## Charged ferroelectric domain walls for

## deterministic ac signal control at the nanoscale

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## **Supplementary Information**

**Material.** High-quality single crystals were grown using the pressurized floating-zone method<sup>1</sup> and oriented by Laue diffraction with the polarization vector in-plane. The samples with a thickness of about 1 mm were cut and lapped with a 9  $\mu$ m-grained Al<sub>2</sub>O<sub>3</sub> water suspension and polished using silica slurry (Ultra-Sol® 2EX, Eminess Technologies, Scottsdale, AZ, USA) to produce a flat surface with a mean roughness of about 1.55 nm (determined by atomic force microscopy considering a 25x25  $\mu$ m<sup>2</sup> scan area).

Local electric characterization. Scanning probe microscopy measurements were performed on an NT-MDT Ntegra Prisma system (NT-MDT, Moscow, Russia). Voltages (a.c. and d.c.) for PFM, cAFM, and AC-cAFM measurements were applied through the bottom electrode using a function generator (Agilent 33220 A, Santa

Clara, CA, USA). All scans were performed using an electrically conductive diamond coated tip (DDESP-10, Bruker, Billerica, MA, USA) with a tip height of 10-15  $\mu$ m and a maximum tip radius of  $\approx$ 150 nm. All measurements were carried out at room temperature ( $T \approx 25$  °C).

For PFM measurements, the sample was excited using an a.c. voltage (f = 40 kHz,  $V_{a.c.}^{in} = 1.5$  V), while the laser deflection was read out by lock-in amplifiers (SR830, Stanford Research Systems, Sunnyvale, CA, USA). The PFM response was calibrated on a periodically out-of-plane poled LiNbO<sub>3</sub> sample (PFM03, NT-MDT, Moscow, Russia). For cAFM scans a d.c. voltage was applied ( $V_{d.c.}^{in} = 0.7$  V), while the sample response was read out using a low current head (SF005, NT-MDT, Moscow, Russia). In this frame, AC-cAFM is an extension of conventional cAFM measurements.<sup>2</sup> Here an a.c. voltage (0.1 MHz < f < 10 MHz, 0.4 V <  $V_{a.c.}^{in} < 1.13$  V) is applied to the bottom electrode. The low current head mimics a low pass filter with a cutoff frequency around 1 Hz, making the 0 Hz (also termed d.c. or rectified) component accessible. The recorded analog signal is then transferred to a digital signal and spatial resolution of the 0 Hz component (referred to as  $I_{d.c.}^{out}$ ) is provided by the atomic force microscope (a detailed description is provided in Figure S1).

**Macroscopic dielectric spectroscopy.** Macroscopic dielectric spectroscopy was carried out on the same single crystal also used for local electric characterization. Measurements were performed in a plate capacitor geometry, while both surfaces were coated with silver paint. Measurements were performed using an Alpha Analyzer (Novocontrol, Montabaur, Germany) together with a voltage booster option (HVB300, Novocontrol, Montabaur, Germany), covering a frequency range of 10<sup>-4</sup> to 10 MHz with varying applied bipolar voltages from  $V_{a.c.}^{in} = 1 - 20$  V. The measurement was performed at room temperature (T~25°C). More details can be found in ref. 3. The fits of the macroscopic data were done using an equivalent circuit model, consisting of two *RC* circuits connected in series to describe the behavior of the bulk and the barrier independent of each other over the entire frequency regime. Note that the conductivity of the second *RC* element of this circuit (the internal contributions) consists of a resistor representing the intrinsic conductivity ( $\sigma_{bulk}$  in Figure 1d and 2c). In the macroscopic dielectric measurements, an additional contribution to the conductivity for the universal dielectric response ( $\sigma_{UDR}$ ),<sup>3, 4</sup> covering the influence of hopping transport on  $\sigma'(f) \propto f^n$  with exponent  $n < 1^{5, 6}$  was utilized.



