

24 **Supplementary Notes**

25 **Note S1: Light-to-work energy conversion efficiency**

26 The light-to-work energy conversion efficiency (η) can be given by:

27
$$\eta = \frac{E_{\text{out}}}{E_{\text{in}}} \quad (1)$$

28 where E_{in} is the incident light energy, E_{out} is mainly the elastic energy.

29 The E_{in} and E_{out} were calculated by the following equations:¹

30
$$E_{\text{in}} = PA t \quad (2)$$

31
$$E_{\text{out}} = \frac{E h l w^3}{24 \kappa^{-2}} \quad (3)$$

32 where P is the light intensity (800 mW cm⁻²), A is the surface area of the PP/CB
33 actuator infiltrated with ethanol (0.38 cm²), t is the response time (0.167 s). E is the
34 modulus (0.28 MPa). h , l , w , and κ is the thickness (148.5 μm), length (10.62 cm),
35 width (0.36 cm), and curvature (7.3 cm⁻¹), respectively. All the parameters used in the
36 calculations were obtained after the PP/CB film was immersed in ethanol. The
37 incident light energy and elastic energy are calculated to be about 51 mJ and 0.46 mJ,
38 respectively. So that the energy conversion efficiency is about 0.9%.

39 **Note S2: Natural frequency of the PP/CB oscillators**

40 The natural resonant frequency f of the PP/CB film was defined as follows:²

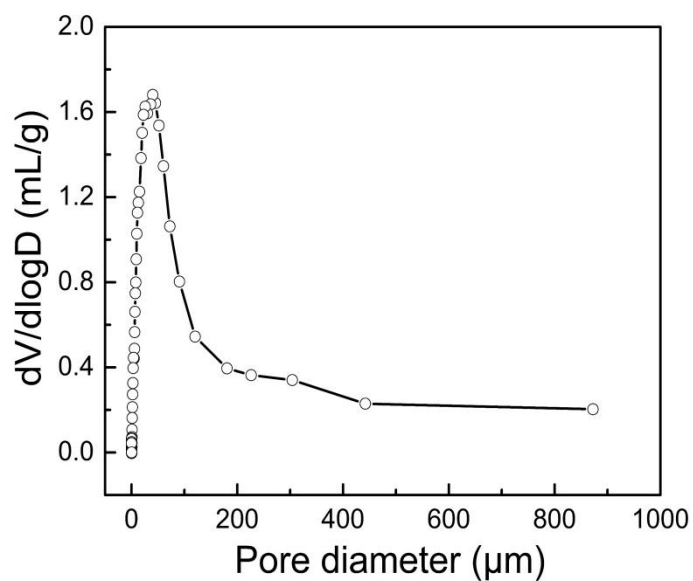
41
$$f = \frac{\alpha^2}{2\pi} \sqrt{\frac{EI}{\rho A l^4}} = \frac{\alpha^2}{2\pi} \sqrt{\frac{\frac{1}{12} E w h^3}{\rho w h l^4}} = \frac{\alpha^2}{4\pi} \sqrt{\frac{E h^2}{3 \rho l^4}} \quad (4)$$

42
$$I = \frac{1}{12} w h^3, \quad A = w h \quad (5)$$

43 In the equation (1), α is 1.875, which depends on the oscillation mode. I , E and A
44 represent the moment of inertia, modulus and sectional area of the film. Besides, the l ,
45 w , and h represent the length, width and height of the film immersed with or without
46 ethanol, respectively. The ρ are calculated to be about 0.13 and 0.67 g cm⁻³, when the
47 100 μm film was immersed with or without ethanol, and the calculated oscillation
48 frequency is about 3.9 and 6.3 Hz. When the film generates oscillation under NIR
49 irradiation, the obtained experimental frequency is between 3.3 and 6 Hz, having a
50 good agreement with the theoretical data.

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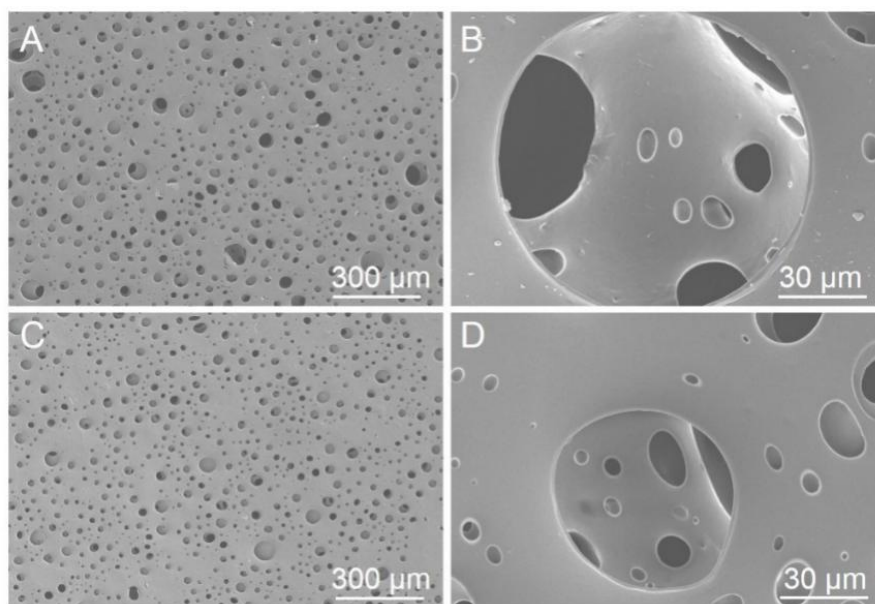
52 **Supplementary figures**



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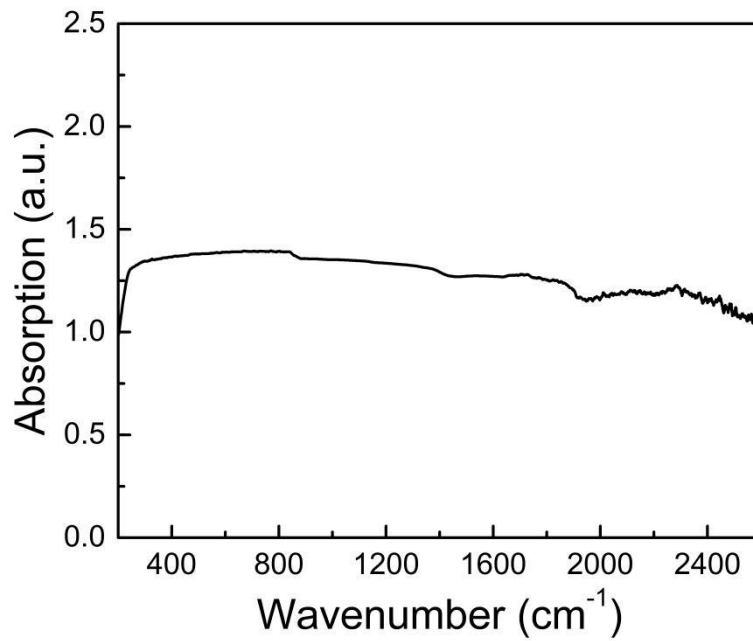
54 **Supplementary Fig. 1.** Pore size distribution of the porous PP/CB film measured by
55 the mercury intrusion method.

56



57

58 **Supplementary Fig. 2.** Low and high magnifications for the porous PP/CB film with
59 thickness of 60 μm (A, B) and 150 μm (C, D).

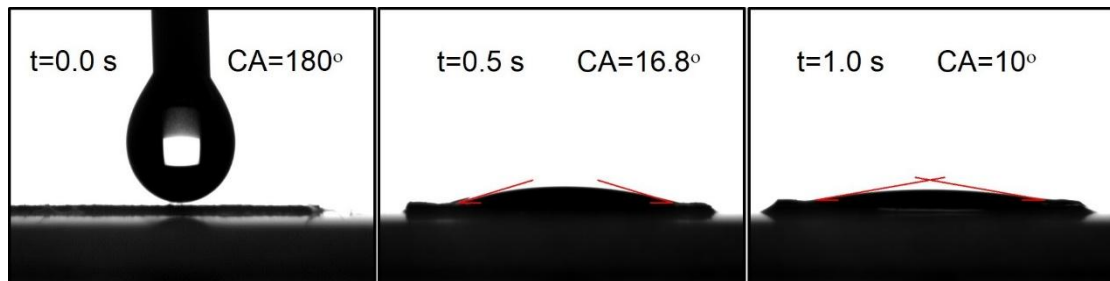


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61 **Supplementary Fig. 3.** Absorption spectra of the PP/CB film.

