

Supplementary Information :

Javanese *Homo erectus* on the move in SE Asia *ca.* 1.8 Ma

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| Lithological facies | Sample | Depth (cm) | Dissolved quartz (g) | [²⁶ Al] (10^5at.g^{-1}) | [¹⁰ Be] (10^5at.g^{-1}) | ²⁶ Al/ ¹⁰ Be |
|----------------------------------|-----------|------------|----------------------|---|---|------------------------------------|
| Tuff and siltstone | SAN18-1 | 2.5 | 10.855 | 1.036 ± 0.178 | 0.296 ± 0.029 | 3.50 ± 0.69 |
| | SAN18-2 | 12.5 | 7.700 | 1.141 ± 0.225 | 0.228 ± 0.029 | 5.02 ± 1.18 |
| | SAN18-3 | 17.5 | 3.128 | 0.944 ± 0.313 | 0.210 ± 0.058 | 4.50 ± 1.94 |
| | SAN18-4 | 60 | 3.817 | 1.245 ± 0.345 | 0.228 ± 0.047 | 5.46 ± 1.88 |
| | SAN18-5 | 85 | 4.835 | 0.933 ± 0.225 | 0.261 ± 0.041 | 3.58 ± 1.03 |
| | SAN18-6 | 32.5 | 1.223 | 0.907 ± 0.412 | 0.242 ± 0.123 | 3.75 ± 2.55 |
| Tuffaceous sand | SAN18-10 | 190 | 0.869 | 1.850 ± 0.847 | 0.550 ± 0.226 | 3.37 ± 2.07 |
| | SAN18-11b | 240 | 3.345 | 0.646 ± 0.289 | 0.159 ± 0.050 | 4.05 ± 2.21 |
| | SAN18-12 | 290 | 13.740 | 0.821 ± 0.123 | 0.277 ± 0.047 | 2.96 ± 0.67 |
| | SAN18-12b | 290 | 9.612 | 0.539 ± 0.237 | 0.224 ± 0.030 | 2.41 ± 1.11 |
| Bedded sand and gravel | SAN18-13 | 350 | 12.479 | 0.857 ± 0.147 | 0.223 ± 0.034 | 3.85 ± 0.88 |
| | SAN18-14 | 400 | 19.986 | 1.083 ± 0.137 | 0.289 ± 0.027 | 3.75 ± 0.59 |
| | SAN18-15 | 450 | 20.004 | 0.792 ± 0.149 | 0.277 ± 0.026 | 2.85 ± 0.60 |
| Conglomerate <i>Grenzbank</i> | SAN18-16 | 475 | 6.293 | 1.422 ± 0.399 | 0.261 ± 0.050 | 5.45 ± 1.85 |
| | SAN18-17 | 500 | 15.904 | 0.734 ± 0.109 | 0.268 ± 0.029 | 2.74 ± 0.50 |
| | SAN18-18 | 545 | 9.020 | 0.978 ± 0.222 | 0.239 ± 0.030 | 4.08 ± 1.06 |

Table 1 Analytical Data. $^{26}\text{Al}/^{10}\text{Be}$ analyses. For each sample, $\sim 150 \mu\text{l}$ of the an in-house phenakite $3.10^{-3} \text{ g.g}^{-1} \text{ }^{9}\text{Be}$ carrier solution was added (S.I. Table 3). ^{27}Al natural concentrations were measured by ICP-OES, and for 8 samples a variable amount of an aluminum carrier solution (Chemlab 983.28 g.g⁻¹) was added. Concentrations were corrected for chemical blank (for samples SAN18-8 to SAN18-18, blank ratios were $1.93 \pm 0.34 \times 10^{-15}$ and $1.93 \pm 1.3 \times 10^{-15}$ for $^{10}\text{Be}/^{9}\text{Be}$ and $^{26}\text{Al}/^{27}\text{Al}$ ratios, respectively; for samples SAN18-1 to SAN18-6, SAN18-11b and SAN18-12b blank ratios were $1.58 \pm 0.35 \times 10^{-15}$ and $1.06 \pm 1.05 \times 10^{-15}$ for $^{10}\text{Be}/^{9}\text{Be}$ and $^{26}\text{Al}/^{27}\text{Al}$ ratios, respectively). Density is set to 2 g.cm^{-3} . Uncertainties ($\pm 1\sigma$) include only analytical uncertainties. χ^2 at 95% confidence level, for ^{10}Be and ^{26}Al concentrations, and $^{26}\text{Al}/^{10}\text{Be}$ ratios are respectively 14, 14, and 9, while theoretical χ^2 (for $n=16$) is 25. The Mean Squared Weighted Deviation (MSWD) within the sample population are respectively 0.95, 0.93 and 0.64.

