

1. Supplementary experimental section

Polarity determination

 First, 1.25 mM pyrene stock solution was prepared in anhydrous ethanol. A 50 µL of the pyrene stock solution was added in a 1.5 mL centrifuge tube, followed by vacuum-dried to remove ethanol. The residual pyrene was dissolved in different solvents (studied nine HDESs, other three reported HDESs, conventional hydrophilic DESs and organic solvents) under 10 min of ultrasound and 2 min of vortex. Then, the emission spectrum of the obtained solution was measured by fluorescence spectrophotometer (Hitachi F-460, Japan) at an excitation wavelength of 335 nm, and the fluorescence 28 intensity ratio (I_1/I_3) of the first peak (I_1 , 373.5 \pm 0.5 nm) and the third peak (I_3 , 384.5 \pm 0.5 nm) was defined as the polarity of solvent.

Hydrophobicity and water-stability study of HDES

31 In order to initially explore the hydrophobicity of HDESs, 450 μL, 400 μL, 300 μL, 200 μL and 150 μL of HDES, as well as 150 μL, 200 μL, 300 μL, 400 μL, 450 μL of water (containing 0.1 mM rhodamine B as indicator) were added in a 1.5 mL centrifuge tube to obtain a HDES-water mixture at the volume ratio of 3:1, 2:1, 1:1, 1:2, 1:3, respectively. The mixture was vortexed for 10 min and centrifuged at 6000 rpm for 10 min, and then the appearance phenomenon was recorded. The hydrophobicity and water-stability of HDESs was further studied by evaluating mutual solubility of HDES and water. 1 mL of HDES and 1 mL of deionized water were mixed in a 5 mL centrifuge tube and then the mixture was vigorously stirred for 1 h in a magnetic heating agitator (DragonLab MS-H-Pro+, China). After centrifuging for 10 min at 6000 rpm, the top phase (HDES phase) and bottom phase (water phase) were taken by a pipette and a syringe, respectively. The water content in the HDES phase was determined by Karl Fischer titration (Metrohm 890 Titrando, 42 Switzerland). The HDES in the water phase was characterized by 1 H-NMR using d₆-DMSO as the deuterated reagent.

Quantification analysis of AQs by HPLC-DAD

 The quantification of AQs were performed on a Dionex UltiMate 3000 HPLC system (Thermo Scientific) equipped with a quaternary pump, a diode array detector and a manual injection system. The data processing was carried out by Chromeleon 7.10 SR1 software. The separation was carried 48 out using a Thermo Syncronis C₁₈ column (250 mm \times 4.6 mm, particle size 5 µm) with the column 49 temperature at 40 °C. The mobile phase was comprised of 0.1% H₃PO₄ water (A) and methanol (B), the gradient elution program was as follows: 0-10 min, 70%-75% B; 10-11 min 75%-85% B; 11-30 51 min 85%-95% B. The flow rate was set at 1.0 mL min⁻¹, the detection wavelength was at 254 nm, and 52 the injection volume was $10 \mu L$.

Experimental design strategy and statistical analysis for extraction optimization

 The extraction conditions were first optimized by single-factor design experiment to determine the values of high and low levels of the extraction factors for Plackett-Burman design (PBD), which was further conducted to screen out the factors that significantly affect the extraction yield. The detailed PBD are shown in Table S5. Subsequently, response surface methodology (RSM) combined with Box-Behnken design (BBD) was adopted to optimize the factors chosen by PBD, namely, extraction temperature (A), liquid-solid ratio (B) and concentration of HCl (C) at three levels. The established 17-run with five central points BBD project are shown in Table S6 with total AQs yield as the response.

 Design Expert version 8.0.6 was used for the design and analysis of PBD and BBD. Besides, analysis of variance (ANOVA) and the lack-of-fit test were performed to evaluate the accuracy of the proposed model. All the experiments were carried out in random order and triplicate.

