

## First-principles study on the electrical and thermal properties of semiconducting

### Sc<sub>3</sub>(CN)F<sub>2</sub> MXene

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**Table S1** presents the linear fitting data to calculate the deformation potential constant, and the linear fittings for the CBM or VBM  $h_1$ ,  $h_2$  under uniaxial strains are shown in **Fig. S1**. The fourth order polynomial function  $y = Intercept + B_1x + B_2x^2 + B_3x^3 + B_4x^4$  is adopted to fit the relationship between the energy data points and the wave vectors along the transport direction for the estimation of the carrier's effective mass. Thirty energy data points near the CBM or VBM (the  $\Gamma$  point  $x = 0.1541$  is included) are adopted. With the fitting function, the second derivative value at  $\Gamma$  point is indeed calculated as:

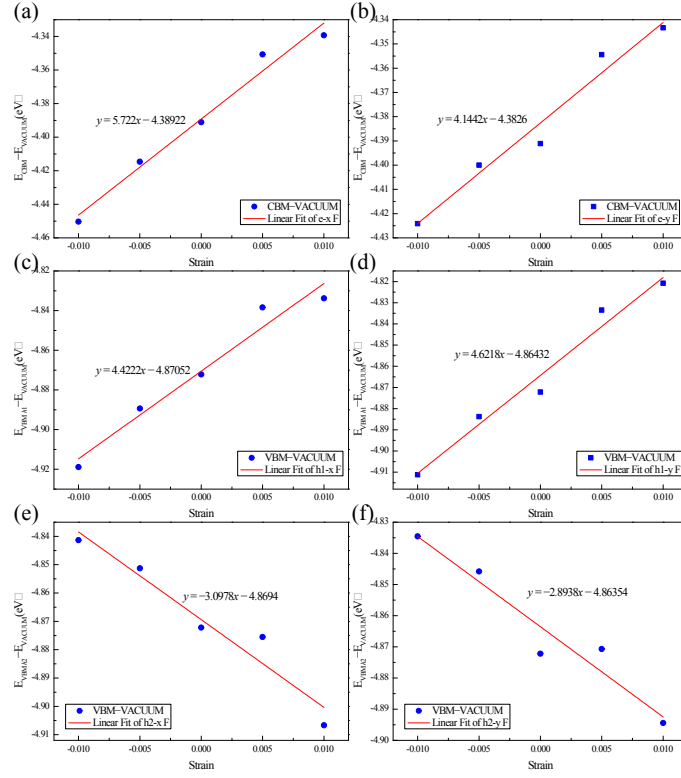
$\left. \frac{\partial^2 y}{\partial x^2} \right|_{x = \Gamma} = 2B_2 + 6B_3x + 12B_4x^2 \Big|_{x = \Gamma}$ . According to the definition of carrier effective mass  $m^* = \frac{\hbar^2 \left( \frac{\partial^2 y}{\partial x^2} \right)^{-1}}{m_0}$ , the electron effective mass is calculated. The CBM and VBM energy data points ( $X \rightarrow \Gamma$  and  $\Gamma \rightarrow Y$ ) polynomial fitting diagrams are shown in **Fig. S2**. The energy data points fitting parameters  $B_2$ ,  $B_3$  and  $B_4$  for effective masses calculations, the second derivative value at  $\Gamma$  point  $\partial^2 y / \partial x^2|_{x = \Gamma}$ , the effective mass  $m^*$ , the electron mass  $m_0$ , and the deformation potential constant  $E$  are listed in **Table S2**.

