

1 **Electronic supplementary information**

2 **Multiplexed fluidic circuit board for controlled perfusion of 3D**

3 **blood vessels-on-a-chip**

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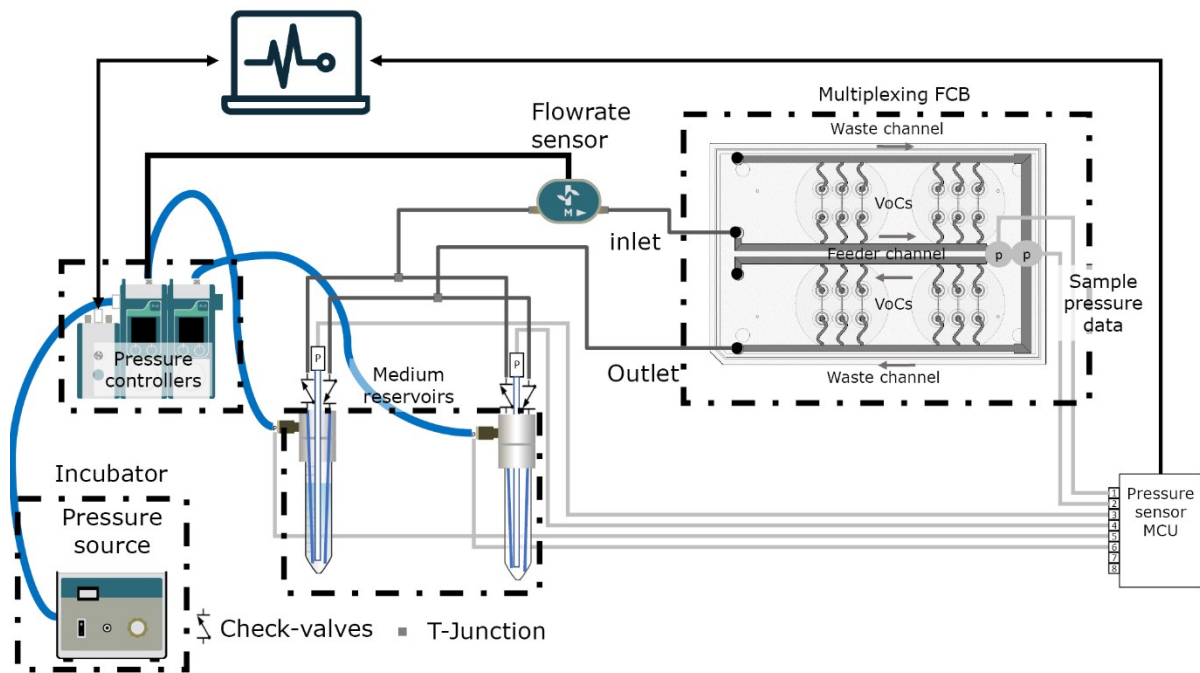
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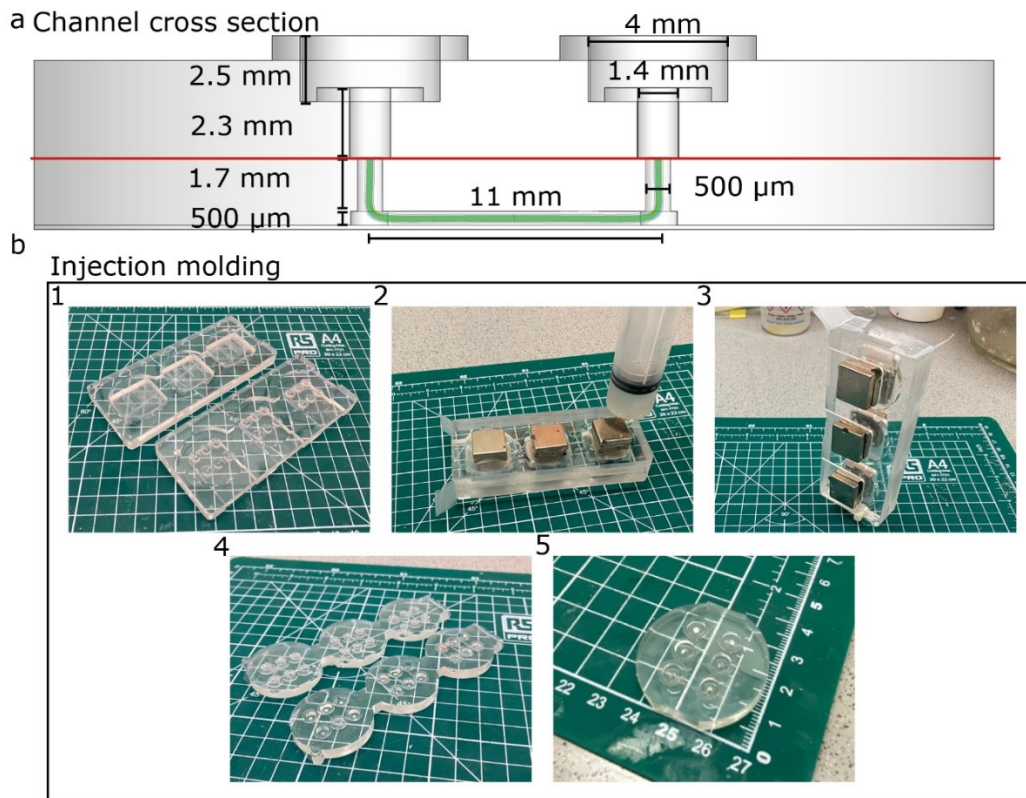
21 **Supplementary Figures**