Pharmacopoeia method

 A reference RRR sample was prepared according to the method listed in Volume 1 of Chinese pharmacopoeia [33]. Firstly, 0.15 g of RRR herb powder (65 mesh) was extracted with 25 mL of methanol by heat-refluxing for 60 min. The obtained solution was cooled to room temperature and then filtered. After that, 5 mL of the continuous filtrate was drawn, transferred to a flask and evaporated to dryness. 10 mL of 8% (v/v) HCl solution was then added and the mixed solution was sonicated for 2 min. Subsequently, 10 mL of chloroform was added and the mixture was heated to reflux for 1 h. After cooling to room temperature, the acid-hydrolyzed solution was transferred to a separation funnel and extracted three times with 10 mL of chloroform each time. The combined chloroform solution was evaporated to dryness under reduced pressure. And the residue was dissolved with methanol and transferred to a 10 mL volumetric flask. Then, methanol was added to the mark. After filtration, the reference RRR sample was obtained and directly used for detection of AQs by HPLC-DAD.

Solubility determination of AQs in HDESs

 The solubility of AQs in nine HDESs, traditional DESs (ChCl–glycerin and ChCl–ethylene glycol), water and common organic solvents (methanol and ethanol) was determined by fully saturated method with 1,8-dihydroxyanthraquinone (1,8-DHAQ) as a representative of AQs. Excess 1,8-DHAQ 81 was added to a tested solvent, and the mixture was stirred (500 rpm) at 25° C for 2 h in order to supersaturate the solvent. After standing and centrifuging (8000 rpm for 10 min) for precipitation, the supernatant was diluted by mobile phase (95:5 v/v methanol-water) and the concentration of 1,8- DHAQ was analyzed by HPLC-DAD at wavelength of 254 nm. The standard curve and method validation results for 1,8-DHAQ analysis are shown in Table S8.

 Method validation of C14 alcohol–*UA DES based extraction method with HPLC-DAD for AQs quantification*

 The method validation was conducted by investigating analytical parameters including specificity, linear equation, linearity, limit of detection (LOD), limit of quantification (LOQ), precision, accuracy, and stability. The linear equation was constructed by plotting peak area of each AQ against eight concentrations of AQs methanol working solutions diluted from the stock solution. The LODs and LOQs were calculated at a signal to-noise (S/N) ratio of 3 and 10, respectively. The intra-day and inter- day precision were evaluated by analysis of 0.1 g RRR under the optimal extraction conditions. And the relative standard deviation (RSD) was credited as an indicator of precision. The accuracy of the method was assessed by studying the recovery of three concentration levels (low 50%, middle 100%, high 150%) of the spiked RRR samples. The relative recovery (RR) was calculated by the following equation:

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RR\% = \frac{C_{found} - C_{real}}{C_{added}} \times 100\%
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99 where C_{found}, C_{real}, C_{added} (mg/g) refer to the determined concentration of AQs in the spiked RRR, the concentration of AQs in the unspiked RRR, and the added concentration of AQs into the RRR sample, respectively. The stability of analytes was investigated by determining the content of analytes in the HDES phase, which was obtained after one-pot extraction, before and after 24 hours of standing.

2. Supplementary results and discussion

Method validation of C14 alcohol–*UA DES based extraction method with HPLC-DAD for AQs*

quantification

 The analytical performance of the proposed method for analysis of AQs in RRR was validated, the representative chromatograms are shown in Fig. S11 and the analytical parameters are summarized in Table S9 and Table S10. The DES and other extracted components do not interfere with the determination of five main AQs. The favorable linearity with correlation coefficients (R) higher than 0.9997 is achieved for five AQs within the chosen concentration ranges. The LODs and LOQs range from 0.008 to 0.018 μg/mL and 0.028 to 0.059 μg/mL, respectively. The RSDs for intra-day and inter- day precision are lower than 2.37% and 3.75%, respectively. And the recoveries are in the reasonable range of 86.9-102.6% with RSD less than 3.84%. The stability test exhibits that the analytes are highly stable in HDESs because no significant difference in analytes content exists before and after 24 h standing. The results above demonstrate that the method, C14 alcohol–UA HDES based extraction coupled with HPLC-DAD, is suitable for quantitative analysis of AQs in RRR sample.