62

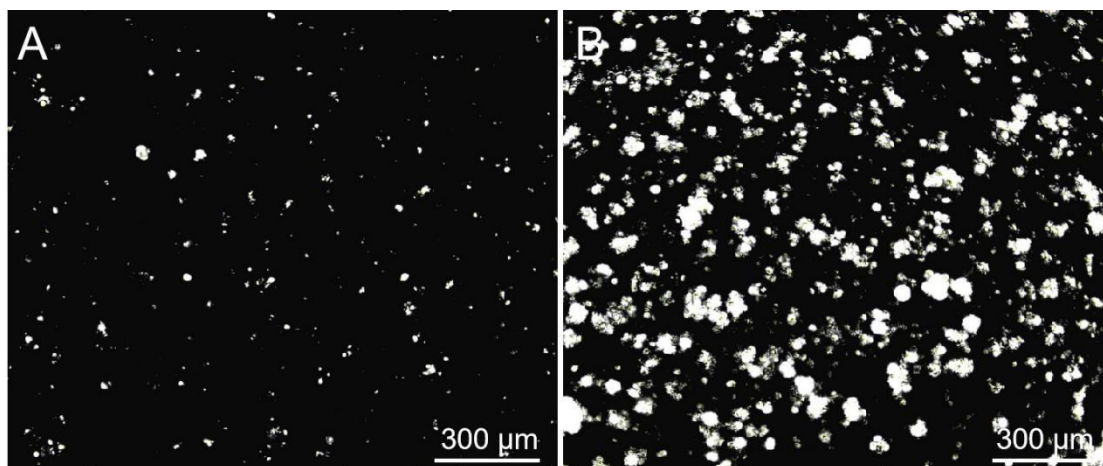
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65 **Supplementary Fig. 4.** Photographs at different time during contact angle
 66 measurement by dropping ethanol on the porous PP/CB film with thickness of 100
 67 μm .

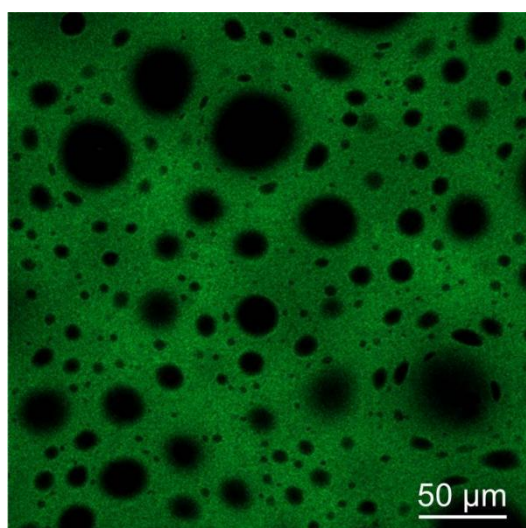
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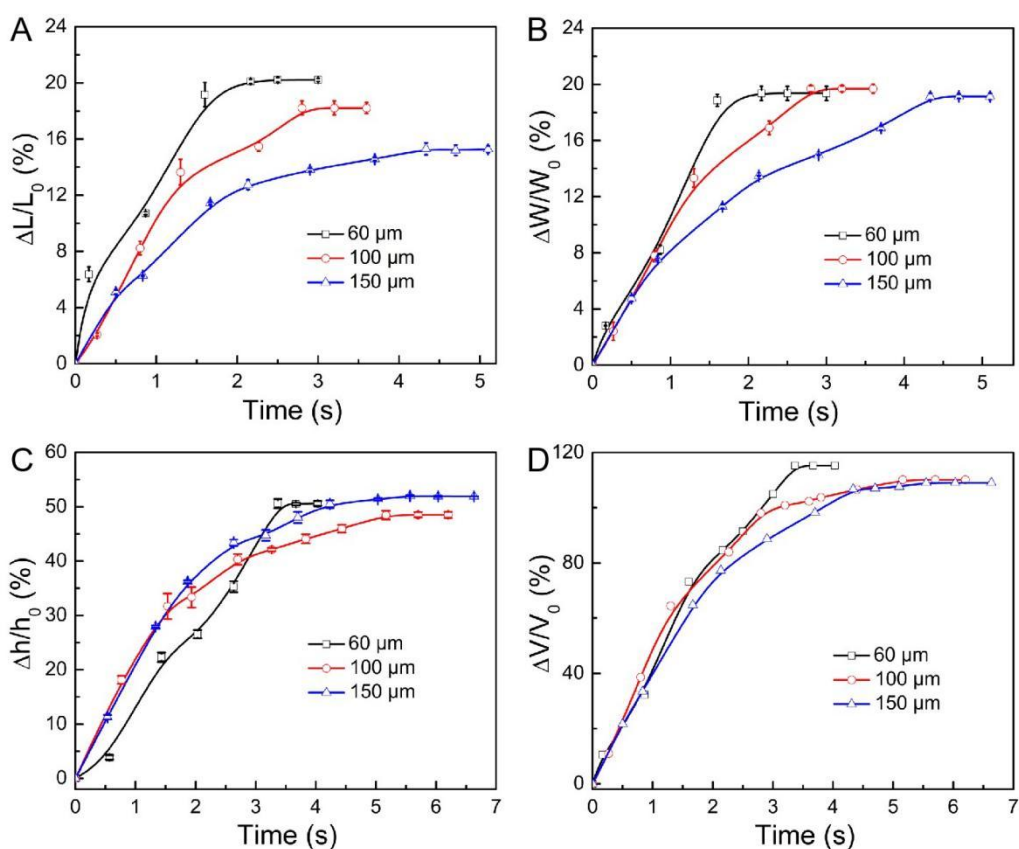
70 **Supplementary Fig. 5.** Optical images of the porous PP/CB film before (A) and after
71 (B) infiltrated with ethanol.

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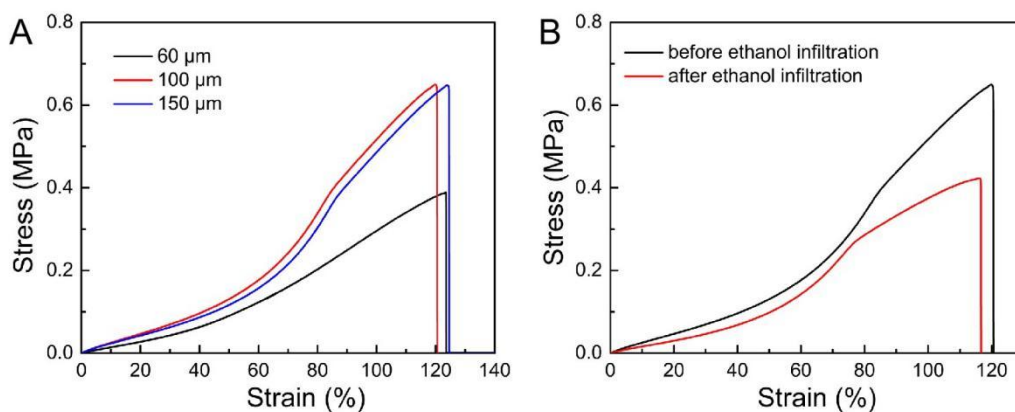
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74 **Supplementary Fig. 6.** Fluorescent image of the 100 μm thickness porous PP/CB
75 film infiltrated with rhodamine/ethanol solution (0.5 mg mL^{-1}).



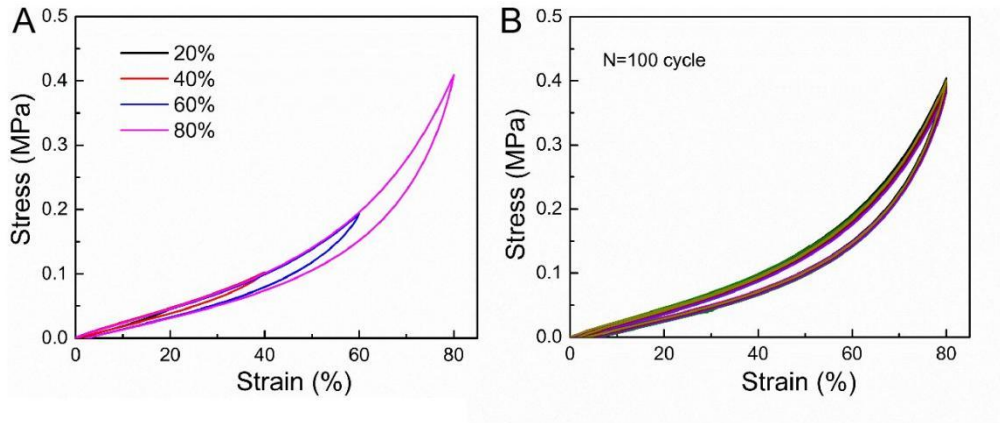
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77 **Supplementary Fig. 7.** Change ratio in length (A), width (B), thickness (C), and
 78 volume (D) as a function of time for the porous PP/CB film with different thickness
 79 by absorbing ethanol. The original size of the PP film is 3 cm × 1 cm × 100 μm. Error
 80 bars denote the standard deviation.



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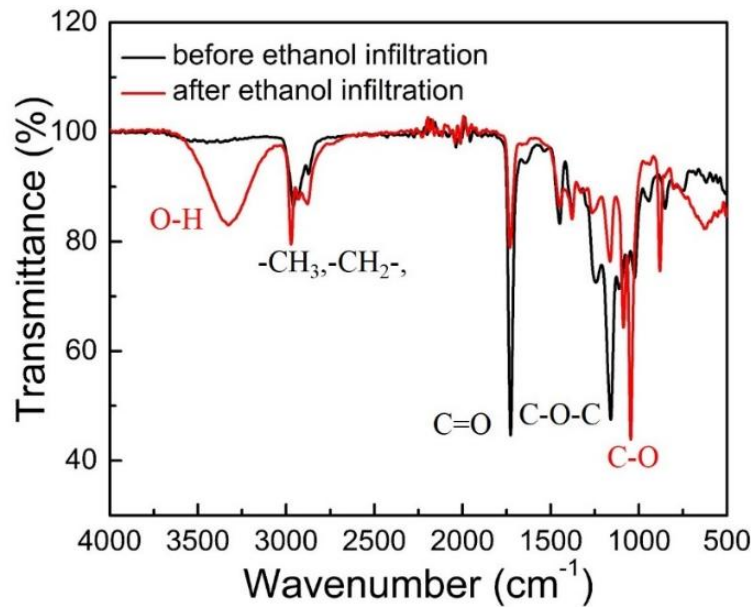
82 **Supplementary Fig. 8.** Stress-strain curves for the porous PP/CB film (A) with
 83 different thickness, and (B) before and after infiltration of ethanol. The stretch rate is
 84 0.5% s⁻¹. The original size of the PP film is 2 cm × 1 cm × 100 μm.



