

## Supplementary Information

### Electrocatalytic Upcycling of Polyethylene Terephthalate to Commodity Chemicals and H<sub>2</sub> fuel

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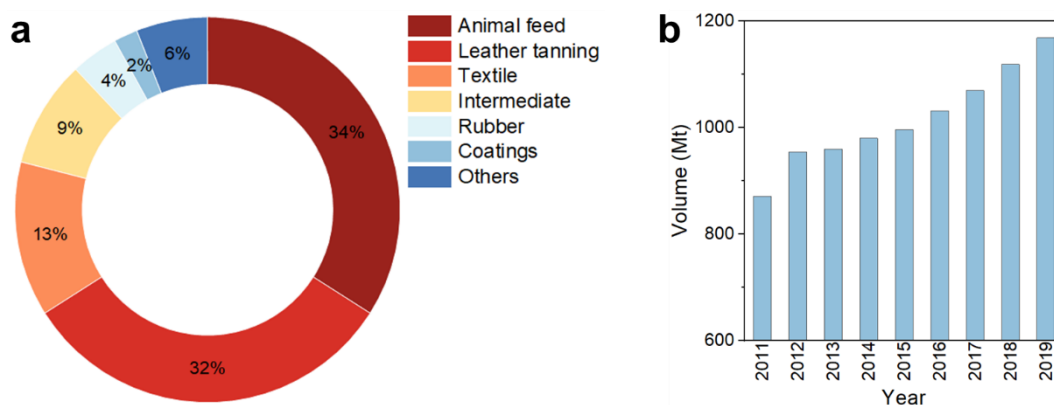
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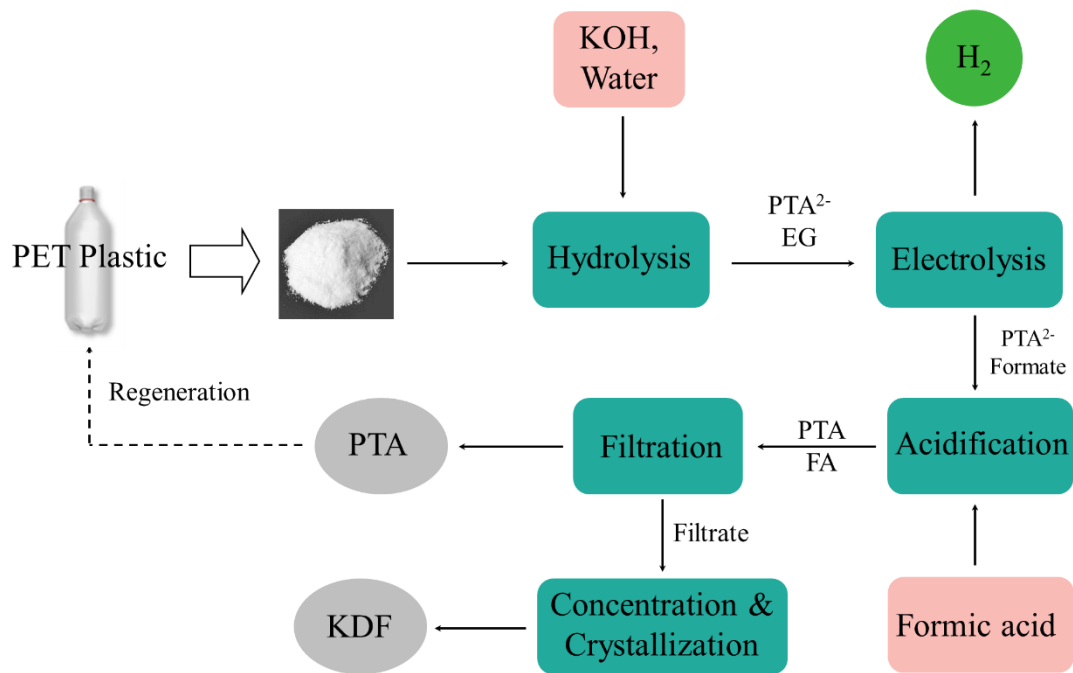
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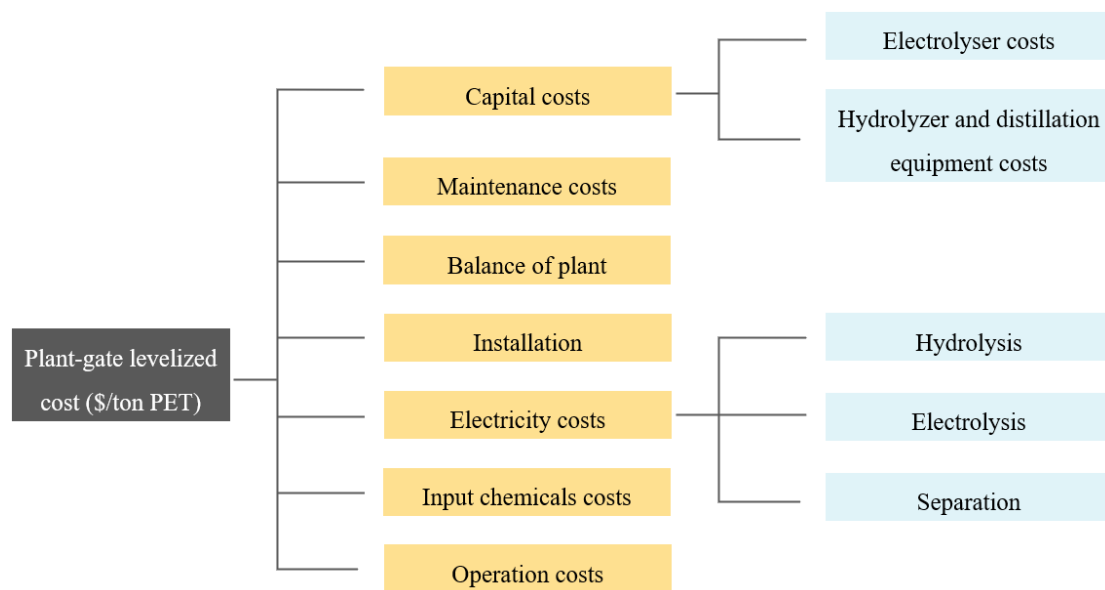
### Supplementary Figures



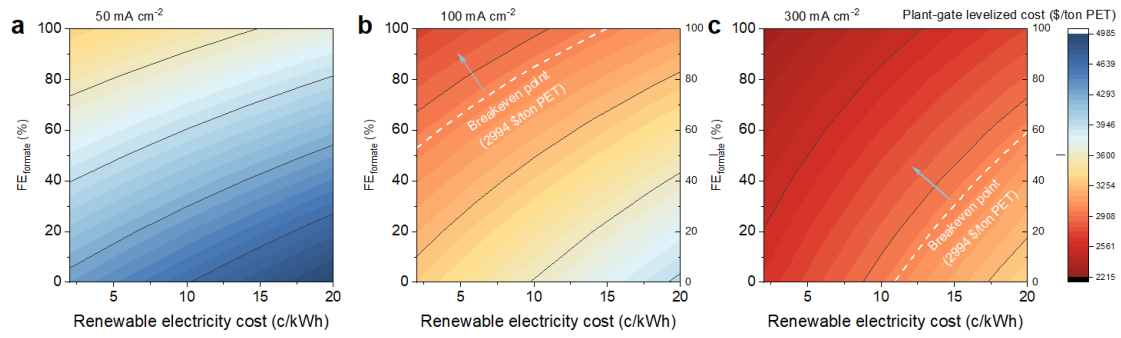
**Supplementary Figure 1 Trends of formic acid market. a** Application field of formic acid. The data are obtained from online, <https://www.oxfa.eu/en/markets/>. **b** The increasing demand of formic acid for feed additives. The data are obtained from Mordor Intelligence. <https://www.mordorintelligence.com/industry-reports/formic-acid-market>.



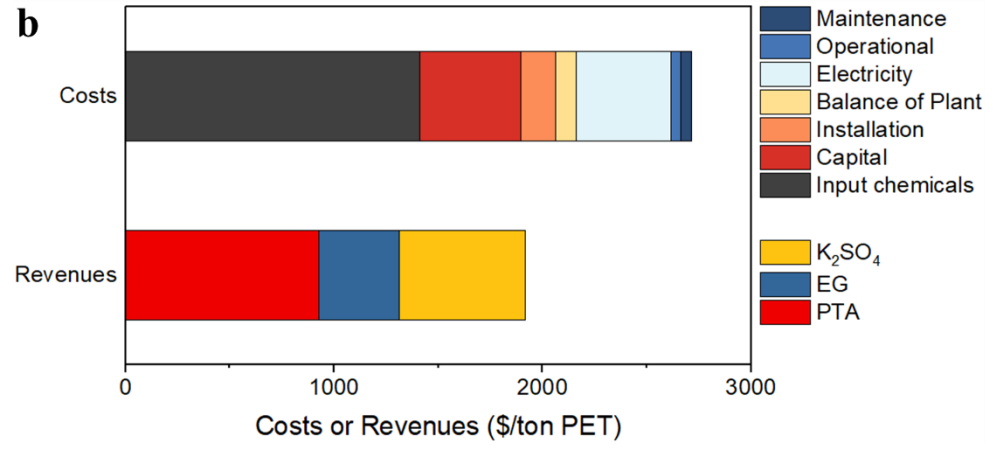
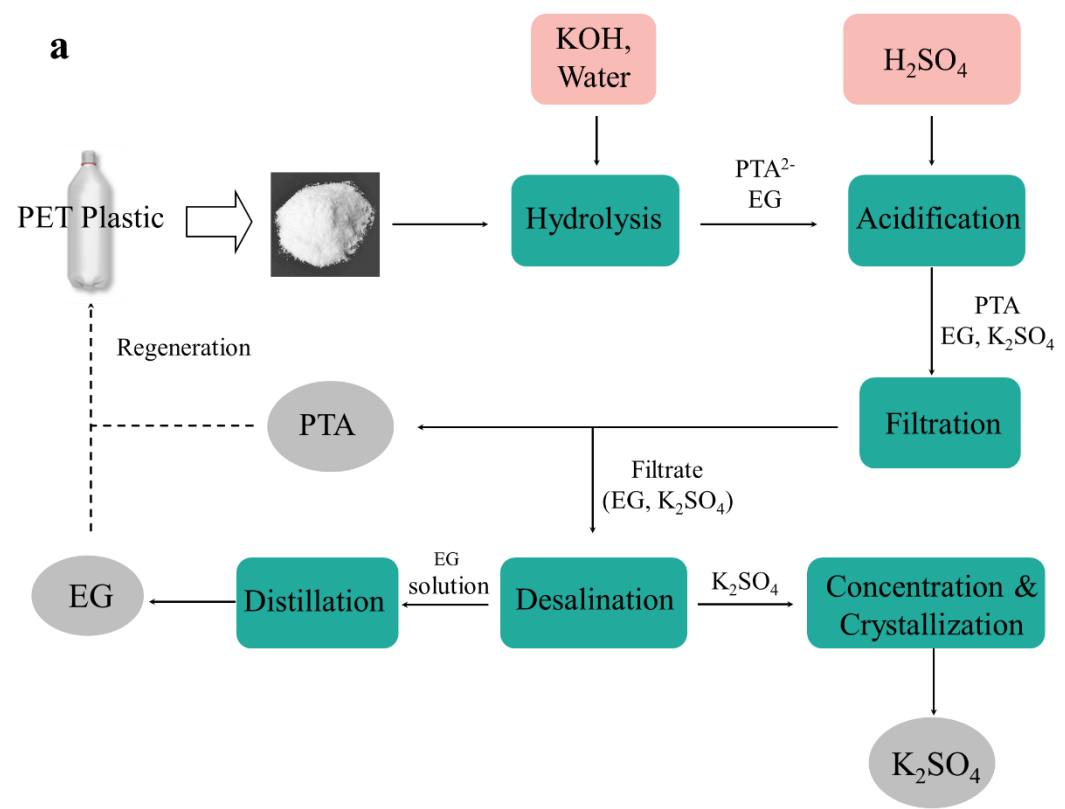
**Supplementary Figure 2** Schematic operating units of the integrated process for PET upcycling (Route I). The targeted products are PTA, H<sub>2</sub>, and KDF.