22

23 **Fig. s1** Fluidic circuit used for long-term perfusion. It requires the
24 addition of two T or Y-connectors and results in a unidirectional flow.

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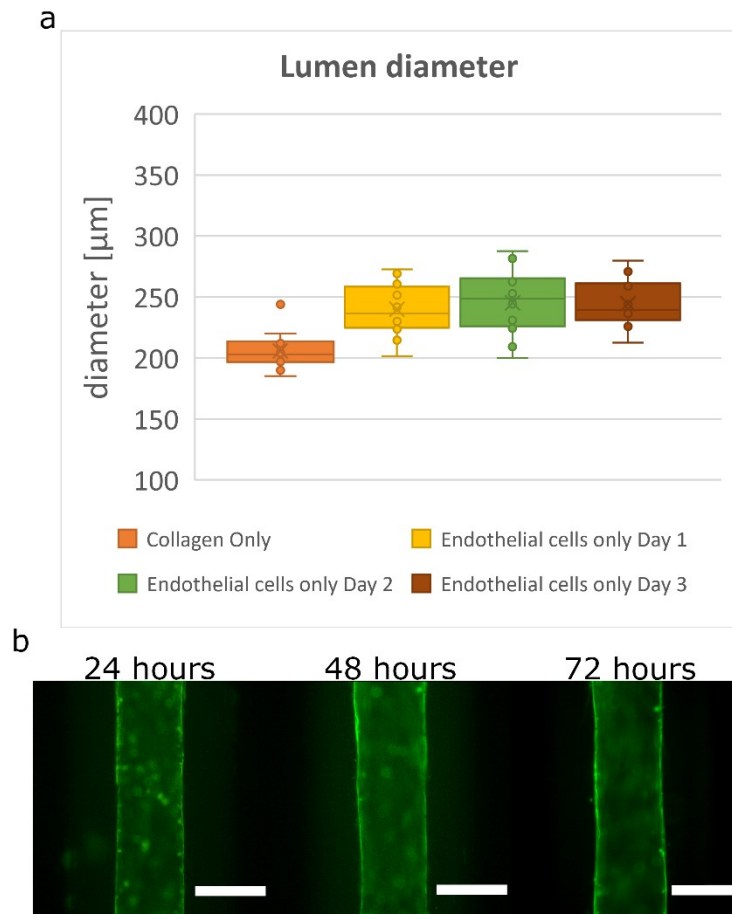
27 **Fig. s2 Chip design and Microfabrication using injection moulding.**

28 (a) Chip design and channel dimensions, green represents the modelled
29 lumen, the red line indicates where the two mould halves have contact.

30 (b) Injection moulding. Two separate mould halves show the fluidic
31 channels and medium reservoirs (1). Injection moulds are assembled
32 using strong magnets and PDMS is injected using a syringe (2). The
33 injection mould is placed vertically and allowed to set at room
34 temperature for at least 16 hours (3) followed by 1 hour at 75 °C.

35 Magnets are removed and the PDMS is peeled of (4) excess PDMS is cut
36 off (5) and the chip is assembled with air plasma treatment. (c) Defects

37 at the contact points of the injection-moulds result in small membranes of
38 various sizes.