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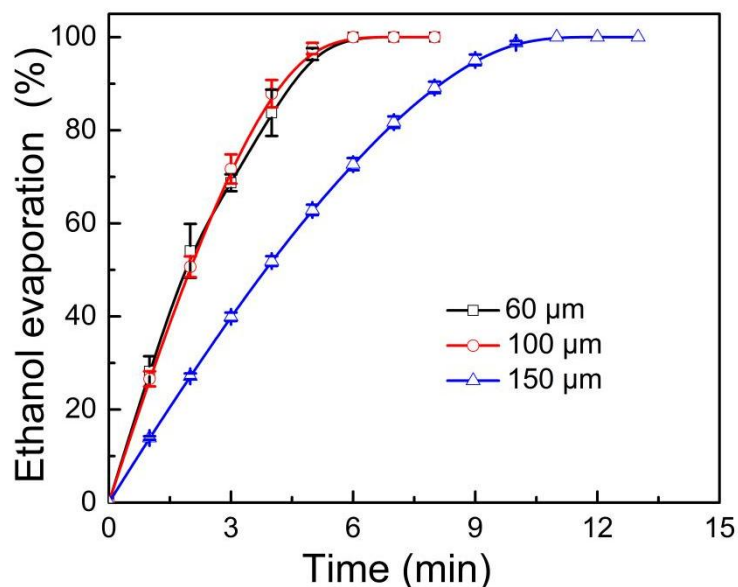
86 **Supplementary Fig. 9.** Stress-strain curves with progressively increasing strain (A)
 87 and cyclic stress-strain tests (B) for the porous PP/CB film. The stretch rate is 0.5 %
 88 s^{-1} . The original size of the PP/CB film is 2 cm \times 1 cm \times 100 μm .

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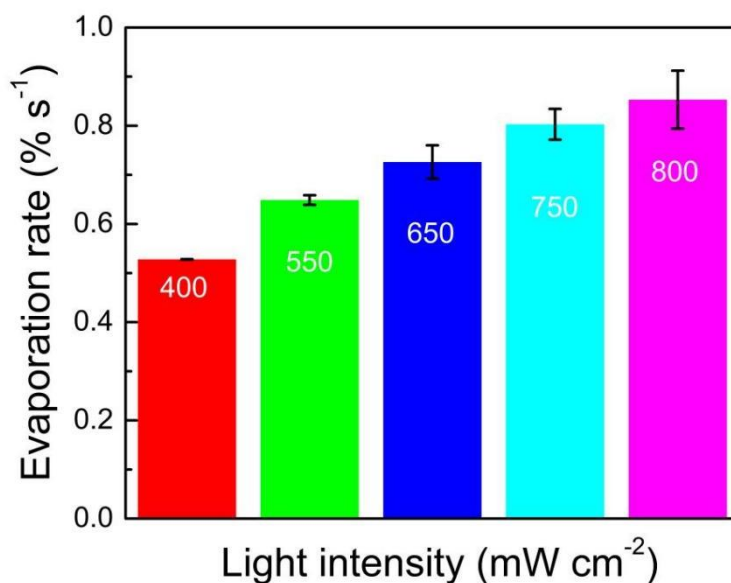


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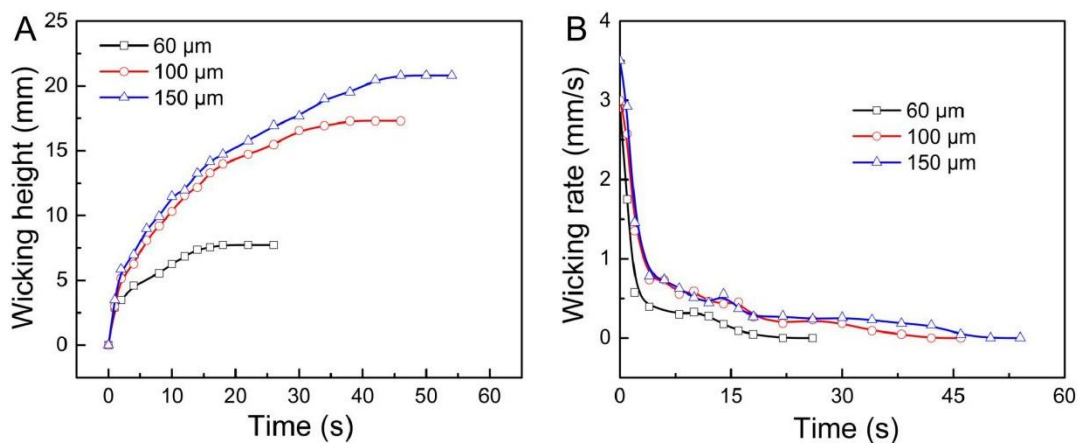
91 **Supplementary Fig. 10.** FTIR spectra for the porous PP/CB film before and after
 92 ethanol filtration.



93
 94 **Supplementary Fig. 11.** Mass percent of the ethanol evaporation for the porous PP
 95 film infiltrated with ethanol as a function of time in open air. Error bars denote the
 96 standard deviation.



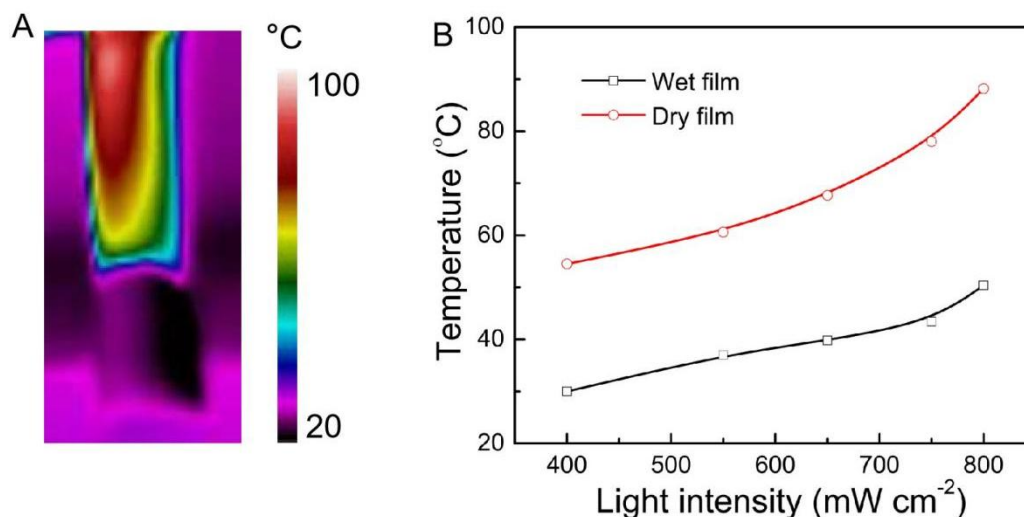
97
 98 **Supplementary Fig. 12.** Ethanol evaporation rate for the 100 μm thickness porous
 99 PP/CB film under different light intensities. The evaporation rate (v) was calculated
 100 by the percent mass decrease for the porous PP film infiltrated with ethanol divided
 101 by the time during complete ethanol evaporation. $v = m_{PP} / ((m_{PP} + m_{ethanol}) \cdot t)$, where
 102 m_{PP} , $m_{ethanol}$, and t are the mass of dry porous PP film, the mass of the ethanol for full
 103 infiltration, and the time for complete ethanol evaporation. Error bars denote the
 104 standard deviation.



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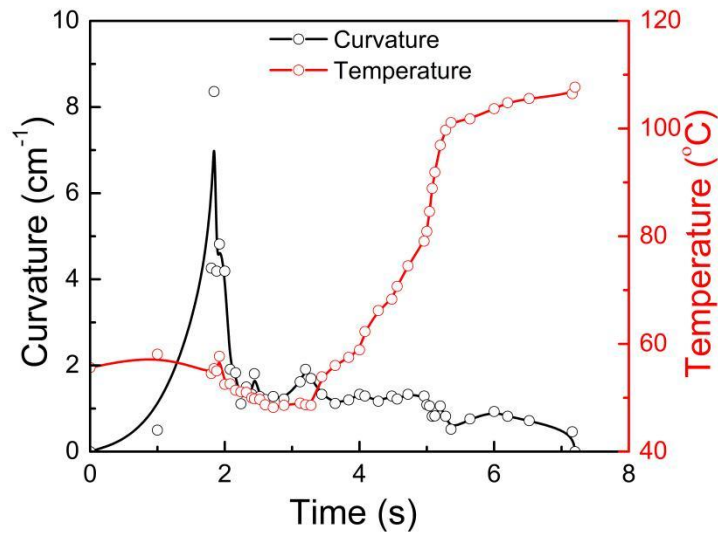
106 **Supplementary Fig. 13.** Wicking height (A) and wicking rate (B) as a function of
 107 time for the porous PP/CB film with different thickness. The original length and width
 108 of the film are 5 cm × 1 cm.

