Supporting Information: Overcoming nitrogen reduction to ammonia detection challenges: The case for leapfrogging to gas diffusion electrode platforms

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Miniaturized alkaline impurity trap

The removal of NH_3 and NO_x contamination from the gas feed of the cell is crucial to avoid false positives while testing catalysts for NRR. Purifiers to achieve this typically consist of an inner and an outer tube. The inner tube is immersed into the outer tube which is filled with an oxidizing solution that traps the NH_3/NO_x. During operation, gas is bubbled into the oxidizing solution through the inner tube. The gas exits the outer tube through its headspace. Typically, both outer tube and inner tube are made of glass, because glass is very inert and easy to reshape. However, the smallest commercially available impurity traps of this design have several mL of headspace volume which would make them very expensive to flush during a $^{15}N_2$ experiment. Therefore, we propose to use an impurity trap made from inert polymers instead, as shown in Figure S1. The working principle of the design is identical to that of glass impurity traps but the inner and outer tube are made of inert polymer tubing. The headspace of the 1/32" outer diameter (OD) inner tubing and the tee is negligible so that the total headspace of the purifier can be estimated from the headspace of the ¼" outer diameter (OD) outer tube. In our experience approximately 1 cm of headspace in the outer tube is sufficient to prevent liquid from entering the gas channel. With an inner diameter (ID) of 5.6 mm the headspace of the outer tube is approximately 250 µL. This low headspace makes it ideal for cheap $^{15}N_2$ experiments in GDE cell. Additionally, it is comprised of standard connectors for easy, leak-tight, contamination-free connections. Unlike with glass impurity traps, it is possible to easily adjust the length of the outer tube depending on the required removal efficiency. The trap only consists of readily available, off-the-shelf parts which should improve standardization of this critical component.
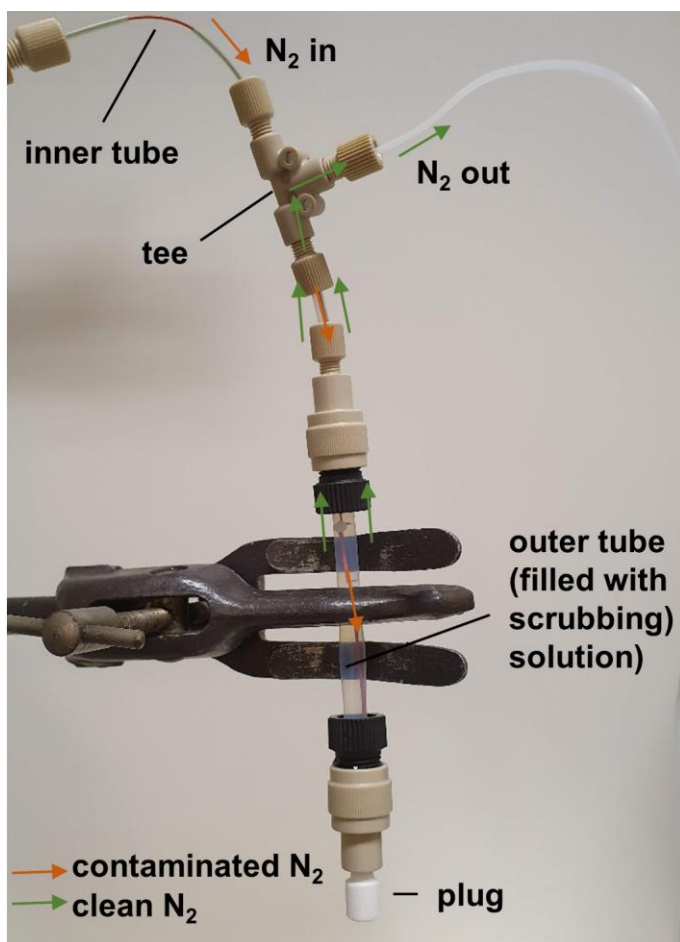
Figure S1 Photograph of a miniaturized purifier to clean NH₃/NOₓ contaminated gas streams with minimal additional headspace.

Table S1. Order list for an impurity trap with low headspace volume.

