

# Neural Network Similarity: A New Measure to Assist Decision Making in Chemical Toxicology

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#### **Links to source code and models generated**

Python 3 code for fingerprint generation, chemical clustering, model construction, and model recall and network similarity calculation, as well as data used for training and testing the models and model files for optimized models can be found in GitHub ([https://github.com/teha2/chemical\\_toxicology](https://github.com/teha2/chemical_toxicology)) and in the University of Cambridge repository (<https://doi.org/10.17863/CAM.50429>).

## **DNN Model Details**

The cost function used in DNN training was sparse categorical cross-entropy including class weights to allow for binary classification with an imbalanced data set. The Adam optimizer was used to provide efficient model training. L2 regularization was added to the cost function to prevent overfitting.

A multi-class multi-label predictor was considered for this task, incorporating several biological targets into a single network. This dataset would have contained many “unknown” labels (cases where a compound was tested against one target but not against others) leaving holes in the dataset that caused difficulty in training and evaluation. As a result of this, several binary classification networks were pursued, each predicting the activity at a single biological target without the requirement for any “unknown” data labels.

## **Hyperparameters.**

The learning rate was adjusted on a case by case basis to give a smooth training curve and fast gradient descent. The regularization rate for L2 regularization was adjusted to prevent a large gap between the statistical performance values of the training and validation data. In addition, early stopping was used to prevent overfitting, by reducing the number of training iterations while maintaining a smooth training curve.

## **Performance Statistics.**

Values provided in the output layer of each of the DNNs were interpreted using the Argmax and Softmax functions, yielding binary predictions of molecular activity and probability of positive activity respectively. The Argmax function yielded numbers of true positives (chemical predicted positive, experimentally positive, TP), false positives (chemical predicted positive, experimentally negative, FP), true negatives (chemical predicted negative, experimentally negative, TN) and false negatives (chemical predicted negative, experimentally positive FN). These values were used to calculate evaluation statistics on the training and test sets, including sensitivity (SE), specificity (SP), accuracy (ACC) and Matthews correlation coefficient.

$$SE = \frac{TP}{TP + FN}$$

$$SP = \frac{TN}{TN + FP}$$

$$ACC = \frac{TP + TN}{TP + TN + FP + FN}$$

$$MCC = \frac{TP \times TN - FP \times FN}{\sqrt{(TP + FP)(TP + FN)(TN + FP)(TN + FN)}}$$

The SE, SP and ACC give percentages based on the number of positives, negatives and molecules correctly assigned respectively. The MCC gives a value between -1 and +1 and removes bias in the available data. An MCC value of +1 is obtained if every prediction is correct, a value of -1 if every prediction is incorrect, and 0 if predictions are random.

The positive probability values generated using the Softmax function allow for the plotting of a receiver operating curve (ROC) and the calculation of the area under this curve (ROC-AUC). This value can be between 0 and 1 and represents the probability that an experimentally positive compound is given a higher positive probability than an experimentally negative one. Higher SE, SP, ACC, MCC and ROC-AUC values are associated with better predictive models.

For each network architecture, for each biological target five networks were produced, changing the chemical cluster used in the test set and randomizing the training/validation shuffle and split seeding values to provide five-fold clustered cross-validation. The performance on each of the training, validation and test sets were then averaged to prevent any single cluster affecting the overall results.

The highest performing networks provide optimized predictive models for use in safety evaluation. These models are provided via GitHub ([https://github.com/teha2/chemical\\_toxicology](https://github.com/teha2/chemical_toxicology)) and in the University of Cambridge repository (<https://doi.org/10.17863/CAM.50429>).

**Initial investigations into fingerprints and activation functions**

[10]		Training					Test				
Fingerprint		SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>MACCS</b>		86.7	76.7	85.6	0.673	0.89	85.9	74.3	85.1	0.648	0.87
<b>ECFP6 1000</b>		88.0	82.4	88.7	0.743	0.92	87.5	81.3	87.9	0.728	0.90
<b>ECFP6 5000</b>		89.0	85.4	90.1	0.775	0.94	88.1	83.8	89.0	0.750	0.92
<b>ECFP6 10000</b>		89.4	81.8	89.0	0.754	0.93	87.7	79.0	87.1	0.708	0.90
<b>ECFP4 1000</b>		87.7	83.4	89.0	0.749	0.93	86.7	80.6	87.2	0.708	0.91
<b>ECFP4 5000</b>		87.9	88.0	90.7	0.788	0.94	85.9	84.6	88.2	0.732	0.91
<b>ECFP4 10000</b>		88.5	87.2	90.5	0.785	0.94	87.1	85.9	89.6	0.760	0.92
<b>ECFP4 20000</b>		89.3	87.0	90.8	0.791	0.94	86.3	82.6	87.9	0.726	0.91
[10,10]		Training					Test				
Fingerprint		SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>MACCS</b>		87.1	74.6	85.4	0.666	0.88	81.8	74.4	79.6	0.593	0.88
<b>ECFP6 1000</b>		88.0	84.7	89.3	0.756	0.93	86.2	83.4	87.7	0.722	0.92
<b>ECFP6 5000</b>		88.5	90.4	91.6	0.811	0.95	86.4	86.3	89.1	0.750	0.92
<b>ECFP6 10000</b>		88.4	88.3	91.3	0.800	0.95	85.8	84.6	88.7	0.739	0.92
<b>ECFP4 1000</b>		88.3	86.9	89.9	0.770	0.94	86.6	82.6	87.5	0.715	0.91
<b>ECFP4 5000</b>		88.5	90.8	92.2	0.820	0.96	85.9	85.0	88.6	0.740	0.92
<b>ECFP4 10000</b>		89.4	89.4	91.9	0.814	0.95	86.4	85.5	88.9	0.747	0.92
<b>ECFP4 20000</b>		89.2	86.4	90.7	0.789	0.94	87.7	82.2	88.0	0.735	0.91
[10,10,10]		Training					Test				
Fingerprint		SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>MACCS</b>		86.7	81.9	87.5	0.715	0.90	85.6	81.6	86.9	0.701	0.89
<b>ECFP6 1000</b>		92.3	96.3	95.4	0.897	0.98	84.8	86.0	87.6	0.722	0.91
<b>ECFP6 5000</b>		96.1	98.5	98.2	0.957	1.00	87.4	86.7	89.1	0.756	0.92
<b>ECFP6 10000</b>		98.9	99.4	99.3	0.985	1.00	88.4	86.2	89.2	0.757	0.93
<b>ECFP4 1000</b>		93.0	95.8	95.7	0.903	0.98	86.8	85.4	88.3	0.730	0.91
<b>ECFP4 5000</b>		98.9	99.5	99.4	0.987	1.00	86.8	84.9	87.7	0.723	0.92
<b>ECFP4 10000</b>		99.1	99.6	99.5	0.988	1.00	87.8	87.2	89.1	0.752	0.92
<b>ECFP4 20000</b>		98.4	99.7	99.3	0.984	1.00	86.4	89.4	89.8	0.771	0.93

Table S1. A summary of the results shown in Table S2 comparing the model performance of several chemical fingerprints across three network architectures and five biological targets. Highest accuracy (ACC) Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC) values are highlighted in red. ECFP4 at length 10000 was chosen as the best performing fingerprint across the single

layer [10] and two layer [10,10] networks of 10 neurons, and three-layer networks [10,10,10] were dropped from further investigation due to high levels of overfitting.

MACCS Keys		Training Data					Test Data				
	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[10]	ADORA2A	98.2	85.9	93.9	0.865	0.97	97.8	85.7	93.6	0.858	0.97
	hERG	88.1	51.5	73.4	0.434	0.79	89.3	49.4	73.7	0.432	0.75
	AR	60.7	96.0	86.5	0.638	0.86	57.2	95.7	85.9	0.602	0.84
	AChE	87.8	68.4	79.4	0.579	0.86	86.4	67.4	78.6	0.552	0.85
	SERT	98.7	81.6	94.9	0.849	0.97	98.8	73.3	93.5	0.795	0.95
	avg	86.7	76.7	85.6	0.673	0.89	85.9	74.3	85.1	0.648	0.87
[10,10]	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
	ADORA2A	97.9	87.6	94.4	0.874	0.97	97.6	87.1	93.8	0.865	0.96
	hERG	94.9	35.4	71.2	0.394	0.75	64.2	37.8	42.6	0.016	0.75
	AR	57.3	96.5	86.1	0.621	0.85	61.3	96.6	87.1	0.655	0.86
	AChE	86.7	71.1	80.0	0.589	0.86	86.7	69.5	79.3	0.574	0.86
	SERT	98.7	82.6	95.2	0.854	0.97	99.2	81.0	95.1	0.856	0.97
[10,10,10]	avg	87.1	74.6	85.4	0.666	0.88	81.8	74.4	79.6	0.593	0.88
	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
	ADORA2A	97.9	89.5	95.0	0.889	0.98	97.9	89.6	95.0	0.889	0.98
	hERG	87.7	57.0	75.5	0.476	0.81	87.3	60.8	77.4	0.505	0.79
	AR	63.2	97.0	88.1	0.677	0.87	60.7	97.0	87.0	0.660	0.86

		AChE	86.4	77.2	82.5	0.641	0.85	84.3	72.1	79.0	0.569	0.85
		SERT	98.5	88.9	96.4	0.892	0.98	98.0	88.5	95.9	0.880	0.97
		avg	86.7	81.9	87.5	0.715	0.90	85.6	81.6	86.9	0.701	0.89
<b>ECFP6 1000</b>												
[10]	<b>Training Data</b>						<b>Test Data</b>					
	Model	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	
	ADORA2A	97.9	90.3	95.3	0.894	0.98	98.4	86.8	94.3	0.875	0.97	
	hERG	92.9	50.7	76.2	0.498	0.84	91.1	48.9	74.0	0.453	0.81	
	AR	62.4	98.5	88.9	0.705	0.88	61.3	98.4	88.5	0.694	0.87	
	AChE	87.9	84.8	86.6	0.726	0.93	87.9	84.8	86.6	0.726	0.90	
	SERT	98.8	87.7	96.3	0.892	0.99	98.8	87.7	96.3	0.892	0.97	
[10,10]	avg	88.0	82.4	88.7	0.743	0.92	87.5	81.3	87.9	0.728	0.90	
	Model	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	
	ADORA2A	97.7	91.7	95.6	0.903	0.98	97.6	91.1	95.4	0.897	0.98	
	hERG	89.7	64.6	79.9	0.570	0.88	87.8	61.1	76.6	0.514	0.88	
	AR	65.4	98.0	89.4	0.716	0.88	62.5	97.5	88.0	0.683	0.86	
	AChE	88.4	80.1	84.8	0.690	0.92	85.5	79.6	83.0	0.652	0.90	
	SERT	98.8	89.3	96.7	0.902	0.99	97.6	87.6	95.5	0.865	0.99	
[10,10,10]	avg	88.0	84.7	89.3	0.756	0.93	86.2	83.4	87.7	0.722	0.92	
	Model	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	
[10,10,10]	ADORA2A	99.4	98.5	99.0	0.979	1.00	96.4	92.2	95.0	0.889	0.98	

		hERG	90.6	90.5	90.6	0.805	0.96	77.8	72.6	75.7	0.500	0.83
		AR	76.6	98.8	93.0	0.815	0.93	66.7	95.2	87.5	0.669	0.85
		AChE	94.9	94.3	94.7	0.892	0.99	84.9	85.3	85.1	0.697	0.90
		SERT	99.9	99.4	99.8	0.993	1.00	98.1	84.6	95.0	0.855	0.97
		avg	92.3	96.3	95.4	0.897	0.98	84.8	86.0	87.6	0.722	0.91
<b>ECFP6 5000</b>		<b>Training Data</b>						<b>Test Data</b>				
		Model	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>
[10]	ADORA2A	97.9	95.9	97.2	0.938	0.99	97.4	91.0	95.2	0.894	0.99	
	hERG	89.7	63.3	79.2	0.560	0.87	87.9	59.3	76.7	0.500	0.83	
	AR	69.9	99.3	91.5	0.778	0.93	67.4	98.8	90.2	0.748	0.87	
	AChE	88.2	85.5	87.0	0.736	0.94	88.8	83.9	86.7	0.729	0.92	
	SERT	99.0	83.1	95.5	0.866	0.99	98.8	85.9	96.0	0.880	0.98	
	avg	89.0	85.4	90.1	0.775	0.94	88.1	83.8	89.0	0.750	0.92	
		Model	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>
[10,10]	ADORA2A	97.5	91.3	95.4	0.897	0.99	97.6	92.1	95.7	0.904	0.98	
	hERG	88.1	82.9	86.0	0.709	0.93	83.2	71.2	78.6	0.545	0.86	
	AR	69.8	99.0	91.3	0.771	0.91	65.6	98.2	89.4	0.721	0.86	
	AChE	87.9	89.5	88.6	0.770	0.95	87.3	85.9	86.7	0.730	0.93	
	SERT	98.9	89.5	96.9	0.907	0.99	98.1	84.1	95.0	0.852	0.98	
	avg	88.5	90.4	91.6	0.811	0.95	86.4	86.3	89.1	0.750	0.92	
		Model	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-</b>

		AUC					AUC					
		Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[10,10,10]	ADORA2A	99.7	98.9	99.4	0.987	1.00	96.7	92.3	95.2	0.893	0.98	
	hERG	98.5	96.6	97.8	0.953	1.00	83.4	70.4	78.1	0.542	0.85	
	AR	83.1	99.8	95.4	0.881	0.98	69.9	96.6	89.4	0.721	0.87	
	AChE	99.3	98.9	99.2	0.983	1.00	88.6	82.4	85.9	0.712	0.92	
	SERT	99.7	98.4	99.4	0.982	1.00	98.5	91.7	96.9	0.913	0.99	
	avg	96.1	98.5	98.2	0.957	1.00	87.4	86.7	89.1	0.756	0.92	
ECFP 10000		Training Data					Test Data					
[10]	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	
	ADORA2A	97.6	91.7	95.5	0.901	0.99	96.4	91.9	94.8	0.885	0.98	
	hERG	95.4	42.9	74.3	0.470	0.84	94.9	39.7	73.5	0.433	0.81	
	AR	66.2	98.9	90.4	0.742	0.89	63.6	98.2	88.3	0.705	0.86	
	AChE	89.1	86.5	88.0	0.755	0.94	85.4	83.0	84.4	0.684	0.90	
	SERT	98.9	89.0	96.7	0.903	0.99	98.1	82.1	94.7	0.836	0.97	
[10,10]	avg	89.4	81.8	89.0	0.754	0.93	87.7	79.0	87.1	0.708	0.90	
[10,10]	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	
	ADORA2A	97.9	93.7	96.4	0.921	0.99	96.3	93.3	95.3	0.895	0.98	
	hERG	91.7	77.6	85.9	0.706	0.93	86.9	67.7	79.6	0.560	0.86	
	AR	63.7	99.3	89.8	0.732	0.89	59.8	99.2	88.9	0.703	0.85	
	AChE	89.8	87.6	88.9	0.773	0.95	87.0	82.5	85.1	0.694	0.92	
	SERT	98.9	83.3	95.5	0.865	0.98	98.8	80.3	94.7	0.842	0.98	
	avg	88.4	88.3	91.3	0.800	0.95	85.8	84.6	88.7	0.739	0.92	

		Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[10,10,10]	ADORA2A	99.9	99.4	99.8	0.995	1.00	96.9	92.6	95.4	0.898	0.99	
	hERG	99.3	99.5	99.4	0.987	1.00	83.2	72.0	78.7	0.554	0.85	
	AR	96.1	99.6	98.6	0.965	1.00	73.3	93.8	88.3	0.694	0.86	
	AChE	99.5	98.7	99.2	0.983	1.00	89.1	82.6	86.4	0.720	0.93	
	SERT	99.9	99.7	99.8	0.995	1.00	99.3	90.3	97.4	0.921	1.00	
	avg	98.9	99.4	99.3	0.985	1.00	88.4	86.2	89.2	0.757	0.93	
ECFP4 1000		Training Data						Test Data				
[10]	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	
	ADORA2A	98.1	89.7	95.2	0.893	0.98	96.6	88.5	93.8	0.863	0.97	
	hERG	91.3	58.1	78.2	0.538	0.86	89.0	54.7	74.9	0.474	0.83	
	AR	61.0	98.6	88.7	0.697	0.89	62.5	98.2	88.4	0.698	0.87	
	AChE	88.9	83.4	86.6	0.725	0.93	87.4	80.2	84.2	0.679	0.90	
	SERT	99.0	87.1	96.3	0.893	0.99	97.9	81.2	94.5	0.825	0.98	
[10,10]	avg	87.7	83.4	89.0	0.749	0.93	86.7	80.6	87.2	0.708	0.91	
	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	
	ADORA2A	98.2	90.1	95.4	0.898	0.99	97.4	90.0	94.8	0.885	0.98	
	hERG	86.8	70.5	80.3	0.584	0.88	81.8	62.9	74.2	0.457	0.82	
	AR	69.0	96.5	89.2	0.711	0.89	66.4	96.1	88.2	0.682	0.85	
[10,10]	AChE	88.9	85.8	87.6	0.747	0.94	89.3	79.6	85.0	0.695	0.91	

	SERT	98.5	91.4	96.9	0.911	0.99	98.2	84.7	95.4	0.855	0.98	
	avg	88.3	86.9	89.9	0.770	0.94	86.6	82.6	87.5	0.715	0.91	
[10,10,10]	Model	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	
	ADORA2A	99.8	99.1	99.6	0.989	1.00	97.6	89.8	95.7	0.881	0.98	
	hERG	94.1	85.0	90.5	0.801	0.96	83.9	68.5	77.9	0.532	0.84	
	AR	76.1	99.4	93.2	0.824	0.95	69.7	94.3	87.7	0.675	0.86	
	AChE	95.2	95.7	95.4	0.907	0.98	86.1	83.6	85.1	0.696	0.91	
	SERT	99.8	99.9	99.8	0.995	1.00	96.5	90.7	95.1	0.868	0.98	
ECFP4 5000	avg	93.0	95.8	95.7	0.903	0.98	86.8	85.4	88.3	0.730	0.91	
	<b>Training Data</b>						<b>Test Data</b>					
	Model	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	
	[10]	ADORA2A	97.9	93.3	96.3	0.917	0.99	96.1	90.7	94.2	0.872	0.98
		hERG	89.0	70.4	81.5	0.612	0.90	85.4	66.5	78.2	0.531	0.85
		AR	65.3	99.3	90.4	0.745	0.90	62.8	98.3	88.4	0.701	0.85
		AChE	88.5	88.9	88.7	0.771	0.94	86.8	82.5	84.9	0.693	0.91
[10,10]		SERT	98.8	87.9	96.5	0.894	0.99	98.4	84.9	95.4	0.864	0.98
		avg	87.9	88.0	90.7	0.788	0.94	85.9	84.6	88.2	0.732	0.91
	Model	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	
	ADORA2A	98.1	93.3	96.5	0.922	0.99	98.0	90.6	95.5	0.899	0.98	
	hERG	91.7	81.4	87.6	0.740	0.95	86.3	65.1	77.8	0.531	0.86	

	AR	62.6	99.4	89.6	0.727	0.90	61.0	98.8	88.8	0.703	0.87
	AChE	90.8	87.8	89.6	0.786	0.95	86.5	83.7	85.2	0.701	0.92
	SERT	99.1	91.8	97.5	0.926	0.99	97.9	86.9	95.4	0.867	0.99
	avg	88.5	90.8	92.2	0.820	0.96	85.9	85.0	88.6	0.740	0.92

	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[10,10,10]	ADORA2A	99.9	99.9	99.9	0.998	1.00	96.3	93.8	95.4	0.900	1.00
	hERG	99.5	99.3	99.4	0.987	1.00	81.6	69.0	76.7	0.508	0.83
	AR	95.3	99.8	98.6	0.965	1.00	72.3	92.2	86.8	0.659	0.85
	AChE	99.7	99.1	99.4	0.989	1.00	85.8	80.2	83.3	0.661	0.91
	SERT	99.9	99.7	99.8	0.996	1.00	98.2	89.1	96.3	0.888	0.99
	avg	98.9	99.5	99.4	0.987	1.00	86.8	84.9	87.7	0.723	0.92

ECFP4 10000											
		Training Data					Test Data				
	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[10]	ADORA2A	97.6	93.0	96.0	0.911	0.99	97.2	91.2	95.3	0.892	0.98
	hERG	91.5	65.2	81.2	0.600	0.89	91.5	65.2	81.2	0.600	0.83
	AR	66.7	98.8	90.4	0.744	0.89	62.1	97.7	87.9	0.685	0.88
	AChE	88.1	87.6	87.9	0.754	0.94	86.2	89.4	87.6	0.751	0.93
	SERT	98.7	91.3	97.0	0.915	0.99	98.6	85.7	96.1	0.871	0.98
	avg	88.5	87.2	90.5	0.785	0.94	87.1	85.9	89.6	0.760	0.92

[10,10]	Model	ADORA2A	97.7	94.1	96.4	0.922	0.99	97.4	93.2	96.0	0.908	0.99	
		hERG	91.0	73.7	84.0	0.665	0.92	87.8	68.3	80.3	0.578	0.88	
[10,10,10]		AR	67.6	99.0	90.8	0.754	0.90	65.0	98.5	89.0	0.723	0.87	
		AChE	91.7	91.0	91.4	0.825	0.97	83.5	84.3	83.8	0.674	0.90	
		SERT	98.9	89.0	96.7	0.904	0.99	98.3	83.4	95.1	0.852	0.97	
		avg	89.4	89.4	91.9	0.814	0.95	86.4	85.5	88.9	0.747	0.92	
		Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	
		ADORA2A	99.9	99.9	99.9	0.998	1.00	95.7	92.0	94.4	0.877	0.98	
ECFP4 20000	Model	hERG	99.3	99.1	99.3	0.985	1.00	82.7	74.6	79.5	0.571	0.86	
		AR	97.0	99.6	98.9	0.972	1.00	74.4	92.7	88.1	0.680	0.87	
		AChE	99.6	99.4	99.5	0.990	1.00	87.8	85.4	86.8	0.731	0.91	
		SERT	99.9	99.9	99.9	0.997	1.00	98.2	91.3	96.7	0.903	0.99	
		avg	99.1	99.6	99.5	0.988	1.00	87.8	87.2	89.1	0.752	0.92	
		Training Data	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	
[10]	Model	ADORA2A	97.9	92.1	95.9	0.909	0.99	98.1	88.6	94.8	0.884	0.99	
		hERG	91.5	66.7	81.6	0.612	0.89	89.7	60.7	78.0	0.536	0.85	
		AR	66.8	98.9	90.2	0.746	0.89	61.7	98.9	89.6	0.712	0.86	
		AChE	91.4	85.8	89.0	0.775	0.95	83.1	79.7	81.7	0.626	0.88	
		SERT	98.7	91.5	97.2	0.915	0.99	98.7	84.9	95.5	0.871	0.98	
		avg	89.3	87.0	90.8	0.791	0.94	86.3	82.6	87.9	0.726	0.91	

	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[10,10]	ADORA2A	97.9	93.8	96.5	0.922	0.99	97.4	90.2	94.8	0.887	0.98
	hERG	93.2	55.4	78.3	0.542	0.88	92.7	49.4	74.7	0.480	0.84
	AR	66.1	99.0	90.3	0.745	0.89	65.8	98.6	89.7	0.732	0.86
	AChE	89.9	91.7	90.7	0.812	0.96	84.9	87.6	86.1	0.721	0.92
	SERT	99.0	92.2	97.5	0.926	0.99	97.8	85.1	94.8	0.853	0.97
	avg	89.2	86.4	90.7	0.789	0.94	87.7	82.2	88.0	0.735	0.91
[10,10,10]	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
	ADORA2A	99.7	99.9	99.8	0.995	1.00	97.3	93.0	95.8	0.907	0.99
	hERG	99.4	99.5	99.4	0.988	1.00	80.8	75.3	78.6	0.557	0.86
	AR	94.1	99.7	98.3	0.955	1.00	68.7	97.0	89.4	0.719	0.86
	AChE	98.9	99.6	99.2	0.983	1.00	86.7	91.1	88.5	0.768	0.93
	SERT	99.9	99.8	99.9	0.996	1.00	98.5	90.7	96.8	0.906	0.99
	avg	98.4	99.7	99.3	0.984	1.00	86.4	89.4	89.8	0.771	0.93

Table S2. Results comparing the model performance of several chemical fingerprints across three network architectures and five biological targets (adenosine A2a receptor = ADORA2A, human ether a go-go related gene channel = hERG, androgen receptor = AR, acetylcholinesterase AChE, serotonin transporter (SERT)). Model performances are reported as sensitivity (SE), specificity (SP), accuracy (ACC), Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC).

[10]	Training					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>Sigmoid</b>	88.5	87.2	90.5	0.785	0.94	87.1	85.9	89.6	0.760	0.92
<b>ReLU</b>	92.6	94.7	95.0	0.887	0.98	87.2	88.2	89.9	0.773	0.93
[10,10]	Training					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>Sigmoid, Sigmoid</b>	89.4	89.4	91.9	0.814	0.95	86.4	85.5	88.9	0.747	0.92
<b>Sigmoid, ReLU</b>	90.7	88.6	92.1	0.822	0.96	88.6	83.3	89.1	0.753	0.93
<b>ReLU, Sigmoid</b>	89.2	88.7	91.8	0.811	0.96	86.8	83.0	88.3	0.733	0.92
<b>ReLU, ReLU</b>	96.0	92.6	95.6	0.903	0.99	90.2	84.0	90.0	0.770	0.93

Table S3. A summary of the results shown in Table S4 comparing the model performance sigmoid and ReLU activation functions across two network architectures and five biological targets. Highest accuracy (ACC) Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC) values are highlighted in red. ReLU was chosen as the best performing activation function in both single and double-layer cases.

[10] ECFP4 10000

Training Data												Test Data			
	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC				
<b>Sigmoid</b>	ADORA2A	97.6	93.0	96.0	0.911	0.99	97.2	91.2	95.3	0.892	0.98				
	hERG	91.5	65.2	81.2	0.600	0.89	91.5	65.2	81.2	0.600	0.83				
	AR	66.7	98.8	90.4	0.744	0.89	62.1	97.7	87.9	0.685	0.88				
	AChE	88.1	87.6	87.9	0.754	0.94	86.2	89.4	87.6	0.751	0.93				
	SERT	98.7	91.3	97.0	0.915	0.99	98.6	85.7	96.1	0.871	0.98				
	avg	88.5	87.2	90.5	0.785	0.94	87.1	85.9	89.6	0.760	0.92				
<b>ReLU</b>	Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC				
	ADORA2A	98.5	96.9	98.0	0.955	1.00	97.1	92.9	95.6	0.904	0.98				
	hERG	95.0	84.9	91.0	0.811	0.97	84.9	71.0	79.3	0.567	0.87				
	AR	77.7	99.2	93.5	0.830	0.96	68.4	97.6	89.9	0.730	0.87				
	AChE	92.4	95.4	93.7	0.873	0.98	87.3	90.2	88.6	0.770	0.93				
	SERT	99.2	97.3	98.8	0.966	1.00	98.3	89.2	96.4	0.891	0.99				
	avg	92.6	94.7	95.0	0.887	0.98	87.2	88.2	89.9	0.773	0.93				

**[10,10] ECFP4 10000**

		Training Data					Test Data					
		Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>Sigmoid,Sigmoid</b>	ADORA2A	97.7	94.1	96.4	0.922	0.99	97.4	93.2	96.0	0.908	0.99	
	hERG	91.0	73.7	84.0	0.665	0.92	87.8	68.3	80.3	0.578	0.88	
	AR	67.6	99.0	90.8	0.754	0.90	65.0	98.5	89.0	0.723	0.87	
	AChE	91.7	91.0	91.4	0.825	0.97	83.5	84.3	83.8	0.674	0.90	
	SERT	98.9	89.0	96.7	0.904	0.99	98.3	83.4	95.1	0.852	0.97	
	avg	89.4	89.4	91.9	0.814	0.95	86.4	85.5	88.9	0.747	0.92	
		Model	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>Sigmoid,ReLU</b>	ADORA2A	98.0	92.7	96.1	0.915	0.99	97.1	92.0	95.4	0.896	0.98	
	hERG	94.6	65.5	83.0	0.646	0.92	92.1	55.2	77.2	0.522	0.86	
	AR	68.8	99.1	91.0	0.765	0.92	66.6	98.3	90.1	0.731	0.92	
	AChE	93.2	92.3	92.8	0.854	0.98	88.5	84.3	86.7	0.727	0.92	
	SERT	98.9	93.3	97.7	0.931	1.00	98.9	86.5	95.9	0.886	0.98	
	avg	90.7	88.6	92.1	0.822	0.96	88.6	83.3	89.1	0.753	0.93	

	<b>Model</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>
<b>ReLU,Sigmoid</b>	ADORA2A	97.6	93.4	96.2	0.915	0.99	97.9	89.1	94.9	0.886	0.98
	hERG	93.3	76.3	86.5	0.717	0.94	87.5	61.9	77.2	0.518	0.86
	AR	65.2	99.2	90.1	0.741	0.90	64.0	98.3	89.3	0.713	0.88
	AChE	91.1	89.4	90.4	0.803	0.96	86.2	85.7	85.9	0.715	0.92
	SERT	98.9	85.3	96.0	0.879	0.99	98.5	80.1	94.4	0.834	0.97
	avg	89.2	88.7	91.8	0.811	0.96	86.8	83.0	88.3	0.733	0.92
<b>ReLU, ReLU</b>	<b>Model</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>
	ADORA2A	99.2	98.2	98.8	0.974	1.00	97.3	92.5	95.7	0.903	0.99
	hERG	96.1	70.2	85.7	0.706	0.94	90.5	58.4	77.9	0.528	0.86
	AR	87.3	99.7	96.4	0.907	0.99	72.8	97.5	90.9	0.759	0.87
	AChE	97.9	98.1	98.0	0.959	1.00	91.8	86.6	89.6	0.786	0.94
	SERT	99.5	97.1	99.0	0.970	1.00	98.7	85.0	95.8	0.872	0.98
	avg	96.0	92.6	95.6	0.903	0.99	90.2	84.0	90.0	0.770	0.93

Table S4. Results comparing the model performance of Sigmoid and ReLU activation function across two network architectures and five biological targets (adenosine A2a receptor = ADORA2A, human ether a go-go related gene channel = hERG, androgen receptor = AR, acetylcholinesterase AChE, serotonin transporter (SERT). Model performances are reported as sensitivity (SE), specificity (SP), accuracy (ACC), Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC).