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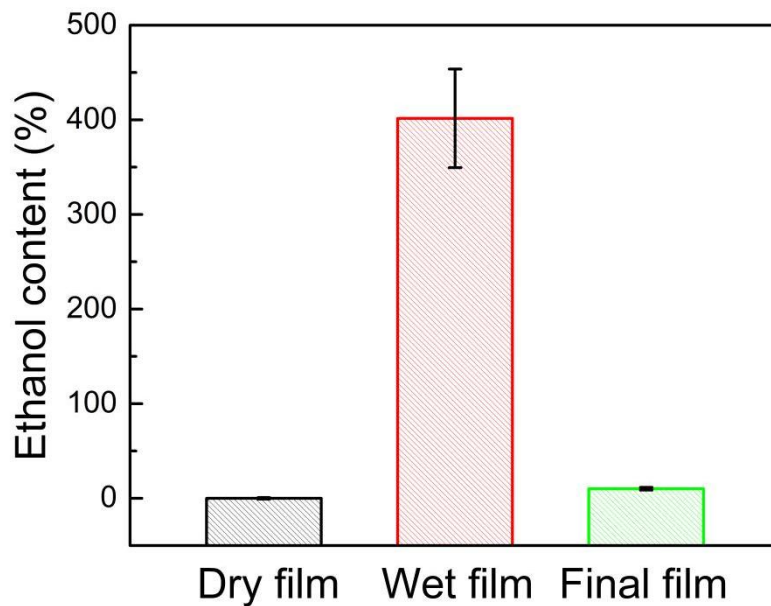


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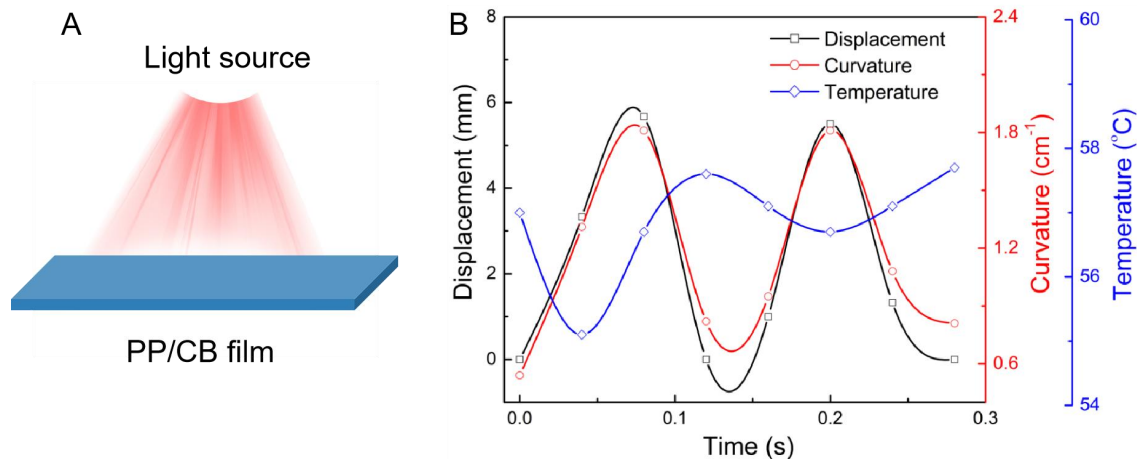
111 **Supplementary Fig. 14.** (A) Infrared image of the PP/CB film when infiltrated with
 112 ethanol and reached the maximum wicking height at under 800 mW cm⁻² NIR light.
 113 (B) Surface temperature of the wet PP/CB film with ethanol infiltration and dry film
 114 without ethanol infiltration at different light intensities.



115
 116 **Supplementary Fig. 15.** Curvature and temperature as a function of time when the
 117 100 μm thickness PP/CB film infiltrated with ethanol was irradiated by 800 mW cm^{-2}
 118 NIR light at a tilt angle of 90° . The original length and width of the film are 9 mm \times 3
 119 mm.

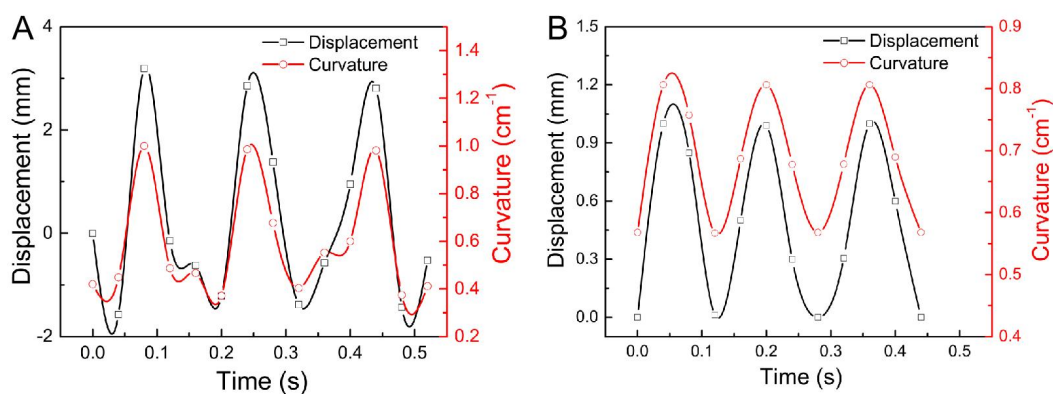


120
 121 **Supplementary Fig. 16.** Ethanol content of the 100 μm thickness PP/CB film at
 122 different states (Dry film indicated the film without ethanol infiltration; Wet film
 123 indicated the film with saturated ethanol infiltration; Final film indicated the film
 124 stopped actuating under NIR light). The original length and width of the film are 9
 125 mm \times 3 mm. Error bars denote the standard deviation.



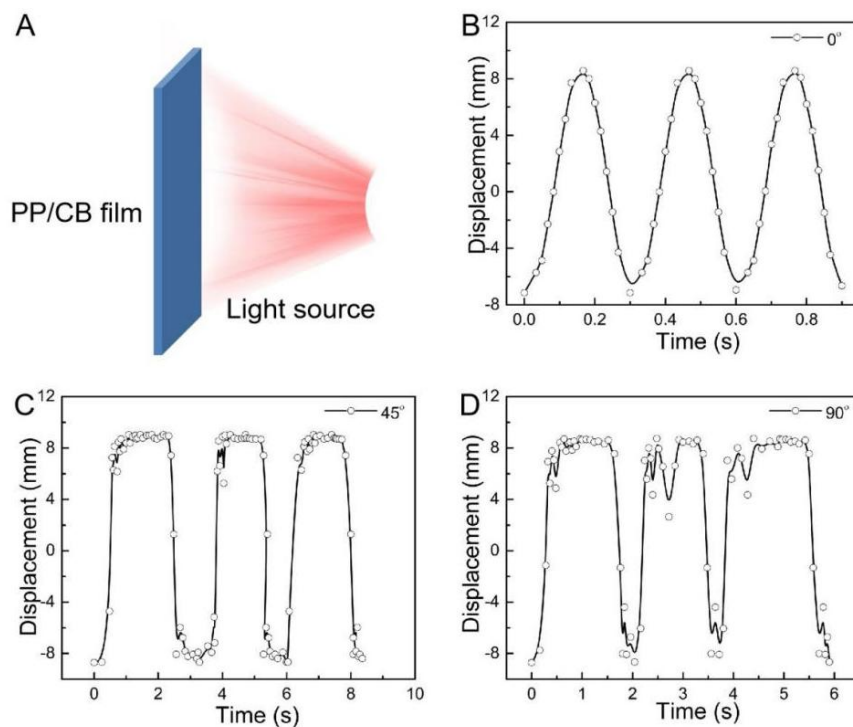
126

127 **Supplementary Fig. 17.** Schematic illustration of the horizontally placed film
 128 irradiated vertically by light (A) and Displacement, curvature, and temperature as a
 129 function of time for the horizontally placed PP/CB film under 800 mW cm^{-2} NIR light
 130 at a tilt angle of 90° (B).