Part #	Name	Quantity	Supplier	Price ($)
1648	Tefzel™ (ETFE) Tubing Natural 1/8" OD x .093" ID x 5ft	1	IDEX Health	33.75
U-665	Adapter Assembly 1/2-20 Female x1/4-28 Female	2	IDEX Health	37.50
P-713	PEEK Low PressureTee Assembly 1/8" PEEK .050 thru hole	1	IDEX Health	38.63
F-247	NanoTight™ Sleeve Green 1/16" OD x .033" ID x 1.6"	4	IDEX Health	2.84
1569	PEEK Tubing Orange 1/32" OD x .020" ID x 5ft	1	IDEX Health	56.93
P-703	Union Assembly PEEK .050 thru hole, for 1/8" OD	2	IDEX Health	24.98
P-249	Super Flangeless™ One-Piece Fitting, 1/4-28 Flat-Bottom, for 1/16" OD	6	IDEX Health	11.02
P-311	Plug Tefzel™ (ETFE) - 1/4-28	1	IDEX Health	2.49
20533	PTFE tubing tubing L x OD x ID 25 ft x 1/4 in. (6.35 mm) x 0.228 in. (5.8 mm)	1	Merck Sigma	88.8

Calculation: nitrogen reduction reaction mass-transport limiting current in H-cell

We estimate the mass transport limiting current of the nitrogen reduction reaction $j_{lim,NRR}$ from the mass-transport limiting current of the CO_2 reduction reaction to CO $j_{lim,CO2RR}$ according to:

$$j_{lim,NRR} \approx j_{\lim,CO2RR} \frac{S_{N_2} D_{N_2} z_{NRR}}{S_{CO_2} D_{CO_2} z_{CO2RR}} \tag{1}$$

$$= 10 \frac{mA}{cm^2} \frac{1.27 \; x \; 10^{-5} \; x \; 1.77 \; x \; 10^{-5} \frac{cm^2}{s} \; x \; 6}{7 \; x \; 10^{-4} \; x \; 1.67 \; x \; 10^{-5} \frac{cm^2}{s} \; x \; 2}$$

$$= 0.6 \frac{mA}{cm^2}$$

, where S_i, D_i, are the solubility and diffusion coefficient of nitrogen and carbon dioxide in water, respectively and z_{NRR}, z_{CO2RR} are the number of electrons transferred in the electrochemical reduction of nitrogen to ammonia and of carbon dioxide to carbon monoxide per molecule of N_2/CO_2, respectively.[1–5]

Calculation: accumulated NH3 in the electrolyte
The concentration of NH_3 in the electrolyte was calculated according to:

$$c_{NH_3} = \frac{i_{NH_3} t}{zFV} \tag{2}$$

, where c_{NH_3} is the concentration of NH_3 after electrolysis, i_{NH_3} is the partial current density of NRR, t is the duration of the experiment, z is the number of electrons transferred per molecule of NH_3 produced, F is the Faraday Constant and V is the half-cell volume of the electrolyte, respectively.

Mathematical modelling of influence of ECSA on ammonia production and faradaic efficiency
The specific activity (defined as the ECSA normalized current density) j_{ECSA} was calculated by assuming Butler-Volmer kinetics according to:

$$j_{ECSA} = j_0(e^{-\alpha f \eta} - e^{(1-\alpha)f\eta})\tag{3}$$

, where j_0 is the exchange current density, α is the symmetry factor, f is the Faraday Constant F divided by the ideal gas constant R and the temperature T and η is the overpotential.[6] The current density normalized by geometric surface area $j_{geometric}$ was calculated by multiplying j_{ECSA} with the roughness factor of the electrode.

The faradaic efficiency was modelled by assuming that a potential window exists where NRR is favorable over HER and that the faradaic efficiency (FE) of NRR within this potential window can be described by a quadratic function:

$$FE = a\eta^2 + b\eta + c\tag{4}$$

, where a,b,c are constant parameters.

The partial current density of NRR j_{NRR} was calculated by multiplying the faradaic efficiency with $j_{geometric}$. The partial current density of NRR including mass transport effects $j_{mt,NRR}$ was calculated by replacing j_{NRR} with the mass transport limiting current $j_{lim,NRR}$ wherever j_{NRR} would otherwise have been lower than $j_{lim,NRR}$:

$$j_{mt,NRR} = \max(j_{NRR}, j_{lim,NRR})\tag{5}$$

Literature summary of reported levels of NH_3/NO_x contamination

*Table S2. Literature summary of ammonia and nitrate contaminations observed in nitrogen reduction studies. *To make reports more comparable, contaminations reported as absolute amounts in nmol or as concentrations in a gas stream were converted into concentrations in the electrolyte by assuming the following parameters: electrolyte volume 10 mL, catalyst area: 1 cm^2, catalyst amount: 1 mg, gas flow rate: 30 mL/min duration of gas flow: 2h.*