**AChE**

	Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC
[10]	1	Train 1	1442	178	947	179	89.0	84.1	87.0	0.731	0.93
	2	Train 2	1313	214	1062	156	86.0	87.2	86.5	0.729	0.93
	3	Train 3	1397	177	964	207	88.8	82.3	86.0	0.713	0.93
	4	Train 4	1394	159	973	219	89.8	81.6	86.2	0.719	0.92
	5	Train 5	1422	164	974	185	89.7	84.0	87.3	0.739	0.93
		Avg	1394	178	984	189	88.7	83.9	86.6	0.726	0.93
		SD	49	22	45	25	1.5	2.2	0.5	0.010	0.00
	Validation	Validation 1	416	80	325	94	83.9	77.6	81.0	0.616	0.90
		Validation 2	434	76	334	71	85.1	82.5	83.9	0.675	0.91
		Validation 3	456	76	323	60	85.7	84.3	85.1	0.697	0.91
		Validation 4	456	73	296	90	86.2	76.7	82.2	0.633	0.89
		Validation 5	434	87	326	68	83.3	82.7	83.1	0.657	0.89
		Avg	439.2	78.4	320.8	76.6	84.9	80.7	83.1	0.655	0.90
		SD	17	5	14	15	1.2	3.4	1.6	0.032	0.01
Test	Test 1	416	80	325	94	83.9	77.6	81.0	0.616	0.88	
	Test 2	468	107	287	53	81.4	84.4	82.5	0.642	0.90	
	Test 3	436	70	320	89	86.2	78.2	82.6	0.648	0.89	
	Test 4	461	69	288	97	87.0	74.8	81.9	0.625	0.89	
	Test 5	419	86	328	82	83.0	80.0	81.6	0.629	0.89	

			Avg	440.0	82.4	309.6	83.0	84.2	78.9	81.9	0.631	0.89
			SD	24	15	20	18	2.3	3.6	0.7	0.013	0.01
		Model Number		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>
[100]	6	Train 1	1411	158	1064	112	89.9	90.5	90.2	0.801	0.96	
	7	Train 2	1396	142	1047	160	90.8	86.7	89.0	0.776	0.95	
	8	Train 3	1419	141	1054	131	91.0	88.9	90.1	0.798	0.96	
	9	Train 4	1429	125	1013	178	92.0	85.1	89.0	0.775	0.95	
	10	Train 5	1437	157	1047	104	90.2	91.0	90.5	0.807	0.96	
		Avg	1418	145	1045	137	90.7	88.4	89.7	0.791	0.96	
		SD	16	14	19	31	0.8	2.5	0.7	0.015	0.01	
		Validation 1	473	74	313	55	86.5	85.1	85.9	0.710	0.92	
		Validation 2	436	63	340	76	87.4	81.7	84.8	0.693	0.91	
		Validation 3	494	52	306	63	90.5	82.9	87.4	0.738	0.93	
		Validation 4	464	64	310	77	87.9	80.1	84.6	0.683	0.91	
		Validation 5	435	78	347	55	84.8	86.3	85.5	0.708	0.91	
		Avg	460.4	66.2	323.2	65.2	87.4	83.2	85.6	0.706	0.92	
		SD	25	10	19	11	2.1	2.5	1.1	0.021	0.01	
		Test 1	413	83	347	72	83.3	82.8	83.1	0.660	0.89	
		Test 2	501	74	277	63	87.1	81.5	85.0	0.682	0.91	
		Test 3	442	64	329	80	87.4	80.4	84.3	0.681	0.91	

			Test 4	478	52	283	102	90.2	73.5	83.2	0.653	0.90
			Test 5	418	87	348	62	82.8	84.9	83.7	0.674	0.91
			Avg	450.4	72.0	316.8	75.8	86.2	80.7	83.8	0.670	0.90
			SD	38	14	34	16	3.1	4.3	0.8	0.013	0.01
[1000]	Model Number	TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC		
		1424	169	942	210	89.4	81.8	86.2	0.715	0.92		
		1292	216	1061	176	85.7	85.8	85.7	0.713	0.93		
		1388	203	979	175	87.2	84.8	86.2	0.719	0.93		
		1388	177	987	193	88.7	83.6	86.5	0.725	0.93		
		1405	172	961	207	89.1	82.3	86.2	0.717	0.93		
		Avg	1379	187	986	192	88.0	83.7	86.2	0.718	0.93	
	Validation	51	21	45	17	1.5	1.7	0.3	0.004	0.00		
		Validation 1	461	62	292	100	88.1	74.5	82.3	0.636	0.89	
		Validation 2	434	95	316	70	82.0	81.9	82.0	0.635	0.89	
	Test	Validation 3	447	68	305	95	86.8	76.3	82.2	0.636	0.90	
		Validation 4	439	78	319	79	84.9	80.2	82.8	0.651	0.89	
		Validation 5	453	77	297	88	85.5	77.1	82.0	0.629	0.89	
		Avg	446.8	76.0	305.8	86.4	85.5	78.0	82.3	0.637	0.89	
		SD	11	13	12	12	2.3	3.0	0.4	0.008	0.00	
	Test	Test 1	418	78	319	100	84.3	76.1	80.5	0.607	0.87	

	Test 2	468	107	285	55	81.4	83.8	82.3	0.637	0.89
	Test 3	434	72	323	86	85.8	79.0	82.7	0.650	0.89
	Test 4	461	69	294	91	87.0	76.4	82.5	0.639	0.89
	Test 5	424	81	325	85	84.0	79.3	81.9	0.633	0.88
	Avg	441.0	81.4	309.2	83.4	84.4	78.8	82.0	0.632	0.88
	SD	22	15	18	17	2.1	3.1	0.9	0.016	0.01

Model Number			TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC
[10,10]	16	Train 1	1424	140	1073	108	91.0	90.9	91.0	0.817	0.96
	17	Train 2	1364	169	1097	115	89.0	90.5	89.7	0.792	0.95
	18	Train 3	1463	148	996	138	90.8	87.8	89.6	0.785	0.96
	19	Train 4	1429	125	1066	125	92.0	89.5	90.9	0.815	0.96
	20	Train 5	1420	145	1058	122	90.7	89.7	90.3	0.802	0.96
		Avg	1420	145	1058	122	90.7	89.7	90.3	0.802	0.96
		SD	36	16	38	11	1.1	1.2	0.7	0.014	0.00
		Validation 1	472	80	310	53	85.5	85.4	85.5	0.701	0.92
		Validation 2	424	80	346	65	84.1	84.2	84.2	0.681	0.91
		Validation 3	430	65	338	82	86.9	80.5	83.9	0.676	0.91
		Validation 4	461	67	308	79	87.3	79.6	84.0	0.672	0.91
		Validation 5	469	73	318	55	86.5	85.3	86.0	0.713	0.93
		Avg	451.2	73.0	324.0	66.8	86.1	82.9	84.7	0.688	0.92
		SD	23	7	17	13	1.3	2.8	1.0	0.018	0.01

		Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC
[100,100]	<b>21</b>	Train 1	1487	113	1037	108	92.9	90.6	91.9	0.835	0.97	
	<b>22</b>	Train 2	1389	122	1110	124	91.9	90.0	91.0	0.819	0.97	
	<b>23</b>	Train 3	1444	126	1074	101	92.0	91.4	91.7	0.832	0.97	
	<b>24</b>	Train 4	1466	108	1060	111	93.1	90.5	92.0	0.837	0.97	
	<b>25</b>	Train 5	1377	194	1106	68	87.7	94.2	90.5	0.811	0.97	
		Avg	1433	133	1077	102	91.5	91.3	91.4	0.827	0.97	
		SD	48	35	31	21	2.2	1.7	0.7	0.011	0.00	
	</											

			Avg	457	67	333	58	87.2	85.3	86.3	0.722	0.92
			SD	11	13	7	14	2.3	3.2	1.3	0.027	0.01
			Test 1	425	71	343	76	85.7	81.9	83.9	0.676	0.90
			Test 2	508	67	284	56	88.3	83.5	86.6	0.714	0.92
			Test 3	430	76	351	58	85.0	85.8	85.4	0.706	0.91
			Test 4	471	59	302	83	88.9	78.4	84.5	0.680	0.91
			Test 5	386	119	373	37	76.4	91.0	83.0	0.672	0.91
			Avg	444	78	331	62	84.9	84.1	84.7	0.690	0.91
			SD	47	24	37	18	5.0	4.7	1.4	0.019	0.01
		Model Number		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>
[1000,1000]	<b>26</b>	Train 1	1452	139	1086	68	91.3	94.1	92.5	0.848	0.98	
	<b>27</b>	Train 2	1444	61	1210	30	95.9	97.6	96.7	0.933	0.99	
	<b>28</b>	Train 3	1528	30	1123	64	98.1	94.6	96.6	0.930	0.99	
	<b>29</b>	Train 4	1475	75	1173	22	95.2	98.2	96.5	0.929	0.99	
	<b>30</b>	Train 5	1526	66	1133	20	95.9	98.3	96.9	0.937	0.99	
		Avg	1485	74	1145	41	95.3	96.5	95.8	0.915	0.99	
		SD	40	40	48	23	2.5	2.0	1.9	0.038	0.00	
			Validation 1	446	79	341	49	85.0	87.4	86.0	0.718	0.92
			Validation 2	480	52	339	44	90.2	88.5	89.5	0.785	0.94
			Validation 3	507	41	295	72	92.5	80.4	87.7	0.741	0.95

Validation 4	448	84	331	52	84.2	86.4	85.1	0.700	0.91
Validation 5	452	63	361	39	87.8	90.3	88.9	0.776	0.94
Avg	467	64	333	51	87.9	86.6	87.4	0.744	0.93
SD	26	18	24	13	3.5	3.8	1.8	0.037	0.02
Test 1	402	94	365	54	81.0	87.1	83.8	0.679	0.91
Test 2	499	76	293	47	86.8	86.2	86.6	0.719	0.93
Test 3	455	51	301	108	89.9	73.6	82.6	0.649	0.91
Test 4	445	85	324	61	84.0	84.2	84.0	0.676	0.91
Test 5	411	94	366	44	81.4	89.3	84.9	0.703	0.92
Avg	442	80	330	63	84.6	84.1	84.4	0.685	0.92
SD	39	18	35	26	3.8	6.1	1.5	0.027	0.01

Table S5. Results comparing model performance for various network architectures at the AChE. Model performances are reported as sensitivity (SE), specificity (SP), accuracy (ACC), Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC). Averages (Avg) and standard deviations (SD) are shown.

## ADORA2A

	Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC
[10]	1	Train 1	2309	57	1141	108	97.6	91.4	95.4	0.899	0.99
	2	Train 2	2279	60	1156	120	97.4	90.6	95.0	0.890	0.98
	3	Train 3	2376	51	1047	141	97.9	88.1	94.7	0.879	0.98
	4	Train 4	2303	65	1113	134	97.3	89.3	94.5	0.877	0.98
	5	Train 5	2316	48	1124	127	98.0	89.8	95.2	0.893	0.98
		Avg	2317	56	1116	126	97.6	89.9	95.0	0.888	0.98
		SD	36	7	42	13	0.3	1.2	0.4	0.009	0.00
		Validation 1	742	18	399	46	97.6	89.7	94.7	0.886	0.98
		Validation 2	744	27	390	44	96.5	89.9	94.1	0.871	0.98
		Validation 3	795	26	350	34	96.8	91.1	95.0	0.885	0.98
Test		Validation 4	759	14	384	48	98.2	88.9	94.9	0.888	0.98
		Validation 5	758	25	387	35	96.8	91.7	95.0	0.890	0.98
		Avg	759.6	22.0	382.0	41.4	97.2	90.2	94.7	0.884	0.98
		SD	21	6	19	6	0.7	1.1	0.4	0.007	0.00
		Test 1	798	19	342	46	97.7	88.1	94.6	0.875	0.98
		Test 2	816	17	328	44	98.0	88.2	94.9	0.880	0.97
		Test 3	671	24	462	48	96.5	90.6	94.0	0.878	0.97
ROC-AUC		Test 4	778	24	360	43	97.0	89.3	94.4	0.874	0.97
		Test 5	769	27	351	58	96.6	85.8	92.9	0.841	0.96

		Avg	766.4	22.2	368.6	47.8	97.2	88.5	94.2	0.871	0.97
		SD	56	4	54	6	0.6	1.8	0.8	0.016	0.01
		Model Number		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
[100]	<b>6</b>	Train 1	2327	52	1150	86	97.8	93.0	96.2	0.915	0.99
	<b>7</b>	Train 2	2287	56	1185	87	97.6	93.2	96.0	0.913	0.99
	<b>8</b>	Train 3	2391	45	1070	109	98.2	90.8	95.7	0.902	0.99
	<b>9</b>	Train 4	2309	59	1175	72	97.5	94.2	96.4	0.920	0.99
	<b>10</b>	Train 5	2301	50	1177	87	97.9	93.1	96.2	0.916	0.99
		Avg	2323	52	1151	88	97.8	92.9	96.1	0.913	0.99
		SD	41	5	47	13	0.3	1.3	0.2	0.007	0.00
		Validation 1	721	26	425	33	96.5	92.8	95.1	0.896	0.98
		Validation 2	747	20	386	52	97.4	88.1	94.0	0.870	0.98
		Validation 3	788	24	360	33	97.0	91.6	95.3	0.892	0.99
		Validation 4	747	26	392	40	96.6	90.7	94.5	0.880	0.98
		Validation 5	773	23	337	32	97.1	91.3	95.3	0.890	0.98
		Avg	755.2	23.8	380.0	38.0	96.9	90.9	94.8	0.886	0.98
		SD	26	2	33	8	0.4	1.7	0.6	0.010	0.00
		Test 1	793	24	349	39	97.1	89.9	94.8	0.879	0.98
		Test 2	824	9	332	40	98.9	89.2	95.9	0.904	0.97
		Test 3	675	20	465	45	97.1	91.2	94.6	0.890	0.98

			Test 4	773	29	372	31	96.4	92.3	95.0	0.888	0.98
			Test 5	768	28	361	48	96.5	88.3	93.7	0.858	0.97
			Avg	766.6	22.0	375.8	40.6	97.2	90.2	94.8	0.884	0.98
			SD	56	8	52	7	1.0	1.6	0.8	0.017	0.01
[1000]	Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC	
		11	Train 1	2284	55	1158	118	97.6	90.8	95.2	0.895	0.98
		12	Train 2	2274	69	1165	107	97.1	91.6	95.1	0.893	0.98
		13	Train 3	2389	52	1030	144	97.9	87.7	94.6	0.875	0.98
		14	Train 4	2295	54	1151	115	97.7	90.9	95.3	0.897	0.98
		15	Train 5	2282	64	1173	96	97.3	92.4	95.6	0.902	0.99
			Avg	2305	59	1135	116	97.5	90.7	95.2	0.893	0.98
			SD	48	7	59	18	0.3	1.8	0.4	0.010	0.00
	Validation		Validation 1	764	23	364	54	97.1	87.1	93.6	0.858	0.97
			Validation 2	743	24	397	41	96.9	90.6	94.6	0.883	0.98
			Validation 3	795	12	351	47	98.5	88.2	95.1	0.889	0.98
			Validation 4	766	26	372	41	96.7	90.1	94.4	0.876	0.97
			Validation 5	776	25	369	35	96.9	91.3	95.0	0.888	0.98
			Avg	768.8	22.0	370.6	43.6	97.2	89.5	94.6	0.879	0.98
			SD	19	6	17	7	0.7	1.8	0.6	0.013	0.01
Test	1		Test 1	798	19	340	48	97.7	87.6	94.4	0.871	0.98

			Test 1	815	18	333	39	97.8	89.5	95.3	0.888	0.97
			Test 2	815	18	333	39	97.8	89.5	95.3	0.888	0.97
			Test 3	673	22	453	57	96.8	88.8	93.4	0.866	0.97
			Test 4	771	31	370	33	96.1	91.8	94.7	0.881	0.98
			Test 5	766	30	360	49	96.2	88.0	93.4	0.853	0.96
			Avg	764.6	24.0	371.2	45.2	97.0	89.1	94.3	0.872	0.97
			SD	55	6	48	9	0.8	1.7	0.8	0.014	0.01
Model Number			TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC	
[10,10]	16	Train 1	2270	59	1166	120	97.5	90.7	95.0	0.891	0.99	
	17	Train 2	2268	54	1217	76	97.7	94.1	96.4	0.922	0.99	
	18	Train 3	2376	49	1084	106	98.0	91.1	95.7	0.902	0.99	
	19	Train 4	2290	45	1194	86	98.1	93.3	96.4	0.920	0.99	
	20	Train 5	2314	57	1170	74	97.6	94.1	96.4	0.920	0.99	
		Avg	2304	53	1166	92	97.8	92.7	96.0	0.911	0.99	
		SD	45	6	50	20	0.3	1.6	0.6	0.014	0.00	
Validation			Validation 1	784	13	373	35	98.4	91.4	96.0	0.911	0.98
			Validation 2	766	22	369	48	97.2	88.5	94.2	0.871	0.97
			Validation 3	808	15	341	41	98.2	89.3	95.4	0.892	0.98
			Validation 4	782	24	361	38	97.0	90.5	94.9	0.883	0.98
			Validation 5	755	21	400	29	97.3	93.2	95.9	0.909	0.98
			Avg	779.0	19.0	368.8	38.2	97.6	90.6	95.3	0.893	0.98
			SD	20	5	21	7	0.6	1.9	0.7	0.017	0.00

			Test 1	797	20	343	45	97.6	88.4	94.6	0.875	0.98
			Test 2	819	14	334	38	98.3	89.8	95.7	0.898	0.97
			Test 3	672	23	466	44	96.7	91.4	94.4	0.886	0.98
			Test 4	776	26	371	32	96.8	92.1	95.2	0.892	0.98
			Test 5	762	34	360	49	95.7	88.0	93.1	0.845	0.97
			Avg	765.2	23.4	374.8	41.6	97.0	90.0	94.6	0.880	0.98
			SD	56	7	53	7	1.0	1.8	1.0	0.021	0.01
		Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC
[100,100]	<b>21</b>	Train 1	2296	39	1196	84	98.3	93.4	96.6	0.925	0.99	
	<b>22</b>	Train 2	2295	29	1164	127	98.8	90.2	95.7	0.906	0.99	
	<b>23</b>	Train 3	2388	58	1108	61	97.6	94.8	96.7	0.925	0.99	
	<b>24</b>	Train 4	2307	45	1185	78	98.1	93.8	96.6	0.925	0.99	
	<b>25</b>	Train 5	2290	56	1224	45	97.6	96.5	97.2	0.939	0.99	
		Avg	2315	45	1175	79	98.1	93.7	96.6	0.924	0.99	
		SD	41	12	43	31	0.5	2.3	0.5	0.012	0.00	
			Validation 1	769	22	364	50	97.2	87.9	94.0	0.867	0.98
			Validation 2	767	19	378	41	97.6	90.2	95.0	0.890	0.98
			Validation 3	775	27	373	30	96.6	92.6	95.3	0.894	0.98
			Validation 4	761	28	379	37	96.5	91.1	94.6	0.880	0.98
			Validation 5	770	31	373	31	96.1	92.3	94.9	0.885	0.98

			Avg	768	25	373	38	96.8	90.8	94.8	0.883	0.98	
			SD	5	5	6	8	0.6	1.9	0.5	0.010	0.00	
			Test 1	800	17	349	39	97.9	89.9	95.4	0.893	0.98	
			Test 2	823	10	318	54	98.8	85.5	94.7	0.875	0.98	
			Test 3	670	25	476	34	96.4	93.3	95.1	0.900	0.98	
			Test 4	774	28	373	30	96.5	92.6	95.2	0.892	0.98	
			Test 5	752	44	368	41	94.5	90.0	92.9	0.843	0.98	
			Avg	764	25	377	40	96.8	90.3	94.7	0.880	0.98	
			SD	59	13	60	9	1.7	3.1	1.0	0.023	0.00	
			Model Number		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>
<b>[1000,1000]</b>	<b>26</b>		Train 1	2318	23	47	1227	99.0	3.7	65.4	0.094	1.00	
	<b>27</b>		Train 2	2292	31	1256	36	98.7	97.2	98.1	0.960	1.00	
	<b>28</b>		Train 3	2412	18	1120	65	99.3	94.5	97.7	0.948	1.00	
	<b>29</b>		Train 4	2337	23	1223	32	99.0	97.5	98.5	0.966	1.00	
	<b>30</b>		Train 5	2348	25	1215	27	98.9	97.8	98.6	0.968	1.00	
			Avg	2341	24	972	277	99.0	78.1	91.7	0.787	1.00	
			SD	45	5	520	531	0.2	41.6	14.7	0.388	0.00	
			Validation 1	737	24	410	34	96.8	92.3	95.2	0.896	0.99	
			Validation 2	765	22	393	25	97.2	94.0	96.1	0.914	0.99	
			Validation 3	800	18	353	34	97.8	91.2	95.7	0.900	0.98	

Validation 4	762	19	383	41	97.6	90.3	95.0	0.890	0.98
Validation 5	752	22	405	26	97.2	94.0	96.0	0.913	0.98
Avg	763	21	389	32	97.3	92.4	95.6	0.903	0.98
SD	23	2	23	7	0.4	1.6	0.5	0.010	0.01
Test 1	773	44	364	24	94.6	93.8	94.4	0.873	0.99
Test 2	817	16	337	35	98.1	90.6	95.8	0.900	0.98
Test 3	674	21	462	48	97.0	90.6	94.3	0.883	0.98
Test 4	780	22	373	30	97.3	92.6	95.7	0.903	0.98
Test 5	767	29	363	46	96.4	88.8	93.8	0.860	0.98
Avg	762	26	380	37	96.7	91.3	94.8	0.884	0.98
SD	53	11	48	10	1.3	2.0	0.9	0.018	0.00

Table S6. Results comparing model performance for various network architectures at the ADORA2A. Model performances are reported as sensitivity (SE), specificity (SP), accuracy (ACC), Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC). Averages (Avg) and standard deviations (SD) are shown.

**AR**

	Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC
[10]	1	Train 1	908	654	4358	32	58.1	99.3	88.5	0.693	0.88
	2	Train 2	884	664	4372	32	57.1	99.3	88.3	0.685	0.88
	3	Train 3	932	699	4285	36	57.1	99.2	87.7	0.681	0.88
	4	Train 4	931	634	4358	29	59.5	99.3	88.9	0.704	0.88
	5	Train 5	938	669	4312	33	58.4	99.2	88.2	0.692	0.88
		Avg	919	664	4337	32	58.0	99.3	88.3	0.691	0.88
		SD	22	24	37	3	1.0	0.1	0.4	0.009	0.00
		Validation 1	304	231	1436	13	56.8	99.1	87.7	0.677	0.86
		Validation 2	327	224	1418	15	59.3	99.0	88.0	0.691	0.87
		Validation 3	342	192	1433	17	64.0	98.8	89.5	0.724	0.87
[11]		Validation 4	273	230	1466	15	54.3	99.0	87.7	0.658	0.88
		Validation 5	311	201	1454	18	60.7	98.8	89.0	0.700	0.87
		Avg	311.4	215.6	1441.4	15.6	59.1	98.9	88.3	0.691	0.87
		SD	26	18	19	2	3.7	0.1	0.8	0.025	0.01
		Test 1	297	243	1432	12	55.0	99.2	87.1	0.665	0.85
		Test 2	298	240	1432	14	55.4	99.0	87.2	0.665	0.85
		Test 3	272	200	1496	16	57.6	98.9	89.1	0.684	0.86
		Test 4	300	269	1399	16	52.7	98.9	85.6	0.638	0.84

		Test 5	305	213	1449	17	58.9	98.8	88.4	0.688	0.88
[100]	Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC
	6	Train 1	1046	493	4365	48	68.0	98.9	90.9	0.756	0.91
[100]	7	Train 2	1172	421	4263	96	73.6	97.8	91.3	0.772	0.91
	8	Train 3	1100	484	4321	47	69.4	98.9	91.1	0.766	0.90
	9	Train 4	996	540	4386	30	64.8	99.3	90.4	0.743	0.91
	10	Train 5	1094	480	4318	60	69.5	98.6	90.9	0.760	0.90
		Avg	1082	484	4331	56	69.1	98.7	90.9	0.759	0.91
		SD	66	42	48	25	3.1	0.6	0.3	0.011	0.01
		Validation 1	344	214	1408	18	61.6	98.7	88.3	0.703	0.85
[100]		Validation 2	344	162	1442	36	68.0	97.6	90.0	0.726	0.85
		Validation 3	393	188	1372	31	67.6	97.8	89.0	0.726	0.88
		Validation 4	248	184	1430	22	57.4	98.5	89.1	0.671	0.87
		Validation 5	360	185	1408	31	66.1	97.8	89.1	0.717	0.88
		Avg	337.8	186.6	1412.0	27.6	64.4	98.1	89.1	0.711	0.87
		SD	54	18	27	7	4.5	0.5	0.6	0.023	0.02
		Test 1	333	207	1427	17	61.7	98.8	88.7	0.706	0.85
		Test 2	376	162	1408	38	69.9	97.4	89.9	0.736	0.86

	Test 3	309	163	1486	26	65.5	98.3	90.5	0.725	0.87
	Test 4	333	236	1397	18	58.5	98.7	87.2	0.679	0.85
	Test 5	351	167	1438	28	67.8	98.1	90.2	0.736	0.88
	Avg	340.4	187.0	1431.2	25.4	64.5	98.3	89.3	0.715	0.86
	SD	25	33	35	9	4.6	0.6	1.3	0.024	0.01

Model Number			<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>
<b>[1000]</b>	<b>11</b>	Train 1	1027	531	4332	62	65.9	98.6	90.0	0.733	0.89
	<b>12</b>	Train 2	1038	555	4298	61	65.2	98.6	89.7	0.728	0.89
	<b>13</b>	Train 3	1032	578	4280	62	64.1	98.6	89.2	0.719	0.89
	<b>14</b>	Train 4	1063	502	4319	68	67.9	98.4	90.4	0.745	0.89
	<b>15</b>	Train 5	983	601	4322	46	62.1	98.9	89.1	0.713	0.89
		Avg	1029	553	4310	60	65.0	98.6	89.7	0.727	0.89
		SD	29	39	21	8	2.2	0.2	0.5	0.012	0.00
		Validation 1	336	203	1412	33	62.3	97.7	88.1	0.687	0.86
		Validation 2	323	183	1447	31	63.8	97.9	89.2	0.703	0.87
		Validation 3	334	221	1408	21	60.2	98.5	87.8	0.688	0.87
		Validation 4	317	186	1454	27	63.0	98.2	89.3	0.703	0.86
		Validation 5	316	219	1432	17	59.1	98.8	88.1	0.687	0.85
		Avg	325.2	202.4	1430.6	25.8	61.6	98.2	88.5	0.693	0.86
		SD	9	18	20	7	2.0	0.5	0.7	0.009	0.01

	Test 1	329	211	1422	22	60.9	98.5	88.3	0.693	0.86
	Test 2	342	196	1418	28	63.6	98.1	88.7	0.703	0.86
	Test 3	284	188	1487	25	60.2	98.3	89.3	0.687	0.87
	Test 4	347	222	1388	27	61.0	98.1	87.4	0.683	0.84
	Test 5	321	197	1447	19	62.0	98.7	89.1	0.707	0.88
	Avg	324.6	202.8	1432.4	24.2	61.5	98.3	88.6	0.695	0.86
	SD	25	14	37	4	1.3	0.3	0.7	0.010	0.01

Model Number			<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>
<b>[10,10]</b>	<b>16</b>	Train 1	1103	479	4337	33	69.7	99.2	91.4	0.775	0.91
	<b>17</b>	Train 2	1025	513	4377	37	66.6	99.2	90.8	0.752	0.91
	<b>18</b>	Train 3	1129	498	4276	49	69.4	98.9	90.8	0.764	0.91
	<b>19</b>	Train 4	1042	542	4316	52	65.8	98.8	90.0	0.737	0.89
	<b>20</b>	Train 5	1017	574	4307	54	63.9	98.8	89.4	0.722	0.89
		Avg	1063	521	4323	45	67.1	99.0	90.5	0.750	0.90
		SD	50	37	38	9	2.5	0.2	0.8	0.021	0.01
		Validation 1	347	168	1446	23	67.4	98.4	90.4	0.741	0.87
		Validation 2	349	212	1402	21	62.2	98.5	88.3	0.702	0.87
		Validation 3	335	203	1422	24	62.3	98.3	88.6	0.700	0.85
		Validation 4	307	177	1481	19	63.4	98.7	90.1	0.720	0.88
		Validation 5	309	219	1435	21	58.5	98.6	87.9	0.677	0.84
		Avg	329.4	195.8	1437.2	21.6	62.7	98.5	89.0	0.708	0.86

		SD	20	22	29	2	3.2	0.1	1.1	0.024	0.02
		Test 1	343	197	1422	22	63.5	98.5	89.0	0.712	0.87
		Test 2	307	231	1426	20	57.1	98.6	87.3	0.667	0.86
		Test 3	312	160	1489	23	66.1	98.5	90.8	0.734	0.87
		Test 4	342	227	1394	21	60.1	98.5	87.5	0.686	0.88
		Test 5	320	198	1449	17	61.8	98.8	89.2	0.709	0.87
		Avg	324.8	202.6	1436.0	20.6	61.6	98.6	88.8	0.701	0.87
		SD	17	29	35	2	3.4	0.2	1.4	0.026	0.01
Model Number											
[100,100]	21	Train 1	1229	340	4340	43	78.3	99.0	93.6	0.831	0.95
	22	Train 2	1231	356	4329	36	77.6	99.2	93.4	0.829	0.94
	23	Train 3	1195	420	4323	14	74.0	99.7	92.7	0.814	0.96
	24	Train 4	1206	354	4372	20	77.3	99.5	93.7	0.836	0.96
	25	Train 5	1162	421	4346	23	73.4	99.5	92.5	0.806	0.95
		Avg	1205	378	4342	27	76.1	99.4	93.2	0.823	0.95
		SD	28	39	19	12	2.3	0.3	0.5	0.012	0.01
Validation											
		Validation 1	373	155	1409	47	70.6	96.8	89.8	0.729	0.87
		Validation 2	356	156	1443	29	69.5	98.0	90.7	0.748	0.86
		Validation 3	371	179	1398	36	67.5	97.5	89.2	0.720	0.88
		Validation 4	346	162	1451	25	68.1	98.3	90.6	0.743	0.88

		Validation 5	377	159	1424	24	70.3	98.3	90.8	0.759	0.88
		Avg	365	162	1425	32	69.2	97.8	90.2	0.740	0.87
		SD	13	10	22	10	1.4	0.7	0.7	0.016	0.01
		Test 1	361	179	1407	37	66.9	97.4	89.1	0.715	0.86
		Test 2	371	167	1412	34	69.0	97.6	89.9	0.735	0.87
		Test 3	318	154	1489	23	67.4	98.5	91.1	0.743	0.88
		Test 4	379	190	1385	30	66.6	97.9	88.9	0.721	0.85
		Test 5	364	154	1450	16	70.3	98.9	91.4	0.772	0.89
		Avg	359	169	1429	28	68.0	98.1	90.1	0.737	0.87
		SD	24	16	41	9	1.6	0.6	1.1	0.023	0.02
	Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC
[1000,1000]	26	Train 1	937	610	4366	39	60.6	99.1	89.1	0.707	0.89
	27	Train 2	1318	290	4298	46	82.0	98.9	94.4	0.855	0.95
	28	Train 3	1180	438	4322	12	72.9	99.7	92.4	0.808	0.96
	29	Train 4	1108	427	4408	9	72.2	99.8	92.7	0.806	0.98
	30	Train 5	1234	336	4352	30	78.6	99.3	93.9	0.840	0.94
		Avg	1155	420	4349	27	73.2	99.4	92.5	0.803	0.94
		SD	144	123	42	16	8.2	0.4	2.1	0.058	0.03
		Validation 1	329	221	1418	16	59.8	98.9	88.1	0.693	0.85
		Validation 2	351	140	1425	68	71.5	95.4	89.5	0.708	0.87

Validation 3	361	186	1421	16	66.0	98.9	89.8	0.739	0.90	
Validation 4	336	197	1438	13	63.0	99.1	89.4	0.723	0.87	
Validation 5	381	168	1395	40	69.4	97.2	89.5	0.729	0.88	
Avg	352	182	1419	31	65.9	97.9	89.3	0.718	0.87	
SD	21	31	16	24	4.7	1.6	0.7	0.018	0.02	
Test 1	313	227	1431	13	58.0	99.1	87.9	0.685	0.86	
Test 2	384	154	1381	65	71.4	95.5	89.0	0.711	0.87	
Test 3	305	167	1497	15	64.6	99.0	90.8	0.737	0.87	
Test 4	328	241	1403	12	57.6	99.2	87.2	0.682	0.85	
Test 5	368	150	1439	27	71.0	98.2	91.1	0.761	0.88	
Avg	340	188	1430	26	64.5	98.2	89.2	0.715	0.87	
SD	35	43	44	22	6.7	1.6	1.7	0.034	0.01	

Table S7. Results comparing model performance for various network architectures at the AR. Model performances are reported as sensitivity (SE), specificity (SP), accuracy (ACC), Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC). Averages (Avg) and standard deviations (SD) are shown.