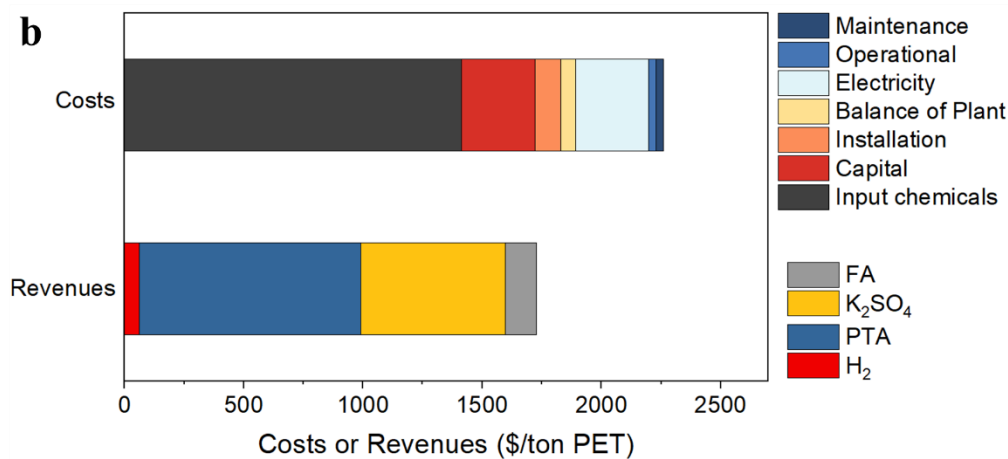
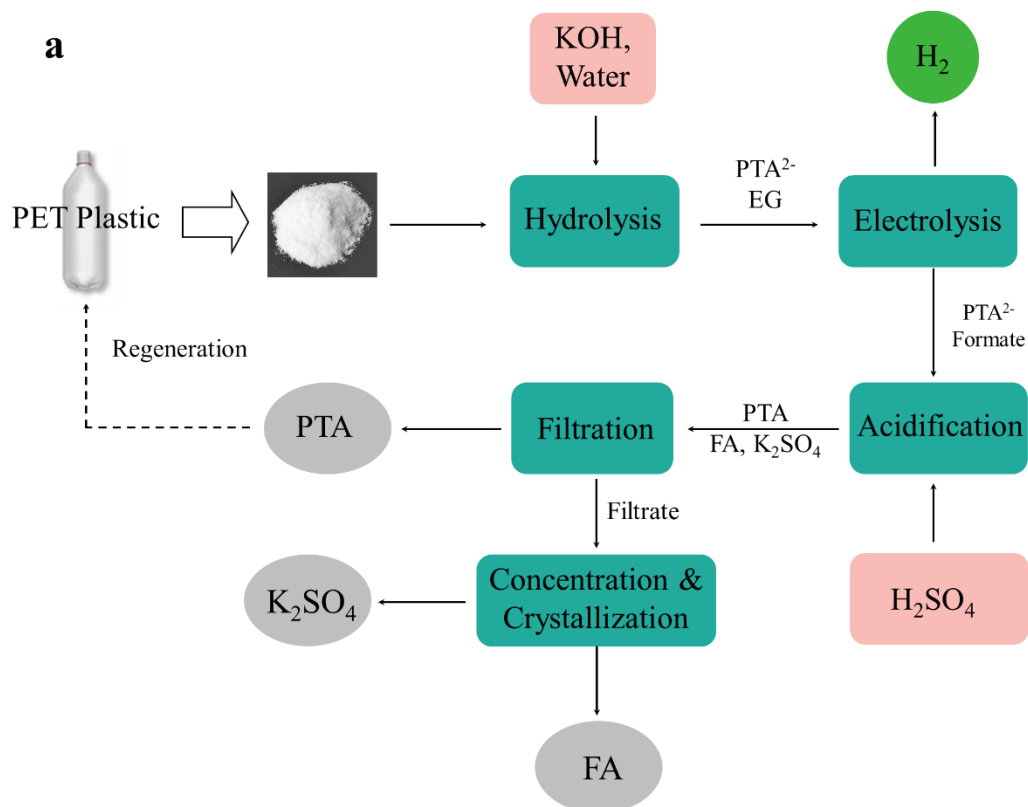
**Supplementary Figure 3** Model used for calculating the plant-gate levelized cost of the process.



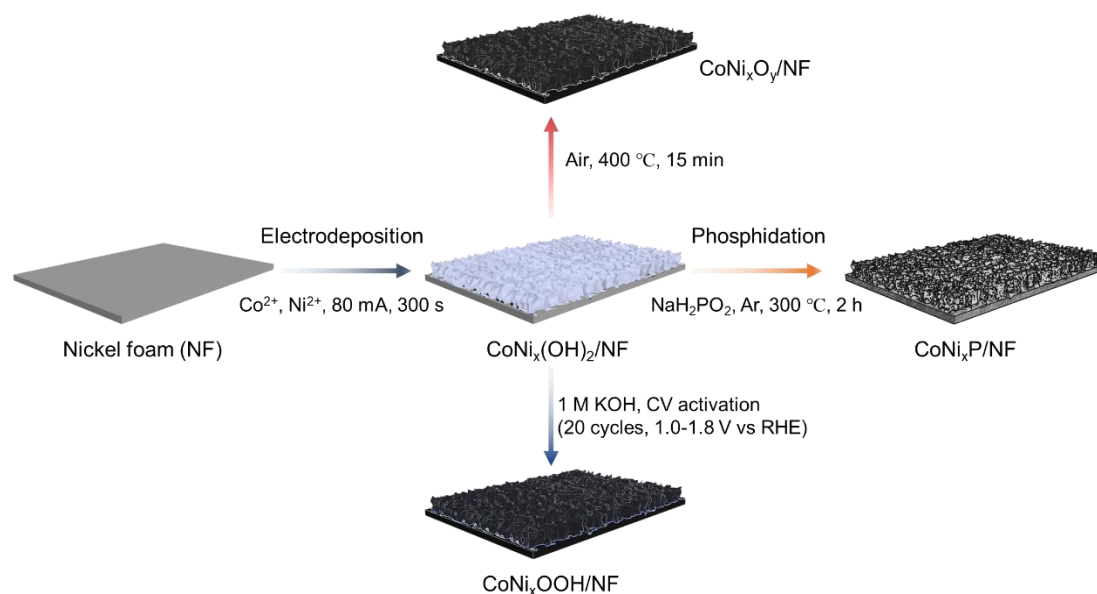
**Supplementary Figure 4 Plant-gate leveled cost for processing PET as function of Faradaic efficiency to formate ( $FE_{\text{formate}}$ ), renewable electricity cost, and current density. a 50 mA cm<sup>-2</sup>, b 100 mA cm<sup>-2</sup>, c 300 mA cm<sup>-2</sup>.**



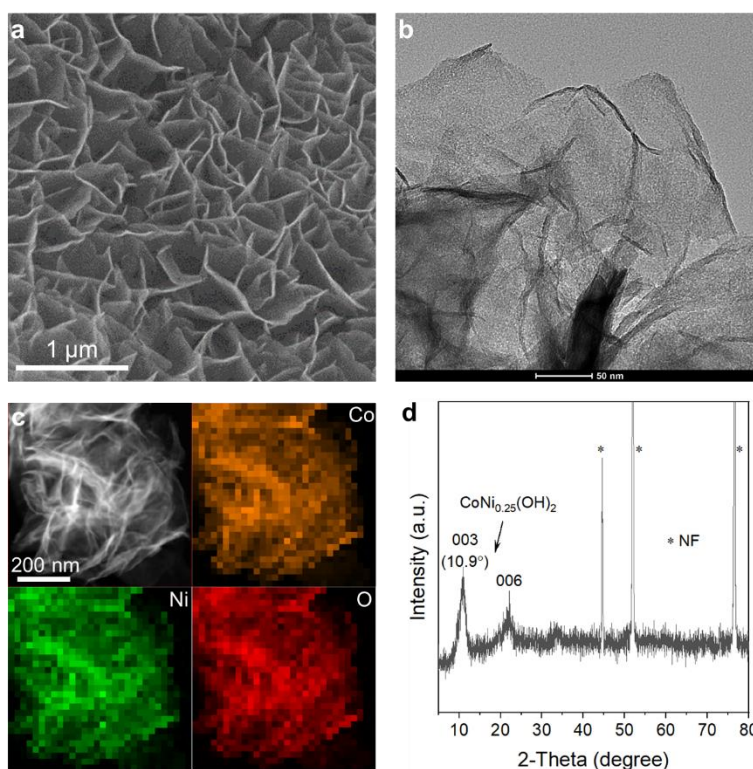
**Supplementary Figure 5 Route II for PTA and EG recycling.** **a** Schematic illustration of the process, the final products are  $K_2SO_4$ , EG, and PTA. **b** TEA analysis of this process. Assuming 90% of  $K_2SO_4$  and 100% of EG are recycled.



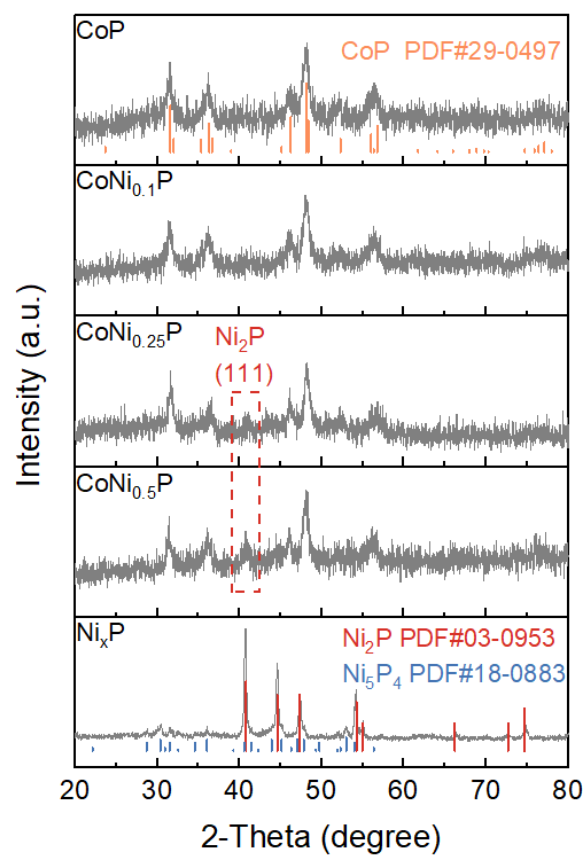
**Supplementary Figure 6 Route III for PET reclaim.** **a** Schematic illustration of the process, the final products are FA,  $K_2SO_4$ , PTA, and  $H_2$ . **b** TEA analysis of this process. Assuming 90% of  $K_2SO_4$  and 100% of FA are recycled.



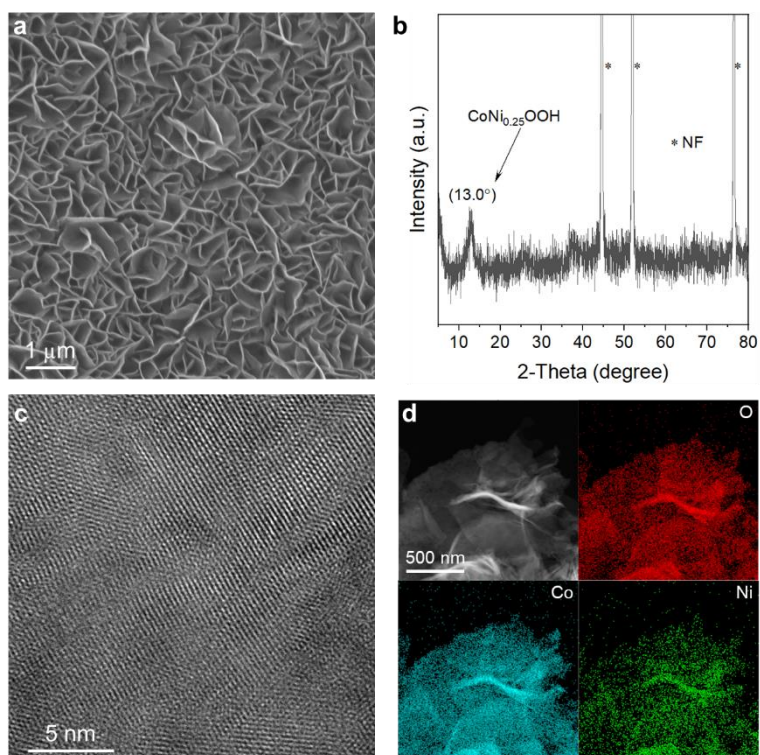
**Supplementary Figure 7** Schematic illustration of the preparation of  $\text{CoNi}_x\text{P}/\text{NF}$  and  $\text{CoNi}_x\text{OOH}/\text{NF}$ .