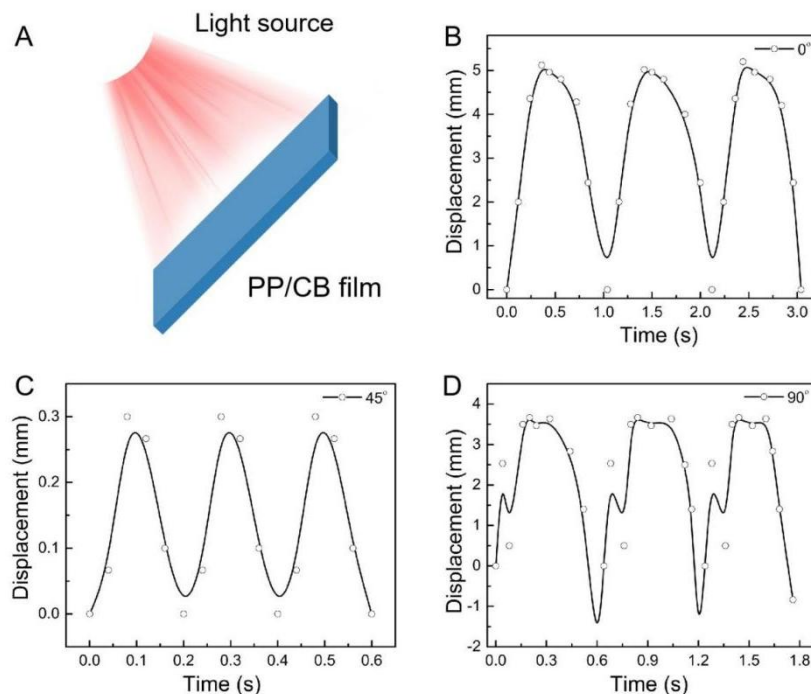
131

132 **Supplementary Fig. 18.** Displacement, and curvature as a function of time for the
 133 horizontally placed PP/CB film under 800 mW cm^{-2} NIR light at a tilt angle of 45° (A)
 134 and 0° (B).



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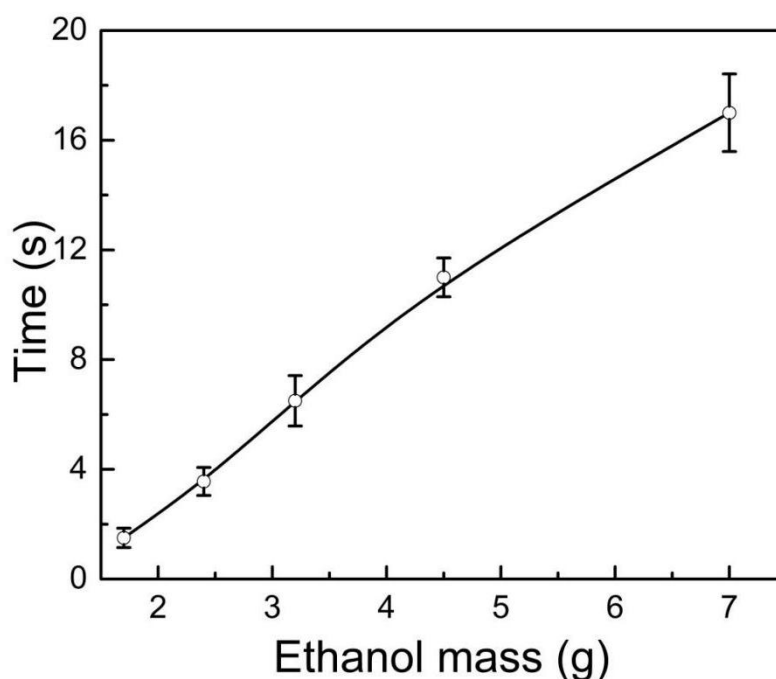
136 **Supplementary Fig. 19.** Schematic illustration of the vertically placed film irradiated
 137 vertically by light (A) and Displacement as a function of time for the actuator film
 138 with 90° tilt angle film under 800 mW cm⁻² NIR light at a tilt angle of 0° (B), 45° (C),
 139 and 90° (D).



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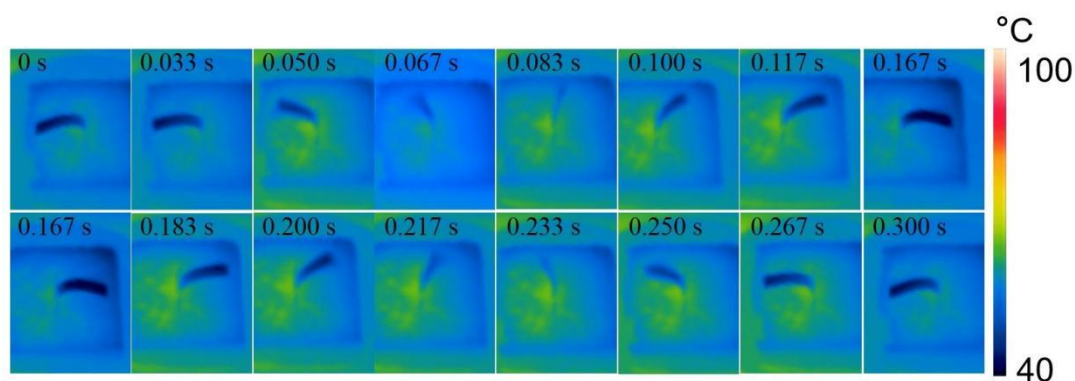
141 **Supplementary Fig. 20.** Schematic illustration of the film with 45° tilt angle
 142 irradiated vertically by light (A) and Displacement as a function of time for the
 143 actuator film with 45° tilt angle film under 800 mW cm⁻² NIR light at a tilt angle of
 144 0° (B), 45° (C), and 90° (D).

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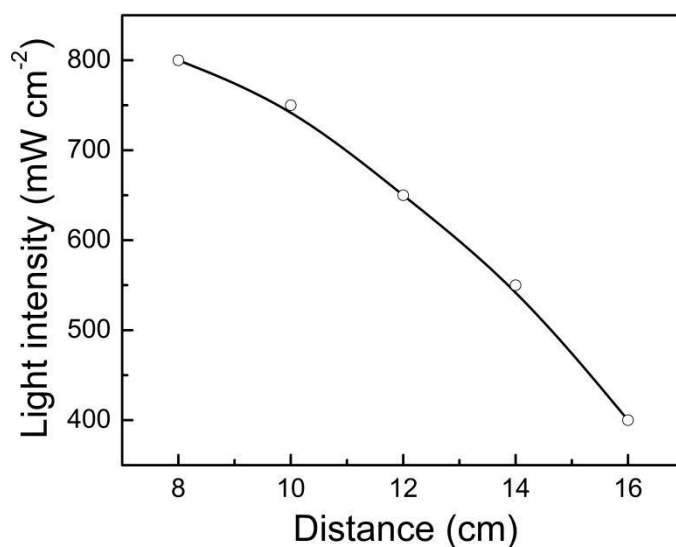
146

147 **Supplementary Fig. 21.** Time as a function of ethanol mass for the PP/CB film
148 reaching to the stable oscillation. The vertically placed porous PP film with original
149 size of 9 mm × 3 mm × 100 μm supplied with ethanol were used as the actuator. The
150 vertically irradiated 800 mW cm⁻² NIR light were used for actuation by photothermal
151 induced solvent irradiation. Error bars denote the standard deviation.



152

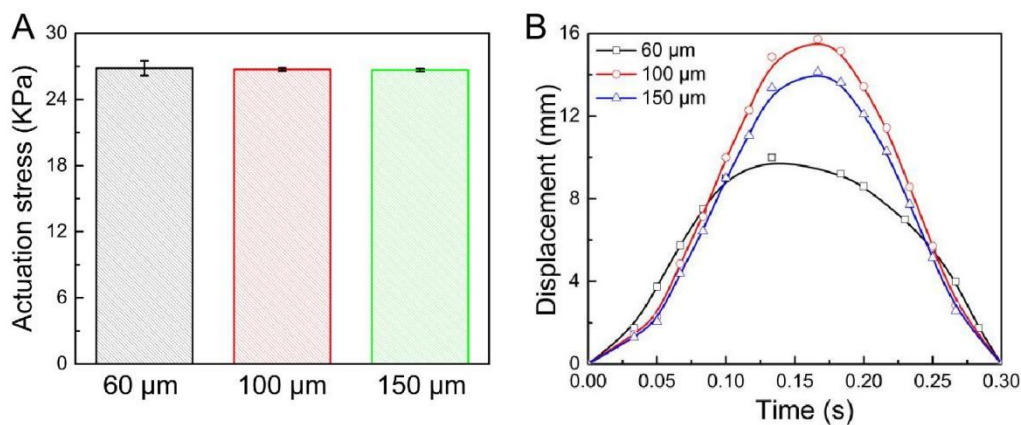
153 **Supplementary Fig. 22.** Infrared images at different time for the oscillating bending
154 actuation. The vertically placed porous PP film with original size of 9 mm × 3 mm ×
155 100 μm supplied with ethanol were used as the actuator. The vertically irradiated 800
156 mW cm⁻² NIR light were used for actuation by photothermal induced solvent
157 irradiation. If not specified, the same size and configuration of the actuator, and the
158 same light intensity and irradiation angle were used in the following oscillating
159 actuation experiments.