Single factor optimization

 Nine HDESs were chosen to screen extraction solvents of AQs from RRR sample. As shown in Fig. S9A, all the nine HDESs showed good extraction performance with total AQs yield more than 19.5 mg/g, but C¹⁴ alcohol–UA showed a relatively higher extraction yield. The reason is that C¹⁴ alcohol with longer alkyl chain can generate stronger hydrophobic interactions with AQs, and UA with 122 an olefinic bond may have an extra π - π interaction with the benzene ring-containing analytes. Thus, C¹⁴ alcohol-UA was adopted as extraction solvent for further study.

124 The effect of different extraction methods, i.e. stirring $(500 \text{ rpm}, 60 \text{ °C}, 60 \text{ min})$, water-bath (60 cm) 125 °C, 60 min), shaking (500 rpm, 60 °C, 60 min) and ultrasound (120 W, 60 °C, 60 min) on the extraction yield were further investigated. As seen in Fig. S9B, stirring was found as the most effective mean (21.09±0.17 mg/g). This is because continuous stirring can make the system be completely mixed, thus intensify the contact between the extraction solvent and target compounds. Although ultrasound can promote the contact between the extraction media and analytes to a certain extent, due to the low density and water-insolubility of HDES, ultrasound cannot achieve sufficient interaction between HDES, water and plant powder. Considering the best extraction effect as well as simple and convenient operation features without special extraction equipment, the stirring method was selected for subsequent research.

 Extraction time and temperature play the important role in the extraction process of AQs. As seen in Fig. S9C, the yield of AQs rose up in the first 20 min and then remained unchanged, indicating 20 min of stirring can reach the equilibrium yield of this method. The effect of temperature on extraction of AQs was investigated with 20 min of stirring. As shown in Fig. S9D, total AQs yield increased 138 significantly at first, then almost kept consistent with temperature more than 60 \degree C. This can be explained by the fact that the increasing temperature can not only reduce the viscosity of C¹⁴ alcohol– UA HDES, but also result in a quicker diffusion of AQs into HDES. Accordingly, 20 min of stirring 141 and 60 \degree C of extraction temperature were selected as the optimal conditions.

 The rise in liquid-solid ratio can increase the concentration difference of analytes between extraction solvent and raw materials, thereby enhancing the driving force of mass transfer. In this work, six liquid-solid ratios were investigated and the results (Fig. S9E) suggested the AQs yield increased apparently as liquid-solid ratio rose up from 5:1 to 10:1, and then reached equilibrium with further increase. To avoid the waste of DES, 10:1 of liquid-solid ratio was selected as suitable ratio for extracting AQs.

 The influence of the concentration of HCl on the yield of total AQs (Fig. S9F) showed that 10% (w/v) HCl was sufficient to provide the maximum yield, probably because the bound AQs (glycoside form of free AQs) were totally hydrolyzed. Besides, the acidic environment facilitated AQs to maintain their molecular form (pKa values in Table S1), thus reducing their distribution in the aqueous phase. Hence, 10% (w/v) was deemed as the optimal HCl concentration.

3. Supplementary figures

Fig. S1. Solid-liquid phase diagrams of C₁₂ alcohol–UA (a), C₁₀ alcohol–UA (b), C₁₂ alcohol–C₁₀ acid (c), C₁₀ alcohol–C₁₀ acid (d), C₁₄ alcohol–C₈ acid (e), C₁₂ alcohol–C₈ acid (f), C₁₀ alcohol–C₈ acid (g) and C₈ alcohol–C₈ acid (f) HDESs, where above the blue curve is the liquid region, below the black line is the solid region. UA: 10 undecenoic acid.

Fig. S2. ¹H NMR spectra of C₁₂ alcohol–UA (a), C₁₀ alcohol–UA (b), C₁₂ alcohol–C₁₀ acid (c), C₁₀ alcohol–C₁₀ acid (d), C_{14} alcohol–C₈ acid (e), C_{12} alcohol–C₈ acid (f), C_{10} alcohol–C₈ acid (g) and C₈ alcohol–C₈ acid (h) HDESs. HBA–HBD mole ratio is at eutectic ratio for each HDES; UA: 10-undecenoic acid.