**Supplementary Figure 8** Characterization of  $\text{CoNi}_{0.25}(\text{OH})_2/\text{NF}$  material. **a** SEM image of  $\text{CoNi}_{0.25}(\text{OH})_2$  nanoarray on NF. **b** TEM image of  $\text{CoNi}_{0.25}(\text{OH})_2$  nanosheet. **c** Elemental mapping of  $\text{CoNi}_{0.25}(\text{OH})_2$  nanosheet. **d** XRD pattern of  $\text{CoNi}_{0.25}(\text{OH})_2/\text{NF}$ . a.u.: arbitrary units.

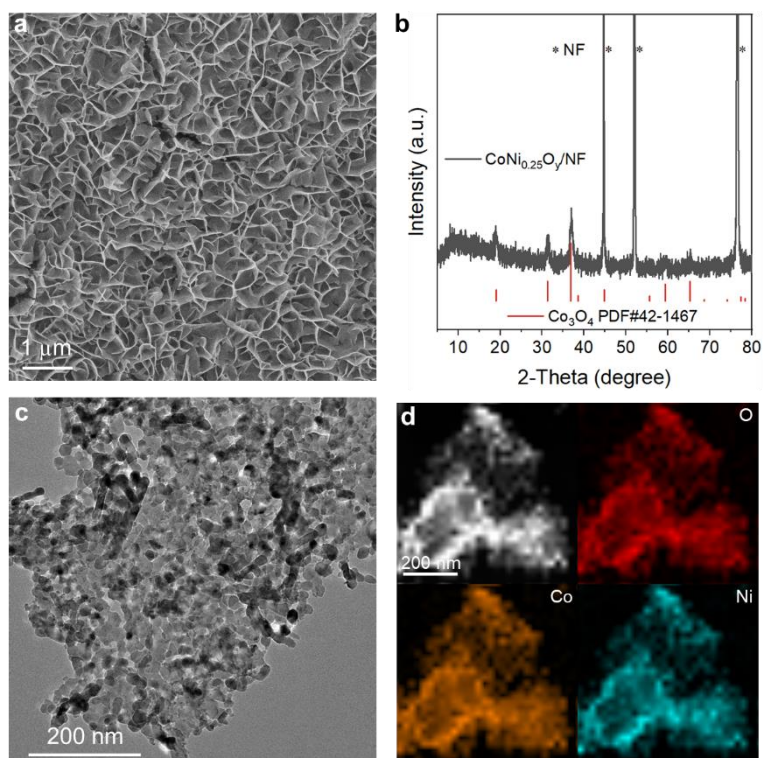


**Supplementary Figure 9** XRD patterns of  $\text{CoNi}_x\text{P}$  and  $\text{Ni}_2\text{P}$ .

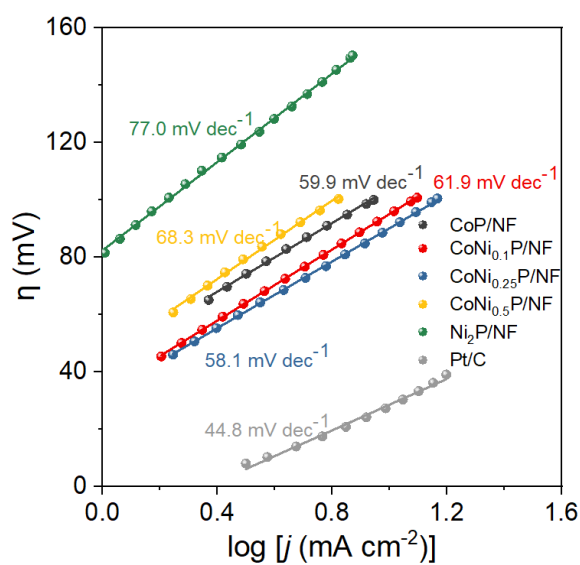


**Supplementary Figure 10** Characterization of crystalline  $\text{CoNi}_{0.25}\text{OOH}/\text{NF}$  material. **a** SEM image of  $\text{CoNi}_{0.25}\text{OOH}$  nanoarray on NF. **b** XRD pattern of  $\text{CoNi}_{0.25}\text{OOH}/\text{NF}$ . **c** HR-TEM image of

CoNi<sub>0.25</sub>OOH nanosheet. **d** Elemental mapping of CoNi<sub>0.25</sub>OOH nanosheet.

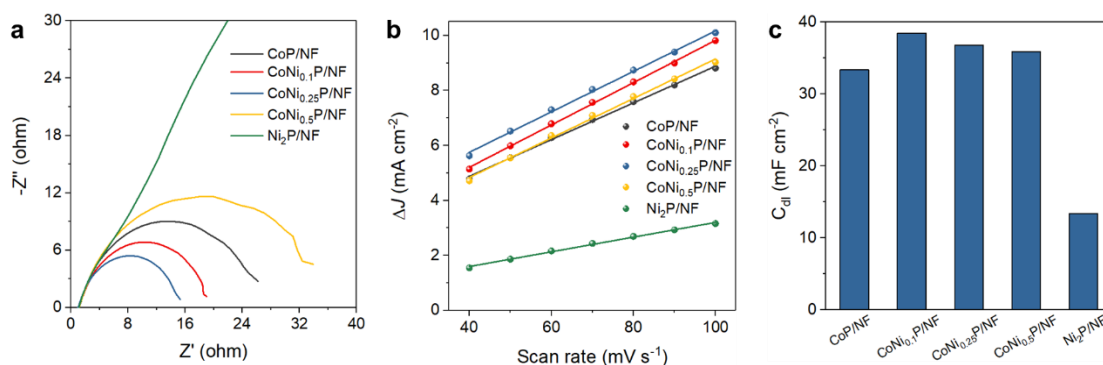


**Supplementary Figure 11 Characterization of CoNi<sub>0.25</sub>O<sub>y</sub>/NF material.** **a** SEM image of CoNi<sub>0.25</sub>O<sub>y</sub> nanoarray on NF. **b** XRD pattern of CoNi<sub>0.25</sub>O<sub>y</sub>/NF. **c** TEM image of CoNi<sub>0.25</sub>O<sub>y</sub> nanosheet. **d** Elemental mapping of CoNi<sub>0.25</sub>O<sub>y</sub> nanosheet.

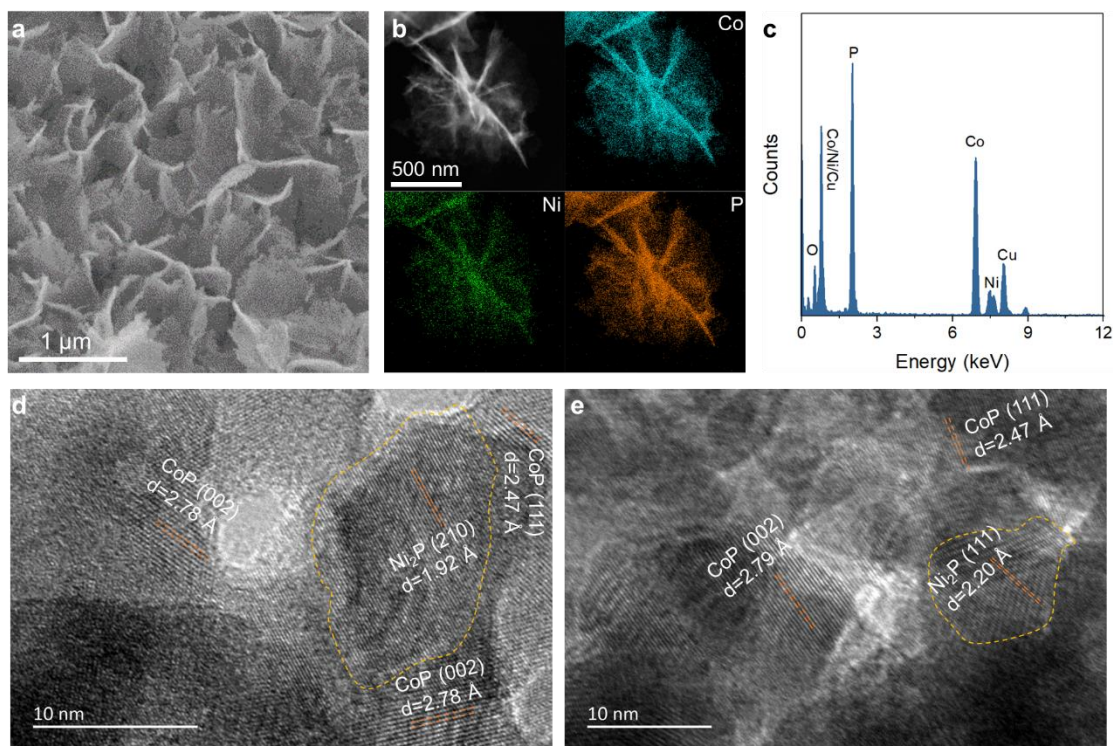


**Supplementary Figure 12 Tafel plots derived from HER polarization curves.**



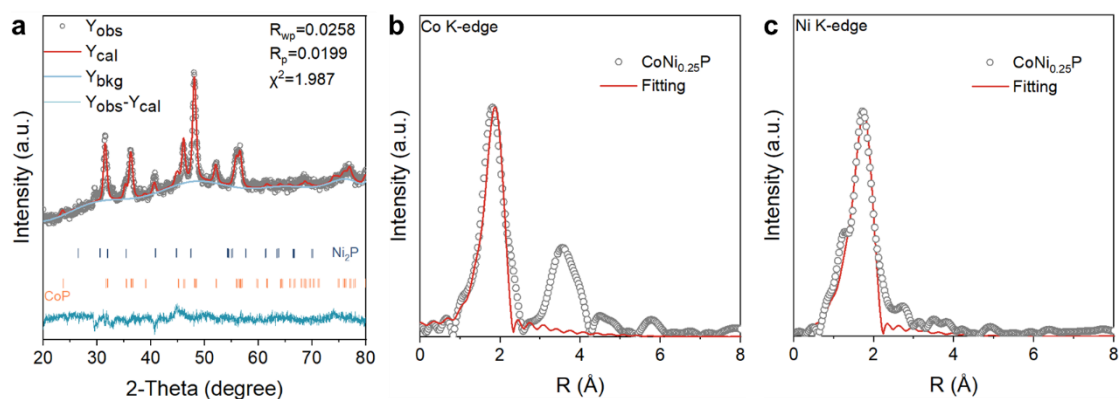


**Supplementary Figure 13 a** Electrochemical impedance spectra (EIS) of  $\text{CoNi}_x\text{P/NF}$  and  $\text{Ni}_2\text{P/NF}$  catalysts at a potential of  $-1.07\text{ V}$  vs RHE. **b** Charging current density differences ( $\Delta J = J_a - J_c$ ) plotted against scan rates. The linear slope is equivalent to twice of the double-layer capacitance ( $C_{dl}$ ). **c**  $C_{dl}$  of  $\text{CoNi}_x\text{P/NF}$  and  $\text{Ni}_2\text{P/NF}$  catalysts.