160

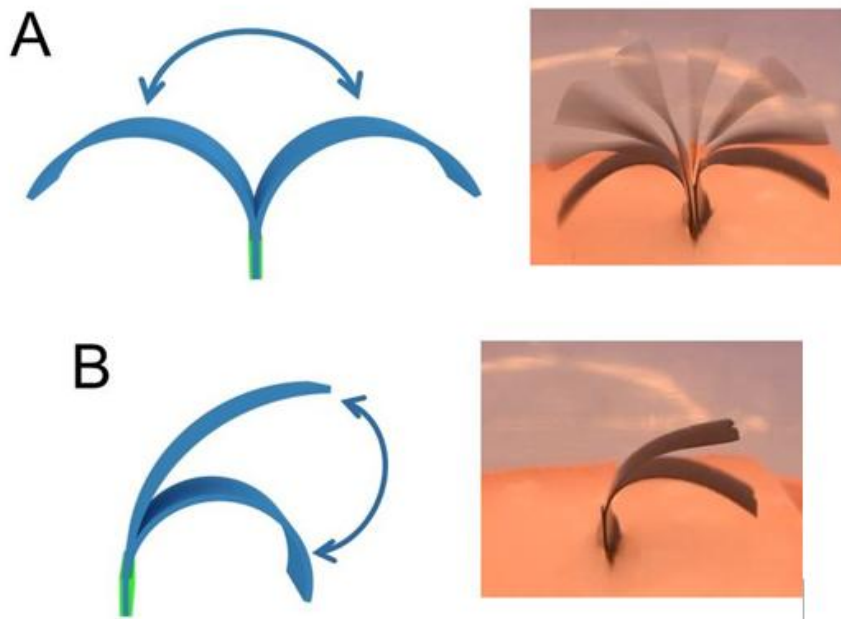
161 **Supplementary Fig. 23.** Light intensity as a function of distance of the actuator under
 162 NIR light.

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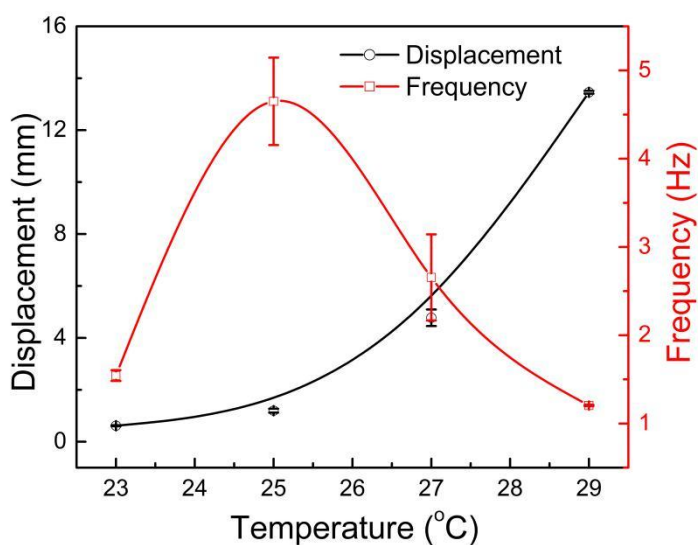
164

165 **Supplementary Fig. 24.** Actuation stress for the porous PP/CB film (2 cm × 1 cm)
 166 with different thickness (A), and displacement as a function of time for the oscillating
 167 bending actuation under NIR light with 800 mW cm⁻² for the porous PP/CB film with
 168 different thickness (B). The original length and width of the film are 9 and 3 mm,
 169 respectively. Error bars denote the standard deviation.



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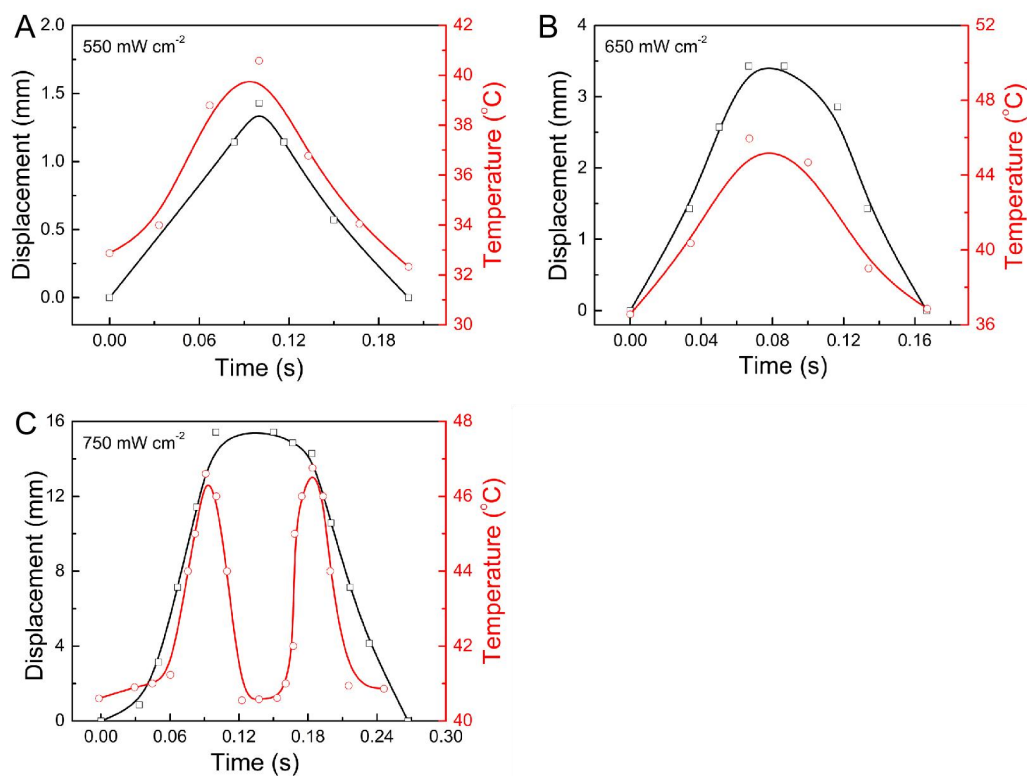
171 **Supplementary Fig. 25.** Schematic illustration (left) and photographs (right) for the
 172 oscillating actuation under NIR light with 800 mW cm^{-2} (A) and 400 mW cm^{-2} light
 173 intensities.



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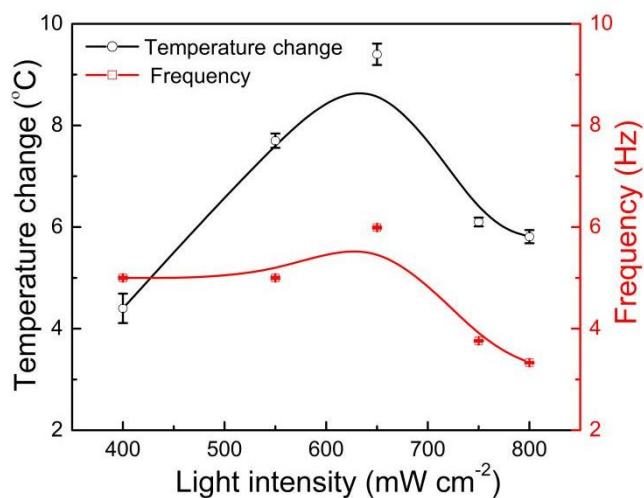
175 **Supplementary Fig. 26.** Displacement and actuation frequency of the PP/CB porous
 176 film as a function of environmental temperature under NIR light with 400 mW cm^{-2} .
 177 The size of the PP/CB film is $9 \text{ mm} \times 3 \text{ mm} \times 100 \text{ }\mu\text{m}$. Error bars denote the standard
 178 deviation.

179



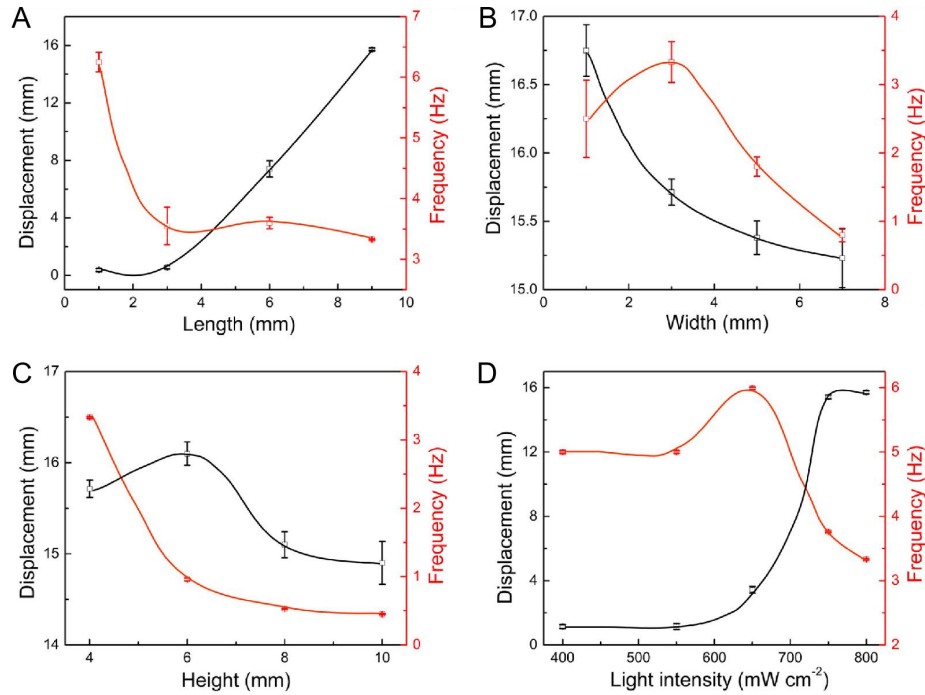
180

181 **Supplementary Fig. 27.** Displacement and maximum surface temperature as a
 182 function of time for the oscillating bending actuation under NIR light with 550 mW
 183 cm⁻² (A), 650 mW cm⁻² (B), and 750 mW cm⁻² (C).