**Table S1** Linear fitting data to calculate the deformation potential constant.

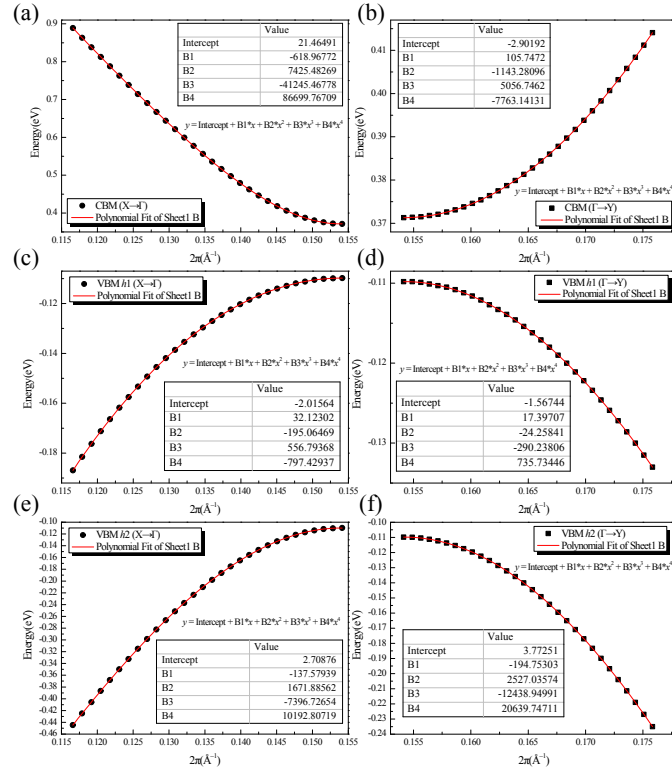
| (eV)      | Strain   | CBM/VBM- $E_F$ | $E_F$   | CBM/VBM | VACUUM  | CBM/VBM-VACUUM |         |
|-----------|----------|----------------|---------|---------|---------|----------------|---------|
| <i>e</i>  | <i>x</i> | -0.010         | 0.3054  | -1.563  | -1.2578 | 3.1926         | -4.4504 |
|           |          | -0.005         | 0.3281  | -1.580  | -1.2519 | 3.1628         | -4.4147 |
|           |          | 0.000          | 0.3713  | -1.617  | -1.2460 | 3.1451         | -4.3911 |
|           |          | 0.005          | 0.3975  | -1.638  | -1.2400 | 3.1107         | -4.3507 |
|           |          | 0.010          | 0.3935  | -1.631  | -1.2371 | 3.1022         | -4.3393 |
|           | <i>y</i> | -0.010         | 0.3391  | -1.579  | -1.2395 | 3.1846         | -4.4241 |
|           |          | -0.005         | 0.3525  | -1.596  | -1.2435 | 3.1565         | -4.4000 |
|           |          | 0.000          | 0.3713  | -1.617  | -1.2460 | 3.1451         | -4.3911 |
|           |          | 0.005          | 0.3885  | -1.638  | -1.2494 | 3.1050         | -4.3544 |
|           |          | 0.010          | 0.4064  | -1.659  | -1.2530 | 3.0903         | -4.3433 |
| <i>h1</i> | <i>x</i> | -0.010         | -0.1631 | -1.563  | -1.7263 | 3.1926         | -4.9189 |
|           |          | -0.005         | -0.1466 | -1.580  | -1.7266 | 3.1628         | -4.8894 |
|           |          | 0.000          | -0.1098 | -1.617  | -1.7271 | 3.1451         | -4.8722 |
|           |          | 0.005          | -0.0902 | -1.638  | -1.7277 | 3.1107         | -4.8384 |
|           |          | 0.010          | -0.1010 | -1.631  | -1.7316 | 3.1022         | -4.8338 |
|           | <i>y</i> | -0.010         | -0.1480 | -1.579  | -1.7266 | 3.1846         | -4.9112 |
|           |          | -0.005         | -0.1313 | -1.596  | -1.7273 | 3.1565         | -4.8838 |
|           |          | 0.000          | -0.1098 | -1.617  | -1.7271 | 3.1451         | -4.8722 |
|           |          | 0.005          | -0.0906 | -1.638  | -1.7285 | 3.1050         | -4.8335 |
|           |          | 0.010          | -0.0711 | -1.659  | -1.7305 | 3.0903         | -4.8208 |
| <i>h2</i> | <i>x</i> | -0.010         | -0.0856 | -1.563  | -1.6488 | 3.1926         | -4.8414 |
|           |          | -0.005         | -0.1085 | -1.580  | -1.6885 | 3.1628         | -4.8513 |
|           |          | 0.000          | -0.1098 | -1.617  | -1.7271 | 3.1451         | -4.8722 |
|           |          | 0.005          | -0.1273 | -1.638  | -1.7648 | 3.1107         | -4.8755 |
|           |          | 0.010          | -0.1739 | -1.631  | -1.8045 | 3.1022         | -4.9067 |
|           | <i>y</i> | -0.010         | -0.0713 | -1.579  | -1.6499 | 3.1846         | -4.8345 |
|           |          | -0.005         | -0.0933 | -1.596  | -1.6893 | 3.1565         | -4.8458 |
|           |          | 0.000          | -0.1098 | -1.617  | -1.7271 | 3.1451         | -4.8722 |
|           |          | 0.005          | -0.1278 | -1.638  | -1.7657 | 3.1050         | -4.8707 |
|           |          | 0.010          | -0.1447 | -1.659  | -1.8041 | 3.0903         | -4.8944 |