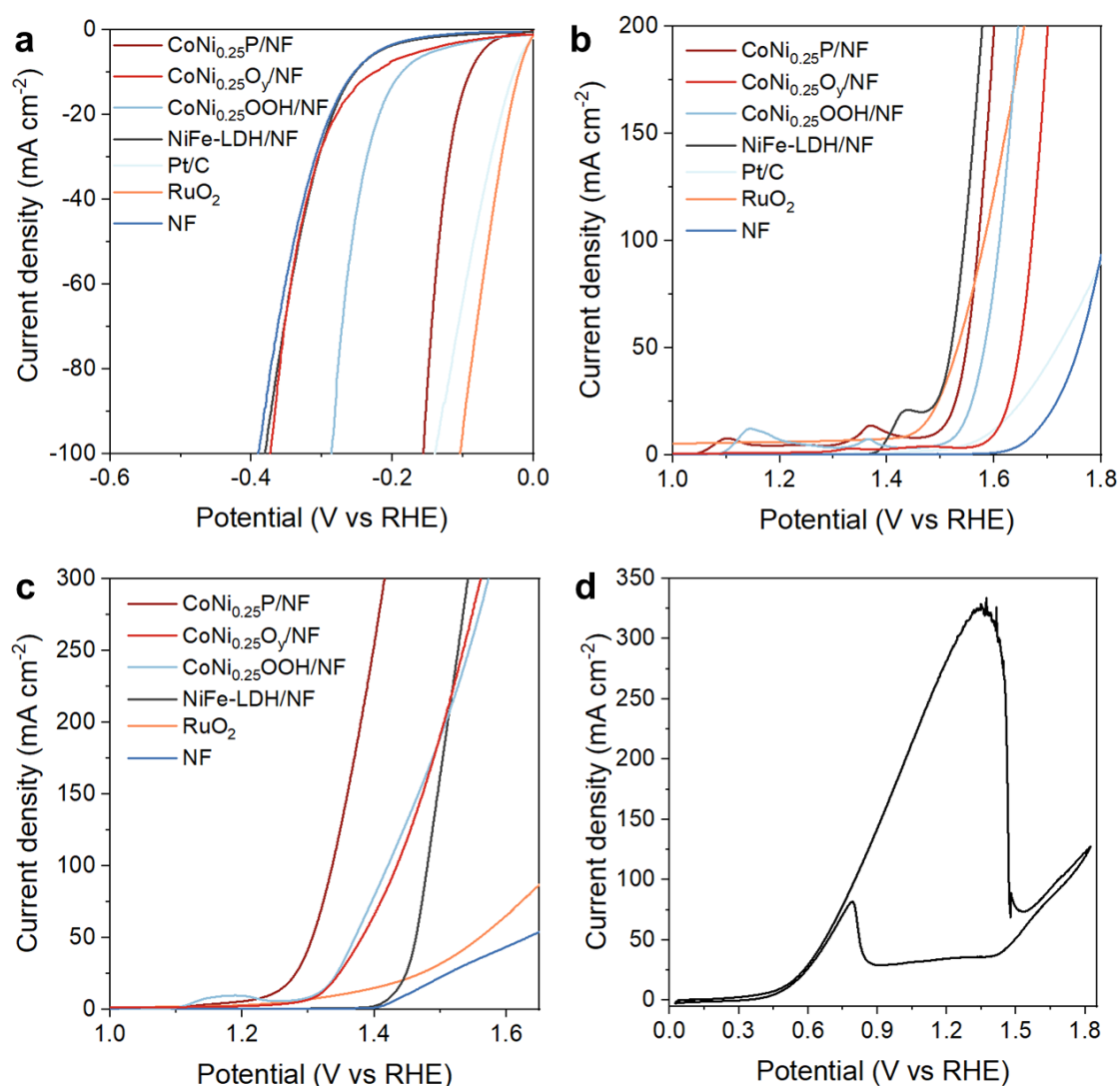


**Supplementary Figure 14 Characterization of  $\text{CoNi}_{0.25}\text{P/NF}$  material.** **a** SEM image of  $\text{CoNi}_{0.25}\text{P}$  nanoarray on NF. **b** Elemental mapping of  $\text{CoNi}_{0.25}\text{P}$  nanosheet. **c** EDS spectrum, **d**, **e** HRTEM images of  $\text{CoNi}_{0.25}\text{P}$  nanosheet at different regions.

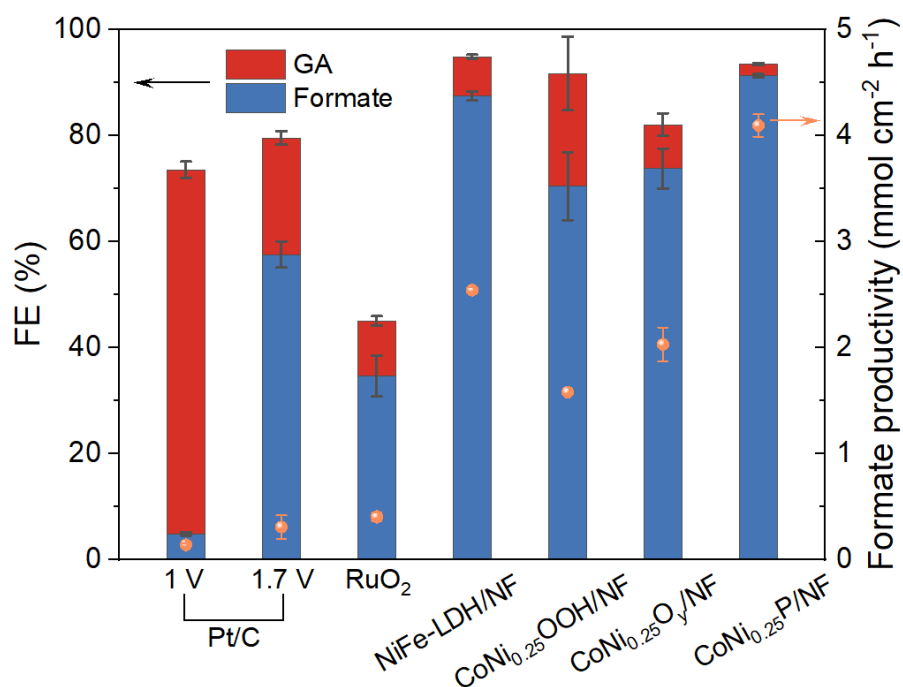




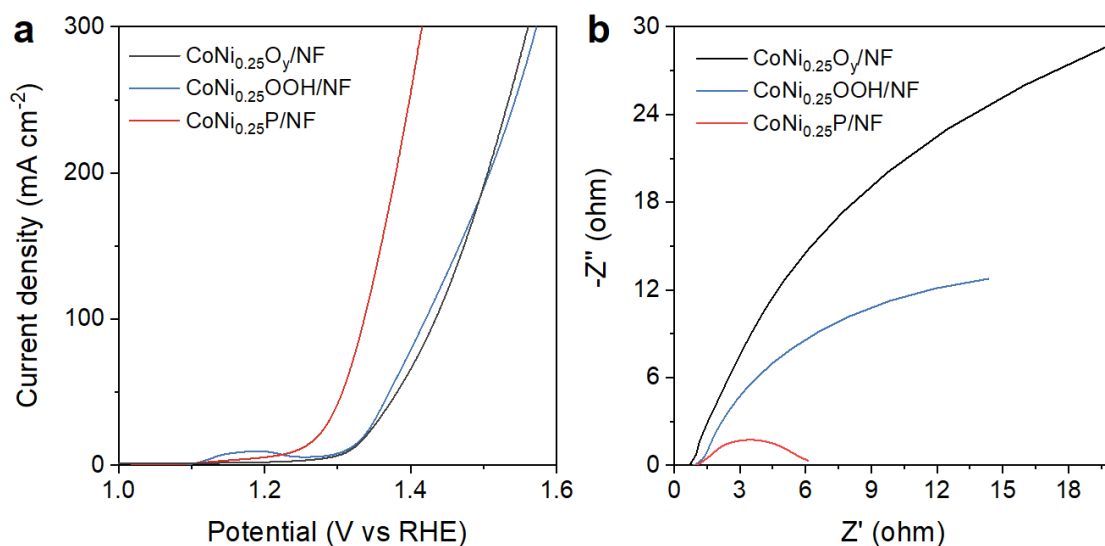
**Supplementary Figure 15** a XRD Rietveld refinement and EXAFS fitting of **b** Co K-edge and **c** Ni K-edge of  $\text{CoNi}_{0.25}\text{P}$  material.



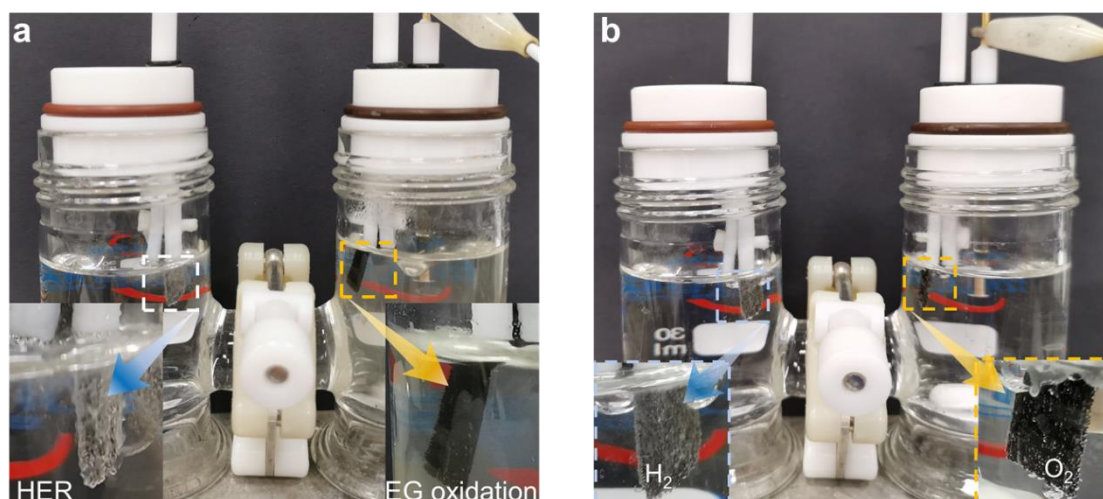
**Supplementary Figure 16** Comparison of the catalytic activities of  $\text{CoNi}_{0.25}\text{P}/\text{NF}$  and common electrocatalysts. **a** LSV curves of catalysts for HER. **b** LSV curves of catalysts for OER. **c** LSV curves of catalysts for EG oxidation. **d** CV polarization curve of Pt/C for EG oxidation.



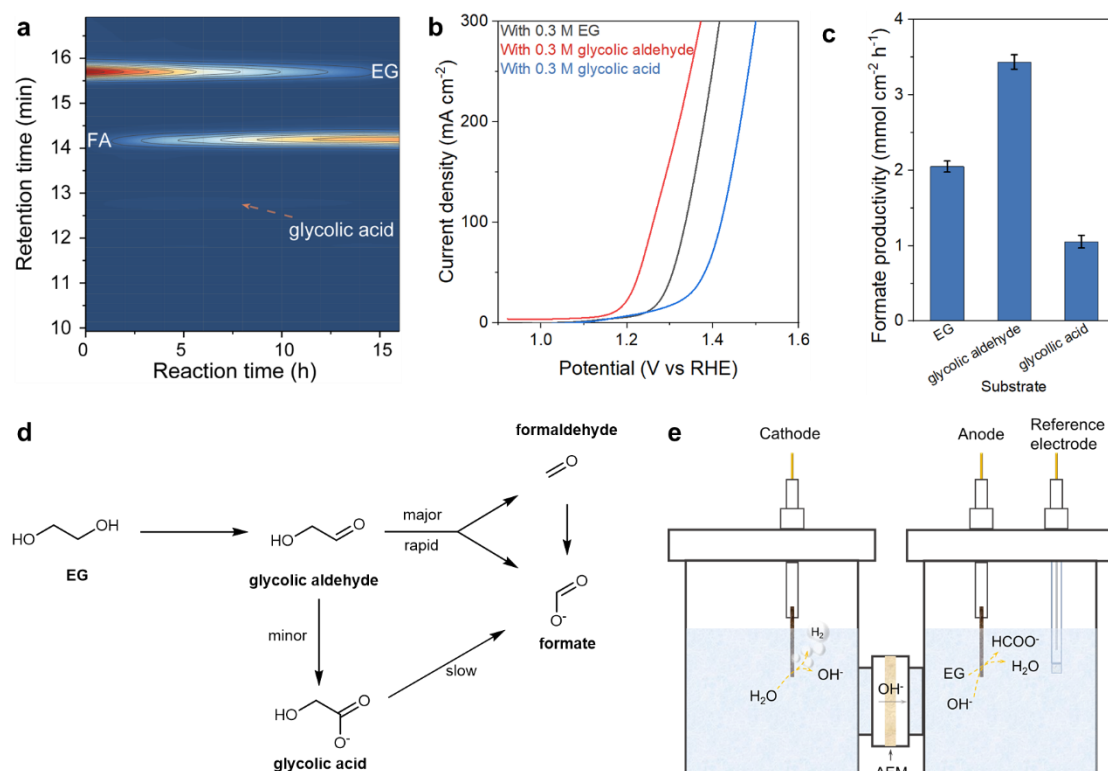
**Supplementary Figure 17 FE of EG oxidation over various catalysts.** Reaction conditions: 0.3 M EG in 1 M KOH electrolyte at 1.7 V vs RHE for 0.5 h over RuO<sub>2</sub>, NiFe-LDH/NF, CoNi<sub>0.25</sub>OOH/NF, CoNi<sub>0.25</sub>O<sub>y</sub>/NF, and CoNi<sub>0.25</sub>P/NF. Error bars correspond to the standard deviation of three measurements.



**Supplementary Figure 18 Electrochemical evaluation of CoNi<sub>0.25</sub>(OH)<sub>2</sub>/NF derived phosphide, oxy(hydroxide), and oxide for EG oxidation.** **a** LSV curves (85% iR corrected) of materials in 1M KOH with 0.3 M EG. **b** EIS of materials for EG oxidation at a potential of 1.25 V vs RHE.

