

S1 Appendix: Details on the design of experiments

The mean and standard deviation (SD) values of the diameters and lengths of the carotid and cerebral arteries of the seven patients (Table 1) were generally similar to those reported in the literature [1-5]. In the case of diameters, we determined that $\pm 50\%$ of the values reported by Liang et al. [6, 7] covered nearly a $\pm 3SD$ range around the mean of the patients' and literature values; therefore, we adopted this range. The circle of Willis (CoW) is known to exhibit anatomical variations, wherein one or several arteries may be missing [8]. In case of the commonly absent arteries, the lower bound for the diameter was set to 0.1 mm, which allows only a negligible amount of flow ($\bar{Q} \sim 10^{-2}$ mL/min) to pass. By representing the missing artery as an extremely narrow artery with a diameter of 0.1 mm, we could perform simulations efficiently without altering the arterial network topology.

Large differences were observed in the values of arterial lengths between the patient cohort and the literature in the case of the common carotid and vertebral arteries. This can be attributed to racial differences, as most of the values reported in the literature were collected considering Westerners, whereas the seven patients in this study were Asian (Japanese). Therefore, we adopted a range covering the mean $\pm 3SD$ of both the patients' and literature values for the common carotid and vertebral arteries. However, for the other arteries, we adopted the ranges of mean $\pm 3SD$ of the seven patients only.

The ranges of stenosis parameters considered the mean $\pm 3SD$ of the seven patients for D_n ; 0% (intact) to 100% (occlusion) for SR ; and 1.0 to 2.699 for K_t [9]. As indicated in Equation (5), R_v is maximum when the lumen has the minimum diameter $D_{s,\min}$ throughout the stenosis.

$$R_{v,\max} = \frac{128\mu L_{s,\max}}{\pi D_{s,\min}^4} = \frac{128\mu L_{s,\max}}{\pi D_{n,\min}^4 (1 - SR)^4}, \quad (A1)$$

where $D_{n,\min}$ denotes the lower bound of D_n , and $L_{s,\max}$ indicates the maximum stenosis length (assumed to be 40 mm here). To avoid meaningless sampling and ensure that $R_v \leq R_{v,\max}$, the upper bound of R_v was defined based on SR . Additionally, although $R_{v,\max}$ approaches infinity as SR approaches 100%, we limited R_v to less than 500 mmHg s mL⁻¹. Even at the maximum possible pressure gradient (approximately 50 mmHg) in vivo, $R_v = 500$ mmHg s mL⁻¹ resulted in a flow rate of less than 6 mL/min (significantly less than the normal flow rate, which is approximately 257 mL/min [10]); therefore, it represents a nearly occluded lumen. Thus, a higher R_v has been proven to have no physiological significance.

Although the ranges of the peripheral resistances (PRs) of the CoW were widely set, we ensured that they were physiologically acceptable. For instance, the upper bound of the PR at the middle cerebral artery allows a flow rate of less than 30 mL/min in this artery for pressures defined in the physiological range. Considering that the measured flow rate for the seven patients was 132 ± 27 mL/min, and the flow rate reported in the literature is 146 ± 31 mL/min [10], the range of PR was sufficiently wide to cover a physiologically relevant range of flow rate. Similarly, the range of the scaling factor for the total PR was set such that the simulated mean arterial pressure ranged from 73.3 mmHg (low blood pressure) to 133.3 mmHg (severe hypertension).

References

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