Contamination source	NH_3/NO_x concentration	Reference
Human Breath	0.3-3 ppm NH_3 in gas	[7]
Human Breath	0.28-1.4 ppm NH_3 in gas	[8]
0.05 M H_2SO_4 open to air for 1h	1.7 µM NH_3	[9]
0.05 M H_2SO_4 sealed for 1h	0.6 µM NH_3	[9]
DI water open to air for 400 min	8.8 µM NH_3	[10]
Nitrile gloves sonicated for 1h in DI water	155.1 µM NH_3	[7]
Polypropylene sample storage container (initially)	0.3 - 49.8 µM NO_x	[11]
Polypropylene sample storage container (after 10 days)	3.4 - 65.3 µM NO_x	[11]
Cell, electrolyte, epoxy, electrodes	18.9-21.5 µM NO_x	[11]
N impurities in CoMo film	10 µM NH_3	[11]

Rubber septa	630 µM NH₃, 270 µM NOₓ		[12]
Ar	1.3 ppb NOₓ in gas (0.02 µM NOₓ)*		[11]
N₂	3.1 ppb NOₓ in gas(0.046 µM NOₓ)*		[11]
Ar, N₂, ¹⁵N₂	200ppb N₂O in gas (3 µM NOₓ)*		[13]
¹⁵N₂	0.024 - 420 ppm ¹⁵NOₓ in gas (0.36-6290 µM ¹⁵NOₓ)* 0.014 - 1900 ppm ¹⁵NH₃ in gas (0.21 – 28454 µM ¹⁵NH₃)*		[14]
Bi₂O₃, Al₂O₃, Fe₂O₃	10-120 µmol/g catalyst NOₓ (1-12 µM NOₓ)*		[15]
Commercial metallic iron	16343 – 406469 µM total N		[15]
¹⁵N₂ scrubbing solution	18.5 µM ¹⁴NH₃, 33 µM ¹⁵NH₃		[11]
Potential induced generation of NH₃ from Fe loaded onto stainless steel	10 µM NH₃		[13]
Release of NH₃ from Nafion 117 membrane soaked in electrolyte containing 0.1 µg/mL of NH₃	17.6 µM NH₃		[16]
Background	1.5 µM NH₃		[17]
Background	2 µM NOₓ		[13]
Background	0.5 µM NH₃		[7]

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Literature summary of experimental parameters used during aqueous nitrogen electroreduction experiments

Table S3. Literature summary of experimental parameters used during aqueous NRR studies.

Ref	Gas flow rate (mL/min)	Electrolyte volume (mL)	Electrode Area (cm²)	Electrolysis time (h)	¹⁵N? [a]	QT? [b]	Flow rate ¹⁵N (ml/min)	Electrolysis time ¹⁵N (h)
[18]	n.a.	n.a.	1	2	yes	no	n.a.	10
[19]	0.48	100	n.a.	2	yes	no	0.48	2
[20]	250	n.a.	6.25	1	yes	no	5	1
[21]	n.a.	30	1	n.a.	yes	no	n.a.	2
[22]	n.a.	30	1	2	no	no	n.a.	n.a.
[23]	n.a.	90	2	6	yes	no	20 mL every 10 min	6
[24]	no flow?	30	2	2	yes	no	n.a.	2
[25]	20	n.a.	n.a.	2	yes	no	n.a.	n.a.
[26]	n.a.	50	1	2	yes	no	n.a.	2
[27]	n.a.	n.a.	1	n.a.	no	no	n.a.	n.a.
[28]	n.a.	n.a.	1.5	n.a.	no	no	n.a.	n.a.
[29]	n.a.	30	1	2	yes	yes	n.a.	10
[30]	n.a.	n.a.	1	2	no	no	n.a.	n.a.
[31]	n.a.	35	1	2	no	no	n.a.	n.a.
[32]	n.a.	25	1	n.a.	yes	no	20 mL every 10 min	6
[33]	10	30	0.07	3	yes	no	n.a.	n.a.

| 34 | 60 | 10 | n.a. | n.a. | yes | yes | static | 0.5 |
| $\tilde{x}$ | 40 | 30 | 1 | 2 | | | | |

[a] [15]N?: Were control experiments with ^{15}N performed?

[b] QT?: Was a quantitative agreement between [14]NH$_3$ and [15]NH$_3$ data demonstrated?

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