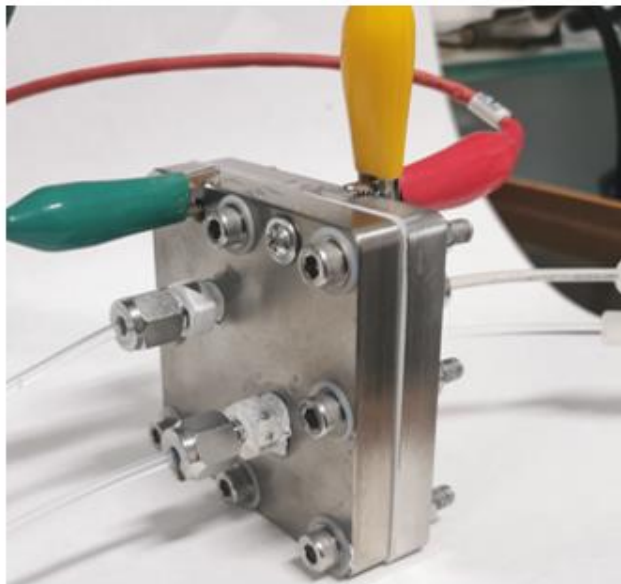


**Supplementary Figure 19** **a** Photograph of H-cell configuration for HER//EG oxidation, showing the evolution of H<sub>2</sub> over CoNi<sub>0.25</sub>P/NF. **b** Photograph of H-cell configuration for HER//OER, showing the evolution of H<sub>2</sub> and O<sub>2</sub> bubbles over CoNi<sub>0.25</sub>P/NF at cathode and anode, respectively.

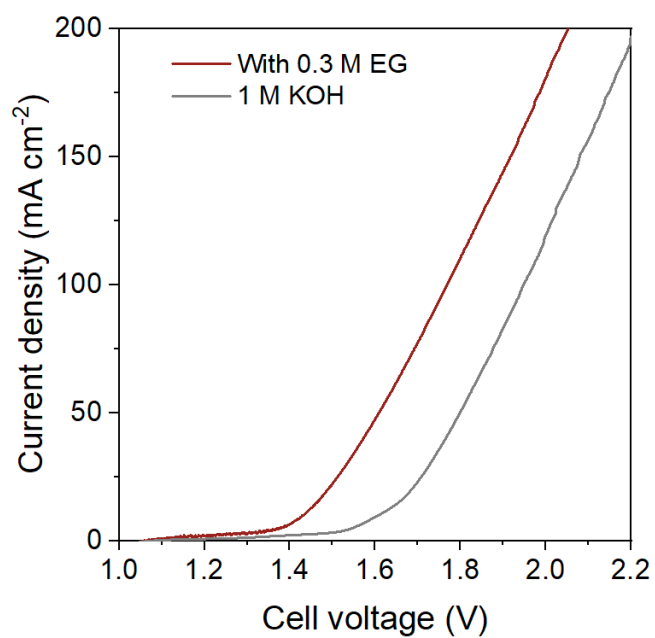


**Supplementary Figure 20** **a** HPLC chromatograms of EG oxidation as function of reaction time. Reaction conditions: 0.3 M EG in 1 M KOH electrolyte at 1.5 V vs RHE over CoNi<sub>0.25</sub>P/NF anode. **b** LSV curves (85% iR corrected) for organic oxidation in 1 M KOH with 0.3 M substrate. **c** Formate

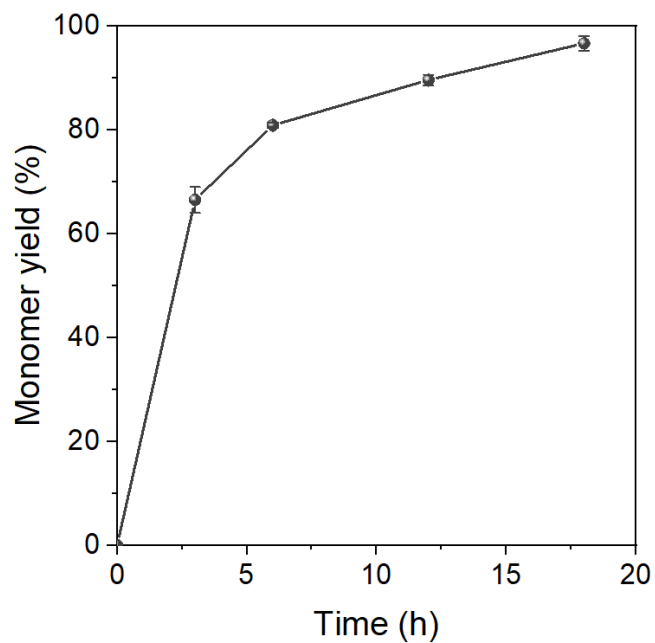
productivity at constant potential (1.5 V vs RHE) for different substrate. **d** Proposed reaction route for electrocatalytic EG oxidation. **e** The schematic illustration of whole electrolysis reaction.



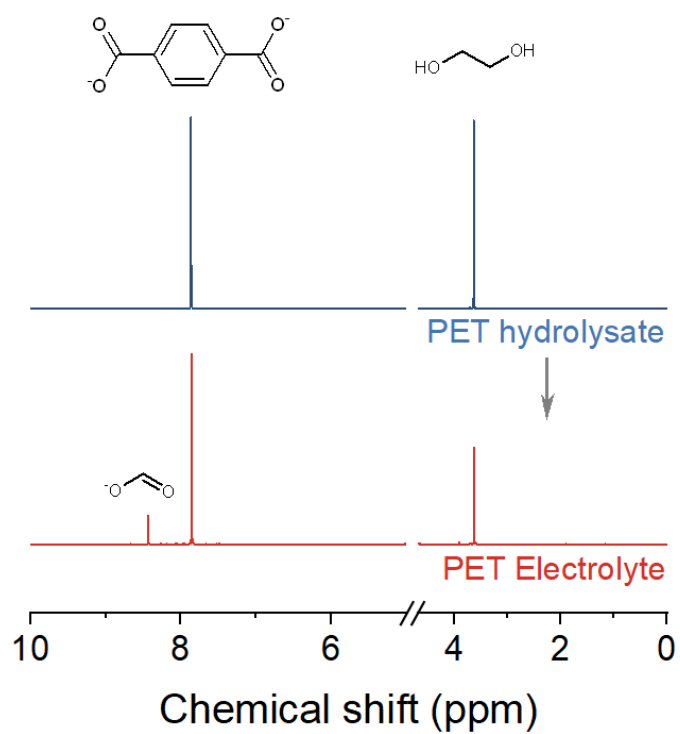
**Supplementary Figure 21** Photograph of MEA for experiments.



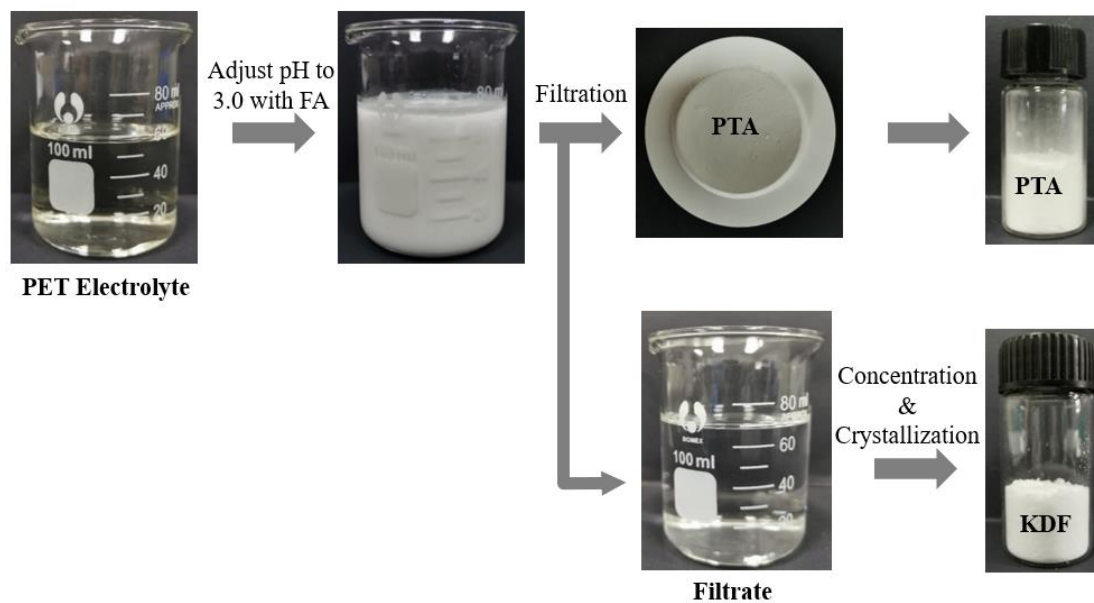
**Supplementary Figure 22** LSV curves for OER and EG oxidation in single cell.



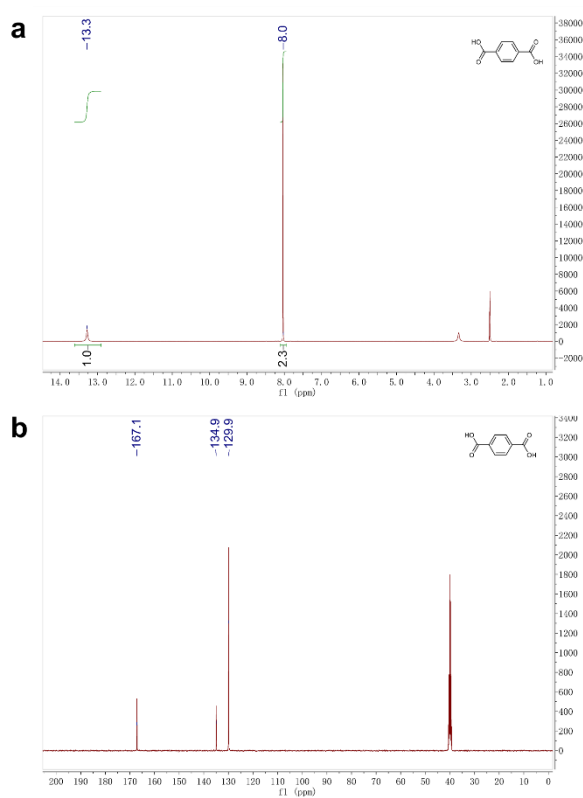
**Supplementary Figure 23** Monomer yield of PET hydrolysis as the function of time, 0.3 M PET in 2 M KOH at 60 °C.



**Supplementary Figure 24**  $^1\text{H}$  NMR spectra of PET hydrolysate and electrolyte.

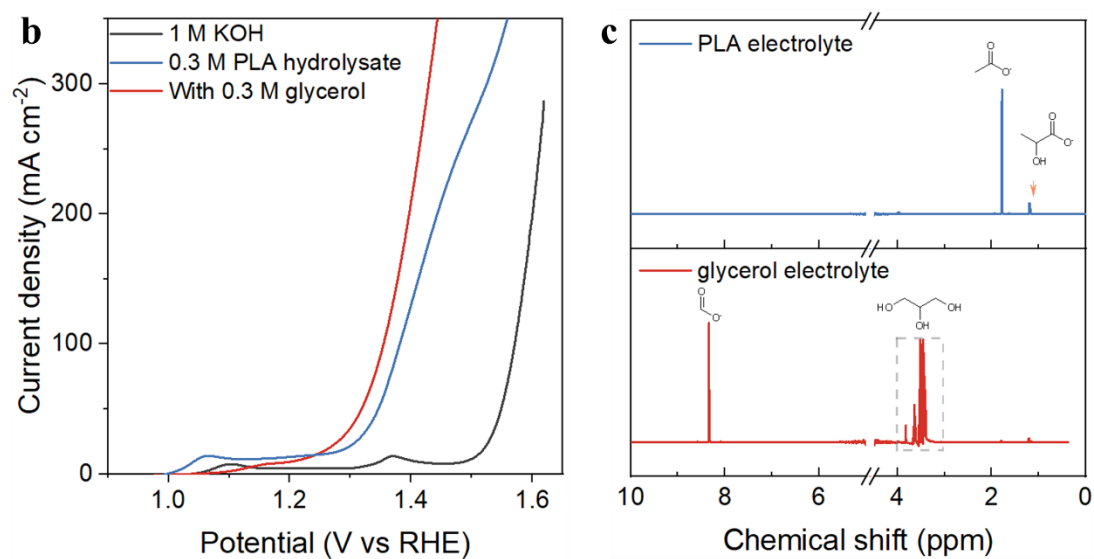
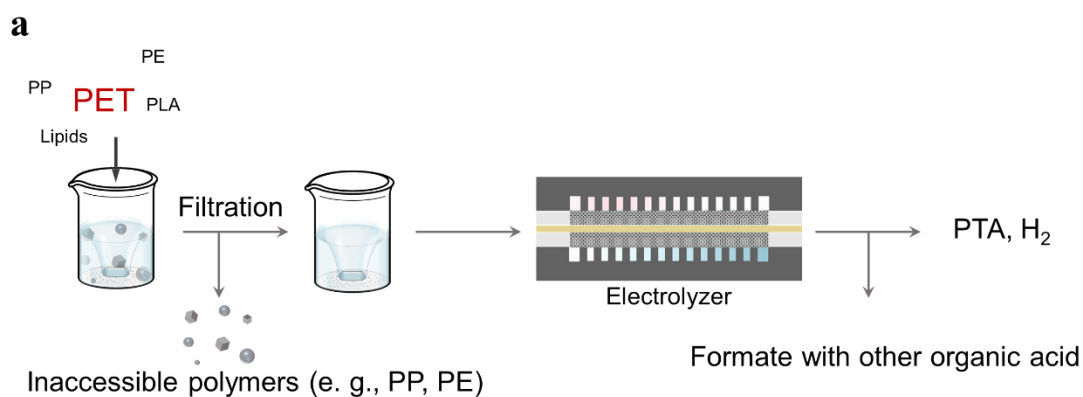