| | | | End-member case: Total burial <i>without</i> post-production | | Generic case: Burial <i>with</i> post-production | | | | |
|------------------------|-----------|------------|---|--------------------------------|---|--------------------------------|----------------------------------|------------------------------------|------------------------------------|
| Lithological facies | Sample | Depth (cm) | Burial age (Ma) | Denudation rate, source (m/Ma) | age (Ma) | Denudation rate, source (m/Ma) | Denudation rate, post-deposition | % [¹⁰ Be], post-burial | % [²⁶ Al], post-burial |
| Tuff and siltstone | SAN18-1 | 2.5 | 1.49 ± 0.30 | 46 | 1.78 ± 0.35 | 54 | 436 | 22.8 | 47.4 |
| | SAN18-2 | 12.5 | 0.76 ± 0.18 | 88 | | 69 | | 27.2 | 39.8 |
| | SAN18-3 | 17.5 | 0.98 ± 0.42 | 85 | | 78 | | 28.3 | 46.2 |
| | SAN18-4 | 60 | 0.58 ± 0.20 | 96 | | 59 | | 18.9 | 26.0 |
| | SAN18-5 | 85 | 1.44 ± 0.42 | 53 | | 53 | | 14.2 | 29.9 |
| | SAN18-6 | 32.5 | 1.35 ± 0.92 | 60 | | 66 | | 21.8 | 43.0 |
| Tuffaceous sand | SAN18-10 | 190 | 1.54 ± 0.95 | 23 | 1.78 ± 0.35 | 21 | 436 | 4.3 | 9.8 |
| | SAN18-11b | 240 | 1.20 ± 0.66 | 101 | | 84 | | 13.3 | 24.7 |
| | SAN18-12 | 290 | 1.83 ± 0.42 | 41 | | 49 | | 7.1 | 17.6 |
| | SAN18-12b | 290 | 2.25 ± 1.04 | 41 | | 61 | | 8.8 | 26.7 |
| Bedded sand and gravel | SAN18-13 | 350 | 1.30 ± 0.30 | 68 | 1.78 ± 0.35 | 55 | 436 | 8.2 | 15.3 |
| | SAN18-14 | 400 | 1.35 ± 0.21 | 50 | | 41 | | 6.1 | 11.3 |
| | SAN18-15 | 450 | 1.90 ± 0.40 | 39 | | 46 | | 6.1 | 14.5 |
| Conglomerate Grenzbank | SAN18-16 | 475 | 0.58 ± 0.20 | 83 | 1.78 ± 0.35 | 44 | 436 | 6.4 | 7.8 |
| | SAN18-17 | 500 | 1.99 ± 0.37 | 39 | | 50 | | 6.2 | 14.8 |
| | SAN18-18 | 545 | 1.18 ± 0.31 | 67 | | 50 | | 6.7 | 10.5 |