## KCNH2

	Model Number		TP	FN	TN	FP	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[10]	1	Train 1	2707	194	1073	910	0.87	93.3	54.1	77.4	0.531	0.87
	2	Train 2	2753	195	1064	872	0.87	93.4	55.0	78.2	0.541	0.87
	3	Train 3	2748	169	922	1045	0.86	94.2	46.9	75.1	0.484	0.86
	4	Train 4	2690	247	1227	720	0.88	91.6	63.0	80.2	0.582	0.88
	5	Train 5	2823	148	925	991	0.86	95.0	48.3	76.7	0.511	0.86
		Avg	2744	191	1042	908	0.87	93.5	53.5	77.5	0.529	0.87
		SD	52	37	126	125	0.01	1.3	6.4	1.9	0.037	0.01
		Validation 1	918	88	327	295	0.83	91.3	52.6	76.5	0.489	0.83
		Validation 2	913	73	296	346	0.82	92.6	46.1	74.3	0.452	0.82
		Validation 3	939	51	303	335	0.83	94.8	47.5	76.3	0.501	0.83
[11]		Validation 4	836	136	340	316	0.80	86.0	51.8	72.2	0.408	0.80
		Validation 5	889	66	290	383	0.81	93.1	43.1	72.4	0.431	0.81
		Avg	899.0	82.8	311.2	335.0	0.82	91.6	48.2	74.3	0.454	0.82
		SD	39	33	21	33	0.01	3.4	4.0	2.0	0.039	0.01
		Test 1	890	98	290	350	0.78	90.1	45.3	72.5	0.406	0.78
		Test 2	875	86	314	353	0.82	91.1	47.1	73.0	0.436	0.82
		Test 3	929	59	273	367	0.81	94.0	42.7	73.8	0.445	0.81
		Test 4	886	100	351	291	0.83	89.9	54.7	76.0	0.486	0.83
		Test 5	921	51	268	388	0.81	94.8	40.9	73.0	0.440	0.81

		Avg	900.2	78.8	299.2	349.8	0.81	92.0	46.1	73.7	0.441	0.81	
		SD	23	23	34	36	0.02	2.3	5.3	1.4	0.029	0.02	
		Model Number		TP	FN	TN	FP	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100]	6	Train 1	2698	212	1053	921	0.87	92.7	53.3	76.8	0.516	0.87	
	7	Train 2	2782	172	996	934	0.87	94.2	51.6	77.4	0.525	0.87	
	8	Train 3	2718	201	1027	938	0.86	93.1	52.3	76.7	0.513	0.86	
	9	Train 4	2764	157	942	1021	0.85	94.6	48.0	75.9	0.500	0.85	
	10	Train 5	2800	117	869	1098	0.86	96.0	44.2	75.1	0.491	0.86	
		Avg	2752	172	977	982	0.86	94.1	49.9	76.4	0.508	0.86	
		SD	43	38	73	76	0.01	1.3	3.8	0.9	0.013	0.01	
		Validation 1	902	95	317	314	0.82	90.5	50.2	74.9	0.456	0.82	
		Validation 2	893	87	297	351	0.81	91.1	45.8	73.1	0.426	0.81	
		Validation 3	920	68	308	332	0.81	93.1	48.1	75.4	0.478	0.81	
		Validation 4	917	71	264	347	0.79	92.8	43.2	73.9	0.430	0.79	
		Validation 5	939	67	258	364	0.81	93.3	41.5	73.5	0.423	0.81	
		Avg	914.2	77.6	288.8	341.6	0.81	92.2	45.8	74.2	0.443	0.81	
		SD	18	13	26	19	0.01	1.3	3.6	1.0	0.024	0.01	
		Test 1	893	95	288	352	0.78	90.4	45.0	72.5	0.407	0.78	
		Test 2	895	66	298	369	0.81	93.1	44.7	73.3	0.446	0.81	
		Test 3	911	77	307	333	0.80	92.2	48.0	74.8	0.462	0.80	

		Test 4	918	68	295	347	0.80	93.1	46.0	74.5	0.459	0.80
		Test 5	930	42	242	414	0.80	95.7	36.9	72.0	0.421	0.80
		Avg	909.4	69.6	286.0	363.0	0.80	92.9	44.1	73.4	0.438	0.80
		SD	16	19	26	31	0.01	1.9	4.2	1.2	0.024	0.01
	Model Number		TP	FN	TN	FP	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[1000]	11	Train 1	2447	483	1459	495	0.88	83.5	74.7	80.0	0.582	0.88
	12	Train 2	2718	238	1188	740	0.87	91.9	61.6	80.0	0.576	0.87
	13	Train 3	2686	248	1167	783	0.87	91.5	59.8	78.9	0.555	0.87
	14	Train 4	2703	265	1182	734	0.87	91.1	61.7	79.5	0.564	0.87
	15	Train 5	2667	279	1234	704	0.87	90.5	63.7	79.9	0.573	0.87
		Avg	2644	303	1246	691	0.87	89.7	64.3	79.7	0.568	0.87
		SD	112	102	122	113	0.00	3.5	6.0	0.5	0.011	0.00
		Validation 1	776	201	445	206	0.83	79.4	68.4	75.0	0.478	0.83
		Validation 2	877	101	371	279	0.81	89.7	57.1	76.7	0.505	0.81
		Validation 3	882	91	320	335	0.81	90.6	48.9	73.8	0.446	0.81
		Validation 4	833	265	1182	734	0.83	75.9	61.7	66.9	0.362	0.83
		Validation 5	863	114	374	277	0.82	88.3	57.5	76.0	0.490	0.82
		Avg	846.2	154.4	538.4	366.2	0.82	84.6	59.5	72.7	0.458	0.82
		SD	44	76	363	211	0.01	6.7	7.1	4.0	0.057	0.01
		Test 1	763	225	406	234	0.78	77.2	63.4	71.8	0.408	0.78

	Test 2	859	102	346	321	0.81	89.4	51.9	74.0	0.454	0.81
	Test 3	890	98	335	305	0.81	90.1	52.3	75.2	0.469	0.81
	Test 4	884	102	344	298	0.82	89.7	53.6	75.4	0.474	0.82
	Test 5	863	109	353	303	0.82	88.8	53.8	74.7	0.463	0.82
	Avg	851.8	127.2	356.8	292.2	0.81	87.0	55.0	74.2	0.450	0.81
	SD	51	55	28	34	0.02	5.5	4.8	1.5	0.027	0.02

Model Number			TP	FN	TN	FP	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	
<b>[10,10]</b>	<b>16</b>	Train 1	2771	150	1698	265	0.97	94.9	86.5	91.5	0.823	0.97	
	<b>17</b>	Train 2	2856	117	1556	355	0.97	96.1	81.4	90.3	0.797	0.97	
	<b>18</b>	Train 3	2755	161	1662	306	0.97	94.5	84.5	90.4	0.800	0.97	
	<b>19</b>	Train 4	2693	247	1599	345	0.95	91.6	82.3	87.9	0.746	0.95	
	<b>20</b>	Train 5	2773	194	1729	188	0.97	93.5	90.2	92.2	0.836	0.97	
		Avg	2770	174	1649	292	0.97	94.1	85.0	90.5	0.800	0.97	
		SD	58	49	71	68	0.01	1.7	3.5	1.6	0.035	0.01	
			Validation 1	846	140	453	189	0.87	85.8	70.6	79.8	0.572	0.87
			Validation 2	836	125	405	262	0.86	87.0	60.7	76.2	0.501	0.86
			Validation 3	854	137	422	215	0.86	86.2	66.2	78.4	0.539	0.86
			Validation 4	853	116	433	226	0.87	88.0	65.7	79.0	0.558	0.87
			Validation 5	798	158	484	188	0.85	83.5	72.0	78.7	0.559	0.85
			Avg	837.4	135.2	439.4	216.0	0.86	86.1	67.0	78.4	0.545	0.86
			SD	23	16	30	31	0.01	1.7	4.5	1.3	0.028	0.01

	Test 1	848	140	410	230	0.82	85.8	64.1	77.3	0.515	0.82
	Test 2	864	97	402	265	0.85	89.9	60.3	77.8	0.535	0.85
	Test 3	860	128	386	254	0.85	87.0	60.3	76.5	0.498	0.85
	Test 4	846	140	432	226	0.86	85.8	65.7	77.7	0.529	0.86
	Test 5	808	164	450	206	0.85	83.1	68.6	77.3	0.523	0.85
	Avg	845.2	133.8	416.0	236.2	0.85	86.3	63.8	77.3	0.519	0.85
	SD	22	24	25	23	0.02	2.5	3.6	0.5	0.015	0.02

Model Number			TP	FN	TN	FP	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	
[100,100]	21	Train 1	2852	83	1672	277	0.98	97.2	85.8	92.6	0.847	0.98	
	22	Train 2	2860	84	1736	204	0.99	97.1	89.5	94.1	0.877	0.99	
	23	Train 3	2830	135	1796	123	0.98	95.4	93.6	94.7	0.889	0.98	
	24	Train 4	2786	150	1834	114	0.98	94.9	94.1	94.6	0.888	0.98	
	25	Train 5	2835	102	1740	207	0.98	96.5	89.4	93.7	0.868	0.98	
		Avg	2833	111	1756	185	0.98	96.2	90.5	93.9	0.874	0.98	
		SD	29	30	62	67	0.00	1.0	3.4	0.8	0.017	0.00	
			Validation 1	847	125	446	210	0.88	87.1	68.0	79.4	0.567	0.88
			Validation 2	852	138	416	222	0.85	86.1	65.2	77.9	0.528	0.85
			Validation 3	772	170	514	172	0.87	82.0	74.9	79.0	0.569	0.87
			Validation 4	803	170	481	174	0.85	82.5	73.4	78.9	0.560	0.85
			Validation 5	855	131	430	212	0.86	86.7	67.0	78.9	0.552	0.86

		Avg	826	147	457	198	0.86	84.9	69.7	78.8	0.555	0.86
		SD	37	22	40	23	0.01	2.4	4.2	0.6	0.016	0.01
		Test 1	858	130	376	264	0.82	86.8	58.8	75.8	0.481	0.82
		Test 2	832	129	429	238	0.85	86.6	64.3	77.5	0.527	0.85
		Test 3	820	168	441	199	0.85	83.0	68.9	77.5	0.524	0.85
		Test 4	822	164	452	190	0.85	83.4	70.4	78.3	0.542	0.85
		Test 5	834	138	426	230	0.84	85.8	64.9	77.4	0.523	0.84
		Avg	833	146	425	224	0.84	85.1	65.5	77.3	0.519	0.84
		SD	15	19	29	30	0.01	1.8	4.6	0.9	0.023	0.01
Model Number			<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>ROC-AUC</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>
<b>[1000,1000]</b>	<b>26</b>	Train 1	2945	32	1405	502	0.98	98.9	73.7	89.1	0.777	0.98
	<b>27</b>	Train 2	2864	66	1612	342	0.98	97.7	82.5	91.6	0.828	0.98
	<b>28</b>	Train 3	2606	329	1918	31	0.99	88.8	98.4	92.6	0.857	0.99
	<b>29</b>	Train 4	2708	221	1850	105	0.98	92.5	94.6	93.3	0.863	0.98
	<b>30</b>	Train 5	2863	83	1704	234	0.98	97.2	87.9	93.5	0.864	0.98
		Avg	2797	146	1698	243	0.98	95.0	87.4	92.0	0.838	0.98
		SD	137	125	203	188	0.00	4.3	9.8	1.8	0.037	0.00
		Validation 1	858	72	362	336	0.86	92.3	51.9	74.9	0.494	0.86
		Validation 2	914	90	355	269	0.85	91.0	56.9	77.9	0.523	0.85
		Validation 3	694	278	530	126	0.85	71.4	80.8	75.2	0.512	0.85

Validation 4	766	214	513	135	0.87	78.2	79.2	78.6	0.564	0.87
Validation 5	864	113	429	222	0.86	88.4	65.9	79.4	0.565	0.86
Avg	819	153	438	218	0.86	84.3	66.9	77.2	0.532	0.86
SD	88	89	82	89	0.01	9.1	12.9	2.0	0.032	0.01
Test 1	916	72	306	334	0.81	92.7	47.8	75.1	0.469	0.81
Test 2	871	90	371	296	0.84	90.6	55.6	76.3	0.505	0.84
Test 3	693	295	515	125	0.84	70.1	80.5	74.2	0.494	0.84
Test 4	767	219	510	132	0.86	77.8	79.4	78.4	0.562	0.86
Test 5	834	138	423	233	0.83	85.8	64.5	77.2	0.519	0.83
Avg	816	163	425	224	0.84	83.4	65.6	76.2	0.510	0.84
SD	88	93	90	94	0.02	9.4	14.4	1.7	0.035	0.02

Table S8. Results comparing model performance for various network architectures at the KCNH2. Model performances are reported as sensitivity (SE), specificity (SP), accuracy (ACC), Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC). Averages (Avg) and standard deviations (SD) are shown.

**SLC6A4**

	Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC
[10]	1	Train 1	2426	19	458	202	99.2	69.4	92.9	0.779	0.98
	2	Train 2	2373	17	513	202	99.3	71.7	92.9	0.795	0.98
	3	Train 3	2422	16	438	229	99.3	65.7	92.1	0.756	0.98
	4	Train 4	2441	18	472	174	99.3	73.1	93.8	0.805	0.98
	5	Train 5	2392	23	563	127	99.0	81.6	95.2	0.857	0.99
		Avg	2411	19	489	187	99.2	72.4	93.4	0.799	0.98
		SD	28	3	50	39	0.1	5.9	1.2	0.038	0.00
	Validation	Validation 1	791	10	150	84	98.8	64.1	90.9	0.727	0.98
		Validation 2	786	10	161	78	98.7	67.4	91.5	0.750	0.98
		Validation 3	792	5	150	88	99.4	63.0	91.0	0.736	0.96
		Validation 4	800	6	145	84	99.3	63.3	91.3	0.736	0.97
		Validation 5	813	4	159	59	99.5	72.9	93.9	0.811	0.97
		Avg	796.4	7.0	153.0	78.6	99.1	66.1	91.7	0.752	0.97
		SD	11	3	7	12	0.4	4.2	1.2	0.034	0.01
Test	Test 1	793	2	151	89	99.7	62.9	91.2	0.745	0.96	
	Test 2	846	9	126	54	98.9	70.0	93.9	0.776	0.98	
	Test 3	797	9	150	79	98.9	65.5	91.5	0.741	0.98	
	Test 4	768	8	173	86	99.0	66.8	90.9	0.750	0.97	
	Test 5	797	12	167	59	98.5	73.9	93.1	0.791	0.98	

		Avg	800.2	8.0	153.4	73.4	99.0	67.6	92.1	0.760	0.97
		SD	28	4	18	16	0.5	4.2	1.3	0.022	0.01
		Model Number		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
[100]	<b>6</b>	Train 1	2435	21	577	72	99.1	88.9	97.0	0.908	0.99
	<b>7</b>	Train 2	2358	30	651	66	98.7	90.8	96.9	0.912	0.99
	<b>8</b>	Train 3	2410	25	618	52	99.0	92.2	97.5	0.926	0.99
	<b>9</b>	Train 4	2430	22	570	83	99.1	87.3	96.6	0.896	0.99
	<b>10</b>	Train 5	2416	24	575	90	99.0	86.5	96.3	0.889	0.99
		Avg	2410	24	598	73	99.0	89.2	96.9	0.906	0.99
		SD	31	4	35	15	0.2	2.4	0.4	0.014	0.00
		Validation 1	777	13	203	42	98.4	82.9	94.7	0.849	0.98
		Validation 2	784	14	202	35	98.2	85.2	95.3	0.863	0.98
		Validation 3	784	16	207	28	98.0	88.1	95.7	0.877	0.98
		Validation 4	798	15	177	45	98.2	79.7	94.2	0.822	0.98
		Validation 5	785	7	202	41	99.1	83.1	95.4	0.868	0.98
		Avg	785.6	13.0	198.2	38.2	98.4	83.8	95.1	0.856	0.98
		SD	8	4	12	7	0.4	3.1	0.6	0.021	0.00
		Test 1	791	4	197	43	99.5	82.1	95.5	0.870	0.97
		Test 2	842	13	155	25	98.5	86.1	96.3	0.870	0.99
		Test 3	793	13	202	27	98.4	88.2	96.1	0.886	0.98

			Test 4	765	11	213	46	98.6	82.2	94.5	0.850	0.98
			Test 5	795	14	175	51	98.3	77.4	93.7	0.810	0.98
			Avg	797.2	11.0	188.4	38.4	98.6	83.1	95.2	0.857	0.98
			SD	28	4	23	12	0.5	4.2	1.1	0.030	0.01
[1000]	Model Number	TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC		
		2396	22	473	214	99.1	68.9	92.4	0.770	0.99		
		2380	14	552	159	99.4	77.6	94.4	0.839	0.98		
		2394	24	558	129	99.0	81.2	95.1	0.853	0.99		
		2446	17	518	124	99.3	80.7	95.5	0.858	0.98		
		2404	19	530	152	99.2	77.7	94.5	0.835	0.98		
		Avg	2404	19	526	156	99.2	77.2	94.4	0.831	0.98	
	Validation	25	4	34	36	0.2	5.0	1.2	0.035	0.01		
		822	6	136	71	99.3	65.7	92.6	0.755	0.96		
		778	14	178	65	98.2	73.3	92.4	0.779	0.97		
[10000]	Model Number	807	10	172	46	98.8	78.9	94.6	0.832	0.97		
		792	10	180	53	98.8	77.3	93.9	0.820	0.98		
		799	10	166	60	98.8	73.5	93.2	0.794	0.98		
		Avg	799.6	10.0	166.4	59.0	98.8	73.8	93.3	0.797	0.97	
		SD	16	3	18	10	0.4	5.1	0.9	0.031	0.01	
		Test 1	793	2	156	84	99.7	65.0	91.7	0.760	0.96	

	Test 2	847	8	140	40	99.1	77.8	95.4	0.832	0.98
	Test 3	796	10	184	45	98.8	80.3	94.7	0.841	0.98
	Test 4	768	8	193	66	99.0	74.5	92.9	0.805	0.97
	Test 5	799	10	165	61	98.8	73.0	93.1	0.791	0.98
	Avg	800.6	7.6	167.6	59.2	99.1	73.9	93.5	0.805	0.97
	SD	29	3	21	18	0.4	5.8	1.5	0.033	0.01

Model Number			TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC
<b>[10,10]</b>	<b>16</b>	Train 1	2428	26	593	58	98.9	91.1	97.3	0.917	0.99
	<b>17</b>	Train 2	2362	32	655	56	98.7	92.1	97.2	0.919	0.99
	<b>18</b>	Train 3	2412	20	566	107	99.2	84.1	95.9	0.877	0.99
	<b>19</b>	Train 4	2426	25	601	53	99.0	91.9	97.5	0.924	0.99
	<b>20</b>	Train 5	2418	22	594	71	99.1	89.3	97.0	0.910	0.99
		Avg	2409	25	602	69	99.0	89.7	97.0	0.909	0.99
		SD	27	5	33	22	0.2	3.3	0.6	0.019	0.00
		Validation 1	785	7	191	52	99.1	78.6	94.3	0.838	0.98
		Validation 2	785	7	199	44	99.1	81.9	95.1	0.860	0.97
		Validation 3	798	5	176	56	99.4	75.9	94.1	0.826	0.98
		Validation 4	804	10	192	29	98.8	86.9	96.2	0.886	0.99
		Validation 5	778	14	213	30	98.2	87.7	95.7	0.880	0.99
		Avg	790.0	8.6	194.2	42.2	98.9	82.1	95.1	0.857	0.98
		SD	11	4	13	12	0.4	5.1	0.9	0.026	0.01

		Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC	ROC-AUC
[100,100]	<b>21</b>	Train 1	2407	17	647	34	99.3	95.0	98.4	0.952	1.00	
	<b>22</b>	Train 2	2373	16	685	31	99.3	95.7	98.5	0.957	1.00	
	<b>23</b>	Train 3	2418	15	647	25	99.4	96.3	98.7	0.962	1.00	
	<b>24</b>	Train 4	2442	15	628	20	99.4	96.9	98.9	0.966	1.00	
	<b>25</b>	Train 5	2400	14	659	32	99.4	95.4	98.5	0.957	1.00	
		Avg	2408	15	653	28	99.4	95.8	98.6	0.959	1.00	
		SD	25	1	21	6	0.0	0.8	0.2	0.005	0.00	

			Avg	795	15	194	31	98.2	86.1	95.6	0.867	0.98
			SD	10	3	11	4	0.4	1.9	0.2	0.009	0.00
			Test 1	791	4	201	39	99.5	83.8	95.8	0.882	0.98
			Test 2	846	9	159	21	98.9	88.3	97.1	0.897	0.99
			Test 3	790	16	210	19	98.0	91.7	96.6	0.901	0.99
			Test 4	764	12	226	33	98.5	87.3	95.7	0.882	0.98
			Test 5	795	14	188	38	98.3	83.2	95.0	0.849	0.99
			Avg	797	11	197	30	98.6	86.8	96.0	0.882	0.99
			SD	30	5	25	9	0.6	3.5	0.8	0.021	0.01
		Model Number		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>	<b>ROC-AUC</b>
[1000,1000]	<b>26</b>	Train 1	2401	26	671	7	98.9	99.0	98.9	0.969	1.00	
	<b>27</b>	Train 2	2375	13	703	14	99.5	98.0	99.1	0.976	1.00	
	<b>28</b>	Train 3	2394	18	686	7	99.3	99.0	99.2	0.977	1.00	
	<b>29</b>	Train 4	2446	8	636	15	99.7	97.7	99.3	0.978	1.00	
	<b>30</b>	Train 5	2417	9	662	17	99.6	97.5	99.2	0.975	1.00	
		Avg	2407	15	672	12	99.4	98.2	99.1	0.975	1.00	
		SD	27	7	25	5	0.3	0.7	0.1	0.003	0.00	
			Validation 1	803	16	198	18	98.0	91.7	96.7	0.900	0.99
			Validation 2	786	12	216	21	98.5	91.1	96.8	0.909	0.99
			Validation 3	795	23	199	13	97.2	93.9	96.5	0.895	0.99

Validation 4	797	14	201	23	98.3	89.7	96.4	0.893	0.99
Validation 5	792	14	204	25	98.3	89.1	96.2	0.889	0.99
Avg	795	16	204	20	98.1	91.1	96.5	0.897	0.99
SD	6	4	7	5	0.5	1.9	0.2	0.008	0.00
Test 1	782	13	215	25	98.4	89.6	96.3	0.896	0.98
Test 2	847	8	162	18	99.1	90.0	97.5	0.911	0.99
Test 3	788	18	221	8	97.8	96.5	97.5	0.929	0.98
Test 4	762	14	228	31	98.2	88.0	95.7	0.882	0.99
Test 5	796	13	200	26	98.4	88.5	96.2	0.888	0.99
Avg	795	13	205	22	98.4	90.5	96.6	0.901	0.99
SD	32	4	26	9	0.5	3.4	0.8	0.019	0.01

Table S9. Results comparing model performance for various network architectures at the SLC6A4. Model performances are reported as sensitivity (SE), specificity (SP), accuracy (ACC), Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC). Averages (Avg) and standard deviations (SD) are shown.

AChE	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	91.5	91.3	91.4	0.827	0.97	87.2	85.3	86.3	0.722	0.92	84.9	84.1	84.7	0.690	0.91
	2.2	1.7	0.7	0.011	0.00	2.3	3.2	1.3	0.027	0.01	5.0	4.7	1.4	0.019	0.01
<b>[1000,1000]</b>	95.3	96.5	95.8	0.915	0.99	87.9	86.6	87.4	0.744	0.93	84.6	84.1	84.4	0.685	0.92
	2.5	2.0	1.9	0.038	0.00	3.5	3.8	1.8	0.037	0.02	3.8	6.1	1.5	0.027	0.01
ADORA2A	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	98.1	93.7	96.6	0.924	0.99	96.8	90.8	94.8	0.883	0.98	96.8	90.3	94.7	0.880	0.98
	0.5	2.3	0.5	0.012	0.00	0.6	1.9	0.5	0.010	0.00	1.7	3.1	1.0	0.023	0.00
<b>[1000,1000]</b>	99.0	78.1	91.7	0.787	1.00	97.3	92.4	95.6	0.903	0.98	96.7	91.3	94.8	0.884	0.98
	0.2	41.6	14.7	0.388	0.00	0.4	1.6	0.5	0.010	0.01	1.3	2.0	0.9	0.018	0.00
AR	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	76.1	99.4	93.2	0.823	0.95	69.2	97.8	90.2	0.740	0.87	68.0	98.1	90.1	0.737	0.87
	2.3	0.3	0.5	0.012	0.01	1.4	0.7	0.7	0.016	0.01	1.6	0.6	1.1	0.023	0.02
<b>[1000,1000]</b>	73.2	99.4	92.5	0.803	0.94	65.9	97.9	89.3	0.718	0.87	64.5	98.2	89.2	0.715	0.87
	8.2	0.4	2.1	0.058	0.03	4.7	1.6	0.7	0.018	0.02	6.7	1.6	1.7	0.034	0.01

KCNH2	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	96.2	90.5	93.9	0.874	0.98	84.9	69.7	78.8	0.555	0.86	85.1	65.5	77.3	0.519	0.84
	1.0	3.4	0.8	0.017	0.00	2.4	4.2	0.6	0.016	0.01	1.8	4.6	0.9	0.023	0.01
[1000,1000]	95.0	87.4	92.0	0.838	0.98	84.3	66.9	77.2	0.532	0.86	83.4	65.6	76.2	0.510	0.84
	4.3	9.8	1.8	0.037	0.00	9.1	12.9	2.0	0.032	0.01	9.4	14.4	1.7	0.035	0.02
SLC6A4	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	99.4	95.8	98.6	0.959	1.00	98.2	86.1	95.6	0.867	0.98	98.6	86.8	96.0	0.882	0.99
	0.0	0.8	0.2	0.005	0.00	0.4	1.9	0.2	0.009	0.00	0.6	3.5	0.8	0.021	0.01
[1000,1000]	99.4	98.2	99.1	0.975	1.00	98.1	91.1	96.5	0.897	0.99	98.4	90.5	96.6	0.901	0.99
	0.3	0.7	0.1	0.003	0.00	0.5	1.9	0.2	0.008	0.00	0.5	3.4	0.8	0.019	0.01
ADRA2A	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	93.2	97.9	95.7	0.915	0.99	88.8	92.9	91.1	0.821	0.96	88.3	93.3	90.9	0.817	0.96
	0.3	0.2	0.1	0.003	0.00	3.5	2.7	1.7	0.034	0.01	3.9	2.7	1.4	0.031	0.01
[1000,1000]	95.4	98.7	97.2	0.944	0.99	88.6	93.4	91.2	0.823	0.96	88.4	93.7	91.2	0.822	0.96
	1.1	0.5	0.4	0.007	0.00	1.3	0.6	0.7	0.014	0.01	4.2	1.6	1.9	0.039	0.01

ADRB1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	94.3	91.8	93.1	0.862	0.98	92.8	93.9	93.2	0.864	0.97	92.4	91.5	92.1	0.839	0.96
	0.3	0.5	0.2	0.004	0.00	2.0	1.0	0.8	0.016	0.01	1.9	0.8	0.9	0.018	0.01
<b>[1000,1000]</b>	96.1	93.6	94.9	0.898	0.99	92.1	91.0	91.6	0.831	0.96	92.5	91.5	92.1	0.839	0.97
	0.6	0.8	0.4	0.008	0.00	1.4	1.4	1.4	0.028	0.01	1.7	0.4	1.0	0.021	0.01
ADRB2	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	76.8	95.5	86.4	0.739	0.96	69.9	92.3	81.3	0.642	0.89	69.1	92.0	80.7	0.629	0.88
	5.6	0.9	2.1	0.035	0.00	3.5	3.4	1.2	0.025	0.01	5.9	2.5	2.2	0.038	0.01
<b>[1000,1000]</b>	75.1	95.4	85.4	0.722	0.95	68.7	91.9	80.6	0.626	0.88	67.6	92.4	80.4	0.624	0.88
	4.8	1.7	1.7	0.027	0.00	4.8	2.8	1.1	0.010	0.01	6.6	3.4	1.6	0.031	0.02
OPRD1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	97.6	87.5	94.6	0.869	0.99	96.4	81.7	92.3	0.805	0.97	96.5	81.6	92.3	0.807	0.96
	0.3	1.2	0.2	0.006	0.00	0.8	1.9	0.5	0.013	0.00	1.0	5.7	1.1	0.028	0.01
<b>[1000,1000]</b>	98.2	91.0	96.1	0.905	0.99	96.0	84.2	92.7	0.818	0.97	96.4	82.1	92.3	0.809	0.97
	0.2	1.9	0.5	0.013	0.00	1.1	2.6	0.4	0.012	0.01	1.6	6.3	1.0	0.027	0.01

DRD1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	83.9	98.3	92.5	0.846	0.97	78.4	93.9	87.7	0.742	0.94	78.5	94.8	88.2	0.755	0.93
	1.1	0.3	0.3	0.006	0.01	1.2	0.9	0.7	0.014	0.01	3.5	1.6	1.5	0.028	0.01
[1000,1000]	83.9	97.6	92.1	0.837	0.97	79.3	95.7	89.1	0.774	0.94	78.7	94.0	87.7	0.746	0.93
	1.7	0.3	0.6	0.011	0.00	3.5	0.5	1.3	0.026	0.00	4.4	2.3	1.6	0.029	0.01
DRD2	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	99.1	83.6	96.6	0.872	0.99	98.8	79.2	94.8	0.832	0.97	98.8	78.0	95.3	0.824	0.97
	0.2	1.6	0.2	0.009	0.00	0.4	2.6	1.7	0.020	0.01	0.7	5.0	1.1	0.034	0.01
[1000,1000]	99.1	90.7	97.7	0.916	0.99	98.4	83.4	95.9	0.848	0.98	98.3	82.2	95.6	0.838	0.97
	0.2	2.2	0.2	0.012	0.00	0.7	2.5	0.6	0.016	0.00	0.8	4.5	0.8	0.015	0.01
SLC6A3	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	95.9	97.6	96.7	0.933	0.99	92.1	92.1	92.1	0.840	0.97	91.8	91.8	91.8	0.834	0.96
	0.5	0.7	0.3	0.005	0.00	1.3	1.9	0.9	0.018	0.00	2.0	1.5	1.3	0.025	0.01
[1000,1000]	95.1	96.0	95.5	0.910	0.99	92.3	91.9	92.1	0.841	0.97	91.9	90.7	91.4	0.826	0.97
	1.7	3.1	0.6	0.012	0.00	3.0	4.7	1.3	0.027	0.01	2.2	5.7	1.4	0.029	0.01

EDNRA	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	98.0	96.3	97.2	0.943	0.99	96.3	94.7	95.5	0.910	0.97	96.2	95.4	95.8	0.916	0.97
	0.7	0.2	0.3	0.007	0.00	0.7	2.6	1.3	0.025	0.02	1.9	1.1	1.0	0.020	0.02
<b>[1000,1000]</b>	98.5	96.6	97.6	0.952	0.99	96.8	94.8	95.9	0.918	0.98	96.4	95.2	95.8	0.915	0.97
	0.4	0.7	0.2	0.004	0.01	1.5	0.3	0.8	0.016	0.01	1.7	1.1	1.2	0.024	0.02
NR3C1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	74.4	99.5	91.9	0.809	0.95	69.1	98.9	90.0	0.759	0.90	69.7	98.7	90.0	0.759	0.89
	1.3	0.2	0.3	0.007	0.00	2.3	0.5	0.6	0.012	0.01	4.2	0.7	0.7	0.020	0.01
<b>[1000,1000]</b>	74.9	99.2	91.9	0.807	0.94	69.7	98.2	89.6	0.750	0.89	69.6	98.6	89.8	0.756	0.89
	3.4	0.3	0.8	0.019	0.00	4.2	0.9	0.7	0.017	0.01	3.1	0.9	0.8	0.016	0.02
HRH1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	95.6	95.2	95.4	0.908	0.99	93.3	91.6	92.4	0.849	0.98	92.0	91.1	91.7	0.832	0.97
	0.8	2.0	0.6	0.012	0.00	1.7	3.3	1.7	0.032	0.01	2.1	4.0	2.7	0.056	0.01
<b>[1000,1000]</b>	97.5	95.8	96.7	0.934	0.99	94.7	91.4	93.2	0.863	0.98	93.6	89.8	91.8	0.835	0.97
	0.6	1.1	0.3	0.006	0.00	1.9	2.6	2.1	0.041	0.01	0.6	4.9	2.2	0.045	0.01

OPRM1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	97.7	96.7	97.3	0.943	0.99	96.2	91.6	94.4	0.882	0.98	95.6	91.6	94.0	0.874	0.98
	0.6	0.8	0.1	0.001	0.00	1.4	1.7	1.5	0.031	0.00	1.1	1.3	0.4	0.007	0.00
<b>[1000,1000]</b>	97.6	95.8	96.9	0.935	0.99	95.8	90.6	93.8	0.869	0.98	95.2	91.1	93.6	0.865	0.98
	0.4	1.6	0.4	0.009	0.00	1.3	1.5	0.9	0.018	0.00	0.9	1.3	0.1	0.003	0.00
CHRM1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	97.2	91.4	95.0	0.894	0.99	95.2	85.0	91.2	0.814	0.96	94.5	86.1	91.3	0.814	0.96
	0.5	2.0	0.4	0.010	0.00	1.2	2.8	0.9	0.018	0.01	2.0	2.3	1.3	0.030	0.02
<b>[1000,1000]</b>	98.1	93.5	96.4	0.923	0.99	95.0	87.1	92.0	0.830	0.96	95.2	86.5	91.9	0.826	0.96
	0.6	1.9	0.6	0.014	0.00	1.4	2.4	0.9	0.016	0.01	0.6	3.2	1.3	0.025	0.01
CHRM2	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	94.0	97.4	95.9	0.917	0.99	89.1	95.4	92.6	0.850	0.98	87.3	95.2	91.7	0.833	0.97
	2.6	1.1	0.7	0.014	0.00	3.9	1.4	1.5	0.027	0.01	5.2	1.8	1.8	0.036	0.01
<b>[1000,1000]</b>	96.6	97.4	97.0	0.940	0.99	92.7	92.4	92.6	0.852	0.97	91.9	92.7	92.4	0.846	0.97
	1.3	1.5	0.4	0.007	0.00	3.3	2.6	1.1	0.022	0.01	3.0	2.0	1.2	0.024	0.01

CHRM3	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	95.9	94.3	95.2	0.902	0.99	92.9	89.1	91.3	0.821	0.97	92.9	88.1	90.9	0.813	0.96
	0.6	1.1	0.3	0.005	0.00	1.1	1.5	0.8	0.016	0.01	2.1	3.2	1.1	0.023	0.01
<b>[1000,1000]</b>	96.6	96.8	96.7	0.933	1.00	93.6	89.7	92.0	0.834	0.97	92.4	89.4	91.2	0.820	0.97
	1.2	1.3	0.4	0.007	0.01	1.9	1.6	0.5	0.011	0.01	3.4	3.1	1.2	0.023	0.01
SLC6A2	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	95.5	95.9	95.7	0.911	0.99	94.0	91.4	92.9	0.854	0.97	94.0	91.8	93.2	0.858	0.97
	0.9	0.8	0.3	0.006	0.00	0.5	2.2	1.1	0.023	0.00	2.2	1.9	1.1	0.023	0.00
<b>[1000,1000]</b>	96.1	96.6	96.3	0.924	0.99	94.8	92.6	93.9	0.873	0.97	94.0	92.0	93.2	0.860	0.97
	0.6	0.8	0.2	0.003	0.00	0.6	1.7	0.5	0.011	0.01	2.1	2.1	0.9	0.018	0.01
HTR2A	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	99.0	92.8	97.7	0.932	0.99	98.7	88.9	96.7	0.895	0.98	98.5	87.2	96.1	0.882	0.98
	0.1	1.4	0.2	0.007	0.00	0.4	5.0	1.2	0.035	0.01	0.4	2.1	0.6	0.018	0.00
<b>[1000,1000]</b>	99.3	95.4	98.4	0.954	1.00	98.6	88.4	96.5	0.893	0.98	98.5	88.4	96.3	0.890	0.98
	0.2	1.2	0.2	0.004	0.00	0.5	2.7	0.5	0.014	0.01	0.5	2.4	0.5	0.016	0.01

HTR3A	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	85.9	99.2	95.3	0.886	0.98	79.6	98.2	92.3	0.821	0.97	78.5	98.2	92.4	0.815	0.96
	6.6	0.6	1.6	0.041	0.01	6.0	1.6	1.4	0.022	0.01	15.2	1.6	3.7	0.090	0.02
<b>[1000,1000]</b>	91.7	99.8	97.3	0.937	0.99	83.9	96.9	93.3	0.830	0.96	82.5	98.1	93.5	0.842	0.97
	2.4	0.1	0.7	0.016	0.00	5.4	0.9	1.3	0.035	0.01	8.1	0.7	2.0	0.050	0.02
LCK	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	98.0	83.9	94.7	0.850	0.98	96.9	78.1	92.6	0.783	0.96	97.1	73.6	91.8	0.758	0.95
	0.5	2.6	0.4	0.011	0.01	0.8	5.3	1.6	0.039	0.02	1.5	3.7	2.3	0.031	0.02
<b>[1000,1000]</b>	98.1	92.3	96.7	0.908	0.99	95.8	83.5	93.1	0.798	0.96	95.6	83.1	93.8	0.805	0.96
	0.6	2.8	0.4	0.008	0.00	1.0	4.6	1.0	0.028	0.01	2.3	9.4	2.4	0.069	0.02
AVPR1A	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	97.6	99.0	98.4	0.967	0.99	95.3	97.0	96.4	0.922	0.99	94.3	97.0	96.1	0.915	0.98
	0.3	0.6	0.3	0.007	0.00	1.8	1.1	1.1	0.025	0.01	3.4	1.3	1.1	0.025	0.01
<b>[1000,1000]</b>	98.3	99.3	98.9	0.977	1.00	96.7	97.1	97.0	0.935	0.99	96.5	97.4	97.0	0.936	0.99
	0.8	0.3	0.3	0.005	0.00	1.3	1.1	0.9	0.019	0.01	1.3	0.7	0.6	0.012	0.00