**Supplementary Figure 25** Photo pictures for demonstrating procedures of products separation from PET electrolyte.

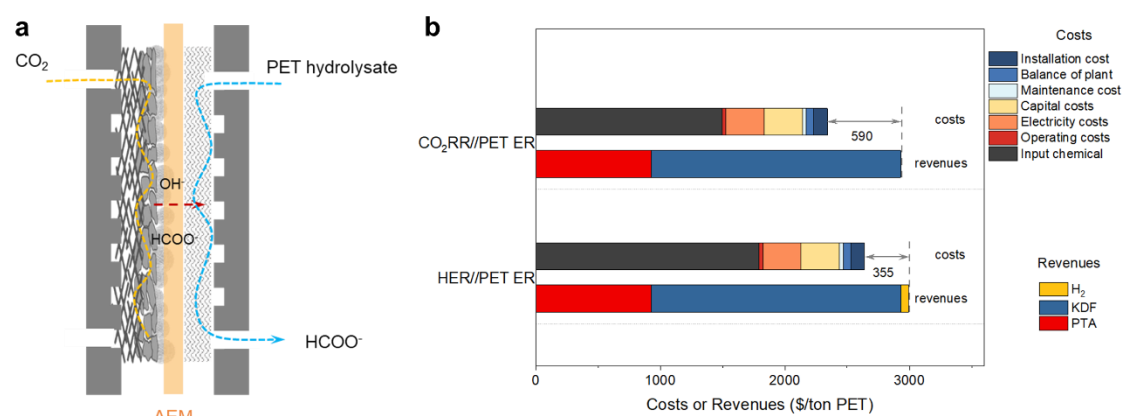


**Supplementary Figure 26** NMR for regenerated PTA. **a**  $^1\text{H}$  NMR spectrum. **b**  $^{13}\text{C}$  NMR spectrum.

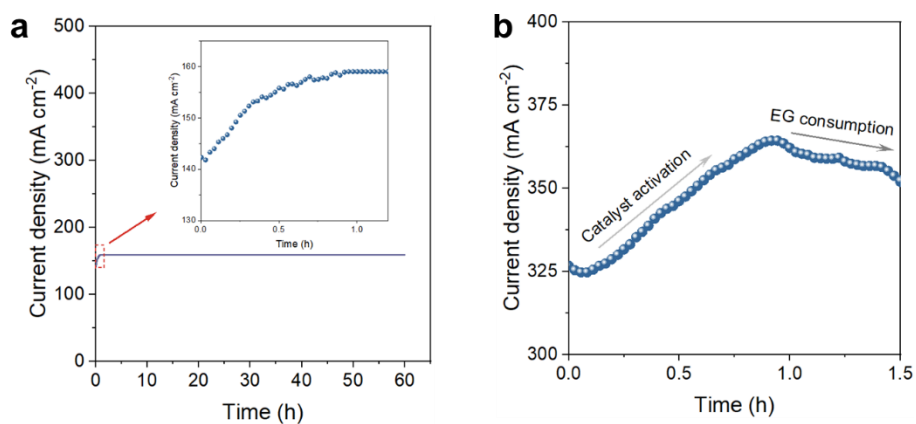




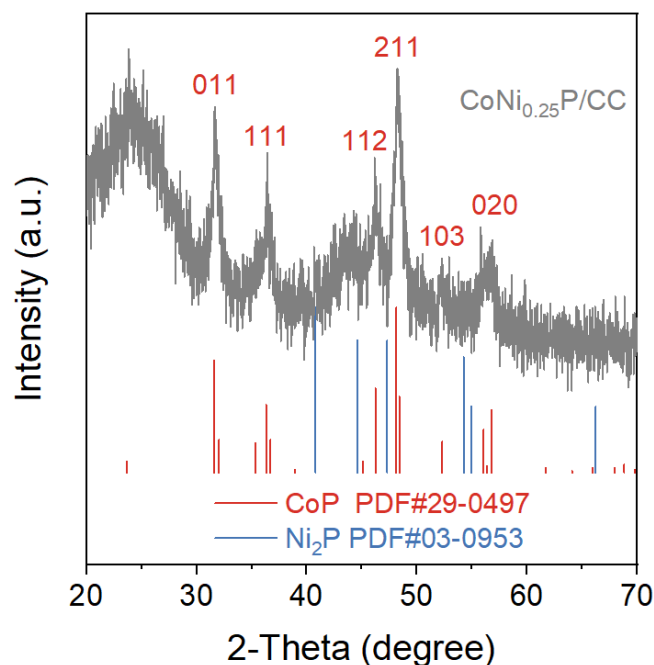
**Supplementary Figure 27 a** Schematic illustration of electrocatalytic upcycling of impure PET. **b** LSV curves (85% iR corrected) for electrooxidation of PLA hydrolysate and lipids-derived glycerol. **c** <sup>1</sup>H NMR spectra of PLA electrolyte and glycerol electrolyte.



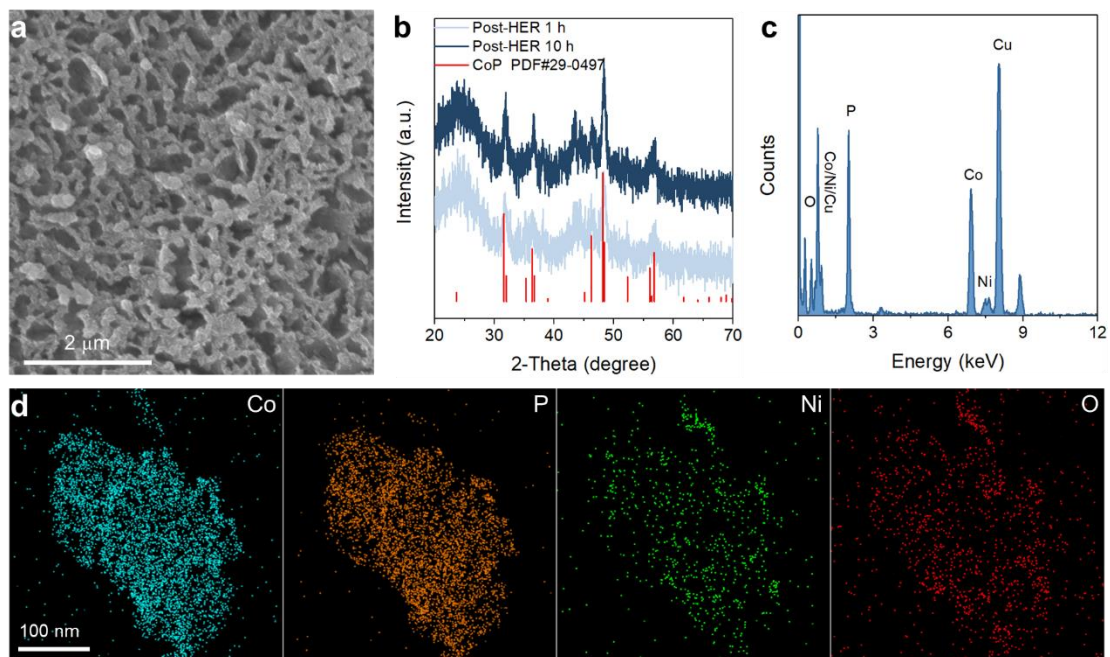
**Supplementary Figure 28 a** Concept of pairing CO<sub>2</sub>RR and PET electroreforming (ER). **b** TEA of HER//PET ER and CO<sub>2</sub>RR//PET ER at 300 mA cm<sup>-2</sup>.



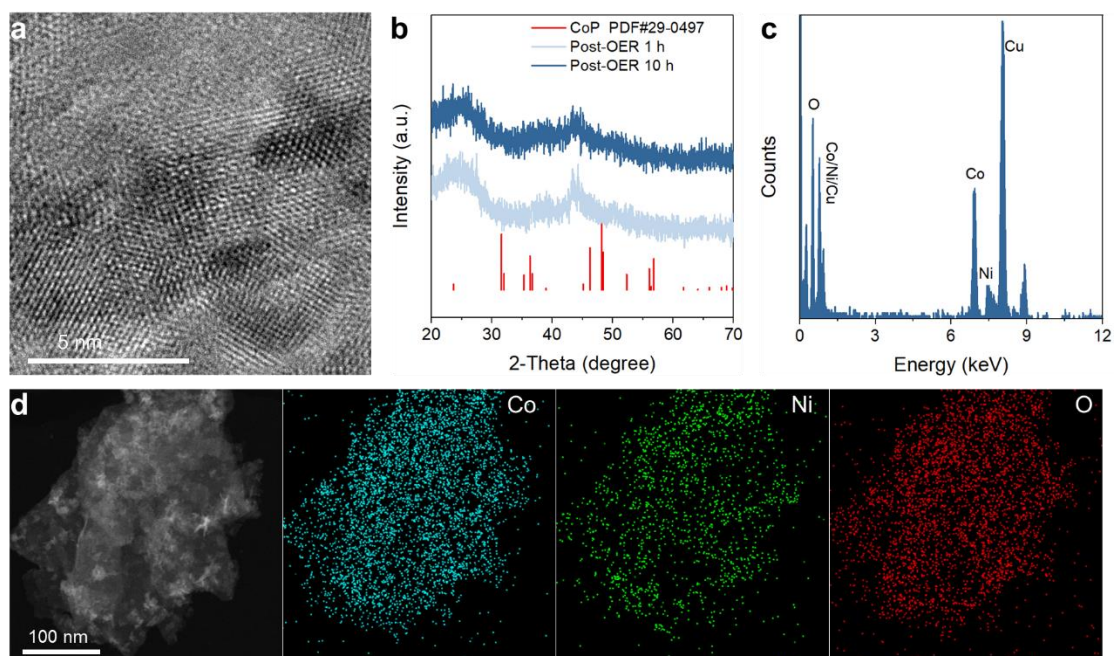
**Supplementary Figure 29** **a** i-t curve for water splitting at 1.7 V vs RHE., the inset amplified figure suggests the activation of virgin CoNi<sub>0.25</sub>P/NF. **b** i-t curve for EG oxidation over a virgin CoNi<sub>0.25</sub>P/NF catalyst at 1.7 V vs RHE. The increase of current density in the initial 1 h is possibly ascribed to catalyst activation, while the decrease of current is induced by the consumption of EG in the electrolyte after 1 h. Reaction conditions: Pt foil (-)// CoNi<sub>0.25</sub>P/NF(+), 1.7 V vs RHE.