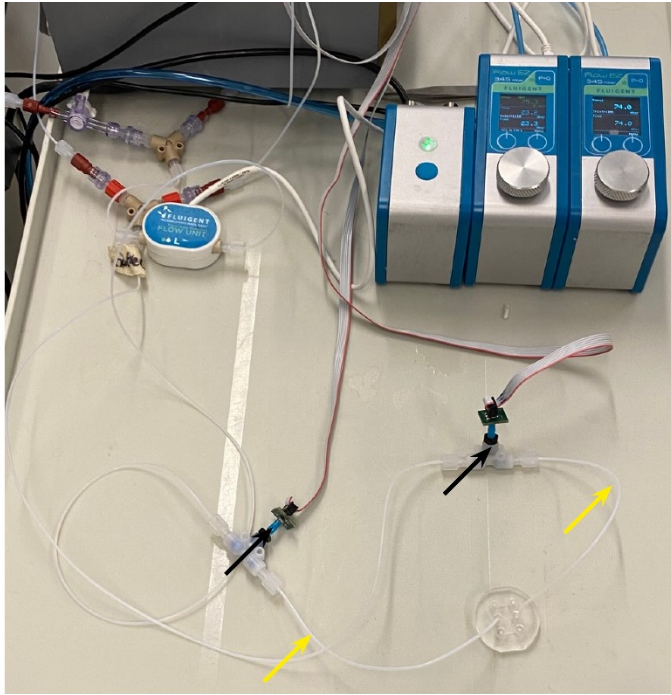


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40 **Fig. s3** (a)Boxplot of VFP luminal diameter. Typical luminal diameter
41 ranges of the 3D-VoC in a single experiment shows a diameter expansion
42 after cell seeding. The seeded lumens remain constant in diameter for at
43 least 3 days.(b) representative images of lumen at day 1, day 2 and day
44 3. Scalebar 200 μm