Fig. S3. FT-IR spectra of HDESs and their components (a: C_{12} alcohol–UA, b: C_{10} alcohol–UA, c: C_{12} alcohol– C_{10} acid, d: C₁₀ alcohol–C₁₀ acid, e: C₁₄ alcohol–C₈ acid, f: C₁₂ alcohol–C₈ acid, g: C₁₀ alcohol–C₈ acid, h: C₈ alcohol– C8 acid), where black lines are pure long chain alkanols, red lines represent pure long chain alkyl carboxylic acids and blue lines refer to corresponding HDESs. HBA-HBD mole ratio is at eutectic ratio for each HDES; UA: 10 undecenoic acid.

Fig. S4. Viscosities of nine HDESs as function of temperature. HBA–HBD mole ratio is at eutectic ratio for each HDES; UA: 10-undecenoic acid.

Fig. S5. The mixtures of C₁₄ alcohol–C₈ acid (a), C₁₂ alcohol–C₈ acid (b), C₁₀ alcohol–C₈ acid (c), C₈ alcohol–C₈ acid (d), C₁₂ alcohol–C₁₀ acid (e), C₁₀ alcohol–C₁₀ acid (f), C_{14} alcohol–UA (g), C_{12} alcohol–UA (h) and C_{10} alcohol–UA (i) with water (containing 0.1 mM rhodamine B as indicator) at volume ratio of 3:1, 2:1, 1:1, 1:2 and 1:3 (from left to right) after vortex and centrifugation. HBA-HBD mole ratio is at eutectic ratio for each HDES; UA: 10-undecenoic acid.

Fig. S6. ¹H NMR spectra of the aqueous phase obtained after HDESs being mixed with water (vortex and centrifugation). HBA–HBD mole ratio is at eutectic ratio for each HDES; UA: 10-undecenoic acid.

Fig. S7. The chromatogram of the aqueous phase obtained after extracting AQs from RRR sample using C¹⁴ alcohol–UA HDES–water two-phase system**.**

Fig. S8. Effect of enzyme concentration (a), enzymatic time (b), enzymatic pH (c), and enzymatic temperature (d) on the total AQs yield.

Fig. S9. Effects of type of HDESs (A), extraction method (B), extraction time (C), extraction temperature (D), liquid-solid ratio (E), and concentration of HCl (F) on the total AQs extraction yield.

Fig. S10. Standardized Pareto chart for Plackett-Burman design. Blue framed columns, positive values; magenta framed column, negative value. The dotted line represents 95% confidence level.

Fig. S11. Representative chromatograms: (a) the HDES-rich phase obtained after extraction of AQs from RRR sample; (b) the HDES-rich phase obtained after extraction of AQs from 50% spiked RRR sample; (c) the blank HDES phase; (d) 10 μg/mLstandard AQs solution. Peak identification: 1, aloeemodin; 2, rhein; 3, emodin; 4, chrysophanol; 5, physcion. HDES: C₁₄ alcohol–UA (1:4).

4. Supplementary tables

Table S1

Chemical structures and physica[l properti](app:ds:properties)es of tested AQs.

^a Data obtained using SciFinder Scholar from Chemical Abstract Service;

 $^b HBA = Hydrogen bond acceptor;$ </sup>

^c HBD = Hydrogen bond donor.

The initial screening result of HDESs.

Black check mark: DES can be formed at room temperature. Red circle: DES can be formed, but it is not a liquid at room temperature.

Red cross: DES cannot be formed. Alkyl carboxylic acid is used as hydrogen bond donor (HBD), and alkanol as HBA (hydrogen bond acceptor).

HDES (HBA-HBD)	Mole ratio (HBA:HBD)	A_n (mPa s)	$B_n(K)$	$C_n(K)$	R^2
C_{14} alcohol-UA	1:4	-3.12	954.04	127.98	0.9985
C_{12} alcohol-UA	1:1	-3.26	1034.52	102.91	0.9974
C_{10} alcohol-UA	2:1	-3.40	898.36	127.80	0.9978
C_{14} alcohol- C_8 acid	1:4	-2.99	888.76	120.69	0.9965
C_{12} alcohol- C_8 acid	1:2	-3.68	1192.63	95.89	0.9973
C_{10} alcohol- C_8 acid	1:1	-3.86	1277.33	81.03	0.9958
C_8 alcohol- C_8 acid	3:1	-3.30	869.29	134.38	0.9964
C_{12} alcohol- C_{10} acid	3:2	-4.11	1191.76	101.36	0.9952
C_{10} alcohol- C_{10} acid	3:1	-3.91	1190.94	104.80	0.9986

Table S3 Fitted parameters of VFT formula and correlation coefficient (R^2) for HDESs.