Table 2 Inversion model outputs, *without* (end-member case) and *with* post-burial production [1, 2]. The first case, considering no cosmogenic nuclides were accumulated in the samples while buried (infinite burial depth), yields minimum burial ages. The second, generic case, conversely considers cosmogenic nuclide production during post-burial exhumation, and yields an actual age. Uncertainties (reported as 1σ) obtained by propagating half-lives uncertainties. Parameters used for calculation: latitude: 7.47° ; altitude: 99 m; pressure: 1001 mbar; mean density: 2 g.cm^{-3} ; Stone scaling: 0.64; $T^{10}\text{Be}$: $1.387 \pm 0.0120 \text{ Ma}$ [3, 4]; $T^{26}\text{Al}$: $0.705 \pm 0.024 \text{ Ma}$ [5, 6]; P10 SLHL: $4.03 \pm 0.18 \text{ at.g}^{-1} \cdot \text{a}^{-1}$ [7, 8]; muon contributions and attenuation lengths are based on [2]. $^{26}\text{Al}/^{10}\text{Be}$ spallogenic production ratio: 6.61 ± 0.52 [9].

| Sample | Depth (cm) | Sample mass (g) | Dissolved pure quartz (g) | ^9Be carrier (10^{19} at) | $^{10}\text{Be}/^{9}\text{Be}$ (blank corrected) | ASTER total counts (10^{19} at.g $^{-1}$) | ^{27}Al carrier (10^{19} at) | ^{27}Al (blank corrected) | $^{26}\text{Al}/^{27}\text{Al}$ total counts (^{26}Al) |
|-----------|------------|-----------------|---------------------------|---------------------------------------|--|---|--|------------------------------------|---|
| SAN18-1 | 2.5 | 1224 | 10.86 | 3.022 | 1.064 ± 0.104 | 202 | 0.575 ± 0.011 | 0 | 1.697 ± 0.327 |
| SAN18-2 | 12.5 | 1181 | 7.70 | 3.048 | 0.575 ± 0.073 | 135 | 0.569 ± 0.011 | 0 | 1.899 ± 0.409 |
| SAN18-3 | 17.5 | 1910 | 3.13 | 3.021 | 0.217 ± 0.060 | 59 | 1.313 ± 0.026 | 2.204 | 0.614 ± 0.261 |
| SAN18-4 | 60 | 2084 | 3.82 | 3.077 | 0.283 ± 0.058 | 109 | 1.066 ± 0.021 | 1.813 | 1.063 ± 0.341 |
| SAN18-5 | 85 | 2128 | 4.83 | 3.043 | 0.414 ± 0.065 | 131 | 0.837 ± 0.017 | 1.255 | 1.010 ± 0.289 |
| SAN18-6 | 32.5 | 1737 | 1.22 | 3.058 | 0.097 ± 0.049 | 54 | 3.361 ± 0.067 | 3.265 | 0.165 ± 0.162 |
| SAN18-10 | 190 | 140 | 0.87 | 3.023 | 0.158 ± 0.065 | 45 | 4.756 ± 0.095 | 3.442 | 0.196 ± 0.224 |
| SAN18-11b | 240 | 1197 | 3.35 | 3.044 | 0.175 ± 0.055 | 61 | 1.660 ± 0.033 | 0 | 0.283 ± 0.203 |
| SAN18-12 | 290 | 151 | 13.74 | 3.042 | 1.252 ± 0.214 | 47 | 0.416 ± 0.008 | 0 | 1.679 ± 0.318 |
| SAN18-12b | 290 | 1421 | 9.61 | 3.051 | 0.912 ± 0.137 | 110 | 0.450 ± 0.009 | 0 | 1.611 ± 0.348 |
| SAN18-13 | 350 | 137 | 12.48 | 3.051 | 0.912 ± 0.137 | 80 | 0.450 ± 0.009 | 0 | 1.611 ± 0.348 |
| SAN18-14 | 400 | 194 | 19.99 | 3.057 | 1.887 ± 0.173 | 170 | 0.385 ± 0.008 | 0 | 2.517 ± 0.373 |
| SAN18-15 | 450 | 181 | 20.00 | 3.066 | 1.811 ± 0.170 | 148 | 0.369 ± 0.007 | 0 | 1.849 ± 0.419 |
| SAN18-16 | 475 | 292 | 6.29 | 3.050 | 0.539 ± 0.103 | 80 | 0.644 ± 0.013 | 1.111 | 2.015 ± 0.634 |
| SAN18-17 | 500 | 181 | 15.90 | 3.016 | 1.414 ± 0.152 | 123 | 0.281 ± 0.006 | 0 | 2.313 ± 0.404 |
| SAN18-18 | 545 | 140 | 9.02 | 3.026 | 0.714 ± 0.090 | 123 | 0.448 ± 0.009 | 0.842 | 1.991 ± 0.515 |