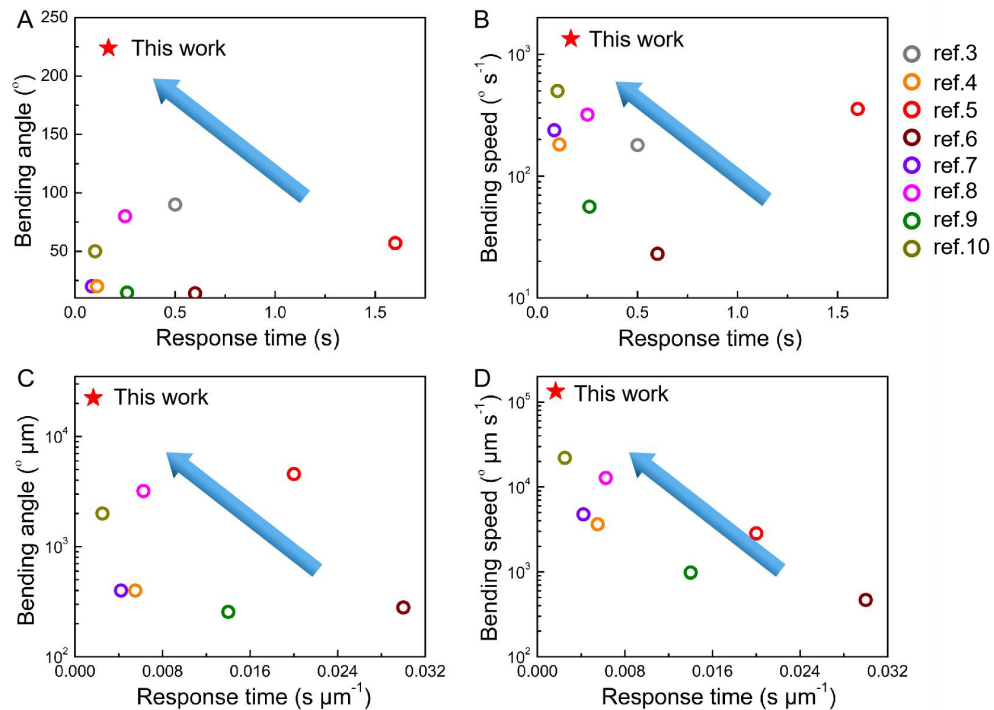
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185 **Supplementary Fig. 28.** Temperature change and oscillating frequency of the
 186 actuator as a function of light intensity. Error bars denote the standard deviation.



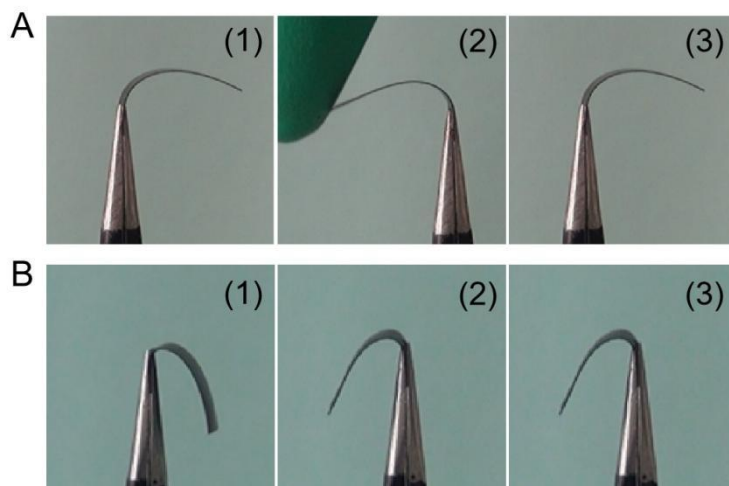
187

188 **Supplementary Fig. 29.** Displacement and oscillation frequency as a function of
 189 actuating film with different lengths (A), widths (B), wetting heights of the solvent in
 190 the film (C), light intensities (D). The original size of the PP/CB film is 9 mm \times 3 mm
 191 \times 100 μm . Error bars denote the standard deviation.

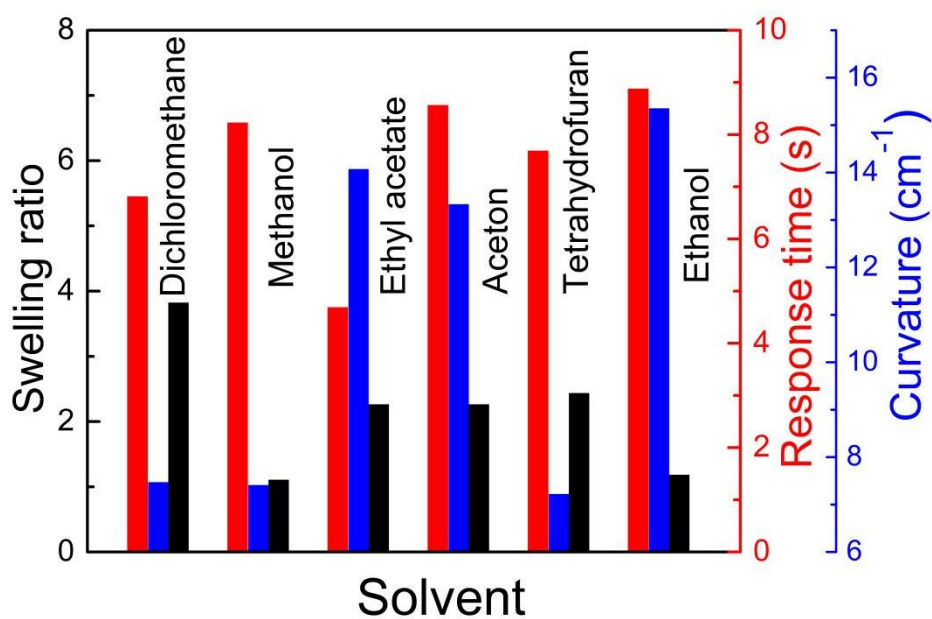


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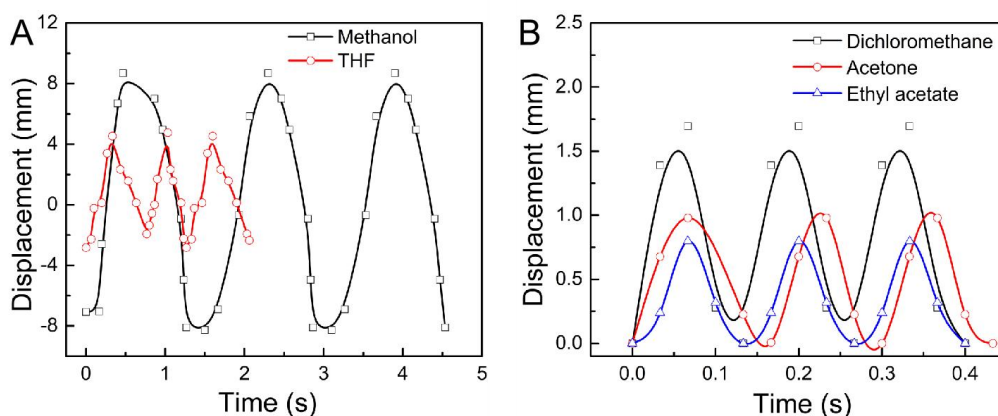
193 **Supplementary Fig. 30.** Comparison of the bending angle and response time,
 194 bending speed and their values normalized with thickness with other oscillating
 195 actuators.



196
 197 **Supplementary Fig. 31.** Photographs of the dry PP/CB film (A) and wet PP/CB film
 198 infiltrated with ethanol (B) at different states. (1) the initial shape; (2) the bending
 199 state under the external force of the finger; (3) the final state on removing the external
 200 force.



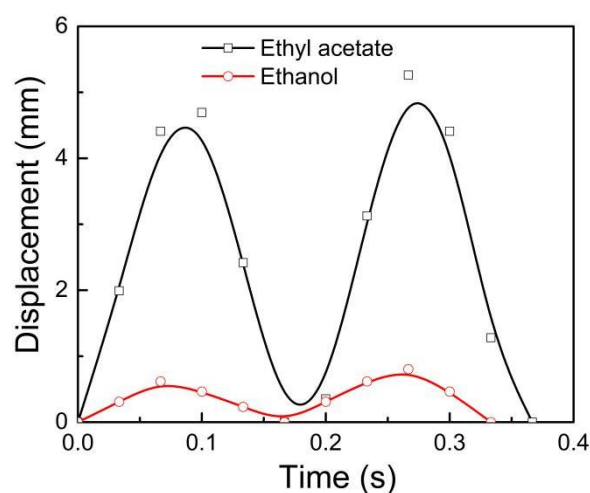
201
 202 **Supplementary Fig. 32.** Swelling ratio, response time and curvature of the 100 μm
 203 thick film in different solvent systems.



204

205 **Supplementary Fig. 33.** Displacement as a function of time for the oscillating
 206 bending actuation under NIR light with different solvents supply, (A) methanol and
 207 tetrahydrofuran (THF), (B) dichloromethane, acetone, and ethyl acetate.