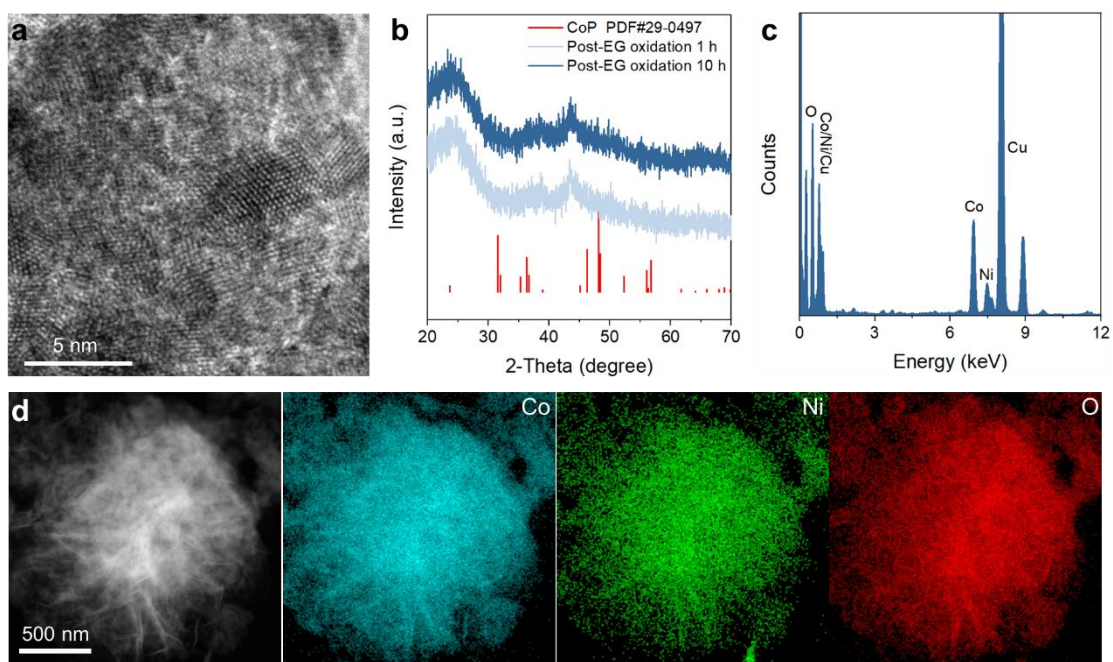
**Supplementary Figure 30** XRD pattern of CoNi<sub>0.25</sub>P/CC. This material was used for investigating the structural evolution of CoNi<sub>0.25</sub>P catalyst in HER, OER, and EG oxidation to eliminate the interference of nickel foam in XAFS, XRD, and XPS analysis.



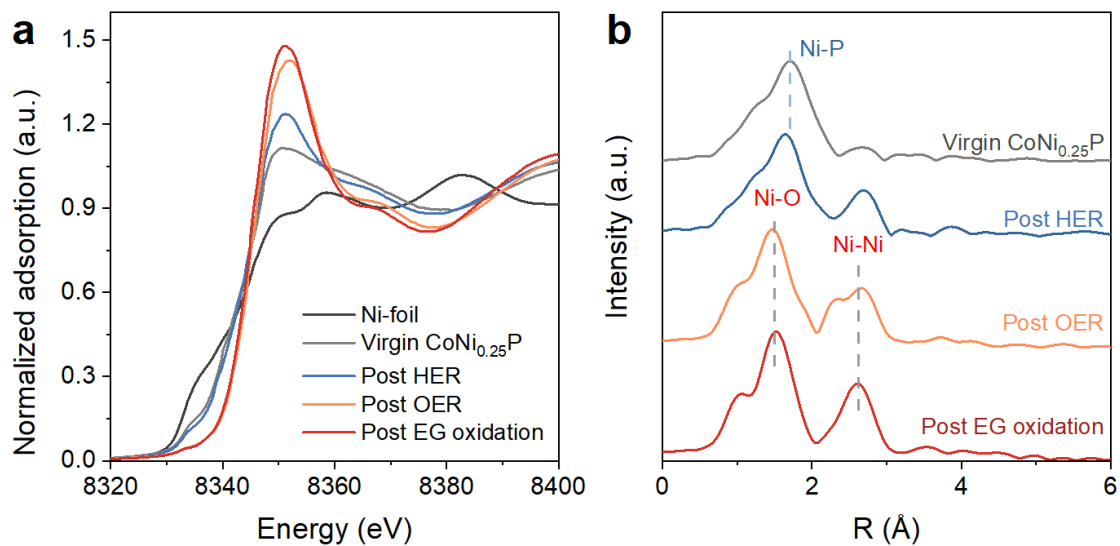
**Supplementary Figure 31** Characterization of  $\text{CoNi}_{0.25}\text{P}$  catalyst post-HER. **a** SEM image, **b** XRD pattern, **c** EDS spectrum, **d** elemental mapping of  $\text{CoNi}_{0.25}\text{P}$  catalyst post-HER.



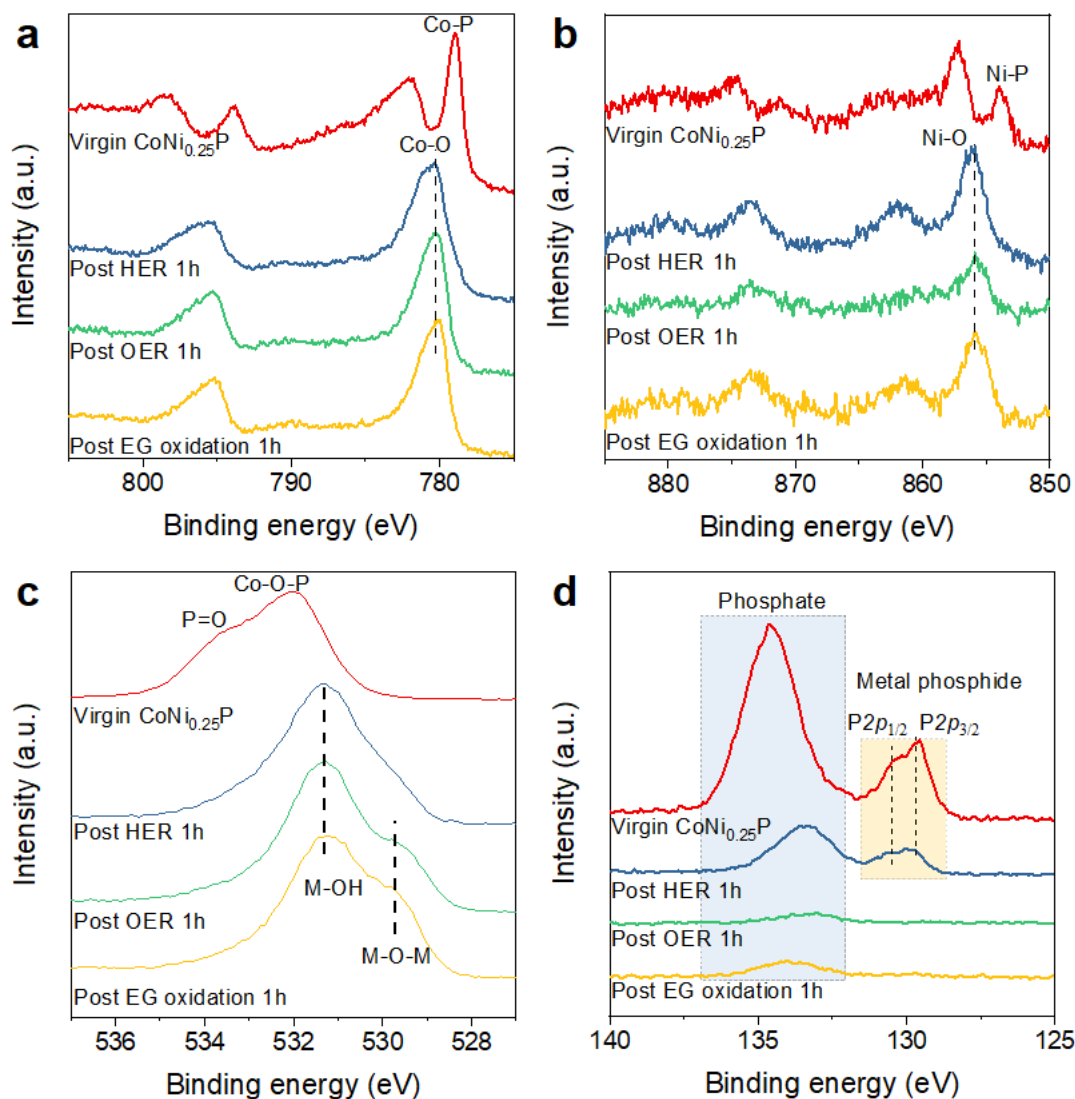
**Supplementary Figure 32** Characterization of  $\text{CoNi}_{0.25}\text{P}$  catalyst post-OER. **a** HR-TEM image, **b** XRD pattern, **c** EDS spectrum, **d** elemental mapping of  $\text{CoNi}_{0.25}\text{P}$  catalyst post-OER.



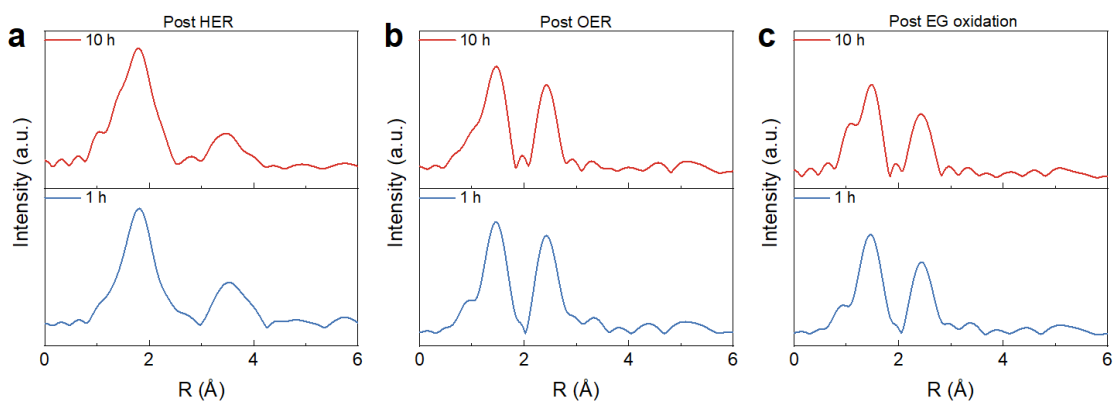
**Supplementary Figure 33** Characterization of  $\text{CoNi}_{0.25}\text{P}$  catalyst post-EG oxidation. **a** HR-TEM image, **b** XRD pattern, **c** EDS spectrum, **d** elemental mapping of  $\text{CoNi}_{0.25}\text{P}$  catalyst post-EG oxidation.



**Supplementary Figure 34** XAFS profiles of Ni K-edge in  $\text{CoNi}_{0.25}\text{P}$  materials. **a** Normalized Ni K-edge XANES spectra. **b** Fourier-transformed (FT)  $k^3$ -weighted Ni K-edge EXAFS spectra.



**Supplementary Figure 35 XPS spectra of  $\text{CoNi}_{0.25}\text{P}$  materials. a  $\text{Co}2p$  spectra. b  $\text{Ni}2p$  spectra. c  $\text{O}1s$  spectra. d  $\text{P}2p$  spectra.**



**Supplementary Figure 36 Fourier-transformed (FT)  $k^3$ -weighted Co K-edge EXAFS spectra of  $\text{CoNi}_{0.25}\text{P}$  catalyst after a HER, b OER, and c EG oxidation conditioned for 1 h and 10 h.**





## Supplementary Tables

**Supplementary Table 1** Literatures of PET reforming toward H<sub>2</sub> and formate.

Catalyst	Energy input	Reaction conditions	FE <sub>formate</sub> (%)	Formate productivity (mmol cm <sup>-2</sup> h <sup>-1</sup> )	H <sub>2</sub> productivity	Total TON of catalyst of long-term operation (mmol g <sup>-1</sup> ) <sup>a</sup>		Ref.
						Formate	H <sub>2</sub>	
CoNi <sub>0.25</sub> P	electricity	1 cm <sup>-2</sup> electrode (2.85 mg/cm <sup>2</sup> metal phosphide), 1 M KOH with 0.3 M substrate	91.3	4.01	2215.4 mmol g <sup>-1</sup> h <sup>-1</sup> / 6.31 mmol cm <sup>-2</sup> h <sup>-1</sup>	7.3×10 <sup>4</sup>	1.2×10 <sup>5</sup>	This work
CdS/CdO <sub>x</sub>	solar	1 nmol catalyst, 10 M NaOH with 25 g/L substrate	Non-selective	-	12.4 mmol g <sup>-1</sup> h <sup>-1</sup>	-	~298	1
CN <sub>x</sub>  Ni <sub>2</sub> P	solar	40 mg catalyst, 1 M KOH with 25 g/L substrate	Non-selective	-	0.05 mmol g <sup>-1</sup> h <sup>-1</sup>	-	~1	2
Nano Ni-P	solar	1 cm <sup>-2</sup> photoelectrode, 2 M KOH with 40 g/L substrate	~100	0.24	0.0031 mmol cm <sup>-2</sup> h <sup>-1</sup>	-	-	3

<sup>a</sup> TON: turnover number

**Supplementary Table 2** Comparison of HER performance of CoNi<sub>0.25</sub>P/NF with other non-noble metal catalysts in 1 M KOH.