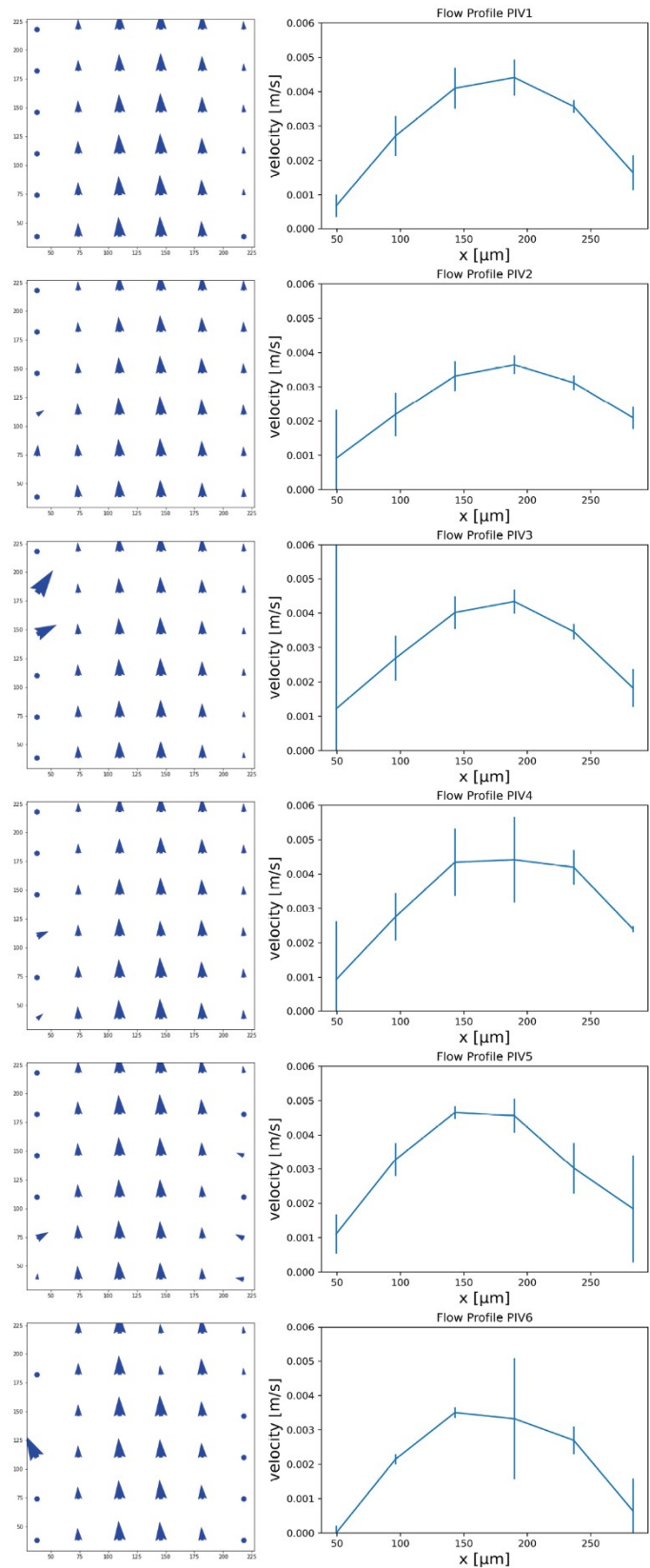
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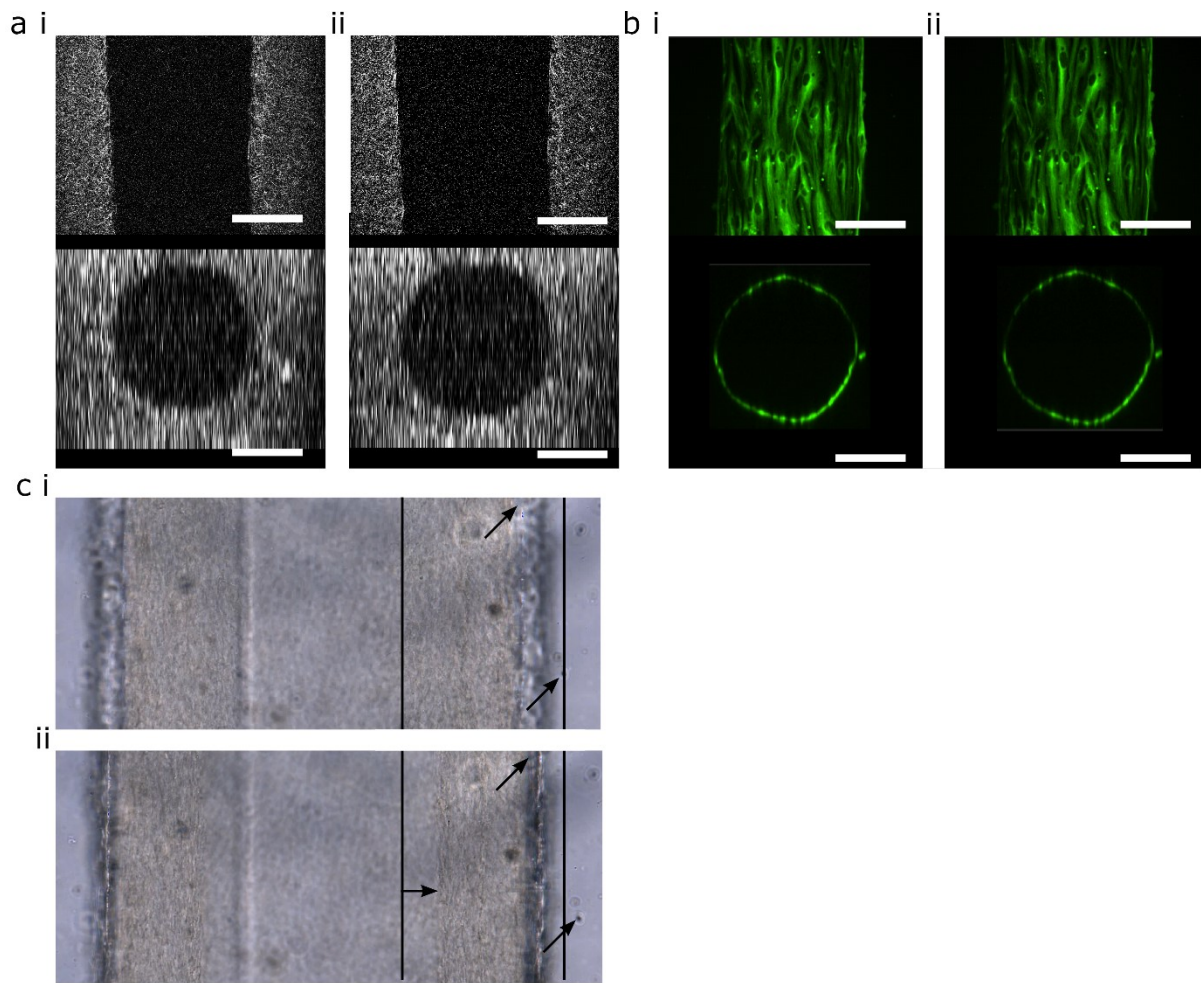
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48 **Fig. s4** Set-up for measuring individual shear stress. A total of 52 cm of
49 tubing (yellow arrows) was used and placed between the pressure
50 sensors (black arrows) and the samples. The pressure difference was
51 controlled by custom software.