208



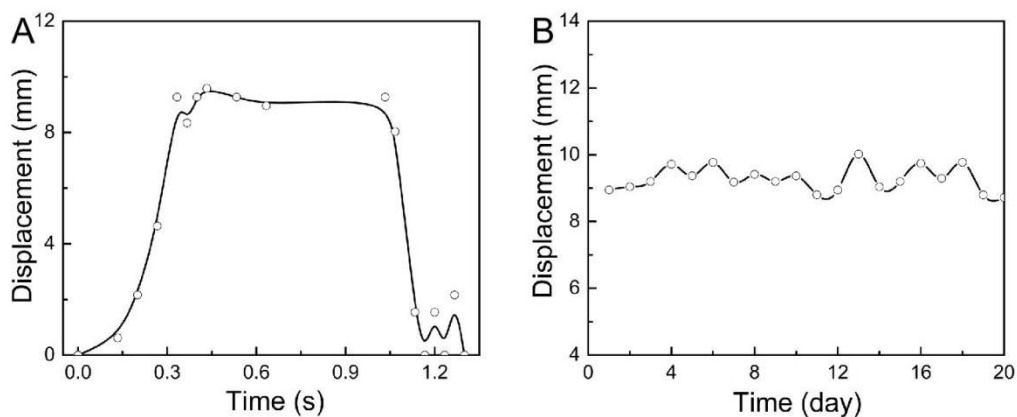
209

210 **Supplementary Fig. 34.** Displacement as a function of time for the porous PDMS
 211 film under NIR light with ethanol and ethyl acetate supply. The original dimension of
 212 the film is 5 mm × 2 mm × 35 μm.

213

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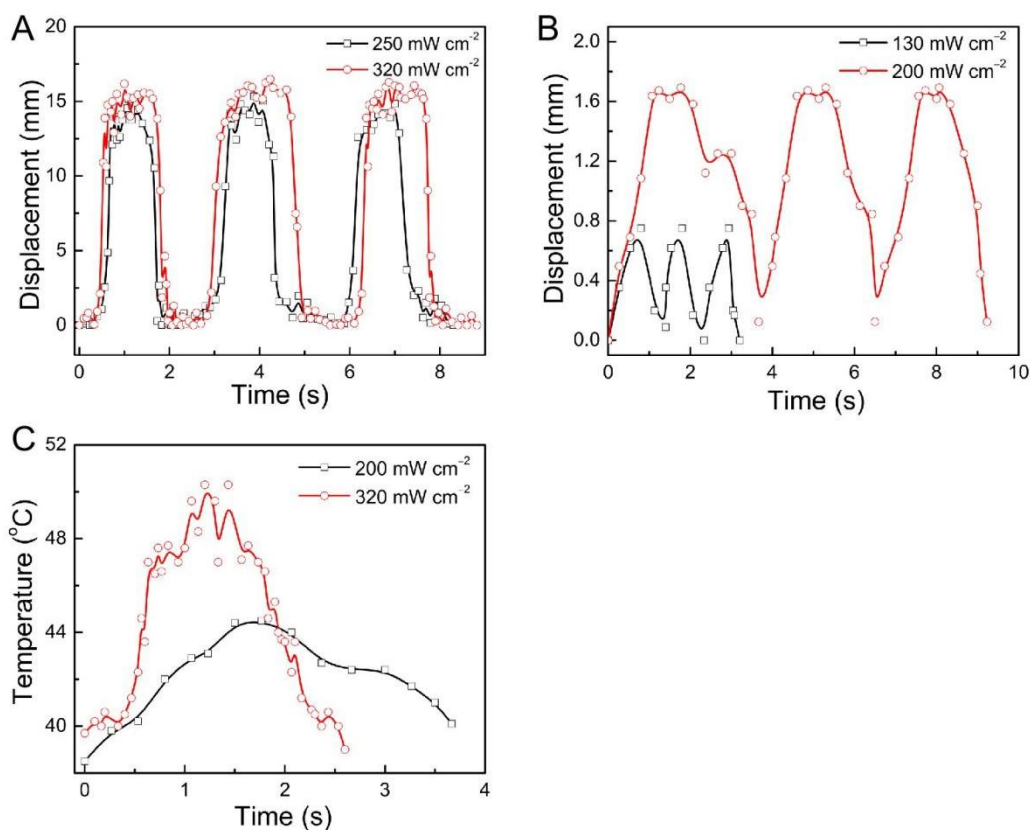
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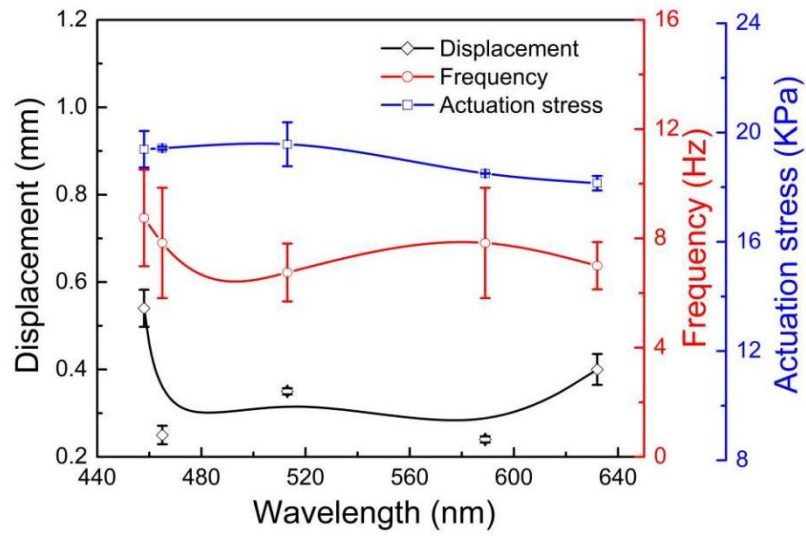
217 **Supplementary Fig. 35.** Displacement as a function of time for the porous PP/CB
 218 film under the intense light with an irradiation temperature of about 36 °C (A) and the
 219 performance stability test for 20 days (B).

220



221

222 **Supplementary Fig. 36.** Displacement as a function of time for the oscillating
 223 bending actuation under Xe lamp at different light intensities, (A) 250 mW cm⁻² and
 224 320 mW cm⁻², (B) 130 mW cm⁻² and 200 mW cm⁻². (C) Temperature as a function of
 225 time for the oscillating bending actuation under Xe lamp at 200 mW cm⁻² and 320
 226 mW cm⁻².



227

228 **Supplementary Fig. 37.** Displacement, actuation frequency, and actuation stress as a
 229 function of incident light wavelength. Error bars denote the standard deviation.



230

231 **Supplementary Fig. 38.** Photographs of the oscillating actuation at different time by
 232 carrying 1.9-times load. The original size of the PP/CB is 9.5 mm length and 5 mm
 233 width.

234 **Supplementary Table 1.** Comparison of the light-induced oscillating bending
 235 actuation of this work with those of typical photo-induced oscillators.

Materials	PP/CB (this work)	AuNPs- PNIPAM ³	F-azo ⁶	LC Photonic ⁸	CNT/PDMS ⁵	PDA-LCN ⁴	Azo-LCN-Kapton ⁹	M1-LCN ¹⁰
Light source	NIR	Laser	532 nm	Visible	White	NIR	365 nm	UV
Light intensity (mW cm ⁻² /mW)	800/-	-/500	35/-	100/-	330/-	2500/-	100/-	200/-
Thickness <i>d</i> (μm)	100	-	20	40	80	20	17.5	40
Curvature κ /angle θ (cm ⁻¹ /°)	7.3/224°	1.1/90°	0.2/14°	0.7/80°	0.8/57°	0.3/20°	0.25/14.6°	0.35/50°
$\kappa \times d$ (10 ⁻⁴)	730	-	4	28	64	6	4.38	14
Response time <i>t</i> (s)	0.167	0.5	0.6	0.25	1.6	0.11	0.26	0.1
$\theta \times d$ (° μm)	22400	-	280	3200	4560	400	255.5	2000
<i>t/d</i> (s μm ⁻¹)	0.00167	-	0.03	0.00625	0.02	0.0055	0.0149	0.0025
κ/t (cm ⁻¹ s ⁻¹)	43.7	2.2	0.33	2.8	0.5	2.73	0.96	3.5
θ/t (° s ⁻¹)	1341	180	23.3	320	356.25	182	56.15	500
$\kappa \times d/t$ (10 ⁻⁴ s ⁻¹)	4371	-	6.7	112	40	54.5	16.8	140
$\theta \times d/t$ (° μm ⁻¹ s ⁻¹)	134131	-	466.7	12800	2850	3636	982.7	22000
Displacement (mm)	15.7	0.5	3.08	-	13.9	6.7	-	-
D/L	1.74	0.029	0.193	-	1.1	0.67	-	-
T _{max} (°C)	48.5	34.3	31	84.6	99	60	37	-
ΔT (°C)	5.8	3.7	7	58.7	29	35	2.9	-
Frequency (Hz)	6	0.9	0.7	0.15	0.3	9	2.2	5
Divergent light	Yes	Yes	No	No	No	No	Yes	No
Local light	No	No	Yes	Yes	Yes	Yes	Yes	Yes

236 Au NP-PNIPAM: gold nanoparticles-poly(*N*-isopropylacrylamide); F-azo: ortho-Fluor
 237 azobenzene; LCN: liquid crystal polymer network; CNT: carbon nanotube; PDMS:
 238 polydimethylsiloxane; PDA: polydopamine.

239 **Supplementary References**

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