AGTR1	Train						Validation						Test					
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC			
<b>[100,100]</b>	87.2	100.0	94.8	0.895	0.99	85.2	99.2	93.6	0.869	0.97	82.6	99.2	92.8	0.849	0.97			
	2.2	0.1	0.8	0.016	0.00	2.9	0.6	1.0	0.019	0.01	7.0	0.3	1.8	0.047	0.01			
<b>[1000,1000]</b>	91.8	99.9	96.6	0.930	0.99	85.9	98.8	93.7	0.870	0.97	84.4	99.1	93.5	0.861	0.97			
	1.9	0.1	0.6	0.013	0.00	3.4	0.8	1.2	0.023	0.01	7.6	0.6	1.9	0.047	0.02			
AKT1	Train						Validation						Test					
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC			
<b>[100,100]</b>	97.6	92.8	96.1	0.909	0.99	96.3	89.8	94.3	0.866	0.98	95.9	88.7	93.7	0.851	0.97			
	0.3	1.3	0.3	0.007	0.01	0.6	3.3	0.9	0.023	0.01	1.2	3.5	1.9	0.038	0.01			
<b>[1000,1000]</b>	98.4	94.8	97.3	0.936	0.99	97.3	89.4	95.0	0.878	0.98	96.1	88.9	93.9	0.854	0.97			
	0.4	1.2	0.2	0.005	0.00	0.6	2.2	0.7	0.016	0.01	0.9	4.3	1.6	0.035	0.01			
BACE1	Train						Validation						Test					
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC			
<b>[100,100]</b>	96.8	90.3	94.8	0.877	0.98	95.5	86.8	92.9	0.830	0.97	95.4	85.6	92.5	0.819	0.97			
	0.7	1.1	0.2	0.002	0.00	0.8	1.8	0.4	0.010	0.00	0.7	2.9	1.0	0.023	0.01			
<b>[1000,1000]</b>	97.7	90.3	95.4	0.891	0.99	96.3	84.5	92.6	0.825	0.97	95.8	84.8	92.6	0.821	0.97			
	0.6	2.6	0.5	0.012	0.00	1.2	2.3	0.5	0.011	0.01	1.5	5.1	0.7	0.018	0.00			

BCHE	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	85.6	96.8	92.4	0.841	0.97	76.8	93.0	86.7	0.719	0.93	76.1	93.1	86.3	0.713	0.93
	3.1	1.0	0.7	0.015	0.00	4.6	2.5	0.7	0.009	0.01	4.6	1.1	1.8	0.032	0.01
<b>[1000,1000]</b>	89.1	96.7	93.7	0.868	0.98	80.9	93.5	88.5	0.760	0.94	79.4	92.4	87.1	0.732	0.94
	3.3	1.0	0.8	0.016	0.00	5.2	2.2	1.5	0.032	0.02	6.0	2.6	1.9	0.032	0.01
CASP1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	75.5	97.0	90.5	0.770	0.97	68.4	95.2	87.3	0.683	0.90	67.9	94.7	86.6	0.669	0.89
	1.2	0.6	0.6	0.014	0.00	2.5	0.8	1.1	0.024	0.01	2.9	0.9	1.6	0.034	0.02
<b>[1000,1000]</b>	69.2	97.1	88.8	0.724	0.95	65.5	96.0	86.6	0.676	0.90	62.5	96.0	85.9	0.651	0.89
	4.7	0.8	0.8	0.021	0.00	6.4	1.6	1.7	0.037	0.02	6.8	1.3	1.9	0.040	0.02
CASP3	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	85.0	97.4	92.6	0.844	0.98	79.2	95.3	88.9	0.768	0.94	79.4	95.3	89.1	0.769	0.95
	2.0	0.5	0.6	0.012	0.00	3.7	1.1	1.0	0.017	0.01	3.1	2.0	1.5	0.035	0.01
<b>[1000,1000]</b>	84.1	98.3	92.8	0.851	0.99	77.8	96.1	89.0	0.771	0.96	77.5	95.9	88.7	0.763	0.95
	6.8	1.0	2.0	0.039	0.00	10.1	2.3	2.7	0.052	0.02	5.0	1.5	2.2	0.045	0.01

CASP8	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	88.0	98.6	96.2	0.890	0.98	85.4	98.6	95.7	0.872	0.97	86.6	98.2	95.5	0.871	0.96
	1.9	0.2	0.4	0.012	0.00	4.8	0.6	0.6	0.025	0.01	3.3	0.8	1.3	0.035	0.03
<b>[1000,1000]</b>	89.7	98.9	96.9	0.909	0.99	89.0	98.9	96.6	0.903	0.96	88.0	98.3	96.0	0.883	0.97
	2.5	0.2	0.5	0.015	0.00	4.0	1.0	1.2	0.038	0.02	4.8	0.7	1.1	0.037	0.03
CHRM5	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	91.6	98.1	95.6	0.907	0.99	82.5	95.7	90.5	0.802	0.96	83.8	93.9	90.1	0.791	0.96
	3.4	0.2	1.2	0.025	0.00	5.4	2.1	1.4	0.029	0.01	3.3	3.9	2.2	0.042	0.02
<b>[1000,1000]</b>	92.4	98.7	96.3	0.922	0.99	83.0	96.1	91.1	0.811	0.96	80.6	96.1	90.2	0.792	0.96
	1.9	0.4	0.5	0.010	0.00	1.5	1.9	1.0	0.021	0.01	9.5	1.3	3.9	0.080	0.01
CHUK	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	83.9	99.2	95.8	0.877	0.99	74.4	99.0	93.1	0.804	0.99	72.2	99.1	92.9	0.794	0.98
	11.1	0.5	2.1	0.066	0.00	10.8	0.5	2.2	0.064	0.01	16.0	0.6	4.3	0.106	0.01
<b>[1000,1000]</b>	94.4	98.8	97.8	0.936	0.99	85.6	98.4	95.6	0.869	0.99	82.7	97.8	94.5	0.839	0.98
	4.1	0.6	0.8	0.028	0.00	9.2	1.5	2.5	0.075	0.02	7.3	1.6	0.6	0.021	0.01

CSF1R	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	97.6	98.2	97.9	0.957	1.00	95.2	93.5	94.5	0.888	0.99	95.5	95.0	95.3	0.905	0.99
	0.6	1.2	0.3	0.006	0.00	1.7	1.3	0.6	0.012	0.00	1.7	1.9	1.3	0.027	0.01
<b>[1000,1000]</b>	98.2	97.9	98.1	0.961	1.00	96.3	94.3	95.3	0.907	0.99	95.8	93.1	94.7	0.893	0.99
	0.7	1.8	0.5	0.010	0.00	2.8	2.5	1.3	0.025	0.00	2.4	4.2	1.9	0.038	0.01
CSNK1D	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	94.7	98.8	97.1	0.941	0.99	88.4	94.7	92.2	0.837	0.97	88.6	95.7	92.7	0.850	0.97
	1.2	0.6	0.6	0.012	0.00	4.4	1.2	1.5	0.034	0.01	4.8	1.9	2.4	0.047	0.01
<b>[1000,1000]</b>	89.7	97.5	94.4	0.886	0.99	84.8	94.4	90.4	0.806	0.97	84.8	95.0	90.8	0.813	0.97
	7.7	2.5	1.9	0.037	0.00	6.7	5.6	1.2	0.025	0.01	9.3	3.3	2.6	0.049	0.01
EDNRB	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	94.4	97.6	96.3	0.924	1.00	91.8	96.7	94.9	0.891	0.99	85.4	96.4	91.9	0.830	0.98
	1.9	1.1	0.7	0.014	0.00	2.9	1.2	1.1	0.023	0.00	5.5	2.4	2.7	0.050	0.01
<b>[1000,1000]</b>	97.8	97.5	97.6	0.950	1.00	96.0	94.1	94.9	0.895	0.99	92.6	94.7	93.9	0.870	0.99
	1.3	0.9	0.5	0.011	0.00	1.9	3.7	2.3	0.046	0.01	3.5	2.1	1.6	0.040	0.01

ELANE	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	95.1	95.0	95.0	0.897	0.99	93.2	91.0	92.4	0.840	0.98	91.5	91.1	91.6	0.824	0.97
	0.9	0.9	0.5	0.010	0.00	1.2	2.8	0.7	0.017	0.00	4.0	2.1	1.5	0.022	0.01
[1000,1000]	94.4	96.1	95.1	0.899	0.99	91.3	92.1	91.6	0.826	0.97	90.6	92.4	91.5	0.824	0.97
	1.3	0.7	0.6	0.012	0.00	2.3	1.6	1.4	0.029	0.01	4.9	2.6	2.2	0.037	0.01
EPHA2	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	90.6	99.9	96.9	0.929	1.00	85.1	99.7	94.8	0.885	0.98	82.7	99.8	94.9	0.874	0.98
	0.7	0.2	0.3	0.004	0.01	4.2	0.3	1.8	0.034	0.01	8.0	0.3	1.3	0.045	0.01
[1000,1000]	96.0	99.8	98.6	0.968	1.00	90.9	98.8	96.1	0.913	0.99	89.0	99.0	96.1	0.905	0.98
	1.7	0.2	0.5	0.012	0.00	1.8	0.6	0.7	0.015	0.01	3.7	0.8	0.3	0.012	0.01
FGFR1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	97.2	93.7	96.0	0.912	0.99	95.6	89.8	93.5	0.860	0.98	95.7	89.3	93.5	0.858	0.98
	0.7	1.9	0.3	0.007	0.00	1.7	2.9	1.0	0.021	0.01	3.0	2.1	2.5	0.042	0.01
[1000,1000]	98.1	92.8	96.2	0.917	0.99	96.5	87.4	93.3	0.852	0.98	96.5	86.9	93.1	0.848	0.97
	0.7	2.5	0.5	0.012	0.00	1.5	1.8	0.5	0.012	0.00	1.5	5.7	3.3	0.061	0.01

FKBP1A	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	94.7	98.3	97.4	0.932	0.99	89.5	97.4	95.2	0.879	0.99	93.9	96.0	95.4	0.884	0.99
	3.8	0.9	0.5	0.014	0.01	6.6	2.3	1.4	0.037	0.00	3.4	4.3	2.8	0.068	0.01
<b>[1000,1000]</b>	94.1	97.4	96.2	0.904	1.00	90.6	97.6	95.7	0.886	0.99	89.0	97.5	95.7	0.877	0.99
	3.4	2.9	3.5	0.086	0.01	4.6	1.6	1.1	0.032	0.00	10.1	1.3	2.3	0.085	0.01
FLT1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	95.6	98.9	97.8	0.950	0.99	91.6	97.8	95.7	0.904	0.98	91.2	97.8	95.6	0.901	0.98
	0.9	0.4	0.1	0.003	0.00	1.7	0.8	0.2	0.004	0.01	2.5	0.9	0.8	0.016	0.01
<b>[1000,1000]</b>	96.2	99.4	98.3	0.963	1.00	91.7	98.2	96.0	0.911	0.99	91.3	97.8	95.5	0.901	0.99
	1.4	0.3	0.3	0.007	0.00	3.5	0.8	0.7	0.016	0.01	4.0	1.1	0.9	0.019	0.01
FLT4	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	95.1	99.1	97.5	0.948	0.99	90.3	98.0	95.2	0.896	0.98	89.5	96.7	93.8	0.871	0.98
	1.2	0.5	0.3	0.007	0.00	6.6	0.8	2.3	0.049	0.01	3.4	2.0	1.2	0.022	0.01
<b>[1000,1000]</b>	96.3	99.5	98.3	0.964	0.99	88.9	98.3	94.8	0.890	0.98	86.9	97.6	93.4	0.862	0.98
	2.0	0.3	0.7	0.015	0.01	7.3	1.2	2.4	0.052	0.01	3.8	1.1	1.2	0.021	0.01

FYN	Train						Validation						Test					
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC			
[100,100]	80.9	99.4	94.4	0.857	0.98	62.6	97.5	87.1	0.682	0.93	58.3	97.2	86.1	0.641	0.92			
	4.1	0.2	0.9	0.026	0.01	5.4	1.4	1.6	0.051	0.01	6.5	1.7	2.1	0.035	0.02			
[1000,1000]	84.4	99.7	95.4	0.885	0.98	64.3	96.3	87.1	0.672	0.92	65.9	97.0	88.2	0.696	0.93			
	3.2	0.3	0.6	0.017	0.01	6.1	2.1	1.0	0.018	0.02	8.1	2.1	1.8	0.051	0.01			
GSK3B	Train						Validation						Test					
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC			
[100,100]	97.1	88.9	94.4	0.872	0.98	94.4	80.1	89.8	0.764	0.95	94.8	79.9	89.8	0.767	0.95			
	1.0	2.9	1.2	0.027	0.00	1.8	2.4	1.1	0.022	0.01	1.6	5.3	1.6	0.031	0.01			
[1000,1000]	98.8	90.6	96.1	0.911	0.99	95.9	78.3	90.1	0.772	0.96	96.2	77.3	89.9	0.769	0.95			
	0.3	3.9	1.1	0.024	0.00	1.3	4.3	0.8	0.019	0.01	1.7	4.4	1.6	0.031	0.01			
HDAC3	Train						Validation						Test					
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC			
[100,100]	97.2	95.0	96.1	0.921	0.99	94.5	93.9	94.2	0.884	0.98	94.5	93.3	93.9	0.877	0.97			
	0.5	0.5	0.1	0.001	0.00	1.0	1.9	1.3	0.026	0.01	1.9	2.0	1.5	0.031	0.01			
[1000,1000]	97.1	96.4	96.8	0.935	0.99	94.1	93.8	94.0	0.879	0.97	94.2	93.5	93.8	0.876	0.97			
	1.0	1.3	0.3	0.006	0.00	2.8	2.2	0.4	0.010	0.01	1.9	1.5	0.8	0.016	0.01			

IGF1R	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	97.6	95.8	97.1	0.932	0.99	96.3	90.8	94.6	0.874	0.99	95.6	92.4	94.5	0.877	0.98
	0.7	1.4	0.3	0.005	0.01	0.9	2.9	0.4	0.013	0.00	1.4	2.6	1.8	0.032	0.01
<b>[1000,1000]</b>	97.6	98.2	97.7	0.948	1.00	95.4	94.9	95.2	0.892	0.99	94.6	95.2	95.0	0.889	0.98
	0.8	1.0	0.3	0.009	0.00	2.3	2.6	1.6	0.033	0.00	3.3	3.0	2.3	0.036	0.01
INSR	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	94.8	98.6	96.9	0.938	0.99	91.8	96.6	94.4	0.888	0.99	90.0	96.5	93.9	0.872	0.99
	1.8	1.0	0.6	0.012	0.01	3.1	2.0	0.6	0.012	0.00	4.1	1.8	1.4	0.033	0.01
<b>[1000,1000]</b>	98.3	99.0	98.7	0.973	1.00	91.2	96.4	94.1	0.881	0.99	92.6	96.5	94.8	0.891	0.99
	0.7	0.4	0.3	0.007	0.00	2.2	1.4	0.8	0.015	0.01	2.5	2.4	1.7	0.037	0.00
KDR	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	97.1	73.6	93.2	0.746	0.97	96.7	68.9	91.9	0.702	0.96	96.6	66.5	91.6	0.679	0.95
	0.7	3.6	0.7	0.028	0.01	0.8	4.1	0.7	0.027	0.01	1.0	7.2	0.6	0.037	0.01
<b>[1000,1000]</b>	97.2	91.0	96.1	0.865	0.99	95.6	82.1	93.3	0.769	0.96	95.7	79.2	92.9	0.747	0.95
	1.2	4.2	0.6	0.015	0.00	2.3	6.4	1.1	0.022	0.01	1.6	6.9	0.9	0.030	0.01

LTB4R	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	86.9	99.8	96.6	0.909	0.99	84.5	99.5	95.3	0.883	0.97	81.0	99.6	95.0	0.864	0.97
	3.4	0.2	0.9	0.024	0.00	6.9	0.4	2.7	0.055	0.01	4.7	0.4	0.5	0.024	0.01
[1000,1000]	91.8	99.9	97.9	0.942	1.00	83.7	99.7	95.4	0.883	0.96	84.4	99.8	95.9	0.892	0.97
	1.8	0.1	0.5	0.013	0.01	4.7	0.4	0.9	0.024	0.01	2.8	0.5	0.7	0.015	0.01
LYN	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	90.7	98.8	96.4	0.914	0.99	79.6	97.8	92.3	0.815	0.97	81.5	98.1	93.1	0.833	0.97
	1.4	0.3	0.3	0.009	0.00	2.6	0.8	1.2	0.031	0.01	3.0	0.7	0.7	0.026	0.01
[1000,1000]	91.9	98.6	96.5	0.918	0.99	82.5	97.8	93.2	0.836	0.97	82.5	98.0	93.4	0.839	0.97
	2.8	0.5	0.5	0.013	0.00	7.2	0.8	2.1	0.053	0.01	4.5	0.7	1.1	0.035	0.01
MAPK1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	45.8	99.0	79.9	0.572	0.85	43.4	98.6	78.6	0.543	0.77	42.4	98.4	78.3	0.531	0.77
	5.2	1.0	1.1	0.021	0.01	2.7	1.6	0.6	0.019	0.01	1.9	1.6	0.8	0.037	0.02
[1000,1000]	49.6	97.8	80.4	0.580	0.86	46.4	96.1	78.5	0.527	0.78	45.0	96.2	77.8	0.514	0.77
	9.5	2.6	1.8	0.031	0.01	6.7	4.3	0.9	0.027	0.01	3.1	4.2	1.4	0.054	0.01

MAPK9	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	97.7	97.6	97.7	0.953	1.00	96.0	93.9	95.0	0.900	0.99	94.3	92.7	93.5	0.870	0.99
	0.5	0.3	0.2	0.005	0.00	1.4	1.4	1.0	0.019	0.01	2.7	2.4	0.8	0.017	0.01
<b>[1000,1000]</b>	98.6	98.9	98.7	0.975	1.00	95.3	94.9	95.1	0.901	0.99	94.2	94.9	94.5	0.891	0.99
	0.6	0.6	0.1	0.002	0.00	0.6	3.2	1.1	0.024	0.00	2.3	2.2	0.4	0.009	0.00
MAPKAPK2	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	93.5	96.8	95.4	0.905	0.99	86.6	93.3	90.5	0.803	0.97	85.7	93.6	90.3	0.800	0.96
	2.5	1.1	0.6	0.012	0.00	1.8	1.8	1.1	0.021	0.01	3.5	2.6	1.5	0.023	0.01
<b>[1000,1000]</b>	94.4	96.7	95.8	0.912	0.99	88.1	93.0	90.9	0.815	0.97	86.2	93.3	90.2	0.799	0.96
	1.5	1.3	0.7	0.014	0.00	1.8	1.5	0.4	0.008	0.01	3.0	2.0	1.3	0.019	0.01
MET	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	98.6	94.3	97.3	0.934	1.00	96.7	89.3	94.6	0.867	0.98	97.1	88.8	94.7	0.869	0.98
	0.2	1.2	0.2	0.006	0.01	1.1	2.0	0.4	0.008	0.01	1.2	2.3	0.7	0.012	0.01
<b>[1000,1000]</b>	98.7	95.4	97.8	0.945	1.00	97.9	89.5	95.5	0.889	0.99	97.4	89.6	95.2	0.882	0.98
	0.3	1.1	0.3	0.007	0.00	0.4	2.3	0.8	0.020	0.00	1.1	2.1	0.6	0.011	0.01

MMP13	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	97.8	93.8	96.5	0.919	0.99	96.7	90.1	94.5	0.876	0.98	96.4	90.7	94.6	0.875	0.98
	0.7	1.6	0.1	0.003	0.00	1.5	3.4	0.8	0.017	0.01	1.5	3.7	0.7	0.019	0.01
<b>[1000,1000]</b>	97.8	95.9	97.2	0.935	0.99	95.6	91.7	94.4	0.871	0.98	96.2	91.7	94.7	0.879	0.98
	0.5	1.4	0.2	0.005	0.00	0.8	3.0	1.2	0.029	0.01	1.0	1.4	0.6	0.015	0.01
MMP2	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	96.4	93.7	95.4	0.900	0.99	94.4	89.3	92.5	0.838	0.98	94.0	87.1	91.5	0.816	0.97
	1.2	1.2	0.6	0.014	0.00	0.6	2.9	0.8	0.019	0.01	0.7	3.2	1.3	0.027	0.01
<b>[1000,1000]</b>	96.5	95.0	95.9	0.913	0.99	93.4	90.6	92.4	0.836	0.98	93.0	89.0	91.5	0.818	0.97
	1.2	1.6	0.4	0.008	0.00	1.9	4.1	0.8	0.017	0.01	2.1	3.1	1.5	0.030	0.00
MMP3	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	96.2	94.4	95.5	0.904	0.99	95.6	91.0	93.9	0.869	0.98	94.9	91.0	93.4	0.857	0.98
	0.7	0.7	0.3	0.007	0.00	1.2	2.7	1.2	0.024	0.01	0.5	1.5	0.7	0.014	0.01
<b>[1000,1000]</b>	96.8	94.5	95.9	0.914	0.99	95.4	93.3	94.7	0.885	0.98	94.5	91.0	93.1	0.852	0.98
	0.9	2.5	0.4	0.010	0.00	2.4	2.5	1.4	0.028	0.01	2.2	4.7	0.8	0.016	0.01

MMP9	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	85.9	94.2	89.3	0.790	0.96	84.4	88.9	86.3	0.725	0.93	83.8	88.8	85.9	0.718	0.92
	1.3	0.7	0.8	0.016	0.00	2.1	1.2	1.2	0.022	0.00	3.0	2.0	1.5	0.026	0.01
[1000,1000]	88.1	93.7	90.4	0.810	0.97	84.4	88.3	86.0	0.720	0.93	83.3	87.3	85.1	0.701	0.93
	1.5	1.3	0.5	0.009	0.00	1.0	2.5	1.3	0.026	0.01	3.5	1.8	1.4	0.020	0.01
NEK2	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	83.9	99.4	95.9	0.880	0.99	71.7	98.2	92.7	0.768	0.96	70.7	98.7	92.7	0.773	0.96
	4.2	0.6	0.5	0.016	0.01	5.7	0.8	0.6	0.039	0.02	8.3	0.7	1.7	0.048	0.04
[1000,1000]	89.1	99.5	97.2	0.918	0.99	74.2	98.1	93.0	0.785	0.96	72.1	98.4	92.8	0.776	0.96
	3.6	0.2	0.7	0.019	0.00	7.0	1.4	1.0	0.042	0.01	9.6	1.0	1.2	0.047	0.04
P2RY1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	96.4	99.4	98.4	0.964	1.00	94.4	98.8	97.3	0.940	0.99	93.6	99.2	97.5	0.941	0.98
	1.0	0.3	0.4	0.009	0.01	1.0	0.2	0.3	0.006	0.00	5.7	0.7	1.5	0.038	0.02
[1000,1000]	97.0	99.3	98.5	0.967	1.00	95.4	99.2	98.0	0.954	0.99	93.8	99.2	97.3	0.940	0.98
	1.9	0.4	0.4	0.010	0.00	3.2	0.6	1.0	0.022	0.01	1.3	1.0	0.7	0.018	0.02

PAK4	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	92.6	99.9	98.0	0.949	0.99	80.7	99.1	94.4	0.850	0.97	79.8	99.0	94.1	0.841	0.97
	2.9	0.1	0.6	0.017	0.00	3.7	0.8	1.6	0.035	0.02	10.2	0.9	2.2	0.060	0.02
<b>[1000,1000]</b>	94.9	99.9	98.6	0.965	0.99	85.5	98.9	95.7	0.881	0.97	83.9	98.5	94.7	0.859	0.97
	2.0	0.1	0.4	0.011	0.01	6.8	1.0	1.1	0.035	0.02	8.1	1.9	2.2	0.058	0.02
PDE4A	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	92.3	98.2	95.9	0.914	0.99	88.0	95.8	92.8	0.848	0.96	84.0	95.8	91.5	0.819	0.96
	1.0	0.5	0.3	0.005	0.00	3.8	1.5	1.5	0.031	0.01	9.9	2.0	2.3	0.059	0.01
<b>[1000,1000]</b>	94.9	99.0	97.4	0.946	1.00	88.0	96.8	93.4	0.861	0.97	85.8	96.3	92.5	0.839	0.97
	0.9	0.5	0.4	0.008	0.00	2.7	2.0	0.3	0.007	0.01	8.4	1.0	2.2	0.054	0.01
PDE5A	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	95.6	94.7	95.2	0.903	0.98	92.6	90.0	91.5	0.827	0.96	92.6	89.4	91.1	0.820	0.95
	1.0	1.6	0.5	0.011	0.00	1.3	2.5	0.9	0.017	0.00	2.0	4.3	1.5	0.028	0.03
<b>[1000,1000]</b>	95.9	97.2	96.5	0.929	0.99	92.4	92.7	92.6	0.850	0.97	92.1	91.0	91.6	0.828	0.96
	1.2	1.3	0.3	0.006	0.00	2.6	2.1	0.7	0.011	0.01	2.3	2.9	1.8	0.032	0.02

PIK3CA	Train						Validation						Test					
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC			
<b>[100,100]</b>	99.3	93.3	97.5	0.940	0.99	99.0	90.1	96.2	0.911	0.99	99.0	90.6	96.5	0.917	0.99			
	0.2	1.5	0.4	0.008	0.01	0.4	2.2	0.6	0.013	0.00	0.7	3.1	0.8	0.019	0.00			
<b>[1000,1000]</b>	99.2	95.8	98.2	0.957	1.00	98.4	92.8	96.7	0.922	0.99	98.6	93.1	96.9	0.926	0.99			
	0.2	1.0	0.3	0.006	0.00	0.5	1.7	0.6	0.015	0.00	0.5	1.2	0.6	0.013	0.00			
PPARG	Train						Validation						Test					
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC			
<b>[100,100]</b>	74.7	96.7	88.5	0.754	0.94	71.3	95.5	86.3	0.710	0.90	71.4	95.3	86.4	0.708	0.90			
	2.9	1.3	0.6	0.012	0.00	3.6	1.8	0.7	0.016	0.01	2.9	2.1	1.1	0.021	0.01			
<b>[1000,1000]</b>	74.0	97.7	88.8	0.763	0.95	71.2	96.1	86.9	0.718	0.91	69.6	96.3	86.3	0.708	0.91			
	2.5	0.6	0.7	0.014	0.01	1.6	0.9	0.7	0.012	0.00	1.0	0.8	1.0	0.021	0.01			
PTPN1	Train						Validation						Test					
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC			
<b>[100,100]</b>	87.0	95.5	92.1	0.836	0.98	76.2	90.3	84.7	0.677	0.92	70.4	87.9	80.8	0.595	0.89			
	1.8	1.4	0.3	0.005	0.01	3.0	2.0	1.8	0.042	0.02	6.3	1.4	2.3	0.043	0.02			
<b>[1000,1000]</b>	85.5	96.3	92.0	0.835	0.98	72.1	90.3	82.7	0.647	0.91	70.2	89.5	82.0	0.619	0.89			
	6.5	2.8	1.1	0.021	0.00	9.9	5.1	2.3	0.038	0.01	5.3	4.1	2.8	0.048	0.01			

PTPN11	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	66.8	98.8	91.7	0.747	0.97	37.0	96.7	82.6	0.455	0.88	39.2	97.5	84.2	0.492	0.89
	13.5	0.7	2.6	0.086	0.01	9.5	2.6	3.1	0.063	0.02	11.0	1.8	2.2	0.054	0.05
[1000,1000]	77.6	97.9	93.4	0.803	0.97	48.4	95.9	84.8	0.536	0.88	50.0	96.5	85.9	0.556	0.88
	2.5	0.7	1.0	0.027	0.00	1.8	2.2	1.8	0.052	0.03	14.2	1.1	2.9	0.103	0.05
PTPN2	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	69.9	99.1	92.9	0.778	0.96	56.1	98.8	88.5	0.667	0.92	47.3	98.9	87.6	0.602	0.92
	3.8	0.2	0.6	0.023	0.01	7.5	0.3	2.0	0.054	0.02	18.9	1.1	3.6	0.129	0.02
[1000,1000]	81.9	99.0	95.3	0.859	0.98	75.0	97.4	92.5	0.770	0.94	64.2	97.7	90.4	0.703	0.93
	2.1	0.5	0.6	0.020	0.00	8.8	1.1	2.1	0.054	0.02	13.7	2.2	2.0	0.075	0.02
RAF1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	98.1	99.0	98.5	0.970	1.00	97.2	96.6	96.9	0.938	0.99	96.8	96.8	96.8	0.934	0.99
	0.5	0.4	0.2	0.005	0.00	0.6	1.6	0.5	0.010	0.01	0.9	2.6	0.8	0.016	0.01
[1000,1000]	98.7	99.4	99.0	0.980	1.00	96.9	97.3	97.1	0.942	1.00	96.2	96.9	96.5	0.929	0.99
	0.6	0.5	0.2	0.004	0.00	1.2	1.2	0.7	0.014	0.00	1.6	2.3	0.3	0.005	0.01

RARA	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	57.5	99.9	95.7	0.735	0.95	53.3	99.9	95.5	0.705	0.90	52.7	99.9	95.3	0.703	0.89
	4.7	0.1	0.5	0.030	0.02	9.0	0.1	0.9	0.062	0.03	7.3	0.1	0.6	0.048	0.03
[1000,1000]	73.0	99.9	97.3	0.835	0.98	64.5	99.8	96.1	0.772	0.91	61.9	99.7	96.0	0.752	0.91
	6.9	0.1	0.5	0.037	0.01	5.9	0.2	0.9	0.045	0.02	2.5	0.1	0.6	0.020	0.03
RARB	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	73.2	100.0	97.8	0.841	0.98	69.4	100.0	97.5	0.815	0.97	70.1	99.9	97.5	0.821	0.97
	13.0	0.0	1.0	0.077	0.01	20.9	0.0	1.7	0.138	0.01	8.1	0.1	0.6	0.048	0.03
[1000,1000]	91.4	99.9	99.2	0.947	0.99	86.7	99.9	98.8	0.919	0.97	85.2	99.8	98.6	0.905	0.96
	1.5	0.1	0.1	0.007	0.00	7.6	0.1	0.7	0.043	0.01	5.4	0.2	0.4	0.028	0.03
ROCK1	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	98.0	96.0	97.0	0.941	0.99	94.2	92.3	93.3	0.866	0.98	95.4	92.5	94.1	0.881	0.98
	0.5	1.1	0.5	0.010	0.01	1.5	1.6	0.9	0.018	0.01	1.3	1.8	0.7	0.015	0.00
[1000,1000]	98.9	96.6	97.9	0.957	1.00	95.7	91.8	93.9	0.877	0.98	95.7	91.6	93.8	0.876	0.98
	0.7	0.8	0.3	0.005	0.00	2.1	2.1	0.7	0.015	0.01	1.8	0.8	1.0	0.019	0.01

RPS6KA5	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	79.6	100.0	96.5	0.873	0.99	60.2	99.9	92.6	0.740	0.96	58.2	99.6	92.2	0.714	0.96
	8.3	0.0	1.3	0.052	0.00	7.1	0.2	1.6	0.043	0.02	8.2	0.6	1.6	0.061	0.01
<b>[1000,1000]</b>	88.8	100.0	98.0	0.931	1.00	65.9	99.8	94.2	0.777	0.96	65.5	99.4	93.5	0.760	0.97
	5.5	0.0	1.0	0.034	0.01	10.1	0.3	1.7	0.067	0.03	13.0	0.8	1.9	0.082	0.01
SIRT2	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	78.5	98.9	94.3	0.833	0.98	65.3	97.8	91.1	0.710	0.93	51.7	97.3	87.8	0.593	0.92
	4.7	0.3	0.9	0.028	0.01	9.1	1.0	2.6	0.075	0.02	17.8	1.2	2.6	0.114	0.03
<b>[1000,1000]</b>	83.0	98.5	95.1	0.855	0.98	67.5	96.0	89.8	0.684	0.93	61.8	96.9	89.6	0.663	0.92
	4.5	0.5	0.8	0.029	0.01	9.5	1.9	2.3	0.043	0.02	13.9	0.9	2.1	0.092	0.03
SIRT3	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	79.3	98.9	96.5	0.833	0.97	71.5	98.0	94.9	0.739	0.95	71.1	98.6	95.6	0.761	0.93
	2.6	0.3	0.3	0.007	0.01	7.8	1.0	1.3	0.058	0.02	18.2	1.3	1.5	0.106	0.04
<b>[1000,1000]</b>	78.4	98.8	96.4	0.825	0.98	73.5	98.5	95.5	0.777	0.95	47.2	99.2	92.0	0.599	0.93
	5.4	0.6	0.2	0.015	0.01	17.0	1.1	1.4	0.091	0.03	20.4	0.8	4.5	0.117	0.04

SRC	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	96.3	91.6	94.6	0.883	0.99	92.5	87.8	90.8	0.803	0.97	92.6	86.8	90.5	0.794	0.96
	1.4	1.4	0.4	0.008	0.00	1.3	3.7	0.6	0.017	0.01	2.0	2.1	1.5	0.027	0.01
<b>[1000,1000]</b>	97.8	94.6	96.6	0.927	0.99	93.3	87.6	91.3	0.811	0.97	93.1	88.0	91.1	0.809	0.97
	0.9	1.9	0.3	0.007	0.00	2.7	2.6	1.4	0.026	0.00	2.0	3.6	0.9	0.014	0.01
TACR2	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	88.8	99.7	96.2	0.913	0.98	86.3	99.2	95.2	0.887	0.97	85.1	99.3	95.0	0.881	0.97
	2.2	0.2	0.5	0.013	0.00	2.5	0.3	0.7	0.020	0.01	3.0	0.7	0.6	0.018	0.01
<b>[1000,1000]</b>	90.2	99.8	96.8	0.926	0.99	87.9	99.3	95.8	0.901	0.97	85.5	99.2	95.1	0.884	0.97
	2.1	0.1	0.6	0.015	0.00	1.9	0.5	0.8	0.016	0.01	4.1	1.0	0.8	0.017	0.01
TBXA2R	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>[100,100]</b>	93.2	97.4	95.9	0.910	0.99	90.9	95.8	94.2	0.870	0.97	90.4	96.0	94.1	0.869	0.97
	1.0	0.6	0.2	0.005	0.01	2.9	1.5	1.0	0.020	0.01	3.1	1.6	0.7	0.015	0.01
<b>[1000,1000]</b>	92.5	98.4	96.4	0.919	0.99	90.6	96.6	94.6	0.881	0.98	89.0	96.7	94.0	0.866	0.97
	2.7	0.9	0.6	0.013	0.00	3.8	2.1	0.6	0.013	0.01	3.5	2.0	0.9	0.020	0.01

TEK	Train					Validation					Test				
	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
[100,100]	96.1	97.7	97.0	0.938	0.99	92.9	96.5	95.1	0.898	0.98	93.2	96.5	95.1	0.897	0.98
	1.1	0.8	0.5	0.010	0.00	1.4	1.2	0.9	0.018	0.01	0.4	2.1	1.1	0.025	0.01
[1000,1000]	97.0	98.8	98.1	0.960	1.00	92.9	96.9	95.3	0.902	0.98	93.3	96.3	95.0	0.896	0.98
	0.3	0.7	0.3	0.007	0.00	2.0	2.0	1.0	0.019	0.01	2.3	1.3	0.9	0.021	0.01
AVERAGE	<b>92.1</b>	<b>96.5</b>	<b>95.8</b>	<b>0.901</b>	<b>0.99</b>	<b>86.9</b>	<b>93.2</b>	<b>92.5</b>	<b>0.822</b>	<b>0.96</b>	<b>86.2</b>	<b>92.9</b>	<b>92.2</b>	<b>0.814</b>	<b>0.96</b>
SD	<b>8.8</b>	<b>4.2</b>	<b>3.1</b>	<b>0.069</b>	<b>0.02</b>	<b>11.7</b>	<b>5.9</b>	<b>4.1</b>	<b>0.091</b>	<b>0.04</b>	<b>12.1</b>	<b>6.5</b>	<b>4.2</b>	<b>0.093</b>	<b>0.04</b>

Table S10. Summary model performance results for each target. In each case standard deviations are shown below averages. Model performances are reported as sensitivity (SE), specificity (SP), accuracy (ACC), Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC). The best model was chosen in each case based on Test set performance, with MCC taking preference.