VFT formula: $\ln \eta = A_{\eta} + \frac{B_{\eta}}{\tau - C_{\eta}}$ $\frac{\nu_{\eta}}{T-C_{\eta}}$, where η and T represent the viscosity (mPa·s) and temperature (K). A_n , B_n and C_n are tunable parameters, and the A_n and C_n parameters are corresponding viscosity at

maximum temperature and corresponding temperature at maximum viscosity, respectively (B.D. Ribeiro, C. Florindo, L.C. Iff, et al., Menthol-based eutectic mixtures: hydrophobic low viscosity solvents, ACS Sustain. Chem. Eng. 3 (2015) 2469-2477). UA:10-undecylenic acid.

Table S4

Water content of DES-rich phase obtained after HDES being mixed with water (1:1 volume ratio).

UA: 10-undecylenic acid.

Factor	Unit	Abbreviation	Low level (-1)	High level $(+1)$
Extraction temperature	$\rm ^{o}C$	ET	30	60
Extraction time	min	Et	10	30
Liquid-solid ratio	mL/g	LR	5	10
Concentration of HCl	W/V , %	CH	0.5	10
Vortex time	S	Vt	5	30
Centrifugal time	min	Ct	3	10
Centrifugal rate	rpm	CR	3000	6000

Experimental domain for Plackett-Burman design.

A: extraction	B: liquid-solid	C: concentration of	Response: total
temperature $(^{\circ}C)$	ratio (mL/g)	HCl (w/v, %)	AQs yield (mg/g)
55.00	10.00	7.75	21.065
80.00	15.00	7.75	20.290
80.00	10.00	0.50	18.232
80.00	5.00	7.75	18.463
30.00	15.00	7.75	14.836
55.00	10.00	7.75	20.446
80.00	10.00	15.00	20.246
30.00	10.00	15.00	13.864
55.00	5.00	0.50	16.525
55.00	15.00	0.50	18.018
55.00	15.00	15.00	20.124
30.00	5.00	7.75	11.880
55.00	5.00	15.00	17.340
55.00	10.00	7.75	20.665
30.00	10.00	0.50	13.178
55.00	10.00	7.75	20.432
55.00	10.00	7.75	20.364

Experimental design and response values with different combinations of extraction temperature, liquid-solid ratio and concentration of HCl in the Box-Behnken design.

Source	Sum of	Degree of freedom	Mean	F value	p value	Prob>F
	squares		square			
Model	139.07	$\mathbf{9}$	15.45	263.56	< 0.0001	significant
\boldsymbol{A}	68.88	$\,1$	68.88	1174.88	< 0.0001	
\boldsymbol{B}	10.25	$\mathbf{1}$	10.26	175.08	< 0.0001	
\mathcal{C}_{0}^{0}	3.95	$\mathbf{1}$	3.95	67.36	< 0.0001	
AB	0.32	$\mathbf{1}$	0.32	5.44	0.0525	
AC	0.44	$\mathbf{1}$	0.44	7.59	0.0283	
BC	0.42	$\mathbf{1}$	0.42	7.08	0.0324	
A^2	36.00	$\mathbf{1}$	36.00	613.97		
B^2	7.15	$\mathbf{1}$	7.15	121.96		
C^2	7.00	$\mathbf{1}$	7.00	119.31		
Residual	0.41	$\boldsymbol{7}$	0.059			
Lack of fit	0.082	3	0.027	0.34	0.8019	not significant
Pure error	0.33	$\overline{4}$	0.082			
Cor total	139.48	16				
	$R^2 = 0.9971$		Adjusted $R^2=0.9933$		Predicted $R^2=0.9869$	

ANOVA of the established BBD model.

The standard curve and method validation for HPLC-DAD analysis of 1,8-dihydroxyanthraquinone.

Analytical performance for five AQs analysis by C₁₄ alcohol–UA DES based extraction method with HPLC-DAD.

The stability validation for five AQs analysis by C_{14} alcohol–UA DES based extraction method with HPLC-DAD.