**Table S2** The specific CBM or VBM energy data points fitting parameters for effective masses calculations.  $B_2$ ,  $B_3$ , and  $B_4$  are fitting parameters,  $\partial^2 y / \partial x^2|_{x=\Gamma}$  is the second derivative value at  $\Gamma$  point,  $m^{\ddagger}$  is the effective mass,  $m_0$  is the electron mass, and  $E$  is the deformation potential constant.

| Carrier type | Direction | $B_2$  | $B_3$  | $B_4$  | $\partial^2 y / \partial x^2 _{x=\Gamma}$ | $m^{\ddagger} (\times 10^{31} \text{kg})$ | $m^{\ddagger} / m_0$ | $E(\text{eV})$ |
|--------------|-----------|--------|--------|--------|---|---|----------------------|----------------|
| <i>e</i>     | <i>x</i>  | 7425   | -41245 | 86700  | 1425                                      | 1.923                                     | 0.21                 | 5.722          |
|              | <i>y</i>  | -1143  | 5057   | -7763  | 176.8                                     | 15.50                                     | 1.70                 | 4.144          |
| <i>h1</i>    | <i>x</i>  | -195.1 | 556.8  | -797.4 | -102.5                                    | 26.73                                     | 2.93                 | 4.422          |
|              | <i>y</i>  | -24.26 | -290.2 | 735.7  | -107.2                                    | 25.57                                     | 2.81                 | 4.622          |
| <i>h2</i>    | <i>x</i>  | 1672   | -7397  | 10193  | -591.0                                    | 4.637                                     | 0.51                 | -3.098         |
|              | <i>y</i>  | 2527   | -12439 | 20640  | -565.4                                    | 4.847                                     | 0.53                 | -2.894         |



**Fig. S1** Linear fitting for the CBM (along the directions of  $x$  (a) and  $y$  (b)) or VBM  $h1$  (along the directions of  $x$  (c) and  $y$  (d)),  $h2$  (along the directions of  $x$  (e) and  $y$  (f)) under uniaxial strains.



**Fig. S2** The polynomial fitting for the CBM ( $\Gamma \rightarrow X$  (a) and  $\Gamma \rightarrow Y$  (b)) and VBM  $h1$  ( $\Gamma \rightarrow X$  (c) and  $\Gamma \rightarrow Y$  (d)),  $h2$  ( $\Gamma \rightarrow X$  (e) and  $\Gamma \rightarrow Y$  (f)) energy data points.

Optimized Sc<sub>3</sub>C<sub>2</sub>F<sub>2</sub>

Sc3C2F2 # Please generate POTCAR

```
1.0000000000000000
  3.2428701161833362    0.0000000000000000    0.0000000000000000
 -1.6214350580916681    2.8084079017881591    0.0000000000000000
  0.0000000000000000    0.0000000000000000    30.0054383522162595
Sc   C   F
  3   2   2
```

Direct

```
0.6666666666666643  0.3333333333333357  0.5898118707489317
0.3333333333333357  0.6666666666666643  0.4101881292510754
0.0000000000000000  0.0000000000000000  0.5000000000000000
0.6666666666666643  0.3333333333333357  0.4529075454323319
0.3333333333333357  0.6666666666666643  0.5470924545676752
0.0000000000000000  0.0000000000000000  0.3722785198271623
0.0000000000000000  0.0000000000000000  0.6277214801728448
```