Table 3 Complementary analytical data. Uncertainties ($\pm 1\sigma$) include only analytical uncertainties. To each sample, $\sim 150 \mu\text{l}$ of the LN2C in-house phenakite 3 10^{-3} g.g^{-1} ^9Be carrier solution was added. ^{27}Al natural concentrations were measured by ICP-OES, and 8 of them were supplemented with a variable amount of an aluminum (Chemlab 983.28 g.g^{-1}) carrier solution sufficient to perform measurements. The concentration measurements were corrected for the chemical blank ratios for the first batch of (Samples SAN18-8 to 18) $1.93 \pm 0.34 \text{ } 10^{-15}$ and $1.93 \pm 1.3 \text{ } 10^{-15}$ for $^{10}\text{Be}/^{9}\text{Be}$ and $^{26}\text{Al}/^{27}\text{Al}$ ratios, respectively; and for the second batch (Samples SAN18-1 to 6 and SAN18-11b and SAN18-12b) $1.58 \pm 0.35 \text{ } 10^{-15}$ and $1.06 \pm 1.05 \text{ } 10^{-15}$ for $^{10}\text{Be}/^{9}\text{Be}$ and $^{26}\text{Al}/^{27}\text{Al}$ ratios, respectively.

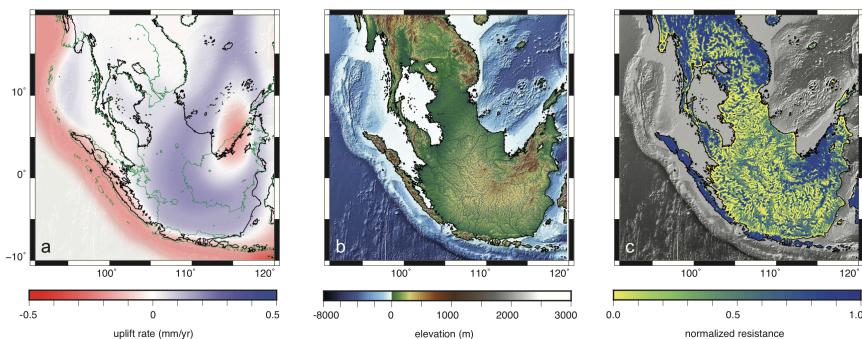
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Fig. 1 Vertical land motion, physiography, and cost surfaces at 1.8 Ma. **a.** Uplift rates, inferred from geomorphological indicators, stratigraphic, and seismic data (adapted from [10, 11]). Green curves delineate present-day shorelines **b.** Reconstructed physiography from landscape evolution model [12]. River width scales with reconstructed water fluxes. **c.** normalized cost map based on distance to rivers and coastlines, river discharge, and topographic slopes, which quantifies the local resistance of the landscape to species displacement (cost values increase with resistance). All maps were made using GMT 5 (www.generic-mapping-tools.org) [13].

