Pt/Os for two
 957 pairs of parental melt compositions. Black lines represent mixing between solid and liquid, at 0 %
 958 solid-100 % liquid, 20 % solid-80 % liquid, and 40 % solid-60 % liquid. (*Upper left and right*)
 959 Fractional crystallization model, which reproduce the HSE patterns observed for the SBT,
 960 calculated for the initial parameters listed in Table 4. (*Bottom left and right*) Fractional
 961 crystallization model with 7 wt. % S and 1 wt. % P, which can reproduce the observed HSE
 962 patterns for Milton metal. This model requires a starting liquid composition of Re = 1,350 ppb, Os
 963 = 11,000 ppb, and Pt = 17,500 ppb. Neither model can reproduce both Re/Os and Pt/Os observed
 964 in Milton metal and the SBT through solid metal-liquid metal mixing.



965

966 **Fig. S5.** CI-normalized HSE parental melt compositions, with varying S and P contents, which
 967 reproduce the Milton HSE pattern as an early (<10 %) fractional crystallizing metal. The parental
 968 melt composition of the SBT is shown for comparison.



969

970 **Fig. S6.** Thermal model results for a 40 km radius body when evaluating the temperature midway
 971 to the center of the body ($r = 20$ km). The model is based on an assumption of instantaneous
 972 differentiation when the temperature reaches 1600 K. Thermal model results are shown for Al
 973 concentrations of 0.86, 1.20, and 1.68 wt. %. The differentiation age of the SBT (2.1 ± 0.8 Myr
 974 after CAI formation; blue solid line \pm blue dashed lines) fits an accretion age range of 1.1 ± 0.5
 975 Myr after CAI formation.

976 **Supplementary References**

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