Supplemental information for:

Simultaneous serotonin and dopamine monitoring across timescales

by rapid pulse voltammetry with partial least squares regression

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Figure S1. Experimental set-up for *in vitro* carbon-fiber microelectrode calibration (flow cell, left) and *in vivo* experiments (right). Photograph courtesy of Wesley Smith.

The rapid pulse voltammetry (RPV) waveform is shown in **Figure S2a**. For this circuit **(Fig. S2b)**, the relationship between the output voltage and the working electrode current is given by the differential equation:

$$
\frac{V_O}{R_F} + C_F \cdot \frac{dV_O}{dt} = -I_{WE} \tag{1}
$$

If the feedback capacitor is not present (Fig. $S2c$), the relationship is given by:

$$
V_O = -R_F \cdot I_{WE} \tag{2}
$$

Transimpedance amplifiers often include a feedback capacitor connected in parallel to the feedback resistor for signal stabilization and filtering purposes [S1,S2]. The drawback of their use is that the feedback capacitor disrupts the direct proportionality between measured current and output voltage (**Equation 1**). Instead, the output signal will deform (*i.e.*, the exponential current decay will be delayed) according to the differential present in Equation 1 (Fig. S2b). In most cases, the latter is not desired.

For RPV, we purposefully included a feedback capacitor (**Fig. S2b**) to allow a smoother, longer duration of the pulse response. Important electrochemical information is present within the nonfaradaic and faradaic currents immediately after a pulse, on the order of tens of microseconds. Without a feedback capacitor, these currents decay too quickly to be sampled with high enough time resolution by the data acquisition system (8 µs sampling rate; 125 kHz). With a feedback capacitor of appropriate capacitance, the output voltage response is spread out over a longer temporal duration. This additional decay time affords the PLSR model more data points to be sampled from key electrochemical events that would otherwise be missed or under-sampled. While we recognize these electronic components preclude the analysis of an electrochemical system by equivalent circuit analysis, due to the deformation of the original working electrode signal, we note our purpose here is to obtain relevant information for the PLSR model, not to gain mechanistic insights at the electrode surface. Furthermore, the capacitor helps to stabilize and to reduce the noise of the output signal.

For these reasons, we implemented the feedback capacitor as shown in **Figure S2b**. The value of the capacitor was determined empirically to produce the desired smoothing and decay time of the signal, depending on the pulse sequence applied. For our set up, this value was found to be approximately 100 pF.

Table S1. Statistical summary.

The *t-*tests were two-tailed and paired or unpaired depending on whether matching numbers of pre- *vs.* post SSRI samples were available.

Supplemental Citations

S1. Orozco L (2013) Programmable-gain transimpedance amplifiers maximize dynamic range in spectroscopy systems. Analog Dialogue. https://www.analog.com/en/analogdialogue/articles/programmable-gain-transimpedance-amplifiers.html. Accessed May 14 2021

S2. Bhat A (2012) Stabilize transimpedance amplifier circuit design (application note 5129). Maxim Integrated. https://www.maximintegrated.com/en/design/technical-documents/appnotes/5/5129.html. Accessed May 14 2021