**Figure S1.** Principle of the AC-cAFM experiment. a) Electronic circuit used in AC-cAFM (wires carrying electrical and mechanical signals are displayed in orange and blue, respectively). An a.c. input voltage (with varying frequency, *f*, and amplitude,  $V_{a.c.}^{in}$ ) is applied to the bottom electrode, while a probe tip is scanned over the surface of the sample in contact mode. Instructive examples for asymmetric and symmetric *I*-*V* characteristics and corresponding AC-cAFM responses are displayed in b), c) and d), e), respectively. b) For a Schottky-like tip-sample contact, the alternating input signal gets rectified.<sup>2, 7</sup> A typical *I*-*V* curve as measured by cAFM on ErMnO<sub>3</sub> is schematically depicted in b).<sup>8</sup> c) Illustration showing how the a.c. input voltage ( $V_{a.c.}^{in}$ ) leads to a d.c. current signal due to the asymmetric *I*-*V* characteristics. The AC-cAFM signal ( $I_{d.c.}^{out} \neq 0$ ) represents the time-averaged current response (schematically illustrated by the orange areas). d), e) same as b), c) for the case or a symmetric *I*-*V* 

curve, leading to  $I_{d.c.}^{out} = 0$ . To correlate the voltage- and time-dependent current representations, specific positions are labelled with numbers 1-9 in b)-e).



**Figure S2.** Positions of the voltage-dependent AC-cAFM scans in Figure 2. a) cAFM image ( $V_{d.c.}^{in} = 0.7$  V) and b) calibrated PFM overview scan at the same position recorded on a (110)-oriented ErMnO<sub>3</sub> single crystal, featuring conductive tail-to-tail and insulating head-to-head domain walls (the polarization orientation, *P*, of the domains is indicated by the arrows). The frequency dependence of the AC-cAFM response of the conductive tail-to-tail domain walls inside the 1.5 x 1.5 µm<sup>2</sup> boxes was systematically investigated under different  $V_{a.c.}^{in}$  (the respective  $V_{a.c.}^{in}$  is indicated). The results are displayed in Figure 2. The conductive domain walls were chosen for this comparative study since they have a quantitatively comparable d.c. conductance response.



**Figure S3.** Spatial resolution of the cutoff frequency. a) A series of AC-cAFM scans is displayed at logarithmically increasing a.c. frequencies at the red and green marked positions at the tail-to-tail domain wall and within a domain. The frequency values (in MHz) are displayed in the respective AC-cAFM images. b) The quantitative value of the measured AC-cAFM contrast is evaluated for these two positions (one pixel corresponding to an area,  $A \sim 71 \cdot 10^3$  nm<sup>2</sup>, estimated by the radius of the tip ( $r \approx 150$  nm)). An exponential decay function ( $f(f) = a \cdot \exp(-f/f_0) + c$ ) is fitted to the experimental data, with *a*,  $f_0$ , and *c* as fitting parameters. Here, *fo* represents the frequency at which 37% of the initial value of the AC-cAFM contrast is reached.<sup>9</sup> Exemplary fits are displayed in b as dashed lines. The cutoff frequency, at which the AC-cAFM contrast vanishes, is finally calculated as  $f_c = 5 \cdot f_0$  and is displayed for the two pixels as solid vertical lines in b. The factor 5 was chosen here, because the AC-cAFM signal reaches a value of less than 1 % of its original value.<sup>9</sup> The analysis was automatized for each pixel within the chosen area using a MatLab program to display the cutoff frequency spatially resolved, exemplarily shown for the investigated scan area in c). Figure 2b displays the results for a broad range of voltages.



**Figure S4.** Frequency- and voltage-dependence of the macroscopic permittivity and conductivity. The frequency dependent permittivity (real,  $\varepsilon'$ , and imaginary,  $\varepsilon''$ , part) and conductivity,  $\sigma'$ , are displayed in a), b), and c), respectively. The data is measured under different voltages,  $V_{a.c.}^{in}$ . The solid lines represent fits of the experimental data utilizing the equivalent circuit model displayed in the inset of Figure 2c (extended by the universal dielectric response,<sup>5, 6</sup> as described in the methods section).

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