**AChE**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	496	0	27	392	100.0	6.4	57.2	0.190
22	Test 2	573	2	21	319	99.7	6.2	64.9	0.180
23	Test 3	499	7	74	335	98.6	18.1	62.6	0.292
24	Test 4	528	2	39	346	99.6	10.1	62.0	0.233
25	Test 5	501	4	68	342	99.2	16.6	62.2	0.292
	Avg	519	3	46	347	99.4	11.5	61.8	0.237
	SD	33	3	24	27	0.5	5.6	2.8	0.054

**ADORA2A**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	809	8	318	70	99.0	82.0	93.5	0.852
27	Test 2	826	7	280	92	99.2	75.3	91.8	0.807
28	Test 3	686	9	375	135	98.7	73.5	88.0	0.766
29	Test 4	791	11	313	90	98.6	77.7	91.6	0.812
30	Test 5	783	13	295	114	98.4	72.1	89.5	0.765
	Avg	779	10	316	100	98.8	76.1	90.9	0.800
	SD	55	2	36	25	0.3	3.9	2.1	0.036

**AR**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	484	56	579	865	89.6	40.1	53.6	0.284
22	Test 2	462	76	859	587	85.9	59.4	66.6	0.403

23	Test 3	407	65	881	631	86.2	58.3	64.9	0.379
24	Test 4	467	102	856	559	82.1	60.5	66.7	0.385
25	Test 5	451	67	913	553	87.1	62.3	68.8	0.433
	Avg	454	73	818	639	86.2	56.1	64.1	0.377
	SD	29	18	135	130	2.7	9.1	6.0	0.056

#### KCNH2

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	972	16	139	501	98.4	21.7	68.2	0.334
22	Test 2	948	13	174	493	98.6	26.1	68.9	0.381
23	Test 3	969	19	189	451	98.1	29.5	71.1	0.404
24	Test 4	986	0	0	642	100.0	0.0	60.6	#DIV/0!
25	Test 5	959	13	156	500	98.7	23.8	68.5	0.361
	Avg	967	12	132	517	98.8	20.2	67.5	#DIV/0!
	SD	14	7	76	73	0.7	11.7	4.0	#DIV/0!

#### SLC6A4

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	793	2	157	83	99.7	65.4	91.8	0.763
27	Test 2	851	4	122	58	99.5	67.8	94.0	0.780
28	Test 3	798	8	169	60	99.0	73.8	93.4	0.803
29	Test 4	775	1	154	105	99.9	59.5	89.8	0.720
30	Test 5	806	3	108	118	99.6	47.8	88.3	0.633
	Avg	805	4	142	85	99.6	62.8	91.5	0.740

	SD	28	3	26	27	0.3	9.9	2.4	0.067
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#### ADRA2A

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	145	3	114	109	98.0	51.1	69.8	0.517
22	Test 2	143	6	120	102	96.0	54.1	70.9	0.518
23	Test 3	168	2	113	88	98.8	56.2	75.7	0.593
24	Test 4	184	5	108	74	97.4	59.3	78.7	0.616
25	Test 5	182	4	103	82	97.8	55.7	76.8	0.591
	Avg	164	4	112	91	97.6	55.3	74.4	0.567
	SD	20	2	6	14	1.0	3.0	3.9	0.046

#### ADRB1

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	254	3	127	84	98.8	60.2	81.4	0.656
27	Test 2	211	3	133	121	98.6	52.4	73.5	0.559
28	Test 3	269	6	114	79	97.8	59.1	81.8	0.641
29	Test 4	254	5	139	70	98.1	66.5	84.0	0.696
30	Test 5	253	2	143	70	99.2	67.1	84.6	0.715
	Avg	248	4	131	85	98.5	61.1	81.1	0.653
	SD	22	2	11	21	0.6	6.1	4.4	0.060

#### ADRB2

Model Number	TP	FN	TN	FP	SE	SP	ACC	MCC
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21	Test 1	388	1	45	357	99.7	11.2	54.7	0.234
22	Test 2	388	2	65	336	99.5	16.2	57.3	0.282
23	Test 3	369	5	44	373	98.7	10.6	52.2	0.191
24	Test 4	355	2	71	363	99.4	16.4	53.9	0.272
25	Test 5	426	7	85	273	98.4	23.7	64.6	0.344
	Avg	385	3	62	340	99.1	15.6	56.5	0.264
	SD	27	3	18	40	0.6	5.3	4.9	0.057

#### OPRD1

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	566	2	113	164	99.6	40.8	80.4	0.554
27	Test 2	605	2	81	157	99.7	34.0	81.2	0.509
28	Test 3	602	10	123	110	98.4	52.8	85.8	0.628
29	Test 4	578	4	119	144	99.3	45.2	82.5	0.585
30	Test 5	636	1	66	142	99.8	31.7	83.1	0.503
	Avg	597	4	100	143	99.4	40.9	82.6	0.556
	SD	27	4	25	21	0.6	8.5	2.1	0.052

#### DRD1

	Model Number	TP	FN	TN	FP	SE	SP	ACC	MCC
[100,100]	21	251	7	170	240	97.3	41.5	63.0	0.428
	22	270	15	189	194	94.7	49.3	68.7	0.473
	23	274	7	162	225	97.5	41.9	65.3	0.447
0.4	24	278	7	157	226	97.5	41.0	65.1	0.443

0.001	25	Test 5	237	4	164	263	98.3	38.4	60.0	0.407
100		Avg	262	8	168	230	97.1	42.4	64.4	0.440
		SD	17	4	12	25	1.4	4.1	3.2	0.025

### DRD2

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	1081	3	79	203	99.7	28.0	84.9	0.473
27	Test 2	1120	9	118	119	99.2	49.8	90.6	0.639
28	Test 3	1156	4	108	98	99.7	52.4	92.5	0.679
29	Test 4	1173	2	75	116	99.8	39.3	91.4	0.588
30	Test 5	1140	6	117	103	99.5	53.2	92.0	0.676
	Avg	1134	5	99	128	99.6	44.5	90.3	0.611
	SD	36	3	21	43	0.2	10.8	3.1	0.086

### SLC6A3

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	500	21	207	157	96.0	56.9	79.9	0.595
22	Test 2	468	8	194	215	98.3	47.4	74.8	0.543
23	Test 3	488	11	215	171	97.8	55.7	79.4	0.608
24	Test 4	506	5	202	172	99.0	54.0	80.0	0.619
25	Test 5	497	5	187	196	99.0	48.8	77.3	0.575
	Avg	492	10	201	182	98.0	52.6	78.3	0.588
	SD	15	7	11	23	1.3	4.2	2.2	0.030

**EDNRA**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	257	0	158	72	100.0	68.7	85.2	0.733
22	Test 2	220	1	208	58	99.5	78.2	87.9	0.782
23	Test 3	251	1	155	80	99.6	66.0	83.4	0.702
24	Test 4	270	12	135	70	95.7	65.9	83.2	0.662
25	Test 5	268	5	142	72	98.2	66.4	84.2	0.698
	Avg	253	4	160	70	98.6	69.0	84.8	0.715
	SD	20	5	29	8	1.7	5.3	1.9	0.045

**NR3C1**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	611	45	487	855	93.1	36.3	55.0	0.313
22	Test 2	537	78	935	448	87.3	67.6	73.7	0.507
23	Test 3	499	74	859	566	87.1	60.3	68.0	0.429
24	Test 4	552	61	767	618	90.0	55.4	66.0	0.425
25	Test 5	514	47	704	733	91.6	49.0	61.0	0.377
	Avg	543	61	750	644	89.8	53.7	64.7	0.410
	SD	43	15	172	156	2.6	11.9	7.1	0.072

**HRH1**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	271	1	107	97	99.6	52.5	79.4	0.615
27	Test 2	253	3	138	82	98.8	62.7	82.1	0.672

28	Test 3	274	4	135	63	98.6	68.2	85.9	0.723
29	Test 4	230	4	146	96	98.3	60.3	79.0	0.631
30	Test 5	228	7	122	119	97.0	50.6	73.5	0.536
	Avg	251	4	130	91	98.5	58.9	80.0	0.636
	SD	22	2	15	21	1.0	7.3	4.6	0.070

#### OPRM1

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	714	8	305	156	98.9	66.2	86.1	0.719
22	Test 2	720	14	307	142	98.1	68.4	86.8	0.725
23	Test 3	739	10	277	157	98.7	63.8	85.9	0.703
24	Test 4	678	5	319	181	99.3	63.8	84.3	0.699
25	Test 5	716	6	302	159	99.2	65.5	86.1	0.719
	Avg	713	9	302	159	98.8	65.5	85.8	0.713
	SD	22	4	15	14	0.5	1.9	0.9	0.012

#### CHRM1

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	362	6	147	136	98.4	51.9	78.2	0.588
27	Test 2	362	3	103	183	99.2	36.0	71.4	0.473
28	Test 3	417	4	103	127	99.0	44.8	79.9	0.565
29	Test 4	431	2	122	96	99.5	56.0	84.9	0.667
30	Test 5	426	1	112	112	99.8	50.0	82.6	0.624
	Avg	400	3	117	131	99.2	47.7	79.4	0.584

SD 35 2 18 33 0.5 7.7 5.2 0.073

CHRM2

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	330	4	223	176	98.8	55.9	75.4	0.589
27	Test 2	317	7	315	94	97.8	77.0	86.2	0.749
28	Test 3	313	5	286	129	98.4	68.9	81.7	0.682
29	Test 4	329	5	275	124	98.5	68.9	82.4	0.691
30	Test 5	317	6	263	147	98.1	64.1	79.1	0.642
	Avg	321	5	272	134	98.3	67.0	81.0	0.671
	SD	8	1	34	30	0.4	7.7	4.0	0.060

CHRM3

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	302	1	126	101	99.7	55.5	80.8	0.640
27	Test 2	303	7	132	88	97.7	60.0	82.1	0.647
28	Test 3	322	5	106	97	98.5	52.2	80.8	0.606
29	Test 4	304	0	95	131	100.0	42.0	75.3	0.542
30	Test 5	291	2	128	109	99.3	54.0	79.1	0.616
	Avg	304	3	117	105	99.0	52.8	79.6	0.610
	SD	11	3	16	16	0.9	6.6	2.6	0.042

SLC6A2

**Model Number**      **TP**      **FN**      **TN**      **FP**      **SE**      **SP**      **ACC**      **MCC**

26	Test 1	595	7	196	172	98.8	53.3	81.5	0.621
27	Test 2	557	13	236	164	97.7	59.0	81.8	0.639
28	Test 3	571	5	172	222	99.1	43.7	76.6	0.544
29	Test 4	559	6	198	207	98.9	48.9	78.0	0.579
30	Test 5	590	7	176	197	98.8	47.2	79.0	0.572
	Avg	574	8	196	192	98.7	50.4	79.4	0.591
	SD	17	3	25	24	0.6	5.9	2.2	0.039

#### HTR2A

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	753	1	93	111	99.9	45.6	88.3	0.626
27	Test 2	743	2	96	117	99.7	45.1	87.6	0.615
28	Test 3	759	2	68	129	99.7	34.5	86.3	0.532
29	Test 4	753	3	82	120	99.6	40.6	87.2	0.577
30	Test 5	739	2	91	126	99.7	41.9	86.6	0.589
	Avg	749	2	86	121	99.7	41.5	87.2	0.588
	SD	8	1	11	7	0.1	4.5	0.8	0.037

#### HTR3A

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	92	6	142	61	93.9	70.0	77.7	0.598
27	Test 2	100	1	160	40	99.0	80.0	86.4	0.748
28	Test 3	79	3	189	30	96.3	86.3	89.0	0.766
29	Test 4	81	2	171	47	97.6	78.4	83.7	0.687

	30	Test 5	78	9	175	39	89.7	81.8	84.1	0.664
		Avg	86	4	167	43	95.3	79.3	84.2	0.693
		SD	10	3	18	12	3.7	6.0	4.2	0.067

#### LCK

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	362	1	14	74	99.7	15.9	83.4	0.346
27	Test 2	364	0	13	74	100.0	14.9	83.6	0.352
28	Test 3	362	0	7	82	100.0	7.9	81.8	0.253
29	Test 4	344	0	6	101	100.0	5.6	77.6	0.208
30	Test 5	298	1	20	132	99.7	13.2	70.5	0.288
	Avg	346	0	12	93	99.9	11.5	79.4	0.289
	SD	28	1	6	25	0.2	4.5	5.5	0.061

#### AVPR1A

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	131	1	161	42	99.2	79.3	87.2	0.768
27	Test 2	108	2	186	39	98.2	82.7	87.8	0.765
28	Test 3	116	2	183	34	98.3	84.3	89.3	0.794
29	Test 4	139	3	157	36	97.9	81.3	88.4	0.784
30	Test 5	116	1	166	52	99.1	76.1	84.2	0.718
	Avg	122	2	171	41	98.6	80.8	87.3	0.766
	SD	13	1	13	7	0.6	3.2	1.9	0.029

**AGTR1**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	193	7	164	33	96.5	83.2	89.9	0.805
27	Test 2	157	2	149	89	98.7	62.6	77.1	0.619
28	Test 3	160	10	154	73	94.1	67.8	79.1	0.623
29	Test 4	169	4	172	52	97.7	76.8	85.9	0.743
30	Test 5	99	5	216	77	95.2	73.7	79.3	0.610
	Avg	156	6	171	65	96.4	72.8	82.3	0.680
	SD	35	3	27	22	1.9	8.0	5.4	0.089

**AKT1**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	614	3	93	87	99.5	51.7	88.7	0.657
27	Test 2	563	7	126	101	98.8	55.5	86.4	0.657
28	Test 3	548	2	122	125	99.6	49.4	84.1	0.626
29	Test 4	518	3	158	118	99.4	57.2	84.8	0.672
30	Test 5	504	3	148	142	99.4	51.0	81.8	0.619
	Avg	549	4	129	115	99.4	53.0	85.2	0.646
	SD	43	2	25	21	0.3	3.3	2.6	0.023

**BACE1**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	1275	4	164	281	99.7	36.9	83.5	0.539
27	Test 2	1186	6	243	289	99.5	45.7	82.9	0.594

28	Test 3	1166	12	354	192	99.0	64.8	88.2	0.726
29	Test 4	1205	8	283	228	99.3	55.4	86.3	0.667
30	Test 5	1140	14	353	217	98.8	61.9	86.6	0.698
	Avg	1194	9	279	241	99.3	52.9	85.5	0.645
	SD	51	4	80	42	0.4	11.6	2.2	0.077

#### BCHE

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	267	14	254	174	95.0	59.3	73.5	0.548
27	Test 2	268	1	185	255	99.6	42.0	63.9	0.460
28	Test 3	297	11	251	150	96.4	62.6	77.3	0.606
29	Test 4	275	6	222	206	97.9	51.9	70.1	0.521
30	Test 5	250	11	252	196	95.8	56.3	70.8	0.520
	Avg	271	9	233	196	96.9	54.4	71.1	0.531
	SD	17	5	30	39	1.8	8.0	4.9	0.053

#### CASP1

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	239	14	321	339	94.5	48.6	61.3	0.400
22	Test 2	224	27	388	274	89.2	58.6	67.0	0.429
23	Test 3	269	11	289	344	96.1	45.7	61.1	0.410
24	Test 4	274	17	308	314	94.2	49.5	63.7	0.425
25	Test 5	264	30	315	304	89.8	50.9	63.4	0.392
	Avg	254	20	324	315	92.7	50.7	63.3	0.411

	SD	22	8	38	28	3.0	4.8	2.4	0.016
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### CASP3

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	253	12	202	134	95.5	60.1	75.7	0.576
22	Test 2	241	6	179	175	97.6	50.6	69.9	0.513
23	Test 3	202	1	186	212	99.5	46.7	64.6	0.472
24	Test 4	229	6	159	207	97.4	43.4	64.6	0.447
25	Test 5	226	1	138	236	99.6	36.9	60.6	0.419
	Avg	230	5	173	193	97.9	47.6	67.1	0.486
	SD	19	5	25	39	1.7	8.6	5.9	0.061

### CASP8

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	59	6	222	5	90.8	97.8	96.2	0.891
27	Test 2	51	8	218	15	86.4	93.6	92.1	0.768
28	Test 3	64	1	214	13	98.5	94.3	95.2	0.875
29	Test 4	51	4	232	5	92.7	97.9	96.9	0.900
30	Test 5	79	7	193	13	91.9	93.7	93.2	0.839
	Avg	61	5	216	10	92.1	95.4	94.7	0.855
	SD	12	3	14	5	4.3	2.2	2.0	0.054

### CHRM5

Model Number	TP	FN	TN	FP	SE	SP	ACC	MCC
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26	Test 1	139	1	131	81	99.3	61.8	76.7	0.617
27	Test 2	152	2	115	83	98.7	58.1	75.9	0.598
28	Test 3	127	2	134	89	98.4	60.1	74.1	0.579
29	Test 4	116	2	144	90	98.3	61.5	73.9	0.573
30	Test 5	131	7	155	59	94.9	72.4	81.3	0.660
	Avg	133	3	136	80	97.9	62.8	76.4	0.606
	SD	13	2	15	13	1.7	5.6	3.0	0.035

### CHUK

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	70	0	155	52	100.0	74.9	81.2	0.655
27	Test 2	76	1	176	24	98.7	88.0	91.0	0.809
28	Test 3	61	1	169	46	98.4	78.6	83.0	0.659
29	Test 4	45	1	199	32	97.8	86.1	88.1	0.698
30	Test 5	59	2	165	51	96.7	76.4	80.9	0.619
	Avg	62	1	173	41	98.3	80.8	84.8	0.688
	SD	12	1	16	12	1.2	5.9	4.5	0.073

### CSF1R

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	275	0	126	76	100.0	62.4	84.1	0.699
22	Test 2	269	0	119	89	100.0	57.2	81.3	0.656
23	Test 3	267	2	133	75	99.3	63.9	83.9	0.696
24	Test 4	267	4	113	93	98.5	54.9	79.7	0.615

25	Test 5	250	2	148	77	99.2	65.8	83.4	0.699
	Avg	266	2	128	82	99.4	60.8	82.5	0.673
	SD	9	2	14	8	0.6	4.6	1.9	0.037

### CSNK1D

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	144	3	111	89	98.0	55.5	73.5	0.562
22	Test 2	131	1	110	105	99.2	51.2	69.5	0.525
23	Test 3	142	3	119	83	97.9	58.9	75.2	0.587
24	Test 4	139	0	112	96	100.0	53.8	72.3	0.564
25	Test 5	141	4	123	79	97.2	60.9	76.1	0.595
	Avg	139	2	115	90	98.5	56.1	73.3	0.567
	SD	5	2	6	10	1.1	3.9	2.6	0.027

### EDNRB

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	218	0	145	46	100.0	75.9	88.8	0.792
27	Test 2	159	0	169	81	100.0	67.6	80.2	0.669
28	Test 3	145	0	200	64	100.0	75.8	84.4	0.725
29	Test 4	167	0	190	52	100.0	78.5	87.3	0.774
30	Test 5	119	1	229	60	99.2	79.2	85.1	0.720
	Avg	162	0	187	61	99.8	75.4	85.1	0.736
	SD	36	0	32	13	0.4	4.6	3.3	0.048

**ELANE**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	480	1	60	160	99.8	27.3	77.0	0.446
22	Test 2	438	3	85	175	99.3	32.7	74.6	0.467
23	Test 3	442	0	59	200	100.0	22.8	71.5	0.396
24	Test 4	366	3	128	204	99.2	38.6	70.5	0.483
25	Test 5	400	1	72	228	99.8	24.0	67.3	0.385
	Avg	425	2	81	193	99.6	29.1	72.2	0.435
	SD	44	1	28	26	0.3	6.5	3.8	0.043

**EPHA2**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	165	2	118	41	98.8	74.2	86.8	0.757
27	Test 2	97	3	204	22	97.0	90.3	92.3	0.836
28	Test 3	78	0	199	49	100.0	80.2	85.0	0.702
29	Test 4	105	2	162	57	98.1	74.0	81.9	0.677
30	Test 5	74	2	212	38	97.4	84.8	87.7	0.732
	Avg	104	2	179	41	98.3	80.7	86.7	0.741
	SD	37	1	39	13	1.2	7.0	3.8	0.061

**FGFR1**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	536	0	79	59	100.0	57.2	91.2	0.718
22	Test 2	421	1	103	149	99.8	40.9	77.7	0.544

23	Test 3	416	2	89	167	99.5	34.8	74.9	0.487
24	Test 4	394	10	130	140	97.5	48.1	77.7	0.552
25	Test 5	383	0	119	172	100.0	40.9	74.5	0.531
	Avg	430	3	104	137	99.4	44.4	79.2	0.566
	SD	61	4	21	46	1.0	8.6	6.9	0.088

#### FKBP1A

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	83	1	174	14	98.8	92.6	94.5	0.881
22	Test 2	99	2	155	16	98.0	90.6	93.4	0.867
23	Test 3	53	1	174	44	98.1	79.8	83.5	0.649
24	Test 4	61	0	193	18	100.0	91.5	93.4	0.840
25	Test 5	54	0	204	14	100.0	93.6	94.9	0.862
	Avg	70	1	180	21	99.0	89.6	91.9	0.820
	SD	20	1	19	13	1.0	5.6	4.8	0.097

#### FLT1

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	205	1	330	97	99.5	77.3	84.5	0.720
22	Test 2	241	5	296	91	98.0	76.5	84.8	0.727
23	Test 3	220	4	299	110	98.2	73.1	82.0	0.683
24	Test 4	202	2	351	78	99.0	81.8	87.4	0.761
25	Test 5	202	6	347	78	97.1	81.6	86.7	0.745
	Avg	214	4	325	91	98.4	78.1	85.1	0.727

	SD	17	2	26	14	0.9	3.7	2.1	0.029
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#### FLT4

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	149	2	147	53	98.7	73.5	84.3	0.723
22	Test 2	123	0	124	104	100.0	54.4	70.4	0.543
23	Test 3	128	6	159	58	95.5	73.3	81.8	0.670
24	Test 4	133	1	118	99	99.3	54.4	71.5	0.550
25	Test 5	130	2	149	70	98.5	68.0	79.5	0.651
	Avg	133	2	139	77	98.4	64.7	77.5	0.627
	SD	10	2	18	23	1.7	9.7	6.2	0.078

#### FYN

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	95	6	120	78	94.1	60.6	71.9	0.524
27	Test 2	72	1	143	83	98.6	63.3	71.9	0.532
28	Test 3	78	11	181	29	87.6	86.2	86.6	0.704
29	Test 4	81	9	142	67	90.0	67.9	74.6	0.532
30	Test 5	63	4	140	92	94.0	60.3	67.9	0.454
	Avg	78	6	145	70	92.9	67.7	74.6	0.549
	SD	12	4	22	25	4.2	10.8	7.1	0.093

#### GSK3B

Model Number	TP	FN	TN	FP	SE	SP	ACC	MCC
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26	Test 1	522	1	96	142	99.8	40.3	81.2	0.558
27	Test 2	489	2	56	214	99.6	20.7	71.6	0.367
28	Test 3	490	4	113	154	99.2	42.3	79.2	0.549
29	Test 4	500	2	108	151	99.6	41.7	79.9	0.557
30	Test 5	537	2	85	137	99.6	38.3	81.7	0.542
	Avg	508	2	92	160	99.6	36.7	78.7	0.514
	SD	21	1	23	31	0.2	9.0	4.1	0.083

### HDAC3

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	209	3	149	77	98.6	65.9	81.7	0.677
22	Test 2	206	3	146	83	98.6	63.8	80.4	0.657
23	Test 3	225	2	135	76	99.1	64.0	82.2	0.680
24	Test 4	183	4	146	105	97.9	58.2	75.1	0.584
25	Test 5	214	2	132	90	99.1	59.5	79.0	0.635
	Avg	207	3	142	86	98.6	62.3	79.7	0.647
	SD	15	1	8	12	0.5	3.3	2.8	0.039

### IGF1R

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	585	3	72	63	99.5	53.3	90.9	0.675
27	Test 2	470	3	176	74	99.4	70.4	89.3	0.769
28	Test 3	521	2	135	65	99.6	67.5	90.7	0.766
29	Test 4	454	2	187	80	99.6	70.0	88.7	0.764

30	Test 5	435	8	186	94	98.2	66.4	85.9	0.710
	Avg	493	4	151	75	99.2	65.5	89.1	0.737
	SD	61	3	49	13	0.6	7.0	2.0	0.042

## INSR

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	255	1	109	31	99.6	77.9	91.9	0.827
27	Test 2	166	2	173	55	98.8	75.9	85.6	0.743
28	Test 3	143	2	165	86	98.6	65.7	77.8	0.628
29	Test 4	139	1	188	68	99.3	73.4	82.6	0.696
30	Test 5	177	1	177	41	99.4	81.2	89.4	0.806
	Avg	176	1	162	56	99.2	74.8	85.5	0.740
	SD	47	1	31	22	0.4	5.8	5.6	0.081

## KDR

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	1629	4	21	225	99.8	8.5	87.8	0.244
27	Test 2	1526	20	151	182	98.7	45.3	89.2	0.585
28	Test 3	1576	6	33	264	99.6	11.1	85.6	0.275
29	Test 4	1485	2	44	348	99.9	11.2	81.4	0.292
30	Test 5	1563	5	69	242	99.7	22.2	86.9	0.418
	Avg	1556	7	64	252	99.5	19.7	86.2	0.363
	SD	54	7	52	61	0.5	15.3	3.0	0.141

**LTB4R**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	52	3	190	31	94.5	86.0	87.7	0.701
27	Test 2	66	5	175	30	93.0	85.4	87.3	0.719
28	Test 3	74	5	168	29	93.7	85.3	87.7	0.738
29	Test 4	71	4	188	13	94.7	93.5	93.8	0.853
30	Test 5	66	4	199	7	94.3	96.6	96.0	0.897
	Avg	66	4	184	22	94.0	89.4	90.5	0.781
	SD	8	1	12	11	0.7	5.3	4.1	0.087

**LYN**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	99	3	135	63	97.1	68.2	78.0	0.620
27	Test 2	78	2	167	53	97.5	75.9	81.7	0.655
28	Test 3	90	3	177	30	96.8	85.5	89.0	0.777
29	Test 4	96	2	179	23	98.0	88.6	91.7	0.830
30	Test 5	79	2	164	55	97.5	74.9	81.0	0.647
	Avg	88	2	164	45	97.4	78.6	84.3	0.706
	SD	10	1	18	17	0.5	8.3	5.8	0.092

**MAPK1**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	1293	31	157	1976	97.7	7.4	41.9	0.108
22	Test 2	1233	12	99	2113	99.0	4.5	38.5	0.096

23	Test 3	1202	0	0	2255	100.0	0.0	34.8	#DIV/0!
24	Test 4	1202	0	21	2234	100.0	0.9	35.4	0.057
25	Test 5	1236	0	0	2221	100.0	0.0	35.8	#DIV/0!
	Avg	1233	9	55	2160	99.3	2.6	37.3	#DIV/0!
	SD	37	14	70	116	1.0	3.3	3.0	#DIV/0!

### MAPK9

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	261	0	131	71	100.0	64.9	84.7	0.714
27	Test 2	237	1	173	52	99.6	76.9	88.6	0.789
28	Test 3	240	2	153	68	99.2	69.2	84.9	0.724
29	Test 4	237	0	152	74	100.0	67.3	84.0	0.716
30	Test 5	246	3	169	45	98.8	79.0	89.6	0.802
	Avg	244	1	156	62	99.5	71.4	86.3	0.749
	SD	10	1	17	13	0.5	6.2	2.6	0.043

### MAPKAPK2

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	161	3	131	102	98.2	56.2	73.6	0.566
22	Test 2	175	2	147	73	98.9	66.8	81.1	0.674
23	Test 3	162	3	108	124	98.2	46.6	68.0	0.491
24	Test 4	133	3	170	91	97.8	65.1	76.3	0.602
25	Test 5	184	3	137	73	98.4	65.2	80.9	0.665
	Avg	163	3	139	93	98.3	60.0	76.0	0.600

SD 19 0 23 21 0.4 8.6 5.5 0.075

MET

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	601	1	93	108	99.8	46.3	86.4	0.621
27	Test 2	541	0	127	135	100.0	48.5	83.2	0.623
28	Test 3	564	3	126	110	99.5	53.4	85.9	0.656
29	Test 4	580	3	132	88	99.5	60.0	88.7	0.709
30	Test 5	576	2	143	82	99.7	63.6	89.5	0.738
	Avg	572	2	124	105	99.7	54.3	86.7	0.669
	SD	22	1	19	21	0.2	7.4	2.5	0.052

MMP13

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	487	5	124	84	99.0	59.6	87.3	0.691
27	Test 2	465	5	141	89	98.9	61.3	86.6	0.696
28	Test 3	482	4	129	85	99.2	60.3	87.3	0.698
29	Test 4	473	3	105	119	99.4	46.9	82.6	0.597
30	Test 5	462	2	123	113	99.6	52.1	83.6	0.638
	Avg	474	4	124	98	99.2	56.0	85.5	0.664
	SD	11	1	13	17	0.3	6.3	2.2	0.045

MMP2

Model Number TP FN TN FP SE SP ACC MCC

26	Test 1	602	5	164	152	99.2	51.9	83.0	0.627
27	Test 2	582	10	182	149	98.3	55.0	82.8	0.630
28	Test 3	594	5	205	119	99.2	63.3	86.6	0.711
29	Test 4	567	4	162	190	99.3	46.0	79.0	0.573
30	Test 5	564	5	210	144	99.1	59.3	83.9	0.672
	Avg	582	6	185	151	99.0	55.1	83.0	0.643
	SD	17	2	22	25	0.4	6.7	2.7	0.052

### MMP3

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	376	5	90	88	98.7	50.6	83.4	0.611
22	Test 2	367	0	80	112	100.0	41.7	80.0	0.565
23	Test 3	370	6	90	93	98.4	49.2	82.3	0.592
24	Test 4	307	1	119	132	99.7	47.4	76.2	0.570
25	Test 5	322	5	93	139	98.5	40.1	74.2	0.500
	Avg	348	3	94	113	99.0	45.8	79.2	0.568
	SD	32	3	15	23	0.7	4.6	3.9	0.042

### MMP9

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	548	2	34	302	99.6	10.1	65.7	0.240
22	Test 2	488	1	41	356	99.8	10.3	59.7	0.237
23	Test 3	514	0	24	348	100.0	6.5	60.7	0.196
24	Test 4	517	2	22	345	99.6	6.0	60.8	0.170

25	Test 5	510	0	0	376	100.0	0.0	57.6	#DIV/0!
	Avg	515	1	24	345	99.8	6.6	60.9	#DIV/0!
	SD	21	1	16	27	0.2	4.2	3.0	#DIV/0!

## NEK2

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	72	1	159	39	98.6	80.3	85.2	0.712
27	Test 2	72	2	130	67	97.3	66.0	74.5	0.564
28	Test 3	53	1	162	55	98.1	74.7	79.3	0.594
29	Test 4	44	0	165	62	100.0	72.7	77.1	0.549
30	Test 5	44	9	175	43	83.0	80.3	80.8	0.538
	Avg	57	3	158	53	95.4	74.8	79.4	0.591
	SD	14	4	17	12	7.0	6.0	4.0	0.071

## P2RY1

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	109	2	189	32	98.2	85.5	89.8	0.799
22	Test 2	137	0	180	15	100.0	92.3	95.5	0.912
23	Test 3	81	4	216	31	95.3	87.4	89.5	0.764
24	Test 4	123	0	184	25	100.0	88.0	92.5	0.855
30	Test 5	100	4	204	24	96.2	89.5	91.6	0.821
	Avg	110	2	195	25	97.9	88.6	91.7	0.830
	SD	21	2	15	7	2.2	2.5	2.4	0.057

**PAK4**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	94	3	169	30	96.9	84.9	88.9	0.779
27	Test 2	64	2	197	33	97.0	85.7	88.2	0.733
28	Test 3	75	3	195	23	96.2	89.4	91.2	0.801
29	Test 4	69	1	185	41	98.6	81.9	85.8	0.707
30	Test 5	66	3	170	57	95.7	74.9	79.7	0.605
	Avg	74	2	183	37	96.9	83.4	86.8	0.725
	SD	12	1	13	13	1.1	5.4	4.4	0.077

