# **@AGU**PUBLICATIONS

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2	Geophysical Research Letters
3	Supporting Information for
4	The impact of basal roughness on inland Thwaites Glacier sliding.
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### **35 S1. Overview**

36 The supplement is organized in two sections of supplement material (figures and table) with a

37 final text section that elaborates upon methods used in the paper. We first present all filtered

38 topographies, surface elevation and surface velocity data used in each model experiment

39 (Figures S1-S3). We then show inversions for all inferred friction coefficient fields (Figures S4-

40 S5) determined from the Tikhonov regularization procedure outlined in Figure S6. Model

41 parameters are detailed in Table S1. We also describe the power-law fitting procedure used to

42 analytically glacier derive slip length from the topography.



49 Supplementary Figure 1. The (A) topographies of the isotropically filtered grids for

50 lower Thwaites Glacier, and the (B) along-flow and (C) transverse anisotropically filtered 51 topographies for the lower Thwaites Glacier grid.

50



54 **Supplementary Figure 2.** The (A) topographies of the isotropically filtered grids for upper

- 55 Thwaites Glacier, and the (B) along-flow and (C) transverse anisotropically filtered
- 56 topographies for the upper Thwaites Glacier grid.
- 55



58 59 Supplementary Figure 3. The (A, B) surface velocity and (C, D) surface elevation for the lower

Thwaites and upper Thwaites grids. Note, color maps are scaled uniquely for each grid.

#### 61 **S3.** Inversions



### 62 65

**Supplementary Figure 4.** The (A) inferred friction coefficient of each of the isotropically 66 filtered lower Thwaites grid simulations, and the (B) along-flow and (C) transverse

67 anisotropically filtered topographies for the lower Thwaites Glacier grids.

66



Supplementary Figure 5. The (A) inferred friction coefficient of each of the isotropically

- 72 filtered upper Thwaites grid simulations, and the (B) along-flow and (C) transverse
- 73 anisotropically filtered topographies for the upper Thwaites Glacier grids.
- 71





Supplementary Figure 6. The Tikhonov regularization curves (cost function plotted against the mean square gradient of beta for  $\log_{10} \lambda = 10e^3$ ,  $10e^4$ ,  $10e^5$ , ...  $10e^{10}$ ) for the (A) lower Thwaites and the (B) upper Thwaites grids where rainbow colors indicate model grid resolution (purple is highest resolution, blue second highest etc.). Between  $10e^{6}$  and  $10e^{7}$ , the cost function increases dramatically, and the L-curve method would select a value in this range as the appropriate regularization parameter (indicated with a star). For both the lower Thwaites and upper Thwaites grids, the highest resolution model domain minimizes the most cost per node.

Parameter	Value	Units	Description
$A_0$	$3.985e^{-13}$	$MPa^{-3} \cdot yr^{-1}$	Spatially uniform rate factor
Q	60 <i>e</i> <sup>3</sup>	J	Spatially uniform activation energy (Patterson 2010)
R	8.314	J/mol · K	Ideal gas constant
λ	10 <i>e</i> <sup>6</sup>	_	Tikhonov regularization coefficients
n	3	_	Glen's flow law exponent
m	1	_	Basal sliding relation exponent

**Supplementary Table 1.** Table of model parameters used across all full-Stokes simulations.

89

#### 87 **S4. Analytic Slip Length Calculation**

88 In glacier sliding theory, slip length (*L*) is defined as:

$$L = \frac{\eta}{\beta} \tag{1}$$

90 where  $\eta$  is ice viscosity and  $\beta$  is the basal drag coefficient. If the slip length is larger than the 91 ice thickness, the basal drag is too small to induce shear in the ice column, and ice slides over 92 the substrate at a uniform velocity with depth (plug flow). If the slip length is smaller than the 93 ice thickness, then basal drag can induce substantial shearing through the ice column, 94 resulting in a depth-variable velocity profile. Slip length is thus a useful metric for 95 distinguishing the ice-flow regime.

96

97 We compare slip lengths calculated from our modeled parameter fields to slip lengths 98 calculated using analytic theory for form drag for ice flow over an undulating bed that requires 99 only bed roughness power spectra as an input (Schoof, 2002). Similar to Hogan et al. (2020), 100 we approximate one-sided periodograms of the along-flow bed roughness profiles derived 101 from the radar swath topographies (Holschuh et al., 2020) using an inverse square power law 102 (equivalent to a random-walk elevation profile), where the periodogram component ( $P_n$ ) 103 associated with each frequency band can be fit by:

104

$$P_n = A f_n^{-2} \tag{2}$$

where *A* is a fit coefficient with units of length and  $f_n = n/a$  is the center frequency of a frequency band of width 1/a, *a* is the length of the fit window, and  $n = 1 \dots N$  with *N* being

frequency band of width 1/a, a is the length of the fit window, and  $n = 1 \dots N$  with N being the total number of components in the periodogram (here N=256). Following Schoof (2002)

and Hogan et al. (2020), for sufficiently high wavenumbers ( $k_n \gg 1/H$  where H is ice