Catalyst	$\eta_{10}$ (mV)	Tafel slope (mV dec <sup>-1</sup> )	Ref.
CoNi <sub>0.25</sub> P/NF	89.9	58.1	This work
Co <sub>2</sub> P/CoNPC	208	83.9	4
B-CoP/CNT	56	69	5
Ni <sub>5</sub> P <sub>4</sub> -Ru	123	56.7	6
MoP@NCHSs	92	62	7
P-MoP/Mo <sub>2</sub> N	54	47	8
MoO <sub>2</sub> -FeP@C	103	48	9
CoP NFs	136	56.2	10
CoP@a-CoO <sub>x</sub>	132	89	11
Ni foam/P-CoMoO <sub>4</sub>	94	93	12
CoNiPS <sub>3</sub> /C	136	60	13
CoP@ BCN	215	52	14
CoP/Co <sub>2</sub> P	103	61.2	15
Ni <sub>2</sub> P-Cu <sub>3</sub> P	78	173	16
S-MoP NPL	104	56	17
Co <sub>0.9</sub> Ni <sub>0.1</sub> Se	185.7	58	18
NiS <sub>0.5</sub> Se <sub>0.5</sub>	70	78	19
m-CoSe <sub>2</sub>	124	37	20
Co/ $\beta$ -Mo <sub>2</sub> C@N-CNT	170	92	21

**Supplementary Table 3** Structural parameters extracted from the XRD Rietveld refinement and EXAFS fitting of CoNi<sub>0.25</sub>P material.

XRD Rietveld refinement						
Phase	Composition (wt. %)	Atomic ratio of Co:Ni	a (Å)	b (Å)	c (Å)	Average M-P length (Å)

CoP	90.2	1:0.13	5.08	3.28	5.61	2.31±0.06
Ni <sub>2</sub> P	9.8		5.74	5.74	3.50	2.23±0.04
EXAFS fitting						
	Path					R (Å)
	Co-P					2.31±0.11
	Ni-P					2.25±0.09

**Supplementary Table 4** The concentration of metal ions in precursor solution and the final ratio of Co:Ni in the CoNi<sub>x</sub>P and Ni<sub>2</sub>P materials.

Nominal designation <sup>a</sup>	Concentration of metal ions in precursor solution (mM) <sup>b</sup>		Determined atomic ratio of Co:Ni in the catalyst <sup>c</sup>	
	Co	Ni	ICP	EDX
CoP	100	-	1:0	1:0
CoNi <sub>0.1</sub> P	100	10	1:0.07	1:0.09
CoNi <sub>0.25</sub> P	100	25	1: 0.14	1: 0.17
CoNi <sub>0.5</sub> P	100	50	1: 0.26	1: 0.23
Ni <sub>2</sub> P	-	100	0	0

<sup>a</sup>: The designation of the materials is according to the ratio of Co/Ni in the metal precursor for electrodeposition.

<sup>b</sup>: The concentration of initial metal ions in electrolyte for electrodeposition.

<sup>c</sup>: The measured atomic ratio of Co:Ni in the obtained catalysts by ICP and EDX. Specifically, the CoNi<sub>x</sub>P nano-array on nickel foam was collected by sonification and further digested by concentrated HNO<sub>3</sub> for ICP analysis.

**Supplementary Table 5** Comparison of catalytic performance of formic acid or formate production from waste.

Substrate	Catalyst	Potential (V vs RHE)	Cell voltage (V)	Current density (mA cm <sup>-1</sup> )	FE (%)	Ref.
EG	CoNi <sub>0.25</sub> P/NF	-	1.77	500	81.4	This work
		1.7	-	350	90	

Methanol	Ni <sub>3</sub> C	1.55	-	120	-	22
Methanol	Co(OH) <sub>2</sub> @HOS/CP	-	1.50	10	100	23
		-	1.6	70	-	
Methanol	CuONS/CF	1.47	-	100	88.4	24
		-	1.52	50	91.3	
Methanol	Ni(OH) <sub>2</sub> /NF	1.36	-	100	~100	25
		-	1.72	150	-	
Glycerol	CuCo <sub>2</sub> O <sub>4</sub>	1.3	-	10	89.1	26
Glycerol	Ni-Mo-N/CFC	-	1.36	10	95	27

**Supplementary Table 6.** Price of feedstocks and products.

Product	Price (\$/ton)	Source
Feedstocks		
Waste PET	390	a
KOH	1280	28
H <sub>2</sub> SO <sub>4</sub>	45	28
H <sub>2</sub> O	0.22	28
Formic acid	400	29
Products		
PTA	1260	30
EG	1400	29
KDF	1590	b
K <sub>2</sub> SO <sub>4</sub>	473	28
H <sub>2</sub>	1900	31

a: The price of PET waste was assumed to be 40% of virgin PET.

(<https://jiage.molbase.cn/hangqing/PET>)

b: Taken from online trade market. (<https://jskolod.en.made-in-china.com/product/aFIJndtVYuch/China-Potassium-Diformate-98-.html>)

## Supplementary Note 1

To investigate the economic feasibility of this process for PET upcycling, we carried out a simplified techno-economic analysis using a model adapted from that of literatures reported by Sargent group.<sup>31-33</sup> The processing capacity of the plant is 200 ton of waste PET per day. Supplementary Figs. 1-2 summarize the model used to calculate the plant-gate levelized cost of processing PET (\$/ton PET) at different current density (50, 100, and 300 mA cm<sup>-2</sup>). The price of input chemicals and products were listed in Supplementary Table 6.

Below is the list of assumptions made for the calculations.

1. The capital costs of electrolyzer is sensitive to the operating current density, we assume a cost of \$10,000 per m<sup>2</sup> of electrolyzer. The total catalyst and membrane cost are 5 % of the electrolyzer cost.<sup>31</sup>
2. The capital costs of hydrolyzer and distillation equipment are dependent on the process capacity of PET. Their combined cost is assumed to be 50% of PET feedstock cost.
3. The capacity factor is expected to be operational on any given day, is assumed to be 0.8, which means the plant will be operational 19.2 hours a day.<sup>31</sup>
4. Input chemicals include PET, potassium hydroxide, formic acid and water. The output products include KDF, PTA, and H<sub>2</sub>. The waste PET contains ~15% of unreacted impurities.<sup>30</sup>
5. The faradaic efficiency and selectivity to formate from EG is 80%, and the faradaic efficiency to H<sub>2</sub> is assumed to be 100 %.<sup>32</sup> The KDF yield from formate is assumed to be 70%.
6. The price of electricity is assumed to be 10 ¢/kWh.<sup>31</sup> The electricity costs comprise 3 components, electrolyzer for EG and water electrolysis, hydrolyzer for PET hydrolysis, separation equipment for distillation and drying. The electricity costs for hydrolysis and products separation are assumed to be equal to electrolysis.
7. Both operation and maintenance costs are assumed to be 10% of the capital costs.

The calculation process

### 1. Capital costs

The electrolyser cost. According to the current required and the assumed operating current density of  $300 \text{ mA cm}^{-2}$ , we can calculate the area of electrolyser needed:

$$\text{Area of electrolyser} = \frac{I}{i} (\text{m}^2)$$

Where  $i$  is current density.

The electrolyser cost can be calculated based on the estimate of \$10000 per  $\text{m}^2$ , therefore:

$$\text{Cost of electrolyser} = \text{Area of electrolyser} \times \$10000 \text{ per m}^2$$

The total catalyst and membrane cost are assumed to be 5 % of electrolyzer cost and is calculated as:

$$\text{Cost of catalyst and membrane} = \text{Cost of electrolyser} \times 5\%$$

The capital costs of hydrolyzer and distillation equipment are assumed to be 50% of PET and are calculated as:

$$\text{The capital costs of hydrolyzer and distillation equipment} = \text{Cost of PET} \times 50\%$$

Therefore, the capital costs component can be calculated as:

$$\text{Capital costs} = \frac{\text{The electrolyser cost} + \text{The catalyst and membrane costs}}{\text{Lifetime of plant}} + \text{The hydrolyzer and distillation equipment costs}$$

### 2. Maintenance cost

This is assumed to be 10% of the capital costs and is calculated as:

$$\text{Maintenance cost per day} = \text{The capital cost} \times 10\%$$

### 3. Balance of plant

$$\text{Balance of plant} = \text{The capital cost} \times \text{Balance of plant factor}$$

### 4. Installation costs

$$\text{Installation cost} = \text{The capital cost} \times \text{Lang factor}$$

### 5. Electricity costs:

Total charge required to treatment per ton of PET can be calculated as follows:



$$Q = \frac{\text{Mass of ethylene glycol (g)} \times F \times N}{\text{Molar mass of ethylene glycol} \left(\frac{\text{g}}{\text{mol}}\right) \times \text{Faradaic efficiency}}$$

Where  $Q$  is the total charge,  $F$  is the Faraday's constant and  $N$  takes the value 2 since ethylene glycol oxidation to formic acid is a six-electron transfer process.

The current required to sustain this process can be calculated as follows, with a capacity factor of 0.8:

$$I = \frac{Q}{\text{Time in a day(s)} \times \text{Capacity factor}}$$

Where  $I$  is the current.

The power required to sustain this process can be calculated as follows, assuming an operating cell potential of 1.7 V:

$$P = \frac{U \times I}{1000} \text{ (kW)}$$

The energy use per day can be calculated as follows:

$$\text{Energy use per day(kWh)} = P \times \text{Time in a day(h)} \times \text{Capacity factor}$$

The electrolyzer electricity cost of per day can be calculated as follows:

$$\text{Electrolyser electricity cost of per day} = \text{Energy use per day} \times \text{Cost per kWh.}$$

The electricity costs for hydrolysis and products separation are assumed to be equal to electrolysis and are calculated as:

$$\begin{aligned} \text{Hydrolysis and products separation electricity costs of per day} \\ = \text{Electrolyser electricity cost of per day} \end{aligned}$$

Therefore, the electricity cost per day can be calculated as:

$$\begin{aligned} \text{Electricity costs per day} \\ = \text{Electrolyser electricity cost of per day} \\ + \text{Hydrolysis and products separation electricity costs of per day} \end{aligned}$$

6. Input chemicals costs: Materials require 1 ton of PET, 828 kg KOH, 1032.5 kg formic acid and 333.3 kg water.

$$\begin{aligned} \text{Input chemicals} = & \text{Cost of PET} \times \text{Mass of PET needed} + \text{Cost of KOH} \times \\ & \text{Mass of KOH needed} + \text{Cost of formic acid} \times \text{Mass of formic acid needed} + \\ & \text{Cost of water} \times \text{Mass of water needed.} \end{aligned}$$

## 7. Operating costs

This is assumed to be 10% of the capital costs and is calculated as:

$$\text{Operating cost per day} = \text{The capital cost} \times 10\%$$

Total plant gate levelized cost

Finally, the total cost can be calculated by adding up all 7 components:

$$\begin{aligned} \text{Total costs} = & \text{Input chemicals} + \text{Electricity cost} + \text{Capital cost} + \text{Operating cost} \\ & + \text{Maintenance cost} + \text{Balance of plant cost} + \text{Installation cost} \end{aligned}$$

The products of this process include terephthalic acid (PTA), potassium dicarboxylate (KDF). Per ton of PET as raw material can obtain 735.5 kg PTA and 1344.3 kg KDF.

Therefore, the product value can be calculated as:

$$\begin{aligned} \text{Product value} = & \text{Cost of PTA} \times \text{Mass of PET obtained} + \text{Cost of KDF} \times \\ & \text{Mass of KOH obtained.} \end{aligned}$$

The profit per day from this process can be calculated as:

$$\text{Profit per ton of PET} = \text{Product value} - \text{Total costs}$$

Cathode hydrogen evolution, which has a 100% faradaic efficiency.

$$\text{Mass of hydrogen produced per day} = \frac{Q \times \text{Molar mass of hydrogen}}{N \times F}$$

Profit from hydrogen can be calculated as:

$$\text{Profit from hydrogen per ton of PET} = \text{Cost of H}_2 \times \text{Mass of H}_2 \text{ obtained}$$

Therefore, total profit per ton PET can be calculated as:

$$\begin{aligned} \text{Total profit per tonne of PET} \\ = & \text{Profit per ton of PET} + \text{Profit from hydrogen per ton of PET} \end{aligned}$$

### **Supplementary Note 2**

To investigate the economic feasibility of pairing electrocatalytic carbon dioxide reduction reaction (CO<sub>2</sub>RR) to formate and PET upcycling, TEA was carried out based on the following assumptions.

1. The operating current density is  $300 \text{ mA cm}^{-2}$ .
2. The faradaic efficiency to formate from  $\text{CO}_2$  is 80%.
3. The cost for producing formic acid from  $\text{CO}_2$  is 185 \$/ton.<sup>29</sup>

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