**PDE4A**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	128	3	114	89	97.7	56.2	72.5	0.551
27	Test 2	142	3	139	50	97.9	73.5	84.1	0.717
28	Test 3	108	2	168	56	98.2	75.0	82.6	0.688
29	Test 4	122	7	141	64	94.6	68.8	78.7	0.621
30	Test 5	131	7	157	39	94.9	80.1	86.2	0.739
	Avg	126	4	144	60	96.7	70.7	80.8	0.663
	SD	12	2	20	19	1.8	9.1	5.4	0.077

**PDE5A**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	280	5	156	104	98.2	60.0	80.0	0.638
27	Test 2	300	5	132	108	98.4	55.0	79.3	0.611

28	Test 3	286	7	137	115	97.6	54.4	77.6	0.588
29	Test 4	346	7	95	97	98.0	49.5	80.9	0.582
30	Test 5	308	7	139	91	97.8	60.4	82.0	0.649
	Avg	304	6	132	103	98.0	55.9	80.0	0.613
	SD	26	1	22	9	0.3	4.5	1.7	0.030

### PIK3CA

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	989	5	296	72	99.5	80.4	94.3	0.855
27	Test 2	915	0	359	88	100.0	80.3	93.5	0.856
28	Test 3	858	4	377	123	99.5	75.4	90.7	0.805
29	Test 4	970	3	281	108	99.7	72.2	91.9	0.800
30	Test 5	975	5	311	71	99.5	81.4	94.4	0.861
	Avg	941	3	325	92	99.6	78.0	93.0	0.835
	SD	54	2	41	23	0.2	4.0	1.6	0.030

### PPARG

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	854	14	326	1135	98.4	22.3	50.7	0.283
22	Test 2	867	24	465	973	97.3	32.3	57.2	0.354
23	Test 3	770	36	620	903	95.5	40.7	59.7	0.383
24	Test 4	808	51	601	869	94.1	40.9	60.5	0.376
30	Test 5	894	44	590	801	95.3	42.4	63.7	0.416
	Avg	839	34	520	936	96.1	35.7	58.4	0.362

SD      49      15      125      127      1.7      8.5      4.9      0.049

PTPN1

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	302	18	196	214	94.4	47.8	68.2	0.460
27	Test 2	333	5	119	273	98.5	30.4	61.9	0.383
28	Test 3	271	9	155	295	96.8	34.4	58.4	0.364
29	Test 4	287	10	231	202	96.6	53.3	71.0	0.522
30	Test 5	223	13	307	187	94.5	62.1	72.6	0.534
	Avg	283	11	202	234	96.2	45.6	66.4	0.453
	SD	41	5	72	47	1.7	13.2	6.1	0.078

PTPN11

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	75	7	136	95	91.5	58.9	67.4	0.444
27	Test 2	56	9	159	89	86.2	64.1	68.7	0.409
28	Test 3	52	8	167	86	86.7	66.0	70.0	0.418
29	Test 4	55	17	164	77	76.4	68.0	70.0	0.379
30	Test 5	74	1	133	105	98.7	55.9	66.1	0.471
	Avg	62	8	152	90	87.9	62.6	68.4	0.424
	SD	11	6	16	10	8.1	5.1	1.7	0.035

PTPN2

Model Number TP FN TN FP SE SP ACC MCC

26	Test 1	69	7	196	37	90.8	84.1	85.8	0.680
27	Test 2	62	3	178	66	95.4	73.0	77.7	0.565
28	Test 3	69	2	172	66	97.2	72.3	78.0	0.589
29	Test 4	53	11	190	55	82.8	77.6	78.6	0.513
30	Test 5	60	3	185	61	95.2	75.2	79.3	0.581
	Avg	63	5	184	57	92.3	76.4	79.9	0.586
	SD	7	4	9	12	5.8	4.8	3.4	0.060

### RAF1

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	276	3	155	53	98.9	74.5	88.5	0.776
22	Test 2	306	1	130	50	99.7	72.2	89.5	0.783
23	Test 3	265	0	119	103	100.0	53.6	78.9	0.621
24	Test 4	269	1	130	87	99.6	59.9	81.9	0.667
30	Test 5	230	0	175	82	100.0	68.1	83.2	0.708
	Avg	269	1	142	75	99.6	65.7	84.4	0.711
	SD	27	1	23	23	0.4	8.7	4.5	0.069

### RARA

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	63	25	603	30	71.6	95.3	92.4	0.653
27	Test 2	51	19	622	29	72.9	95.5	93.3	0.645
28	Test 3	57	14	579	71	80.3	89.1	88.2	0.541
29	Test 4	47	15	645	14	75.8	97.9	96.0	0.742

30	Test 5	46	19	591	65	70.8	90.1	88.3	0.483
	Avg	53	18	608	42	74.3	93.6	91.7	0.613
	SD	7	4	26	25	3.9	3.8	3.3	0.102

### RARB

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	55	4	642	28	93.2	95.8	95.6	0.765
27	Test 2	52	7	663	7	88.1	99.0	98.1	0.871
28	Test 3	59	4	659	7	93.7	98.9	98.5	0.907
29	Test 4	55	3	663	8	94.8	98.8	98.5	0.902
30	Test 5	52	7	658	12	88.1	98.2	97.4	0.832
	Avg	55	5	657	12	91.6	98.1	97.6	0.855
	SD	3	2	9	9	3.2	1.3	1.2	0.059

### ROCK1

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	281	1	109	91	99.6	54.5	80.9	0.636
22	Test 2	272	0	131	79	100.0	62.4	83.6	0.695
23	Test 3	237	1	138	106	99.6	56.6	77.8	0.620
24	Test 4	263	0	132	87	100.0	60.3	82.0	0.673
30	Test 5	236	2	162	82	99.2	66.4	82.6	0.692
	Avg	258	1	134	89	99.7	60.0	81.4	0.663
	SD	20	1	19	11	0.3	4.7	2.2	0.034

**RPS6KA5**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	47	3	183	19	94.0	90.6	91.3	0.767
27	Test 2	38	2	191	21	95.0	90.1	90.9	0.734
28	Test 3	45	3	156	48	93.8	76.5	79.8	0.571
29	Test 4	44	1	180	27	97.8	87.0	88.9	0.721
30	Test 5	39	2	186	25	95.1	88.2	89.3	0.706
	Avg	43	2	179	28	95.1	86.5	88.0	0.700
	SD	4	1	14	12	1.6	5.8	4.7	0.075

**SIRT2**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	90	3	163	73	96.8	69.1	76.9	0.593
27	Test 2	62	8	171	88	88.6	66.0	70.8	0.449
28	Test 3	45	11	217	56	80.4	79.5	79.6	0.488
29	Test 4	74	2	168	85	97.4	66.4	73.6	0.538
30	Test 5	60	6	201	62	90.9	76.4	79.3	0.558
	Avg	66	6	184	73	90.8	71.5	76.0	0.525
	SD	17	4	24	14	6.9	6.1	3.8	0.057

**SIRT3**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	45	3	188	9	93.8	95.4	95.1	0.854
22	Test 2	30	4	200	11	88.2	94.8	93.9	0.769

23	Test 3	12	3	216	14	80.0	93.9	93.1	0.575
24	Test 4	22	5	211	7	81.5	96.8	95.1	0.759
25	Test 5	19	8	213	5	70.4	97.7	94.7	0.717
	Avg	26	5	206	9	82.8	95.7	94.4	0.735
	SD	13	2	12	3	8.9	1.5	0.9	0.102

### SRC

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	544	2	115	186	99.6	38.2	77.8	0.525
27	Test 2	506	3	149	189	99.4	44.1	77.3	0.555
28	Test 3	500	0	175	172	100.0	50.4	79.7	0.613
29	Test 4	580	1	174	92	99.8	65.4	89.0	0.748
30	Test 5	562	6	171	108	98.9	61.3	86.5	0.696
	Avg	538	2	157	149	99.6	51.9	82.1	0.627
	SD	35	2	26	46	0.4	11.4	5.4	0.094

### TACR2

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	169	9	311	69	94.9	81.8	86.0	0.724
27	Test 2	177	11	344	26	94.1	93.0	93.4	0.856
28	Test 3	137	10	361	50	93.2	87.8	89.2	0.756
29	Test 4	128	11	383	36	92.1	91.4	91.6	0.793
30	Test 5	216	8	280	54	96.4	83.8	88.9	0.787
	Avg	165	10	336	47	94.2	87.6	89.8	0.783

	SD	35	1	41	17	1.7	4.8	2.8	0.049
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### TBXA2R

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	210	3	240	128	98.6	65.2	77.5	0.623
22	Test 2	187	3	284	107	98.4	72.6	81.1	0.667
23	Test 3	188	3	252	138	98.4	64.6	75.7	0.597
24	Test 4	169	9	314	89	94.9	77.9	83.1	0.676
25	Test 5	217	13	247	104	94.3	70.4	79.9	0.637
	Avg	194	6	267	113	96.9	70.2	79.4	0.640
	SD	19	5	31	20	2.1	5.5	2.9	0.032

### TEK

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	162	5	160	57	97.0	73.7	83.9	0.708
22	Test 2	172	2	137	73	98.9	65.2	80.5	0.664
23	Test 3	153	4	120	107	97.5	52.9	71.1	0.529
24	Test 4	154	1	128	101	99.4	55.9	73.4	0.574
25	Test 5	132	3	170	79	97.8	68.3	78.6	0.634
	Avg	155	3	143	83	98.1	63.2	77.5	0.622
	SD	15	2	21	21	1.0	8.7	5.2	0.071

Table S11. Model test set performance results for each target where a positive probability value of 0.1 was used as the threshold to assign compounds as predicted active or inactive. In each case standard deviations are shown below averages. Model performances are reported as sensitivity (SE), specificity (SP), accuracy (ACC), Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC).

**AChE**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	185	311	415	4	37.3	99.0	65.6	0.447
<b>22</b>	Test 2	225	350	337	3	39.1	99.1	61.4	0.427
<b>23</b>	Test 3	213	293	403	6	42.1	98.5	67.3	0.473
<b>24</b>	Test 4	258	272	377	8	48.7	97.9	69.4	0.507
<b>25</b>	Test 5	115	390	409	1	22.8	99.8	57.3	0.337
	Avg	199	323	388	4	38.0	98.9	64.2	0.438
	SD	54	47	32	3	9.5	0.7	4.9	0.064

**ADORA2A**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	674	143	384	4	82.5	99.0	87.8	0.767
<b>27</b>	Test 2	736	97	358	14	88.4	96.2	90.8	0.806
<b>28</b>	Test 3	622	73	491	19	89.5	96.3	92.4	0.849
<b>29</b>	Test 4	696	106	399	4	86.8	99.0	90.9	0.820
<b>30</b>	Test 5	681	115	392	17	85.6	95.8	89.0	0.781
	Avg	682	107	405	12	86.5	97.3	90.2	0.805
	SD	41	26	51	7	2.7	1.6	1.8	0.032

**AR**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	219	321	1443	1	40.6	99.9	83.8	0.574
<b>22</b>	Test 2	210	328	1443	3	39.0	99.8	83.3	0.558

<b>23</b>	Test 3	184	288	1512	0	39.0	100.0	85.5	0.572
<b>24</b>	Test 4	210	359	1411	4	36.9	99.7	81.7	0.534
<b>25</b>	Test 5	176	342	1466	0	34.0	100.0	82.8	0.525
	Avg	200	328	1455	2	37.9	99.9	83.4	0.553
	SD	19	26	37	2	2.5	0.1	1.4	0.022

#### KCNH2

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	493	495	572	68	49.9	89.4	65.4	0.404
<b>22</b>	Test 2	481	480	625	42	50.1	93.7	67.9	0.461
<b>23</b>	Test 3	435	553	610	30	44.0	95.3	64.2	0.425
<b>24</b>	Test 4	470	516	604	38	47.7	94.1	66.0	0.440
<b>25</b>	Test 5	482	490	600	56	49.6	91.5	66.5	0.428
	Avg	472	507	602	47	48.2	92.8	66.0	0.432
	SD	22	29	19	15	2.5	2.4	1.4	0.021

#### SLC6A4

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	703	92	227	13	88.4	94.6	89.9	0.759
<b>27</b>	Test 2	796	59	176	4	93.1	97.8	93.9	0.822
<b>28</b>	Test 3	684	122	225	4	84.9	98.3	87.8	0.731
<b>29</b>	Test 4	698	78	250	9	89.9	96.5	91.6	0.805
<b>30</b>	Test 5	737	72	223	3	91.1	98.7	92.8	0.822
	Avg	724	85	220	7	89.5	97.2	91.2	0.788

	SD	45	24	27	4	3.1	1.7	2.4	0.041
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ADRA2A

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	83	65	221	2	56.1	99.1	81.9	0.643
<b>22</b>	Test 2	79	70	221	1	53.0	99.5	80.9	0.627
<b>23</b>	Test 3	90	80	200	1	52.9	99.5	78.2	0.607
<b>24</b>	Test 4	110	79	182	0	58.2	100.0	78.7	0.637
<b>25</b>	Test 5	112	74	184	1	60.2	99.5	79.8	0.648
	Avg	95	74	202	1	56.1	99.5	79.9	0.632
	SD	15	6	19	1	3.2	0.3	1.5	0.016

ADRB1

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	201	56	201	10	78.2	95.3	85.9	0.735
<b>27</b>	Test 2	128	86	251	3	59.8	98.8	81.0	0.651
<b>28</b>	Test 3	200	75	188	5	72.7	97.4	82.9	0.696
<b>29</b>	Test 4	144	115	207	2	55.6	99.0	75.0	0.586
<b>30</b>	Test 5	127	128	209	4	49.8	98.1	71.8	0.532
	Avg	160	92	211	5	63.2	97.7	79.3	0.640
	SD	38	29	24	3	11.9	1.5	5.8	0.082

ADRB2

<b>Model Number</b>	<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
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<b>21</b>	Test 1	178	211	400	2	45.8	99.5	73.1	0.540
<b>22</b>	Test 2	128	262	398	3	32.8	99.3	66.5	0.431
<b>23</b>	Test 3	98	276	415	2	26.2	99.5	64.9	0.386
<b>24</b>	Test 4	134	223	429	5	37.5	98.8	71.2	0.476
<b>25</b>	Test 5	67	366	358	0	15.5	100.0	53.7	0.277
	Avg	121	268	400	2	31.6	99.4	65.9	0.422
	SD	42	61	27	2	11.5	0.4	7.6	0.099

#### OPRD1

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	460	108	271	6	81.0	97.8	86.5	0.744
<b>27</b>	Test 2	457	150	221	17	75.3	92.9	80.2	0.618
<b>28</b>	Test 3	431	181	231	2	70.4	99.1	78.3	0.622
<b>29</b>	Test 4	407	175	261	2	69.9	99.2	79.1	0.641
<b>30</b>	Test 5	517	120	203	5	81.2	97.6	85.2	0.698
	Avg	454	147	237	6	75.6	97.3	81.9	0.665
	SD	41	32	28	6	5.5	2.6	3.7	0.055

#### DRD1

	<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
	<b>21</b>	Test 1	105	153	408	2	40.7	99.5	76.8	0.534
[100,100]	<b>22</b>	Test 2	123	162	382	1	43.2	99.7	75.6	0.546
	<b>23</b>	Test 3	83	198	387	0	29.5	100.0	70.4	0.442
0.4	<b>24</b>	Test 4	125	160	382	1	43.9	99.7	75.9	0.551

0.001	<b>25</b>	Test 5	111	130	424	3	46.1	99.3	80.1	0.579
100		Avg	109	161	397	1	40.7	99.7	75.7	0.530
		SD	17	24	19	1	6.5	0.3	3.5	0.052

DRD2

	<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
	<b>26</b>	Test 1	993	91	266	16	91.6	94.3	92.2	0.792
	<b>27</b>	Test 2	987	142	215	22	87.4	90.7	88.0	0.673
	<b>28</b>	Test 3	911	249	203	3	78.5	98.5	81.6	0.586
	<b>29</b>	Test 4	1057	118	175	16	90.0	91.6	90.2	0.689
	<b>30</b>	Test 5	1000	146	208	12	87.3	94.5	88.4	0.686
		Avg	990	149	213	14	87.0	94.0	88.1	0.685
		SD	52	60	33	7	5.0	3.1	4.0	0.073

SLC6A3

	<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
	<b>21</b>	Test 1	335	186	359	5	64.3	98.6	78.4	0.637
	<b>22</b>	Test 2	364	112	400	9	76.5	97.8	86.3	0.750
	<b>23</b>	Test 3	335	164	378	8	67.1	97.9	80.6	0.662
	<b>24</b>	Test 4	396	115	372	2	77.5	99.5	86.8	0.764
	<b>25</b>	Test 5	362	140	373	10	72.1	97.4	83.1	0.698
		Avg	358	143	376	7	71.5	98.2	83.0	0.702
		SD	25	32	15	3	5.7	0.8	3.6	0.055

## EDNRA

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	139	118	225	5	54.1	97.8	74.7	0.568
<b>22</b>	Test 2	123	98	262	4	55.7	98.5	79.1	0.614
<b>23</b>	Test 3	207	45	231	4	82.1	98.3	89.9	0.811
<b>24</b>	Test 4	111	171	205	0	39.4	100.0	64.9	0.463
<b>25</b>	Test 5	146	127	204	10	53.5	95.3	71.9	0.519
	Avg	145	112	225	5	56.9	98.0	76.1	0.595
	SD	37	46	24	4	15.5	1.7	9.3	0.133

## NR3C1

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	312	344	1340	2	47.6	99.9	82.7	0.612
<b>22</b>	Test 2	248	367	1382	1	40.3	99.9	81.6	0.563
<b>23</b>	Test 3	179	394	1424	1	31.2	99.9	80.2	0.492
<b>24</b>	Test 4	197	416	1384	1	32.1	99.9	79.1	0.495
<b>25</b>	Test 5	207	354	1434	3	36.9	99.8	82.1	0.538
	Avg	229	375	1393	2	37.6	99.9	81.2	0.540
	SD	53	30	38	1	6.7	0.1	1.5	0.050

## HRH1

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	190	82	201	3	69.9	98.5	82.1	0.689
<b>27</b>	Test 2	164	92	219	1	64.1	99.5	80.5	0.666

<b>28</b>	Test 3	193	85	194	4	69.4	98.0	81.3	0.675
<b>29</b>	Test 4	165	69	241	1	70.5	99.6	85.3	0.735
<b>30</b>	Test 5	177	58	238	3	75.3	98.8	87.2	0.764
	Avg	178	77	219	2	69.8	98.9	83.3	0.706
	SD	14	14	21	1	4.0	0.7	2.8	0.042

#### OPRM1

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	532	190	455	6	73.7	98.7	83.4	0.709
<b>22</b>	Test 2	585	149	443	6	79.7	98.7	86.9	0.761
<b>23</b>	Test 3	632	117	424	10	84.4	97.7	89.3	0.794
<b>24</b>	Test 4	529	154	493	7	77.5	98.6	86.4	0.755
<b>25</b>	Test 5	598	124	454	7	82.8	98.5	88.9	0.793
	Avg	575	147	454	7	79.6	98.4	87.0	0.762
	SD	44	29	25	2	4.3	0.4	2.3	0.035

#### CHRM1

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	226	142	280	3	61.4	98.9	77.7	0.627
<b>27</b>	Test 2	262	103	276	10	71.8	96.5	82.6	0.687
<b>28</b>	Test 3	294	127	213	17	69.8	92.6	77.9	0.598
<b>29</b>	Test 4	305	128	213	5	70.4	97.7	79.6	0.644
<b>30</b>	Test 5	288	139	218	6	67.4	97.3	77.7	0.618
	Avg	275	128	240	8	68.2	96.6	79.1	0.635

	SD	32	15	35	6	4.1	2.4	2.1	0.034
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#### CHRM2

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
<b>26</b>	Test 1	261	73	393	6	78.1	98.5	89.2	0.793
<b>27</b>	Test 2	159	165	406	3	49.1	99.3	77.1	0.579
<b>28</b>	Test 3	189	129	413	2	59.4	99.5	82.1	0.666
<b>29</b>	Test 4	206	128	397	2	61.7	99.5	82.3	0.676
<b>30</b>	Test 5	200	123	401	9	61.9	97.8	82.0	0.657
	Avg	203	124	402	4	62.0	98.9	82.5	0.674
	SD	37	33	8	3	10.4	0.7	4.3	0.077

#### CHRM3

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
<b>26</b>	Test 1	153	150	226	1	50.5	99.6	71.5	0.546
<b>27</b>	Test 2	179	131	220	0	57.7	100.0	75.3	0.602
<b>28</b>	Test 3	226	101	200	3	69.1	98.5	80.4	0.664
<b>29</b>	Test 4	227	77	221	5	74.7	97.8	84.5	0.722
<b>30</b>	Test 5	192	101	229	8	65.5	96.6	79.4	0.638
	Avg	195	112	219	3	63.5	98.5	78.2	0.634
	SD	32	29	11	3	9.5	1.4	5.0	0.066

#### SLC6A2

Model Number	TP	FN	TN	FP	SE	SP	ACC	MCC
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<b>26</b>	Test 1	1668	62	1118	62	96.4	94.7	95.7	0.912
<b>27</b>	Test 2	1684	67	1115	44	96.2	96.2	96.2	0.921
<b>28</b>	Test 3	1677	92	1099	42	94.8	96.3	95.4	0.905
<b>29</b>	Test 4	1689	76	1095	50	95.7	95.6	95.7	0.910
<b>30</b>	Test 5	1654	97	1122	37	94.5	96.8	95.4	0.906
	Avg	1674	79	1110	47	95.5	95.9	95.7	0.911
	SD	14	15	12	10	0.9	0.8	0.3	0.006

#### HTR2A

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	668	86	194	10	88.6	95.1	90.0	0.753
<b>27</b>	Test 2	619	126	208	5	83.1	97.7	86.3	0.705
<b>28</b>	Test 3	702	59	192	5	92.2	97.5	93.3	0.825
<b>29</b>	Test 4	663	93	198	4	87.7	98.0	89.9	0.760
<b>30</b>	Test 5	633	108	211	6	85.4	97.2	88.1	0.734
	Avg	657	94	201	6	87.4	97.1	89.5	0.755
	SD	32	25	8	2	3.4	1.2	2.6	0.044

#### HTR3A

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	35	63	202	1	35.7	99.5	78.7	0.509
<b>27</b>	Test 2	59	42	200	0	58.4	100.0	86.0	0.695
<b>28</b>	Test 3	18	64	219	0	22.0	100.0	78.7	0.412
<b>29</b>	Test 4	33	50	217	1	39.8	99.5	83.1	0.555

	<b>30</b>	Test 5	29	58	214	0	33.3	100.0	80.7	0.512
		Avg	35	55	210	0	37.8	99.8	81.5	0.537
		SD	15	9	9	1	13.3	0.3	3.1	0.103

LCK

	<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
	<b>26</b>	Test 1	237	126	83	5	65.3	94.3	71.0	0.474
	<b>27</b>	Test 2	253	111	87	0	69.5	100.0	75.4	0.553
	<b>28</b>	Test 3	305	57	77	12	84.3	86.5	84.7	0.616
	<b>29</b>	Test 4	261	83	103	4	75.9	96.3	80.7	0.623
	<b>30</b>	Test 5	202	97	144	8	67.6	94.7	76.7	0.590
		Avg	252	95	99	6	72.5	94.4	77.7	0.571
		SD	37	26	27	4	7.7	4.9	5.2	0.061

AVPR1A

	<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
	<b>26</b>	Test 1	108	24	202	1	81.8	99.5	92.5	0.848
	<b>27</b>	Test 2	72	38	225	0	65.5	100.0	88.7	0.748
	<b>28</b>	Test 3	52	66	215	2	44.1	99.1	79.7	0.560
	<b>29</b>	Test 4	102	40	193	0	71.8	100.0	88.1	0.771
	<b>30</b>	Test 5	99	18	217	1	84.6	99.5	94.3	0.877
		Avg	87	37	210	1	69.6	99.6	88.7	0.761
		SD	24	19	13	1	16.2	0.4	5.7	0.124

**AGTR1**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	151	49	197	0	75.5	100.0	87.7	0.778
<b>27</b>	Test 2	127	32	238	0	79.9	100.0	91.9	0.839
<b>28</b>	Test 3	128	42	227	0	75.3	100.0	89.4	0.797
<b>29</b>	Test 4	135	38	224	0	78.0	100.0	90.4	0.817
<b>30</b>	Test 5	66	38	293	0	63.5	100.0	90.4	0.750
	Avg	121	40	236	0	74.4	100.0	90.0	0.796
	SD	32	6	35	0	6.4	0.0	1.6	0.035

**AKT1**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	542	75	177	3	87.8	98.3	90.2	0.775
<b>27</b>	Test 2	445	125	221	6	78.1	97.4	83.6	0.687
<b>28</b>	Test 3	432	118	230	17	78.5	93.1	83.1	0.668
<b>29</b>	Test 4	427	94	272	4	82.0	98.6	87.7	0.769
<b>30</b>	Test 5	404	103	281	9	79.7	96.9	85.9	0.737
	Avg	450	103	236	8	81.2	96.9	86.1	0.727
	SD	54	20	42	6	4.0	2.2	3.0	0.048

**BACE1**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	1133	146	407	38	88.6	91.5	89.3	0.750
<b>27</b>	Test 2	985	207	504	28	82.6	94.7	86.4	0.726

<b>28</b>	Test 3	846	332	530	16	71.8	97.1	79.8	0.641
<b>29</b>	Test 4	870	343	491	20	71.7	96.1	78.9	0.620
<b>30</b>	Test 5	768	386	561	9	66.6	98.4	77.1	0.614
	Avg	920	283	499	22	76.3	95.6	82.3	0.670
	SD	142	101	58	11	9.0	2.7	5.3	0.063

**BCHE**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	115	166	428	0	40.9	100.0	76.6	0.543
<b>27</b>	Test 2	133	136	439	1	49.4	99.8	80.7	0.610
<b>28</b>	Test 3	85	223	401	0	27.6	100.0	68.5	0.421
<b>29</b>	Test 4	132	149	427	1	47.0	99.8	78.8	0.586
<b>30</b>	Test 5	117	144	443	5	44.8	98.9	79.0	0.559
	Avg	116	164	428	1	42.0	99.7	76.7	0.544
	SD	19	35	16	2	8.6	0.5	4.8	0.073

**CASP1**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	0	253	660	0	0.0	100.0	72.3	#DIV/0!
<b>22</b>	Test 2	0	251	662	0	0.0	100.0	72.5	#DIV/0!
<b>23</b>	Test 3	57	223	631	2	20.4	99.7	75.4	0.376
<b>24</b>	Test 4	0	291	622	0	0.0	100.0	68.1	#DIV/0!
<b>25</b>	Test 5	0	294	619	0	0.0	100.0	67.8	#DIV/0!
	Avg	11	262	639	0	4.1	99.9	71.2	#DIV/0!

	SD	25	30	21	1	9.1	0.1	3.2	#DIV/0!
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**CASP3**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	104	161	336	0	39.2	100.0	73.2	0.515
<b>22</b>	Test 2	73	174	350	4	29.6	98.9	70.4	0.418
<b>23</b>	Test 3	79	124	397	1	38.9	99.7	79.2	0.538
<b>24</b>	Test 4	101	134	362	4	43.0	98.9	77.0	0.538
<b>25</b>	Test 5	75	152	374	0	33.0	100.0	74.7	0.485
	Avg	86	149	364	2	36.7	99.5	74.9	0.499
	SD	15	20	23	2	5.4	0.6	3.4	0.050

**CASP8**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	16	49	227	0	24.6	100.0	83.2	0.450
<b>27</b>	Test 2	10	49	233	0	16.9	100.0	83.2	0.374
<b>28</b>	Test 3	22	43	227	0	33.8	100.0	85.3	0.533
<b>29</b>	Test 4	2	53	237	0	3.6	100.0	81.8	0.172
<b>30</b>	Test 5	46	40	205	1	53.5	99.5	86.0	0.657
	Avg	19	47	226	0	26.5	99.9	83.9	0.437
	SD	17	5	12	0	18.7	0.2	1.7	0.182

**CHRM5**

<b>Model Number</b>	<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
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<b>26</b>	Test 1	38	102	212	0	27.1	100.0	71.0	0.428
<b>27</b>	Test 2	71	83	197	1	46.1	99.5	76.1	0.561
<b>28</b>	Test 3	62	67	222	1	48.1	99.6	80.7	0.598
<b>29</b>	Test 4	27	91	234	0	22.9	100.0	74.1	0.406
<b>30</b>	Test 5	14	124	213	1	10.1	99.5	64.5	0.234
	Avg	42	93	216	1	30.9	99.7	73.3	0.445
	SD	24	21	14	1	16.1	0.3	6.0	0.144

#### CHUK

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	18	52	206	1	25.7	99.5	80.9	0.434
<b>27</b>	Test 2	14	63	200	0	18.2	100.0	77.3	0.372
<b>28</b>	Test 3	28	34	213	2	45.2	99.1	87.0	0.593
<b>29</b>	Test 4	12	34	231	0	26.1	100.0	87.7	0.477
<b>30</b>	Test 5	15	46	216	0	24.6	100.0	83.4	0.450
	Avg	17	46	213	1	27.9	99.7	83.2	0.465
	SD	6	12	12	1	10.1	0.4	4.4	0.081

#### CSF1R

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	207	68	202	0	75.3	100.0	85.7	0.750
<b>22</b>	Test 2	191	78	208	0	71.0	100.0	83.6	0.719
<b>23</b>	Test 3	177	92	208	0	65.8	100.0	80.7	0.675
<b>24</b>	Test 4	193	78	206	0	71.2	100.0	83.6	0.719

<b>25</b>	Test 5	139	113	225	0	55.2	100.0	76.3	0.606
	Avg	181	86	210	0	67.7	100.0	82.0	0.694
	SD	26	17	9	0	7.8	0.0	3.7	0.056

#### CSNK1D

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	75	72	200	0	51.0	100.0	79.3	0.612
<b>22</b>	Test 2	70	62	215	0	53.0	100.0	82.1	0.642
<b>23</b>	Test 3	63	82	202	0	43.4	100.0	76.4	0.556
<b>24</b>	Test 4	65	74	207	1	46.8	99.5	78.4	0.578
<b>25</b>	Test 5	64	81	202	0	44.1	100.0	76.7	0.561
	Avg	67	74	205	0	47.7	99.9	78.6	0.590
	SD	5	8	6	0	4.2	0.2	2.3	0.036

#### EDNRB

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	131	87	191	0	60.1	100.0	78.7	0.643
<b>27</b>	Test 2	125	34	249	1	78.6	99.6	91.4	0.826
<b>28</b>	Test 3	84	61	261	3	57.9	98.9	84.4	0.664
<b>29</b>	Test 4	71	96	242	0	42.5	100.0	76.5	0.552
<b>30</b>	Test 5	55	65	287	2	45.8	99.3	83.6	0.593
	Avg	93	69	246	1	57.0	99.6	82.9	0.655
	SD	33	24	35	1	14.2	0.5	5.8	0.105

**ELANE**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	344	137	215	5	71.5	97.7	79.7	0.643
<b>22</b>	Test 2	303	138	260	0	68.7	100.0	80.3	0.670
<b>23</b>	Test 3	306	136	258	1	69.2	99.6	80.5	0.670
<b>24</b>	Test 4	236	133	331	1	64.0	99.7	80.9	0.672
<b>25</b>	Test 5	225	176	298	2	56.1	99.3	74.6	0.586
	Avg	283	144	272	2	65.9	99.3	79.2	0.648
	SD	51	18	44	2	6.1	0.9	2.6	0.037

**EPHA2**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	153	14	159	0	91.6	100.0	95.7	0.918
<b>27</b>	Test 2	78	22	226	0	78.0	100.0	93.3	0.843
<b>28</b>	Test 3	51	27	248	0	65.4	100.0	91.7	0.768
<b>29</b>	Test 4	77	30	219	0	72.0	100.0	90.8	0.796
<b>30</b>	Test 5	34	42	250	0	44.7	100.0	87.1	0.619
	Avg	79	27	220	0	70.3	100.0	91.7	0.789
	SD	46	10	37	0	17.3	0.0	3.2	0.111

**FGFR1**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	445	91	137	1	83.0	99.3	86.4	0.702
<b>22</b>	Test 2	273	149	246	6	64.7	97.6	77.0	0.612

<b>23</b>	Test 3	319	99	253	3	76.3	98.8	84.9	0.730
<b>24</b>	Test 4	175	229	270	0	43.3	100.0	66.0	0.484
<b>25</b>	Test 5	214	169	289	2	55.9	99.3	74.6	0.586
	Avg	285	147	239	2	64.6	99.0	77.8	0.623
	SD	105	56	59	2	15.9	0.9	8.3	0.098

#### FKBP1A

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	0	84	188	0	0.0	100.0	69.1	#DIV/0!
<b>22</b>	Test 2	0	101	171	0	0.0	100.0	62.9	#DIV/0!
<b>23</b>	Test 3	11	43	217	1	20.4	99.5	83.8	0.387
<b>24</b>	Test 4	12	49	211	0	19.7	100.0	82.0	0.400
<b>25</b>	Test 5	3	51	218	0	5.6	100.0	81.3	0.212
	Avg	5	66	201	0	9.1	99.9	75.8	#DIV/0!
	SD	6	25	21	0	10.2	0.2	9.3	#DIV/0!