109 thickness) the basal drag components are given by:

110

$$\beta_n = 16\eta \pi^3 A a^{-1} f_n. \tag{3}$$

111 The total form drag coefficient can then be approximated by:

$$\beta = \sum_{n=1}^{N} \beta_n = 16\eta \pi^3 A a^{-2} \sum_{n=1}^{N} n = 8\eta \pi^3 A a^{-2} N(N+1)$$
(4)

113

115

114 and if  $\lambda_n \ll a$  so  $N \gg 1$ , then

$$\beta = 8\eta \pi^3 A \lambda_N^{-2}. \tag{5}$$

116

117 Applying the definition of slip length then gives:

$$L = \frac{\lambda_N^2}{8\pi^3 A}.$$

We apply this analytic theory to our swath topographies to calculate the slip lengths associated with form drag. First, we extract bed topography at 25m posting from the radar swath topography point cloud (Holschuh et al., 2020) at each point in the point cloud along 6.4km long flowlines (distance chosen to be similar to Hogan et al. (2020)) determined using the simulation reference surface velocity field. After removing the linear trend from the bed elevation profile and applying a Hamming window, we calculate the one-sided periodogram

125 using Welch's method (Welch, 1967). The inverse square power law coefficient A was

- 126 calculated using non-linear least squares fitting. The slip length calculated following Equation
- 127 6 is plotted at the center point of each flowline.
- 128

### 129 S5. Consistency with observed subglacial lake activity?

130 An active subglacial lake boundary (lake Thw124; Smith et al., 2017) identified from satellite 131 altimetry lies partially within the lower Thwaites grid. The inferred shear stress inside the lake 132 boundary is nonzero. Satellite observations suggest variability in the lake fill-drain levels on 133 Thwaites Glacier (Hoffman et al., 2020), so volume change estimates of lakes on Thwaites 134 Glacier derived from satellite altimetry are difficult to relate to changes in lake geometry. 135 Because the lake geometry is unknown for the observational period used to constrain the 136 snap-shot inversions, we do not know how much of the lake is buoyantly supporting the 137 overlying ice. This lake had drained prior to the epoch of the surface observations used to 138 constrain the inversion, so the non-zero drag may be evidence of ice regrounding; however, 139 independent GNSS observations suggest that ice velocity is insensitive to lake fill-drain cycles, 140 which would predict low shear stress values in the vicinity of the Thwaites lakes independent 141 of whether the lake is full or empty (Hoffman et al., 2020). The nonzero drag inside the lake 142 could also represent resistance from topographic pinning points that may always protrude 143 above the reported lake depth (Smith et al., 2017; Hoffman et al., 2020), which at ~20 m, is 144 below the root mean square amplitude of subglacial roughness in the boundary of the lake 145 and motivates further study of lake influence on ice-sheet mechanics and glacier sliding. 146 In the two-dimensional spectral variance of 6.0 km windowed bed topography, we see the first 147 indication from independent subglacial datasets of spatial changes in bed properties 148 consistent with the Thw124 lake position. Over the lake outline boundary, the bed appears to 149 be substantially smoother than the surrounding topography (Figure 3A). The SAR focused 150 radargrams, however, show no unambiguous evidence of an ice-lake interface. This suggests 151 that there may not be dielectric contrast across the lake interface that is distinguishable from a 152 wet sediment interface and/or that this interface is very rough.

### 153 S6. Simulations over a uniformly sloped bed topogaphy

154 Fitting a plane to the high-resolution topographies, we can simulate ice flow over a flat bed for

each grid. From these simulations we can relate the basal drag to the more the more

156 traditional horizontal shear stress (a global variable) and compare again the resistance and

157 normal pressure fields. The patterns of the inferred resistance fields are similar to the

158 smoothed topographies. The cost per node for each grid is substantially higher than the

159 isotropically smoothed experiments.



161 169 Supplementary Figure 7. (A) The basal resistance fields, (B) the normal pressure fields and 170 the (C) Tikhonov regularization curves (cost function plotted against the mean square gradient of beta for  $\log_{10} \lambda = 10e^3$ ,  $10e^4$ ,  $10e^5$ , ...  $10e^{10}$ ) for the lower Thwaites (light blue) and the 171 upper Thwaites (coral) flat grids. Again, near  $10e^6$  the cost function increases dramatically, 172 173 and the L-curve method would select a value in this range as the appropriate regularization 174 parameter (indicated with a star). The fields in (A) and (B) are the fields associated with this 175 choice of regularization. The cost per node for both simulations were 15% (lower thwaites) 176 and 5% (upper thwaites) greater than the most isotropically smoothed experiments.

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