Optimized Sc<sub>3</sub>(CN)F<sub>2</sub>

Sc3CNF2 # Please generate POTCAR

```
1.0000000000000000
  3.2436710298252809    0.0000000000000000    0.0000000000000000
 -1.6218355149126404    2.8091015133483213    0.0000000000000000
  0.0000000000000000    0.0000000000000000    30.0038464469823509
Sc   C   N   F
  3   1   1   2
```

Direct

```
0.6666666666666643  0.3333333333333357  0.5844641503799650
0.3333333333333357  0.6666666666666643  0.4136135323868189
0.0000000000000000  0.0000000000000000  0.4981411371576812
0.6666666666666643  0.3333333333333357  0.4560292851414331
0.3333333333333357  0.6666666666666643  0.5489362737651788
0.0000000000000000  0.0000000000000000  0.3758545802140176
0.0000000000000000  0.0000000000000000  0.6229610409549480
```

Optimized Sc<sub>3</sub>N<sub>2</sub>F<sub>2</sub>

Sc3N2F2 # Please generate POTCAR

```
1.0000000000000000
  3.1895811664885794    0.0000000000000000    0.0000000000000000
```

|                     |                    |                     |
|---------------------|--------------------|---------------------|
| -1.5947905832442897 | 2.7622583176115088 | 0.0000000000000000  |
| 0.0000000000000000  | 0.0000000000000000 | 30.0002247438099623 |

|    |   |   |
|----|---|---|
| Sc | N | F |
| 3  | 2 | 2 |

Direct

|                    |                    |                    |
|--------------------|--------------------|--------------------|
| 0.6666666666666643 | 0.3333333333333357 | 0.5832997146798533 |
| 0.3333333333333357 | 0.6666666666666643 | 0.4167002853201538 |
| 0.0000000000000000 | 0.0000000000000000 | 0.5000000000000000 |
| 0.6666666666666643 | 0.3333333333333357 | 0.4548675197202030 |
| 0.3333333333333357 | 0.6666666666666643 | 0.5451324802798041 |
| 0.0000000000000000 | 0.0000000000000000 | 0.3775225975908683 |
| 0.0000000000000000 | 0.0000000000000000 | 0.6224774024091388 |

Optimized Sc<sub>3</sub>(CN)F<sub>2</sub> based on an orthorhombic unit cell

Sc<sub>3</sub>CNF<sub>2</sub>

|                    |                    |                     |
|--------------------|--------------------|---------------------|
| 1.0000000000000000 |                    |                     |
| 3.2436712763298088 | 0.0000000000000000 | 0.0000000000000000  |
| 0.0000000000000000 | 5.6182034536550161 | 0.0000000000000000  |
| 0.0000000000000000 | 0.0000000000000000 | 30.0000000000000000 |

|    |   |   |   |
|----|---|---|---|
| Sc | C | N | F |
| 6  | 2 | 2 | 4 |

Direct

|                    |                    |                    |
|--------------------|--------------------|--------------------|
| 0.5000000000000000 | 0.1666685532117782 | 0.5844726890884644 |
| 0.0000000000000000 | 0.6666685822117770 | 0.5844726890884644 |
| 0.0000000000000000 | 0.3333358719148336 | 0.4136012950260337 |
| 0.5000000000000000 | 0.8333358429148348 | 0.4136012950260337 |
| 0.0000000000000000 | 0.0000185392148424 | 0.4981425315030776 |
| 0.5000000000000000 | 0.5000185392148424 | 0.4981425315030776 |
| 0.5000000000000000 | 0.1666610880145640 | 0.4560221503595585 |
| 0.0000000000000000 | 0.6666611170145629 | 0.4560221503595585 |
| 0.0000000000000000 | 0.3333282471532968 | 0.5489388196952802 |
| 0.5000000000000000 | 0.8333282181532979 | 0.5489388196952802 |
| 0.0000000000000000 | 0.9999907824590508 | 0.3758382280206973 |
| 0.5000000000000000 | 0.4999907824590508 | 0.3758382280206973 |
| 0.0000000000000000 | 0.9999969180316342 | 0.6229743013068969 |
| 0.5000000000000000 | 0.4999969180316342 | 0.6229743013068969 |