#### FLT1

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	94	112	427	0	45.6	100.0	82.3	0.601
<b>22</b>	Test 2	147	99	386	1	59.8	99.7	84.2	0.685
<b>23</b>	Test 3	136	88	407	2	60.7	99.5	85.8	0.697
<b>24</b>	Test 4	83	121	429	0	40.7	100.0	80.9	0.563
<b>25</b>	Test 5	92	116	425	0	44.2	100.0	81.7	0.589
	Avg	110	107	415	1	50.2	99.9	83.0	0.627

	SD	29	13	18	1	9.3	0.2	2.0	0.060
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#### FLT4

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
21	Test 1	38	113	199	1	25.2	99.5	67.5	0.389
22	Test 2	59	64	228	0	48.0	100.0	81.8	0.612
23	Test 3	49	85	217	0	36.6	100.0	75.8	0.513
24	Test 4	54	80	217	0	40.3	100.0	77.2	0.543
25	Test 5	52	80	219	0	39.4	100.0	77.2	0.537
	Avg	50	84	216	0	37.9	99.9	75.9	0.519
	SD	8	18	11	0	8.3	0.2	5.2	0.082

#### FYN

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	27	74	198	0	26.7	100.0	75.3	0.441
27	Test 2	15	58	225	1	20.5	99.6	80.3	0.384
28	Test 3	11	78	210	0	12.4	100.0	73.9	0.300
29	Test 4	12	78	209	0	13.3	100.0	73.9	0.312
30	Test 5	6	61	232	0	9.0	100.0	79.6	0.266
	Avg	14	70	215	0	16.4	99.9	76.6	0.341
	SD	8	10	14	0	7.2	0.2	3.1	0.071

#### GSK3B

Model Number	TP	FN	TN	FP	SE	SP	ACC	MCC
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<b>26</b>	Test 1	396	127	229	9	75.7	96.2	82.1	0.668
<b>27</b>	Test 2	418	73	246	24	85.1	91.1	87.3	0.739
<b>28</b>	Test 3	341	153	258	9	69.0	96.6	78.7	0.629
<b>29</b>	Test 4	308	194	250	9	61.4	96.5	73.3	0.556
<b>30</b>	Test 5	362	177	207	15	67.2	93.2	74.8	0.549
	Avg	365	145	238	13	71.7	94.7	79.2	0.628
	SD	44	47	20	7	9.1	2.5	5.7	0.080

#### HDAC3

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	127	85	218	8	59.9	96.5	78.8	0.610
<b>22</b>	Test 2	95	114	223	6	45.5	97.4	72.6	0.508
<b>23</b>	Test 3	114	113	209	2	50.2	99.1	73.7	0.558
<b>24</b>	Test 4	117	70	251	0	62.6	100.0	84.0	0.699
<b>25</b>	Test 5	116	100	219	3	53.7	98.6	76.5	0.588
	Avg	114	96	224	4	54.4	98.3	77.1	0.593
	SD	12	19	16	3	7.0	1.4	4.5	0.071

#### IGF1R

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	542	46	132	3	92.2	97.8	93.2	0.814
<b>27</b>	Test 2	350	123	249	1	74.0	99.6	82.8	0.700
<b>28</b>	Test 3	424	99	200	0	81.1	100.0	86.3	0.736
<b>29</b>	Test 4	366	90	259	8	80.3	97.0	86.4	0.746

<b>30</b>	Test 5	320	123	278	2	72.2	99.3	82.7	0.701
	Avg	400	96	224	3	79.9	98.7	86.3	0.740
	SD	88	32	59	3	7.8	1.3	4.3	0.046

#### INSR

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	203	53	140	0	79.3	100.0	86.6	0.758
<b>27</b>	Test 2	128	40	228	0	76.2	100.0	89.9	0.805
<b>28</b>	Test 3	99	46	251	0	68.3	100.0	88.4	0.760
<b>29</b>	Test 4	86	54	256	0	61.4	100.0	86.4	0.712
<b>30</b>	Test 5	106	72	218	0	59.6	100.0	81.8	0.669
	Avg	124	53	219	0	68.9	100.0	86.6	0.741
	SD	47	12	47	0	8.7	0.0	3.0	0.052

#### KDR

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	1323	310	239	7	81.0	97.2	83.1	0.580
<b>27</b>	Test 2	905	641	321	12	58.5	96.4	65.2	0.420
<b>28</b>	Test 3	1385	197	273	24	87.5	91.9	88.2	0.669
<b>29</b>	Test 4	1174	313	375	17	79.0	95.7	82.4	0.629
<b>30</b>	Test 5	1299	269	295	16	82.8	94.9	84.8	0.630
	Avg	1217	346	301	15	77.8	95.2	80.8	0.586
	SD	191	171	51	6	11.2	2.0	9.0	0.098

**LTB4R**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	36	19	221	0	65.5	100.0	93.1	0.776
<b>27</b>	Test 2	39	32	205	0	54.9	100.0	88.4	0.689
<b>28</b>	Test 3	42	37	197	0	53.2	100.0	86.6	0.669
<b>29</b>	Test 4	27	48	201	0	36.0	100.0	82.6	0.539
<b>30</b>	Test 5	18	52	206	0	25.7	100.0	81.2	0.453
	Avg	32	38	206	0	47.1	100.0	86.4	0.625
	SD	10	13	9	0	15.9	0.0	4.8	0.128

**LYN**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	64	38	198	0	62.7	100.0	87.3	0.726
<b>27</b>	Test 2	39	41	220	0	48.8	100.0	86.3	0.641
<b>28</b>	Test 3	29	64	206	1	31.2	99.5	78.3	0.473
<b>29</b>	Test 4	30	68	201	1	30.6	99.5	77.0	0.464
<b>30</b>	Test 5	24	57	219	0	29.6	100.0	81.0	0.485
	Avg	37	54	209	0	40.6	99.8	82.0	0.558
	SD	16	14	10	1	14.7	0.3	4.7	0.119

**MAPK1**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	358	966	2133	0	27.0	100.0	72.1	0.431
<b>22</b>	Test 2	290	955	2212	0	23.3	100.0	72.4	0.403

<b>23</b>	Test 3	348	854	2255	0	29.0	100.0	75.3	0.458
<b>24</b>	Test 4	298	904	2255	0	24.8	100.0	73.9	0.421
<b>25</b>	Test 5	361	875	2221	0	29.2	100.0	74.7	0.458
	Avg	331	911	2215	0	26.7	100.0	73.7	0.434
	SD	34	49	50	0	2.6	0.0	1.4	0.024

#### MAPK9

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
<b>26</b>	Test 1	200	61	201	1	76.6	99.5	86.6	0.762
<b>27</b>	Test 2	167	71	224	1	70.2	99.6	84.4	0.725
<b>28</b>	Test 3	166	76	220	1	68.6	99.5	83.4	0.709
<b>29</b>	Test 4	197	40	224	2	83.1	99.1	90.9	0.830
<b>30</b>	Test 5	156	93	214	0	62.7	100.0	79.9	0.661
	Avg	177	68	217	1	72.2	99.5	85.1	0.737
	SD	20	20	10	1	7.9	0.3	4.1	0.063

#### MAPKAPK2

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
<b>21</b>	Test 1	90	74	229	4	54.9	98.3	80.4	0.616
<b>22</b>	Test 2	84	93	219	1	47.5	99.5	76.3	0.570
<b>23</b>	Test 3	85	80	232	0	51.5	100.0	79.8	0.619
<b>24</b>	Test 4	34	102	261	0	25.0	100.0	74.3	0.424
<b>25</b>	Test 5	63	124	210	0	33.7	100.0	68.8	0.460
	Avg	71	95	230	1	42.5	99.6	75.9	0.538

SD 23 20 19 2 12.7 0.7 4.7 0.090

MET

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
26	Test 1	536	66	196	5	89.0	97.5	91.2	0.800
27	Test 2	439	102	260	2	81.1	99.2	87.0	0.757
28	Test 3	487	80	230	6	85.9	97.5	89.3	0.780
29	Test 4	457	126	217	3	78.4	98.6	83.9	0.694
30	Test 5	447	131	224	1	77.3	99.6	83.6	0.695
	Avg	473	101	225	3	82.4	98.5	87.0	0.745
	SD	40	28	23	2	5.0	1.0	3.3	0.048

MMP13

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	360	132	205	3	73.2	98.6	80.7	0.656
<b>27</b>	Test 2	363	107	229	1	77.2	99.6	84.6	0.722
<b>28</b>	Test 3	372	114	211	3	76.5	98.6	83.3	0.694
<b>29</b>	Test 4	414	62	222	2	87.0	99.1	90.9	0.818
<b>30</b>	Test 5	345	119	228	8	74.4	96.6	81.9	0.671
	Avg	371	107	219	3	77.7	98.5	84.3	0.712
	SD	26	27	11	3	5.5	1.1	4.0	0.064

MMP2

**Model Number** TP FN TN FP SE SP ACC MCC

<b>26</b>	Test 1	449	158	313	3	74.0	99.1	82.6	0.693
<b>27</b>	Test 2	382	210	324	7	64.5	97.9	76.5	0.606
<b>28</b>	Test 3	341	258	321	3	56.9	99.1	71.7	0.553
<b>29</b>	Test 4	428	143	348	4	75.0	98.9	84.1	0.719
<b>30</b>	Test 5	354	215	348	6	62.2	98.3	76.1	0.603
	Avg	391	197	331	5	66.5	98.6	78.2	0.635
	SD	47	47	16	2	7.8	0.5	5.1	0.069

#### MMP3

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	231	150	176	2	60.6	98.9	72.8	0.562
<b>22</b>	Test 2	186	181	192	0	50.7	100.0	67.6	0.511
<b>23</b>	Test 3	245	131	180	3	65.2	98.4	76.0	0.600
<b>24</b>	Test 4	191	117	248	3	62.0	98.8	78.5	0.635
<b>25</b>	Test 5	217	110	228	4	66.4	98.3	79.6	0.651
	Avg	214	138	205	2	61.0	98.9	74.9	0.592
	SD	25	29	32	2	6.2	0.7	4.8	0.057

#### MMP9

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	228	322	333	3	41.5	99.1	63.3	0.448
<b>22</b>	Test 2	244	245	390	7	49.9	98.2	71.6	0.531
<b>23</b>	Test 3	234	280	372	0	45.5	100.0	68.4	0.510
<b>24</b>	Test 4	270	249	364	3	52.0	99.2	71.6	0.546

<b>25</b>	Test 5	252	258	375	1	49.4	99.7	70.8	0.538
	Avg	246	271	367	3	47.7	99.3	69.1	0.515
	SD	16	32	21	3	4.2	0.7	3.5	0.040

#### NEK2

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	25	48	198	0	34.2	100.0	82.3	0.525
<b>27</b>	Test 2	32	42	197	0	43.2	100.0	84.5	0.597
<b>28</b>	Test 3	22	32	217	0	40.7	100.0	88.2	0.596
<b>29</b>	Test 4	11	33	227	0	25.0	100.0	87.8	0.467
<b>30</b>	Test 5	3	50	218	0	5.7	100.0	81.5	0.215
	Avg	19	41	211	0	29.8	100.0	84.9	0.480
	SD	12	8	13	0	15.2	0.0	3.1	0.158

#### P2RY1

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	77	34	221	0	69.4	100.0	89.8	0.775
<b>22</b>	Test 2	73	64	195	0	53.3	100.0	80.7	0.633
<b>23</b>	Test 3	53	32	244	3	62.4	98.8	89.5	0.713
<b>24</b>	Test 4	69	54	209	0	56.1	100.0	83.7	0.668
<b>30</b>	Test 5	76	28	228	0	73.1	100.0	91.6	0.807
	Avg	70	42	219	1	62.8	99.8	87.0	0.719
	SD	10	16	19	1	8.4	0.5	4.6	0.072

**PAK4**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	28	69	199	0	28.9	100.0	76.7	0.463
<b>27</b>	Test 2	27	39	230	0	40.9	100.0	86.8	0.591
<b>28</b>	Test 3	28	50	218	0	35.9	100.0	83.1	0.540
<b>29</b>	Test 4	33	37	226	0	47.1	100.0	87.5	0.636
<b>30</b>	Test 5	34	35	227	0	49.3	100.0	88.2	0.653
	Avg	30	46	220	0	40.4	100.0	84.5	0.577
	SD	3	14	13	0	8.3	0.0	4.8	0.077

**PDE4A**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	70	61	202	1	53.4	99.5	81.4	0.632
<b>27</b>	Test 2	93	52	188	1	64.1	99.5	84.1	0.701
<b>28</b>	Test 3	44	66	223	1	40.0	99.6	79.9	0.544
<b>29</b>	Test 4	66	63	204	1	51.2	99.5	80.8	0.616
<b>30</b>	Test 5	48	90	196	0	34.8	100.0	73.1	0.488
	Avg	64	66	203	1	48.7	99.6	79.9	0.596
	SD	20	14	13	0	11.6	0.2	4.1	0.082

**PDE5A**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	153	132	245	15	53.7	94.2	73.0	0.518
<b>27</b>	Test 2	249	56	238	2	81.6	99.2	89.4	0.805

<b>28</b>	Test 3	184	109	249	3	62.8	98.8	79.4	0.647
<b>29</b>	Test 4	261	92	191	1	73.9	99.5	82.9	0.702
<b>30</b>	Test 5	190	125	225	5	60.3	97.8	76.1	0.599
	Avg	207	103	230	5	66.5	97.9	80.2	0.654
	SD	46	30	23	6	11.2	2.1	6.3	0.108

#### PIK3CA

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
<b>26</b>	Test 1	910	84	358	10	91.5	97.3	93.1	0.843
<b>27</b>	Test 2	769	146	443	4	84.0	99.1	89.0	0.788
<b>28</b>	Test 3	723	139	486	14	83.9	97.2	88.8	0.784
<b>29</b>	Test 4	827	146	387	2	85.0	99.5	89.1	0.782
<b>30</b>	Test 5	712	268	380	2	72.7	99.5	80.2	0.649
	Avg	788	157	411	6	83.4	98.5	88.0	0.769
	SD	82	67	52	5	6.8	1.2	4.7	0.072

#### PPARG

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
<b>21</b>	Test 1	409	459	1438	23	47.1	98.4	79.3	0.567
<b>22</b>	Test 2	256	635	1436	2	28.7	99.9	72.6	0.443
<b>23</b>	Test 3	309	497	1518	5	38.3	99.7	78.4	0.529
<b>24</b>	Test 4	202	657	1469	1	23.5	99.9	71.7	0.401
<b>30</b>	Test 5	251	687	1376	15	26.8	98.9	69.9	0.396
	Avg	285	587	1447	9	32.9	99.4	74.4	0.467

	SD	79	102	52	9	9.7	0.7	4.2	0.077
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**PTPN1**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	46	274	408	2	14.4	99.5	62.2	0.278
<b>27</b>	Test 2	101	237	388	4	29.9	99.0	67.0	0.410
<b>28</b>	Test 3	73	207	437	13	26.1	97.1	69.9	0.350
<b>29</b>	Test 4	56	241	433	0	18.9	100.0	67.0	0.348
<b>30</b>	Test 5	34	202	494	0	14.4	100.0	72.3	0.320
	Avg	62	232	432	4	20.7	99.1	67.7	0.341
	SD	26	29	40	5	7.0	1.2	3.8	0.048

**PTPN11**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	9	73	231	0	11.0	100.0	76.7	0.289
<b>27</b>	Test 2	1	64	248	0	1.5	100.0	79.6	0.111
<b>28</b>	Test 3	8	52	251	2	13.3	99.2	82.7	0.281
<b>29</b>	Test 4	0	72	241	0	0.0	100.0	77.0	#DIV/0!
<b>30</b>	Test 5	1	74	238	0	1.3	100.0	76.4	0.101
	Avg	4	67	242	0	5.4	99.8	78.5	#DIV/0!
	SD	4	9	8	1	6.2	0.4	2.7	#DIV/0!

**PTPN2**

<b>Model Number</b>	<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
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<b>26</b>	Test 1	17	59	232	1	22.4	99.6	80.6	0.403
<b>27</b>	Test 2	11	54	244	0	16.9	100.0	82.5	0.372
<b>28</b>	Test 3	6	65	238	0	8.5	100.0	79.0	0.258
<b>29</b>	Test 4	6	58	245	0	9.4	100.0	81.2	0.275
<b>30</b>	Test 5	16	47	246	0	25.4	100.0	84.8	0.462
	Avg	11	57	241	0	16.5	99.9	81.6	0.354
	SD	5	7	6	0	7.6	0.2	2.2	0.086

#### RAF1

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	191	88	208	0	68.5	100.0	81.9	0.694
<b>22</b>	Test 2	212	95	180	0	69.1	100.0	80.5	0.672
<b>23</b>	Test 3	197	68	222	0	74.3	100.0	86.0	0.754
<b>24</b>	Test 4	203	67	217	0	75.2	100.0	86.2	0.758
<b>30</b>	Test 5	146	84	256	1	63.5	99.6	82.5	0.686
	Avg	190	80	217	0	70.1	99.9	83.4	0.713
	SD	26	12	27	0	4.8	0.2	2.6	0.040

#### RARA

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	26	62	633	0	29.5	100.0	91.4	0.519
<b>27</b>	Test 2	12	58	651	0	17.1	100.0	92.0	0.397
<b>28</b>	Test 3	32	39	650	0	45.1	100.0	94.6	0.652
<b>29</b>	Test 4	11	51	659	0	17.7	100.0	92.9	0.406

<b>30</b>	Test 5	34	31	655	1	52.3	99.8	95.6	0.695
	Avg	23	48	650	0	32.4	100.0	93.3	0.534
	SD	11	13	10	0	15.9	0.1	1.8	0.137

#### RARB

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	51	8	670	0	86.4	100.0	98.9	0.924
<b>27</b>	Test 2	13	46	670	0	22.0	100.0	93.7	0.454
<b>28</b>	Test 3	31	32	666	0	49.2	100.0	95.6	0.685
<b>29</b>	Test 4	38	20	671	0	65.5	100.0	97.3	0.798
<b>30</b>	Test 5	29	30	670	0	49.2	100.0	95.9	0.686
	Avg	32	27	669	0	54.5	100.0	96.3	0.709
	SD	14	14	2	0	23.7	0.0	1.9	0.173

#### ROCK1

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	175	107	200	0	62.1	100.0	77.8	0.636
<b>22</b>	Test 2	140	132	210	0	51.5	100.0	72.6	0.562
<b>23</b>	Test 3	155	83	243	1	65.1	99.6	82.6	0.692
<b>24</b>	Test 4	134	129	216	3	51.0	98.6	72.6	0.547
<b>30</b>	Test 5	119	119	243	1	50.0	99.6	75.1	0.573
	Avg	145	114	222	1	55.9	99.6	76.1	0.602
	SD	21	20	20	1	7.1	0.6	4.2	0.060

**RPS6KA5**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	11	39	202	0	22.0	100.0	84.5	0.429
<b>27</b>	Test 2	4	36	212	0	10.0	100.0	85.7	0.292
<b>28</b>	Test 3	13	35	204	0	27.1	100.0	86.1	0.481
<b>29</b>	Test 4	2	43	207	0	4.4	100.0	82.9	0.192
<b>30</b>	Test 5	10	31	211	0	24.4	100.0	87.7	0.461
	Avg	8	37	207	0	17.6	100.0	85.4	0.371
	SD	5	4	4	0	9.8	0.0	1.8	0.124

**SIRT2**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>26</b>	Test 1	49	44	236	0	52.7	100.0	86.6	0.666
<b>27</b>	Test 2	14	56	259	0	20.0	100.0	83.0	0.406
<b>28</b>	Test 3	6	50	273	0	10.7	100.0	84.8	0.301
<b>29</b>	Test 4	12	64	252	1	15.8	99.6	80.2	0.333
<b>30</b>	Test 5	9	57	263	0	13.6	100.0	82.7	0.335
	Avg	18	54	257	0	22.6	99.9	83.5	0.408
	SD	18	8	14	0	17.2	0.2	2.4	0.149

**SIRT3**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	0	48	197	0	0.0	100.0	80.4	#DIV/0!
<b>22</b>	Test 2	0	34	211	0	0.0	100.0	86.1	#DIV/0!

<b>23</b>	Test 3	0	15	230	0	0.0	100.0	93.9	#DIV/0!
<b>24</b>	Test 4	0	27	218	0	0.0	100.0	89.0	#DIV/0!
<b>25</b>	Test 5	0	27	218	0	0.0	100.0	89.0	#DIV/0!
	Avg	0	30	215	0	0.0	100.0	87.7	#DIV/0!
	SD	0	12	12	0	0.0	0.0	4.9	#DIV/0!

**SRC**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
<b>26</b>	Test 1	424	122	290	11	77.7	96.3	84.3	0.709
<b>27</b>	Test 2	332	177	330	8	65.2	97.6	78.2	0.628
<b>28</b>	Test 3	340	160	338	9	68.0	97.4	80.0	0.653
<b>29</b>	Test 4	377	204	262	4	64.9	98.5	75.4	0.591
<b>30</b>	Test 5	369	199	274	5	65.0	98.2	75.9	0.598
	Avg	368	172	299	7	68.1	97.6	78.8	0.636
	SD	36	33	34	3	5.5	0.8	3.6	0.048

**TACR2**

Model Number		TP	FN	TN	FP	SE	SP	ACC	MCC
<b>26</b>	Test 1	132	46	378	2	74.2	99.5	91.4	0.803
<b>27</b>	Test 2	114	74	370	0	60.6	100.0	86.7	0.711
<b>28</b>	Test 3	103	44	411	0	70.1	100.0	92.1	0.796
<b>29</b>	Test 4	86	53	419	0	61.9	100.0	90.5	0.741
<b>30</b>	Test 5	173	51	332	2	77.2	99.4	90.5	0.810
	Avg	122	54	382	1	68.8	99.8	90.3	0.772

	SD	33	12	35	1	7.3	0.3	2.1	0.044
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**TBXA2R**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	59	154	368	0	27.7	100.0	73.5	0.442
<b>22</b>	Test 2	103	87	388	3	54.2	99.2	84.5	0.649
<b>23</b>	Test 3	84	107	388	2	44.0	99.5	81.2	0.575
<b>24</b>	Test 4	33	145	403	0	18.5	100.0	75.0	0.369
<b>25</b>	Test 5	100	130	351	0	43.5	100.0	77.6	0.563
	Avg	76	125	380	1	37.6	99.7	78.4	0.520
	SD	30	28	20	1	14.3	0.4	4.5	0.112

**TEK**

<b>Model Number</b>		<b>TP</b>	<b>FN</b>	<b>TN</b>	<b>FP</b>	<b>SE</b>	<b>SP</b>	<b>ACC</b>	<b>MCC</b>
<b>21</b>	Test 1	102	65	217	0	61.1	100.0	83.1	0.686
<b>22</b>	Test 2	118	56	210	0	67.8	100.0	85.4	0.732
<b>23</b>	Test 3	118	39	227	0	75.2	100.0	89.8	0.801
<b>24</b>	Test 4	90	65	229	0	58.1	100.0	83.1	0.673
<b>25</b>	Test 5	50	85	249	0	37.0	100.0	77.9	0.525
	Avg	96	62	226	0	59.8	100.0	83.9	0.683
	SD	28	17	15	0	14.3	0.0	4.3	0.101

Table S12. Model performance results for each target where a positive probability value of 0.9 was used as the threshold to assign compounds as predicted active or inactive. In each case standard deviations are shown below averages. Model performances are reported as sensitivity (SE), specificity (SP), accuracy (ACC), Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC).

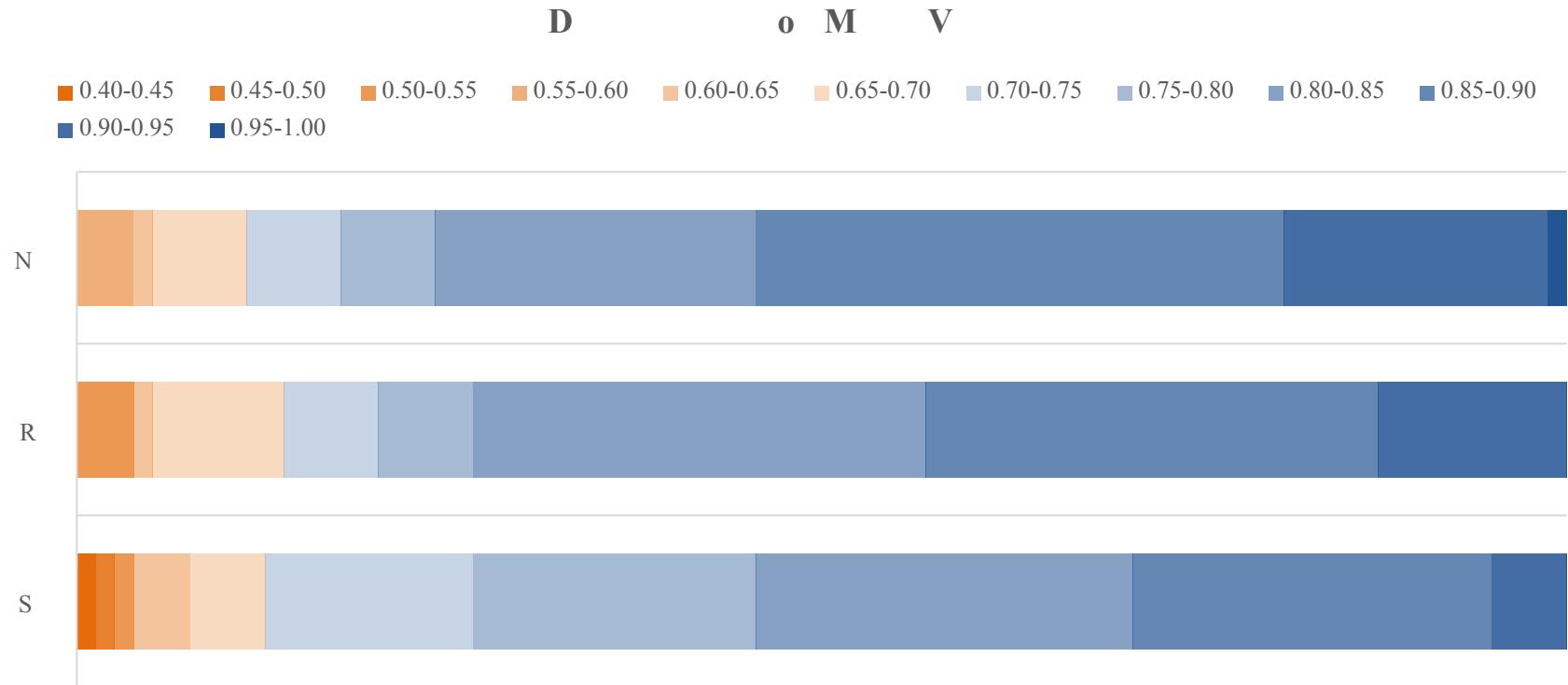
Target Gene	SE			SP			ACC			MCC		
	DNN	ΔSA	ΔRF	DNN	ΔSA	ΔRF	DNN	ΔSA	ΔRF	DNN	ΔSA	ΔRF
<b>AChE</b>	88.4	6.6	-3.2	85.3	-4.6	7.5	87.0	1.6	1.6	0.737	0.024	0.030
<b>ADORA2A</b>	97.6	2.8	-0.5	93.2	2.0	4.2	96.1	2.5	1.1	0.912	0.054	0.024
<b>ADRA2A</b>	91.3	11.2	2.0	93.9	-1.2	-1.2	92.7	4.3	0.2	0.853	0.084	0.004
<b>AR</b>	66.5	-0.8	1.1	99.1	1.4	1.2	90.5	0.8	1.2	0.749	0.026	0.036
<b>ADRB1</b>	92.7	7.0	0.3	89.5	-2.5	1.5	91.2	2.5	0.9	0.823	0.046	0.017
<b>ADRB2</b>	72.9	-2.3	-3.3	89.9	2.2	1.4	81.6	0.0	-0.9	0.639	0.004	-0.014
<b>OPRD1</b>	97.1	1.1	-1.2	81.0	-0.3	4.5	92.4	0.7	0.4	0.813	0.018	0.011
<b>DRD1</b>	77.4	0.9	-3.7	96.6	1.5	4.3	89.2	1.4	1.2	0.773	0.030	0.028
<b>DRD2</b>	98.3	1.9	-1.0	84.8	5.7	7.8	96.1	2.5	0.5	0.855	0.091	0.021
<b>SLC6A3</b>	89.9	1.3	-3.1	94.5	1.9	4.9	91.8	1.5	0.2	0.837	0.032	0.010
<b>EDNRA</b>	93.8	-0.6	-3.4	95.6	1.7	4.8	94.6	0.4	0.4	0.893	0.010	0.009
<b>NR3C1</b>	74.5	2.3	0.7	96.9	0.1	0.6	90.1	0.7	0.6	0.760	0.018	0.015
<b>KCNH2</b>	84.4	15.7	-8.6	70.9	-11.5	17.4	79.1	5.0	1.6	0.558	0.059	0.036
<b>HRH1</b>	95.2	8.0	-0.6	88.4	-5.3	0.7	92.0	1.7	0.0	0.840	0.032	-0.001
<b>OPRM1</b>	94.8	1.2	-1.1	94.5	1.7	3.2	94.7	1.4	0.6	0.889	0.030	0.014
<b>CHRM1</b>	96.6	6.4	0.9	83.3	-2.9	0.7	91.7	2.9	0.8	0.821	0.062	0.019
<b>CHRM2</b>	93.9	2.9	0.0	94.5	1.1	3.2	94.2	1.9	1.8	0.883	0.039	0.035
<b>CHRM3</b>	91.9	3.4	-3.2	93.8	1.8	5.8	92.8	2.8	0.8	0.854	0.053	0.017
<b>SLC6A2</b>	94.9	4.2	-0.2	92.5	-1.0	1.0	93.9	2.0	0.3	0.875	0.039	0.008
<b>HTR2A</b>	99.1	2.4	-0.4	88.2	-0.4	6.1	96.7	1.8	1.0	0.901	0.051	0.030
<b>HTR3A</b>	89.4	5.7	-1.0	98.2	-0.4	0.4	95.8	1.3	0.0	0.893	0.034	0.000
<b>SLC6A4</b>	98.4	2.7	-0.3	89.0	2.1	6.3	96.3	2.5	1.2	0.892	0.070	0.037
<b>LCK</b>	95.5	3.7	0.2	79.8	-2.6	-0.9	92.3	2.5	0.0	0.763	0.054	-0.002

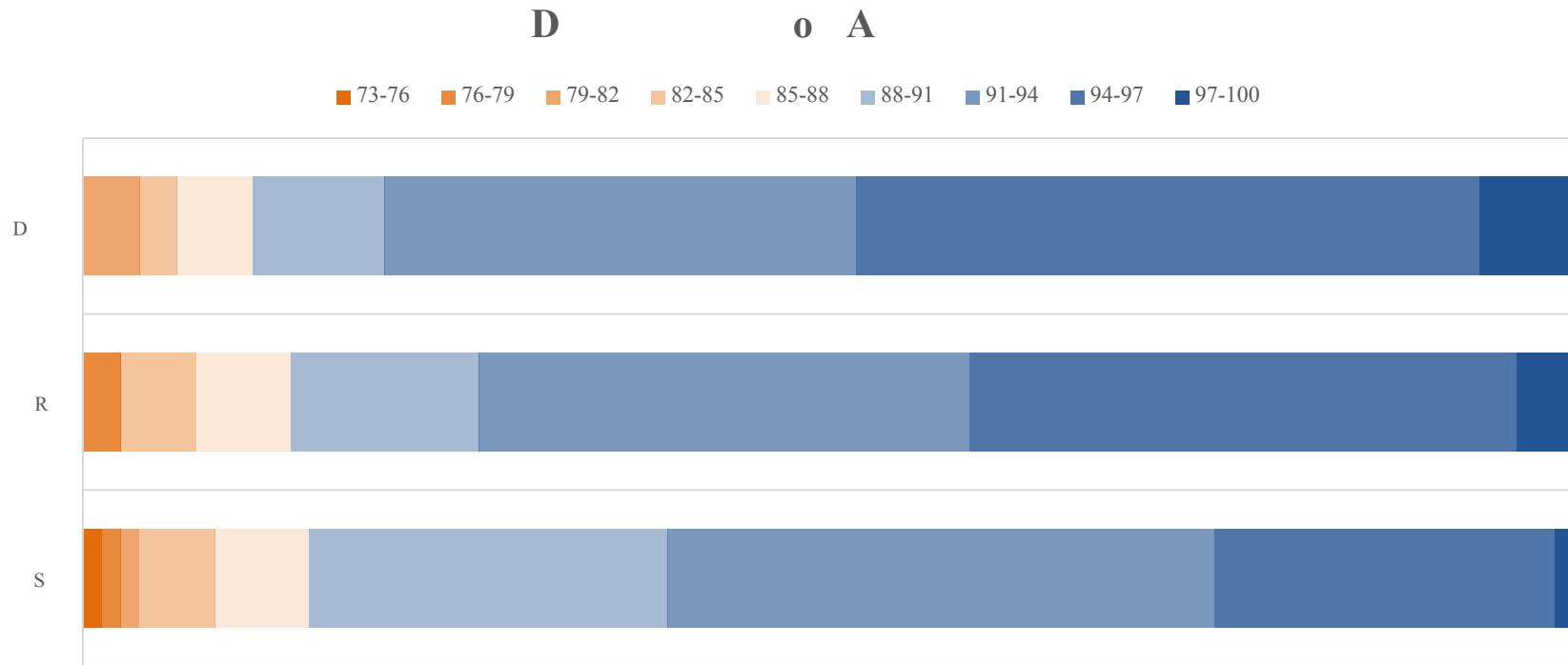
<b>AVPR1A</b>	93.9	1.9	0.6	99.3	1.5	4.8	97.2	1.6	3.2	0.941	0.034	0.068
<b>AGTR1</b>	87.3	0.0	3.4	99.3	1.0	1.9	94.5	0.6	2.6	0.888	0.014	0.054
<b>AKT1</b>	95.4	1.0	-1.4	91.3	4.4	6.6	94.1	2.1	1.1	0.864	0.049	0.028
<b>BACE1</b>	92.0	-1.1	-5.7	93.5	5.7	14.1	92.5	0.9	0.1	0.827	0.028	0.016
<b>BCHE</b>	85.6	7.1	-0.9	93.6	0.6	4.7	90.4	3.3	2.5	0.799	0.067	0.048
<b>CASP1</b>	69.1	5.3	-1.9	94.7	-0.1	-0.1	86.5	1.5	-0.8	0.680	0.039	-0.018
<b>CASP3</b>	84.8	3.4	3.7	94.9	-1.1	-1.1	91.0	0.6	0.7	0.809	0.013	0.015
<b>CASP8</b>	86.8	-4.9	-2.5	95.4	-2.1	-2.8	92.1	-4.1	-4.1	0.832	-0.060	-0.059
<b>CHRM5</b>	87.4	3.6	-4.2	95.3	1.5	4.0	92.3	2.3	0.9	0.835	0.048	0.015
<b>CHUK</b>	88.8	5.7	-3.3	97.4	0.4	0.0	95.2	1.7	-0.9	0.871	0.047	-0.024
<b>CSF1R</b>	94.3	5.9	-2.4	97.0	0.8	3.1	95.5	3.7	0.0	0.910	0.070	0.001
<b>CSNK1D</b>	91.4	12.4	3.8	94.8	-1.6	2.0	93.4	4.4	2.8	0.864	0.085	0.056
<b>EDNRB</b>	96.1	2.0	-0.5	94.4	-0.4	-0.7	95.1	0.6	-0.6	0.899	0.013	-0.012
<b>ELANE</b>	90.9	-0.4	-5.2	93.8	0.2	5.8	92.1	-0.1	-0.8	0.839	-0.001	-0.012
<b>EPHA2</b>	87.2	0.0	-0.7	99.6	1.1	1.8	95.4	0.7	1.0	0.899	0.018	0.023
<b>FGFR1</b>	96.8	5.9	0.8	92.0	-2.8	1.4	95.1	2.8	1.0	0.892	0.054	0.021
<b>FKBP1A</b>	88.1	-3.0	-6.9	97.4	-0.4	1.5	94.8	-1.1	-0.9	0.869	-0.028	-0.025
<b>FLT1</b>	91.6	1.6	-3.0	99.0	0.9	2.5	96.2	1.2	0.4	0.919	0.024	0.008
<b>FLT4</b>	91.9	10.7	0.0	96.5	-0.4	1.2	94.5	4.3	0.6	0.888	0.086	0.014
<b>FYN</b>	77.8	5.1	-3.0	98.2	0.4	1.5	92.7	1.6	0.3	0.809	0.044	0.006
<b>GSK3B</b>	96.8	12.2	-1.1	78.3	-5.2	2.5	90.4	6.2	0.1	0.785	0.121	0.001
<b>HDAC3</b>	94.1	2.3	0.3	94.8	1.5	2.7	94.5	2.0	1.6	0.890	0.039	0.032
<b>IGF1R</b>	94.6	-1.0	-2.1	95.5	1.3	5.1	94.9	-0.2	0.3	0.889	-0.003	0.011
<b>INSR</b>	91.7	1.7	-3.1	98.9	1.2	1.9	95.5	1.4	-0.5	0.912	0.028	-0.007