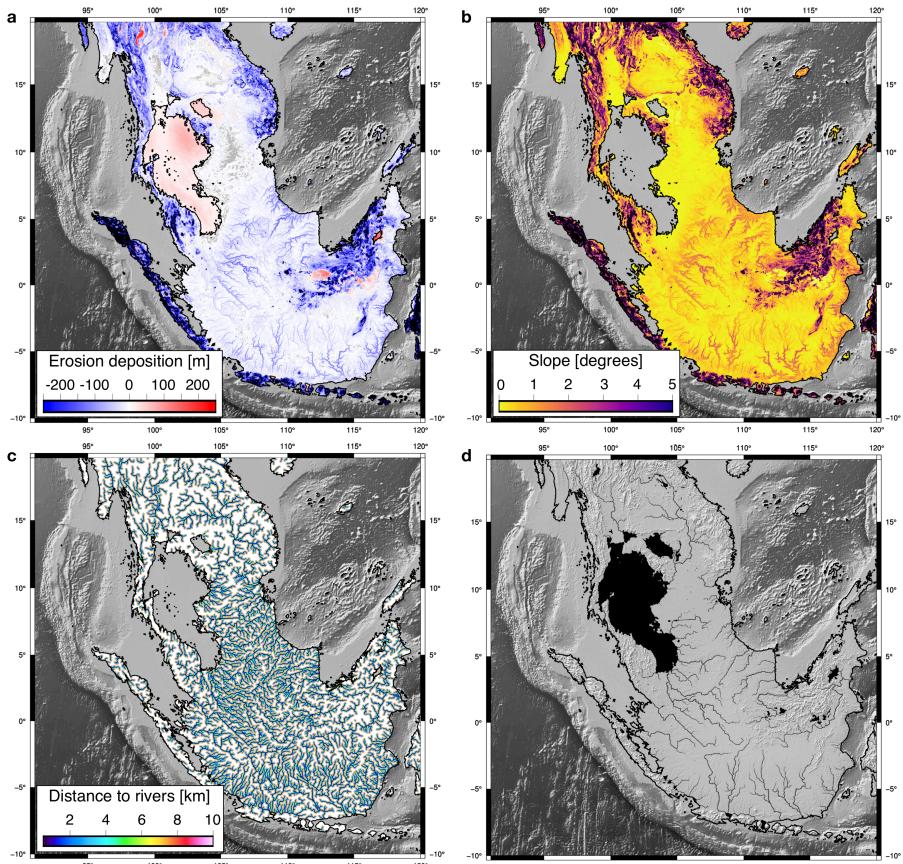


Fig. 2 Physiographic variables used to evaluate resistance to movement. **a.** Simulated cumulative erosion deposition after 10 kyr of landscape evolution induced by riverine and hillslope processes. **b.** Mean slopes for the continental region computed over the 1 km grid. **c.** Extracted distance to rivers (based on the distribution presented in Fig. 1b) used to estimate riparian areas. **d.** Position of the largest rivers defined with a flow rate above $5.5 \times 10^3 \text{ m}^3/\text{s}$ and used to impede movement across the region. All maps were using GMT 5 (www.generic-mapping-tools.org) [13].

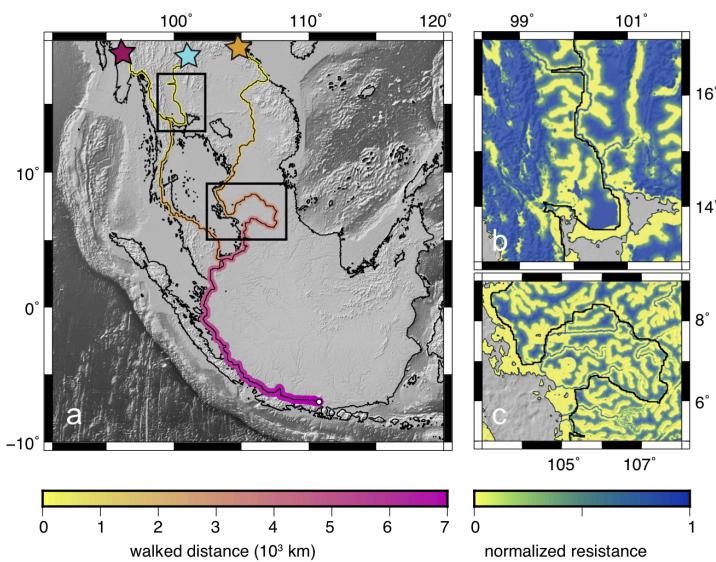
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Fig. 3 Least-cost path routes to Sangiran. a. Computed shortest walked distance assuming 3 different north entry points (Myanmar, Thailand, Vietnam). b., c. Zoomed-in subregions, where the role of the cost surface on calculated paths is highlighted. Black lines correspond to the least-cost paths for the central and eastern routes respectively. All maps were using GMT 5 (www.generic-mapping-tools.org) [13].