<b>KDR</b>	97.4	2.8	-0.3	73.1	-9.7	9.2	93.5	0.8	1.2	0.748	0.005	0.058
<b>LTB4R</b>	91.4	4.3	2.2	98.8	0.0	1.2	96.8	1.2	1.5	0.918	0.030	0.038
<b>LYN</b>	89.1	10.9	-1.8	98.0	2.7	2.7	95.4	5.2	1.4	0.888	0.127	0.030
<b>MAPK1</b>	43.5	-4.4	2.3	99.2	4.0	-0.2	79.3	1.0	0.6	0.557	0.043	0.013
<b>MAPK9</b>	95.5	3.5	-2.9	97.7	2.2	7.9	96.5	2.9	2.0	0.931	0.058	0.040
<b>MAPKAPK2</b>	86.9	5.1	-3.3	94.1	1.4	2.5	91.0	3.0	0.0	0.816	0.062	-0.001
<b>MET</b>	97.7	4.3	-1.0	91.9	3.2	8.4	95.9	4.0	1.9	0.904	0.091	0.045
<b>MMP13</b>	94.9	1.5	-2.1	94.7	3.3	10.6	94.8	2.1	2.3	0.887	0.045	0.054
<b>MMP2</b>	95.5	1.7	0.0	89.2	-3.6	6.0	93.2	-0.2	2.1	0.852	-0.006	0.048
<b>MMP3</b>	94.7	1.8	-1.7	92.4	1.2	8.8	93.8	1.5	2.1	0.868	0.033	0.047
<b>MMP9</b>	81.6	-0.2	-5.0	88.8	-1.5	6.9	84.6	-0.8	0.0	0.696	-0.016	0.011
<b>NEK2</b>	77.0	9.4	-2.7	98.5	0.7	1.0	94.0	2.6	0.3	0.813	0.085	0.007
<b>P2RY1</b>	92.7	-2.4	-2.4	100.0	1.5	3.4	97.7	0.3	1.5	0.947	0.007	0.035
<b>PAK4</b>	89.4	7.0	-4.7	99.3	0.8	1.1	96.9	2.2	-0.3	0.914	0.064	-0.009
<b>PDE4A</b>	90.8	2.9	-1.1	94.9	-0.4	0.5	93.1	1.0	-0.3	0.859	0.020	-0.005
<b>PDE5A</b>	90.1	3.4	-4.8	96.5	2.8	7.3	93.0	3.1	0.6	0.862	0.062	0.016
<b>PIK3CA</b>	98.9	1.5	-0.4	93.3	-1.5	4.6	97.2	0.6	1.2	0.934	0.014	0.027
<b>PPARG</b>	69.5	-0.8	-2.9	96.1	3.4	2.0	86.0	1.8	0.2	0.702	0.041	0.006
<b>PTPN1</b>	76.6	9.5	-3.9	89.7	-2.6	3.1	84.7	2.0	0.4	0.673	0.046	0.005
<b>PTPN11</b>	64.8	26.2	14.8	91.9	-3.4	-3.4	85.7	3.4	0.8	0.584	0.153	0.052
<b>PTPN2</b>	67.9	2.5	2.5	96.0	-1.7	2.3	90.1	-0.7	2.4	0.687	-0.022	0.069
<b>RAF1</b>	99.7	4.2	0.0	95.2	-1.1	1.5	97.7	1.8	0.7	0.954	0.038	0.013
<b>RARA</b>	63.1	1.9	1.9	99.4	1.8	0.0	95.2	1.9	0.3	0.742	0.092	0.013
<b>RARB</b>	85.9	11.3	5.6	99.9	1.1	0.0	98.8	1.9	0.5	0.913	0.137	0.033

<b>ROCK1</b>	94.3	5.4	-2.5	92.0	-3.6	1.1	93.2	1.2	-0.9	0.864	0.021	-0.018
<b>RPS6KA5</b>	73.7	12.3	0.0	100.0	1.5	2.7	95.3	3.4	2.2	0.835	0.135	0.080
<b>SIRT2</b>	70.8	2.3	5.6	95.2	-0.6	-1.6	89.8	0.0	0.0	0.692	0.003	0.006
<b>SIRT3</b>	76.7	-2.4	-4.7	98.5	0.8	0.8	95.4	0.3	0.0	0.802	0.010	-0.005
<b>SRC</b>	94.7	4.6	-2.7	88.7	0.7	8.1	92.4	3.1	1.5	0.839	0.064	0.029
<b>TACR2</b>	87.6	-1.6	-4.4	100.0	2.4	2.4	96.0	1.1	0.2	0.910	0.029	0.008
<b>TBXA2R</b>	88.8	-0.4	-2.1	94.9	-0.4	1.4	93.0	-0.4	0.3	0.838	-0.010	0.003
<b>TEK</b>	89.9	2.5	-4.1	97.8	2.6	1.9	94.5	2.6	-0.6	0.887	0.053	-0.013

**Table S13.** A comparison between DNNs and previously published structural alert (SA) and random forest (RF) models trained on the same training data and evaluated on the same test data. Test data results are shown here, including the change in result from models previously published in Wedlake *et al.*<sup>38</sup> ( $\Delta$ ). These are coloured blue or orange, to show increased or decreased performance respectively. Full results can be found in Table S14. SE=sensitivity, SP=specificity, ACC=accuracy, MCC=Matthews correlation coefficient.





**Figure S1.** Comparison charts for the distribution of test accuracy and MCC values between DNNs and previously published structural alert (SA) and random forest (RF) models trained on the same training data and evaluated on the same test data. Numbers on each category indicate the number of models falling into that class.

Target Gene	Training Set									
	TP	FN	TN	FP	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>AChE</b>	1878	126	1344	123	0.98	93.7	91.6	92.8	0.853	0.98
<b>ADORA2A</b>	2911	46	1545	37	1.00	98.4	97.7	98.2	0.960	1.00
<b>ADRA2A</b>	615	34	758	11	0.99	94.8	98.6	96.8	0.936	0.99
<b>AR</b>	1397	592	5441	28	0.94	70.2	99.5	91.7	0.784	0.94
<b>ADRB1</b>	936	24	745	61	0.99	97.5	92.4	95.2	0.903	0.99
<b>ADRB2</b>	1146	316	1432	69	0.95	78.4	95.4	87.0	0.750	0.95
<b>OPRD1</b>	2197	43	820	84	0.99	98.1	90.7	96.0	0.901	0.99
<b>DRD1</b>	831	198	1462	22	0.97	80.8	98.5	91.2	0.823	0.97
<b>DRD2</b>	4220	42	796	59	0.99	99.0	93.1	98.0	0.929	0.99
<b>SLC6A3</b>	1773	97	1404	41	0.99	94.8	97.2	95.8	0.916	0.99
<b>EDNRA</b>	932	30	834	25	0.99	96.9	97.1	97.0	0.939	0.99
<b>NR3C1</b>	1773	501	5146	97	0.93	78.0	98.1	92.0	0.809	0.93
<b>KCNH2</b>	3463	154	2190	231	0.98	95.7	90.5	93.6	0.867	0.98
<b>HRH1</b>	938	25	792	30	1.00	97.4	96.4	96.9	0.938	1.00
<b>OPRM1</b>	2600	61	1685	38	0.99	97.7	97.8	97.7	0.953	0.99
<b>CHRM1</b>	1465	19	859	78	0.99	98.7	91.7	96.0	0.916	0.99
<b>CHRM2</b>	1187	38	1468	38	0.99	96.9	97.5	97.2	0.944	0.99
<b>CHRM3</b>	1141	49	821	18	0.99	95.9	97.9	96.7	0.933	0.99
<b>SLC6A2</b>	2145	78	1388	61	0.99	96.5	95.8	96.2	0.921	0.99
<b>HTR2A</b>	2775	22	726	45	1.00	99.2	94.2	98.1	0.944	1.00
<b>HTR3A</b>	329	19	775	3	1.00	94.5	99.6	98.0	0.954	1.00
<b>SLC6A4</b>	3041	16	830	22	1.00	99.5	97.4	99.0	0.971	1.00

<b>LCK</b>	1259	24	377	28	0.99	98.1	93.1	96.9	0.915	0.99	
<b>AVPR1A</b>	448	8	782	5	1.00	98.2	99.4	99.0	0.977	1.00	
<b>AGTR1</b>	555	46	878	1	0.99	92.3	99.9	96.8	0.935	0.99	
<b>AKT1</b>	2022	50	865	35	0.99	97.6	96.1	97.1	0.933	0.99	
<b>BACE1</b>	4211	263	1881	94	0.99	94.1	95.2	94.5	0.874	0.99	
<b>BCHE</b>	900	138	1556	57	0.98	86.7	96.5	92.6	0.845	0.98	
<b>CASP1</b>	736	274	2366	62	0.97	72.9	97.4	90.2	0.759	0.97	
<b>CASP3</b>	776	105	1296	58	0.98	88.1	95.7	92.7	0.847	0.98	
<b>CASP8</b>	802	79	1303	51	0.99	91.0	96.2	94.2	0.878	0.99	
<b>CHRM5</b>	475	37	795	15	0.99	92.8	98.1	96.1	0.917	0.99	
<b>CHUK</b>	211	16	794	10	0.99	93.0	98.8	97.5	0.926	0.99	
<b>CSF1R</b>	970	30	782	7	1.00	97.0	99.1	97.9	0.959	1.00	
<b>CSNK1D</b>	499	25	762	14	0.99	95.2	98.2	97.0	0.938	0.99	
<b>EDNRB</b>	595	9	905	26	1.00	98.5	97.2	97.7	0.953	1.00	
<b>ELANE</b>	1488	106	987	31	0.99	93.4	97.0	94.8	0.893	0.99	
<b>EPHA2</b>	374	13	829	0	1.00	96.6	100.0	98.9	0.975	1.00	
<b>FGFR1</b>	1593	43	857	63	0.99	97.4	93.2	95.9	0.910	0.99	
<b>FKBP1A</b>	240	13	728	13	1.00	94.9	98.2	97.4	0.931	1.00	
<b>FLT1</b>	748	41	1576	20	0.99	94.8	98.7	97.4	0.942	0.99	
<b>FLT4</b>	473	15	816	13	0.99	96.9	98.4	97.9	0.954	0.99	
<b>FYN</b>	295	26	805	1	1.00	91.9	99.9	97.6	0.941	1.00	
<b>GSK3B</b>	1905	28	846	84	0.99	98.6	91.0	96.1	0.910	0.99	
<b>HDAC3</b>	769	26	846	43	0.99	96.7	95.2	95.9	0.918	0.99	
<b>IGF1R</b>	1822	55	807	14	1.00	97.1	98.3	97.4	0.941	1.00	

<b>INSR</b>	647	11	825	4	1.00	98.3	99.5	99.0	0.980	1.00	
<b>KDR</b>	5730	101	1003	198	0.99	98.3	83.5	95.7	0.846	0.99	
<b>LTB4R</b>	235	22	784	1	0.99	91.4	99.9	97.8	0.940	0.99	
<b>LYN</b>	330	14	787	6	1.00	95.9	99.2	98.2	0.958	1.00	
<b>MAPK1</b>	2121	2579	8294	59	0.84	45.1	99.3	79.8	0.572	0.84	
<b>MAPK9</b>	894	22	818	5	1.00	97.6	99.4	98.4	0.969	1.00	
<b>MAPKAPK2</b>	567	48	843	30	0.99	92.2	96.6	94.8	0.892	0.99	
<b>MET</b>	2143	36	807	28	1.00	98.3	96.6	97.9	0.947	1.00	
<b>MMP13</b>	1762	62	787	23	0.99	96.6	97.2	96.8	0.926	0.99	
<b>MMP2</b>	2119	66	1158	103	0.99	97.0	91.8	95.1	0.894	0.99	
<b>MMP3</b>	1247	62	740	36	0.99	95.3	95.4	95.3	0.900	0.99	
<b>MMP9</b>	1711	229	1280	104	0.96	88.2	92.5	90.0	0.799	0.96	
<b>NEK2</b>	199	25	779	6	0.99	88.8	99.2	96.9	0.910	0.99	
<b>P2RY1</b>	420	17	829	7	1.00	96.1	99.2	98.1	0.958	1.00	
<b>PAK4</b>	279	16	831	1	0.99	94.6	99.9	98.5	0.961	0.99	
<b>PDE4A</b>	454	26	773	10	1.00	94.6	98.7	97.1	0.939	1.00	
<b>PDE5A</b>	1129	69	869	19	0.99	94.2	97.9	95.8	0.915	0.99	
<b>PIK3CA</b>	3514	28	1462	85	1.00	99.2	94.5	97.8	0.947	1.00	
<b>PPARG</b>	2424	853	5343	160	0.94	74.0	97.1	88.5	0.754	0.94	
<b>PTPN1</b>	1004	133	1559	79	0.98	88.3	95.2	92.4	0.842	0.98	
<b>PTPN11</b>	238	28	903	12	0.98	89.5	98.7	96.6	0.902	0.98	
<b>PTPN2</b>	215	43	897	11	0.99	83.3	98.8	95.4	0.862	0.99	
<b>RAF1</b>	1004	13	800	15	1.00	98.7	98.2	98.5	0.969	1.00	
<b>RARA</b>	169	84	2465	0	0.99	66.8	100.0	96.9	0.804	0.99	

<b>RARB</b>	208	19	2524	0	0.98	91.6	100.0	99.3	0.954	0.98
<b>ROCK1</b>	952	28	813	30	0.99	97.1	96.4	96.8	0.936	0.99
<b>RPS6KA5</b>	154	13	777	0	1.00	92.2	100.0	98.6	0.952	1.00
<b>SIRT2</b>	243	29	946	31	0.98	89.3	96.8	95.2	0.859	0.98
<b>SIRT3</b>	87	21	801	10	0.98	80.6	98.8	96.6	0.831	0.98
<b>SRC</b>	2034	46	1078	62	0.99	97.8	94.6	96.6	0.926	0.99
<b>TACR2</b>	549	77	1384	1	0.99	87.7	99.9	96.1	0.910	0.99
<b>TBXA2R</b>	715	55	1376	34	0.98	92.9	97.6	95.9	0.910	0.98
<b>TEK</b>	540	49	854	7	0.99	91.7	99.2	96.1	0.921	0.99

Target Gene	Test									
	TP	FN	TN	FP	ROC-AUC	SE	SP	ACC	MCC	ROC-AUC
<b>AChE</b>	539	71	423	73	0.92	88.4	85.3	87.0	0.737	0.92
<b>ADORA2A</b>	962	24	467	34	0.98	97.6	93.2	96.1	0.912	0.98
<b>ADRA2A</b>	179	17	230	15	0.97	91.3	93.9	92.7	0.853	0.97
<b>AR</b>	431	217	1798	17	0.88	66.5	99.1	90.5	0.749	0.88
<b>ADRB1</b>	279	22	247	29	0.94	92.7	89.5	91.2	0.823	0.94
<b>ADRB2</b>	352	131	461	52	0.89	72.9	89.9	81.6	0.639	0.89
<b>OPRD1</b>	744	22	255	60	0.98	97.1	81.0	92.4	0.813	0.98
<b>DRD1</b>	250	73	490	17	0.93	77.4	96.6	89.2	0.773	0.93
<b>DRD2</b>	1410	24	239	43	0.98	98.3	84.8	96.1	0.855	0.98
<b>SLC6A3</b>	576	65	446	26	0.97	89.9	94.5	91.8	0.837	0.97
<b>EDNRA</b>	303	20	280	13	0.97	93.8	95.6	94.6	0.893	0.97
<b>NR3C1</b>	554	190	1676	54	0.91	74.5	96.9	90.1	0.760	0.91

	1078	200	585	240	0.85	84.4	70.9	79.1	0.558	0.85
<b>KCNH2</b>	1078	200	585	240	0.85	84.4	70.9	79.1	0.558	0.85
<b>HRH1</b>	298	15	251	33	0.97	95.2	88.4	92.0	0.840	0.97
<b>OPRM1</b>	901	49	553	32	0.98	94.8	94.5	94.7	0.889	0.98
<b>CHRM1</b>	513	18	254	51	0.96	96.6	83.3	91.7	0.821	0.96
<b>CHRM2</b>	386	25	498	29	0.98	93.9	94.5	94.2	0.883	0.98
<b>CHRM3</b>	319	28	258	17	0.97	91.9	93.8	92.8	0.854	0.97
<b>SLC6A2</b>	654	35	455	37	0.97	94.9	92.5	93.9	0.875	0.97
<b>HTR2A</b>	951	9	232	31	0.99	99.1	88.2	96.7	0.901	0.99
<b>HTR3A</b>	93	11	272	5	0.95	89.4	98.2	95.8	0.893	0.95
<b>SLC6A4</b>	970	16	252	31	0.99	98.4	89.0	96.3	0.892	0.99
<b>LCK</b>	429	20	95	24	0.94	95.5	79.8	92.3	0.763	0.94
<b>AVPR1A</b>	153	10	270	2	0.98	93.9	99.3	97.2	0.941	0.98
<b>AGTR1</b>	179	26	301	2	0.98	87.3	99.3	94.5	0.888	0.98
<b>AKT1</b>	662	32	293	28	0.98	95.4	91.3	94.1	0.864	0.98
<b>BACE1</b>	1419	123	590	41	0.97	92.0	93.5	92.5	0.827	0.97
<b>BCHE</b>	310	52	498	34	0.95	85.6	93.6	90.4	0.799	0.95
<b>CASP1</b>	248	111	730	41	0.91	69.1	94.7	86.5	0.680	0.91
<b>CASP3</b>	251	45	450	24	0.96	84.8	94.9	91.0	0.809	0.96
<b>CASP8</b>	257	39	452	22	0.97	86.8	95.4	92.1	0.832	0.97
<b>CHRM5</b>	146	21	262	13	0.97	87.4	95.3	92.3	0.835	0.97
<b>CHUK</b>	79	10	259	7	0.98	88.8	97.4	95.2	0.871	0.98
<b>CSF1R</b>	317	19	256	8	0.99	94.3	97.0	95.5	0.910	0.99
<b>CSNK1D</b>	170	16	238	13	0.97	91.4	94.8	93.4	0.864	0.97
<b>EDNRB</b>	197	8	288	17	0.99	96.1	94.4	95.1	0.899	0.99

<b>ELANE</b>	491	49	335	22	0.97	90.9	93.8	92.1	0.839	0.97	
<b>EPHA2</b>	123	18	272	1	0.98	87.2	99.6	95.4	0.899	0.98	
<b>FGFR1</b>	510	17	265	23	0.99	96.8	92.0	95.1	0.892	0.99	
<b>FKBP1A</b>	89	12	260	7	0.99	88.1	97.4	94.8	0.869	0.99	
<b>FLT1</b>	274	25	479	5	0.99	91.6	99.0	96.2	0.919	0.99	
<b>FLT4</b>	171	15	245	9	0.98	91.9	96.5	94.5	0.888	0.98	
<b>FYN</b>	77	22	266	5	0.94	77.8	98.2	92.7	0.809	0.94	
<b>GSK3B</b>	597	20	256	71	0.96	96.8	78.3	90.4	0.785	0.96	
<b>HDAC3</b>	241	15	239	13	0.98	94.1	94.8	94.5	0.890	0.98	
<b>IGF1R</b>	574	33	298	14	0.99	94.6	95.5	94.9	0.889	0.99	
<b>INSR</b>	211	19	261	3	0.99	91.7	98.9	95.5	0.912	0.99	
<b>KDR</b>	1934	51	277	102	0.97	97.4	73.1	93.5	0.748	0.97	
<b>LTB4R</b>	85	8	244	3	0.97	91.4	98.8	96.8	0.918	0.97	
<b>LYN</b>	98	12	251	5	0.97	89.1	98.0	95.4	0.888	0.97	
<b>MAPK1</b>	657	852	2701	23	0.77	43.5	99.2	79.3	0.557	0.77	
<b>MAPK9</b>	298	14	260	6	0.99	95.5	97.7	96.5	0.931	0.99	
<b>MAPKAPK2</b>	186	28	269	17	0.97	86.9	94.1	91.0	0.816	0.97	
<b>MET</b>	676	16	285	25	0.99	97.7	91.9	95.9	0.904	0.99	
<b>MMP13</b>	535	29	286	16	0.99	94.9	94.7	94.8	0.887	0.99	
<b>MMP2</b>	719	34	372	45	0.98	95.5	89.2	93.2	0.852	0.98	
<b>MMP3</b>	426	24	242	20	0.98	94.7	92.4	93.8	0.868	0.98	
<b>MMP9</b>	524	118	413	52	0.91	81.6	88.8	84.6	0.696	0.91	
<b>NEK2</b>	57	17	271	4	0.97	77.0	98.5	94.0	0.813	0.97	
<b>P2RY1</b>	114	9	267	0	0.99	92.7	100.0	97.7	0.947	0.99	

<b>PAK4</b>	76	9	269	2	0.99	89.4	99.3	96.9	0.914	0.99
<b>PDE4A</b>	157	16	222	12	0.97	90.8	94.9	93.1	0.859	0.97
<b>PDE5A</b>	318	35	278	10	0.98	90.1	96.5	93.0	0.862	0.98
<b>PIK3CA</b>	1169	13	503	36	0.99	98.9	93.3	97.2	0.934	0.99
<b>PPARG</b>	754	331	1707	70	0.91	69.5	96.1	86.0	0.702	0.91
<b>PTPN1</b>	256	78	488	56	0.92	76.6	89.7	84.7	0.673	0.92
<b>PTPN11</b>	57	31	273	24	0.90	64.8	91.9	85.7	0.584	0.90
<b>PTPN2</b>	55	26	289	12	0.90	67.9	96.0	90.1	0.687	0.90
<b>RAF1</b>	333	1	256	13	1.00	99.7	95.2	97.7	0.954	1.00
<b>RARA</b>	65	38	779	5	0.90	63.1	99.4	95.2	0.742	0.90
<b>RARB</b>	61	10	823	1	0.96	85.9	99.9	98.8	0.913	0.96
<b>ROCK1</b>	297	18	253	22	0.99	94.3	92.0	93.2	0.864	0.99
<b>RPS6KA5</b>	42	15	263	0	0.95	73.7	100.0	95.3	0.835	0.95
<b>SIRT2</b>	63	26	296	15	0.89	70.8	95.2	89.8	0.692	0.89
<b>SIRT3</b>	33	10	260	4	0.94	76.7	98.5	95.4	0.802	0.94
<b>SRC</b>	592	33	347	44	0.97	94.7	88.7	92.4	0.839	0.97
<b>TACR2</b>	219	31	532	0	0.99	87.6	100.0	96.0	0.910	0.99
<b>TBXA2R</b>	206	26	469	25	0.96	88.8	94.9	93.0	0.838	0.96
<b>TEK</b>	179	20	265	6	0.98	89.9	97.8	94.5	0.887	0.98

Table S14. Model performance results for each target on the training/test split used to compare model performance to structural alert and random forest models. Performance statistics are shown for the training set first, followed by the test set. Model performances are reported as sensitivity (SE), specificity (SP), accuracy (ACC), Matthews correlation coefficient (MCC) and area under receiver operating characteristic curve (ROC-AUC).

t-Test: Paired Two Sample for Means - Accuracy

	SA vs DNN		RF vs DNN	
	SA	DNN	RF	DNN
Mean	92.81	93.73	93.76	93.73
Variance	12.31	9.82	10.75	9.82
Observations	79	79	79	79
Pearson Correlation	0.91		0.95	
Hypothesized Mean Difference	0		0	
df	78		78	
t Stat	-5.65		0.25	
	1.25861E-07		0.400478763	
P(T<=t) one-tail	1.66		1.66	
	2.51722E-12			
P(T<=t) two-tail	0.07		0.800957526	
t Critical two-tail	1.99		1.99	

t-Test: Paired Two Sample for Means - MCC

	SA vs DNN		RF vs DNN	
	SA	DNN	RF	DNN
Mean	0.7903	0.8321	0.8146	0.8321
Variance	0.0093	0.0079	0.0083	0.0079
Observations	79	79	79	79
Pearson Correlation	0.9196		0.9648	
Hypothesized Mean Difference	0		0	
df	78		78	
t Stat	-9.8296		-6.4893	
	1.3414E-15		3.62582E-09	
P(T<=t) one-tail	1.6646		1.6646	
	2.68279E-15			
P(T<=t) two-tail	0.0000550		7.25164E-09	
t Critical two-tail	1.9908		1.9908	

Z score test - Accuracy

	SA vs DNN		RF vs DNN	
	SA	DNN	RF	DNN
Mean	92.81	93.73	93.76	93.73
Variance	12.31	9.82	10.75	9.82
Z	-3.87		-1.49	
p	0.0000550		0.0679810	

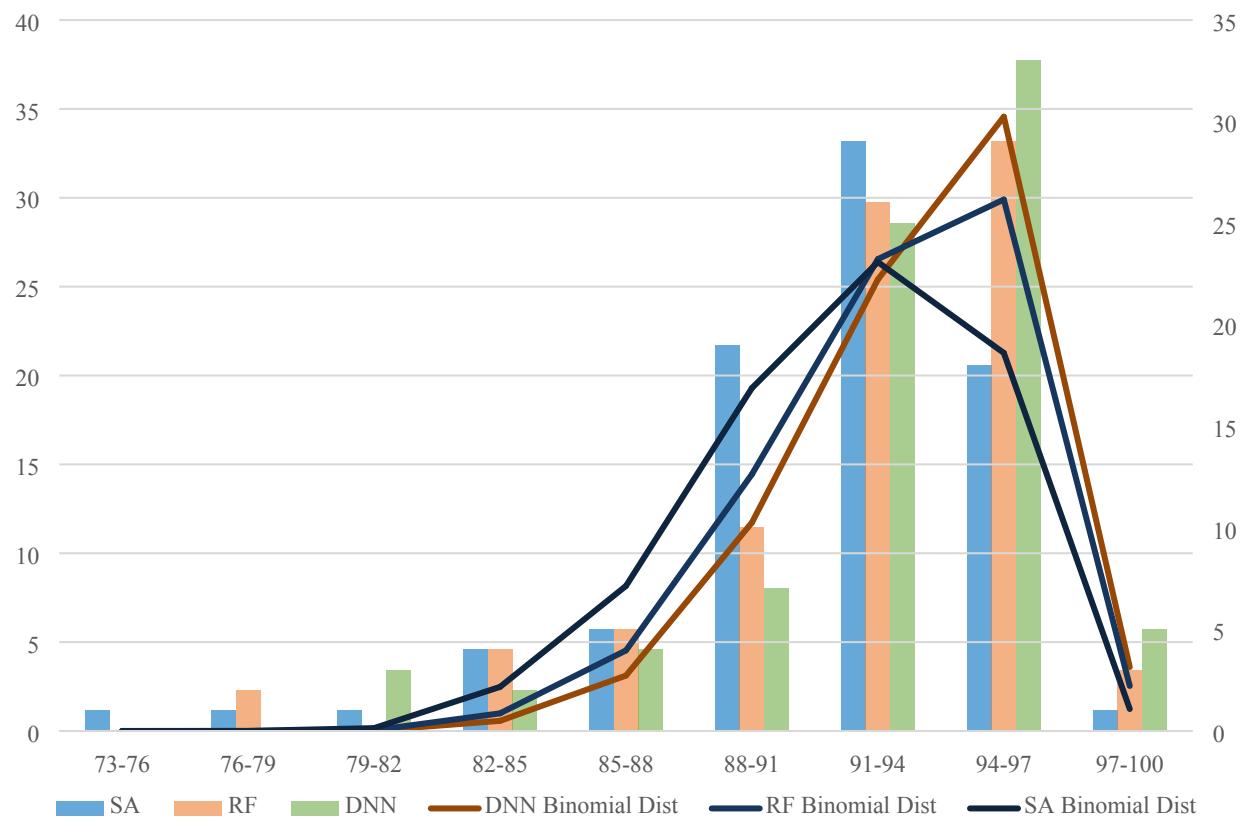
Z score test - MCC

	SA vs DNN		RF vs DNN	
	SA	DNN	RF	DNN

Mean	0.7903	0.8321	0.8146	0.8321
Variance	0.0093	0.0079	0.0083	0.0079
Z	-4.1936		-1.7595	
p	0.000014		0.03929	

Table S15. p-value analysis to show statistical significance between statistical performance for DNN models vs Sa and RF models. At  $\alpha=0.05$  DNNs show statistically significant performance increase in accuracy and MCC over SAs and statistically significant performance increase in MCC over RFs.

## Accuracy Model Comparison Histogram with Binomial Distributions



## MCC Model Comparison Histogram with Binomial Distributions

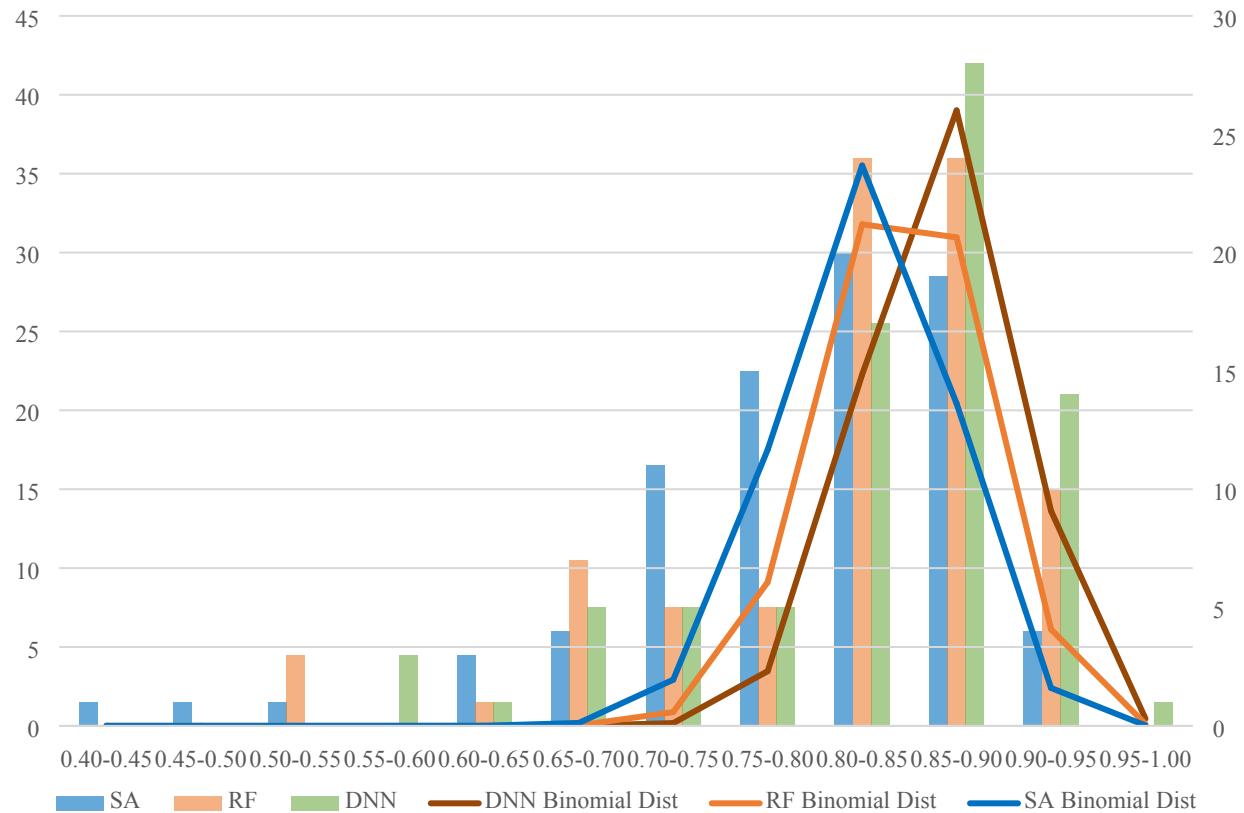


Figure S2. Histograms showing the distribution of test set model performance across the three modelling approaches overlaid with binomial distributions fitted to them. Accuracy binomial distributions are fit to probability values of 0.925 (SA), 0.935 (RF) and 0.94 (MCC) and MCC binomial distributions are fit to probability values of 0.83 (SA), 0.85 (RF) and 0.87 (MCC).