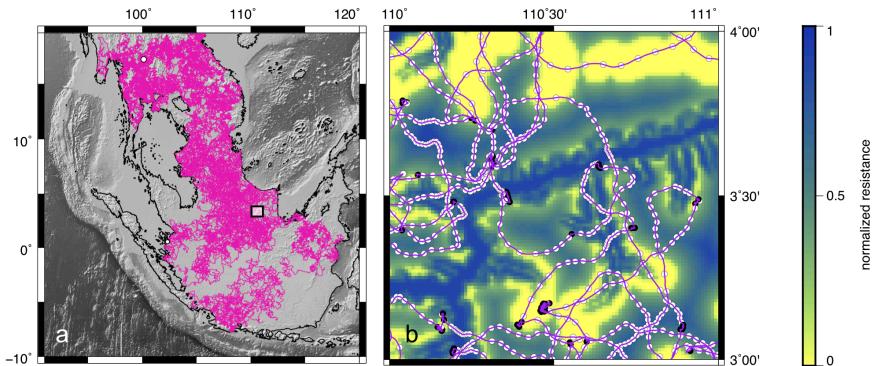


Fig. 4 Markovian walk of *H. erectus* across Sundaland, from the mechanistic spatially-explicit simulation SiMRiv [14]. a. Sample realization (central northern entry point) for 5 millions steps. b. 1° box (white shaded area in a) showing positions every 25 steps and illustrating *H. erectus* dynamics with two-state movements (random walk in purple, and correlated random walk in white) and dependency on landscape heterogeneity. All maps were using GMT 5 (www.generic-mapping-tools.org) [13].

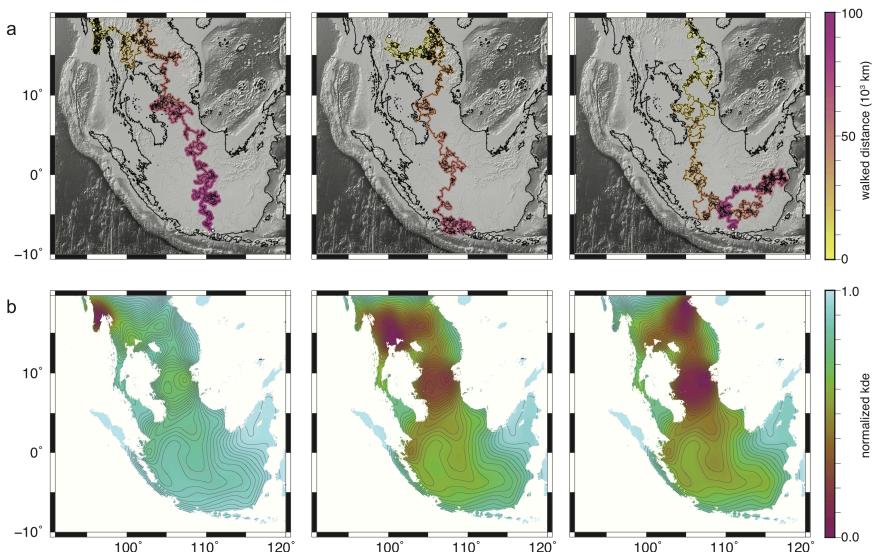


Fig. 5 Successful Markovian walks to Sangiran. **a.** Shortest walked distance (least cost path) realizations for each set of 1000 realizations (for the 3 entry points). **b.** Normalized kernel density estimates (kde) from predicted positions obtained from the mechanistic model and inversely weighted based on the normalized cost surface (Fig. 1c). All maps were using GMT 5 (www.generic-mapping-tools.org) [13].

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