52 **Fig. s5** PIV Vector fields of all analysed samples.

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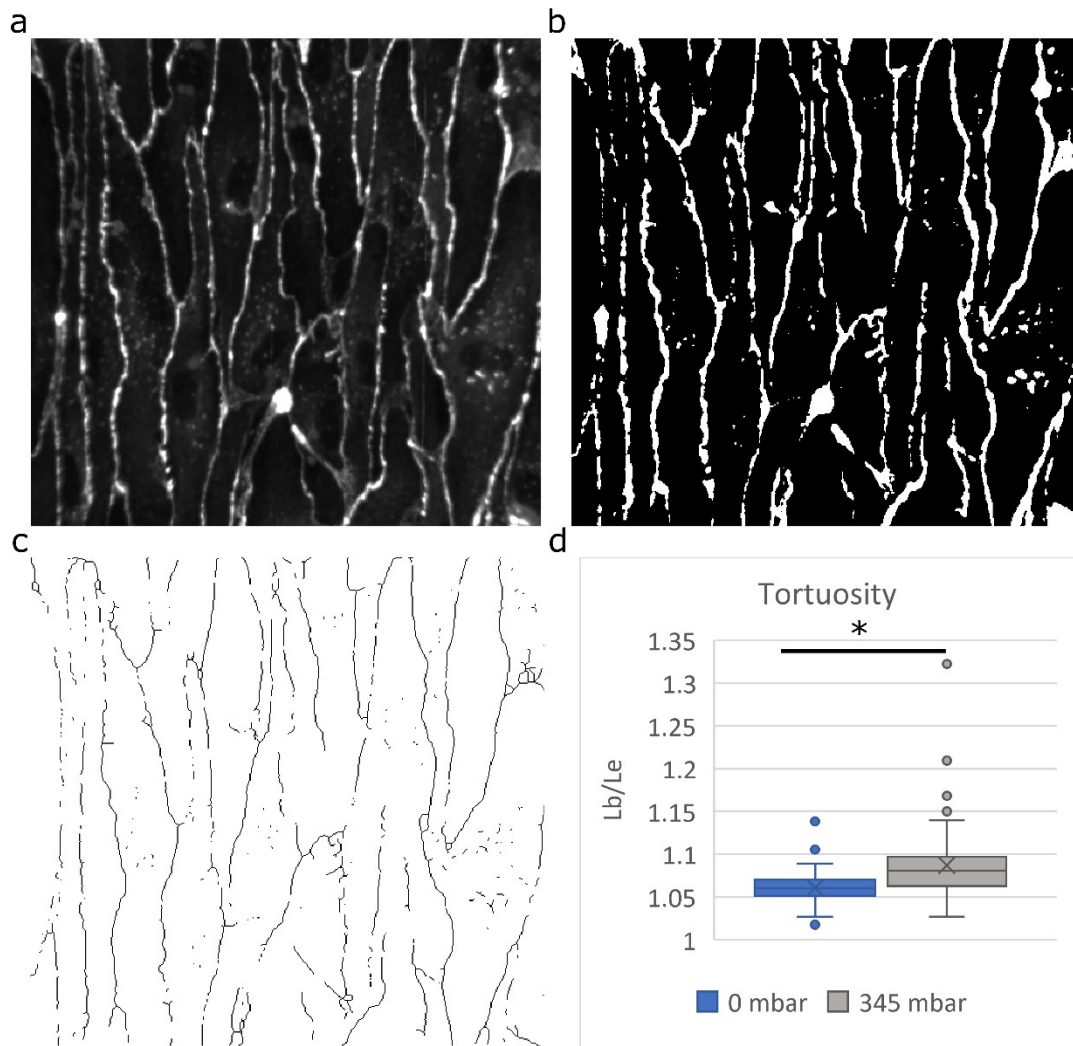
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55 **Fig. s6** Imaging vascular compliance in 3D. (a) 2p-SHG image of the
 56 middle frame and a cross section of the lumen at $P = 0$ mbar (i) and $P =$
 57 345 mbar (ii), see video 3 for the animated sequence. (b) Spinning disc
 58 confocal reconstruction bottom half of the lumen cross section of the
 59 lumen at $P = 0$ mbar (i) and $P = 345$ mbar (ii), see video 4 for the
 60 animated sequence. (c) Frames of video 2 to highlight deformation of the
 61 lumen and the PDMS showing $P = 0$ mbar (i) and $P = \pm 1000$ mbar (ii).
 62 Arrows and lines are visual references to aid comparison. Scale bars 100
 63 μm .

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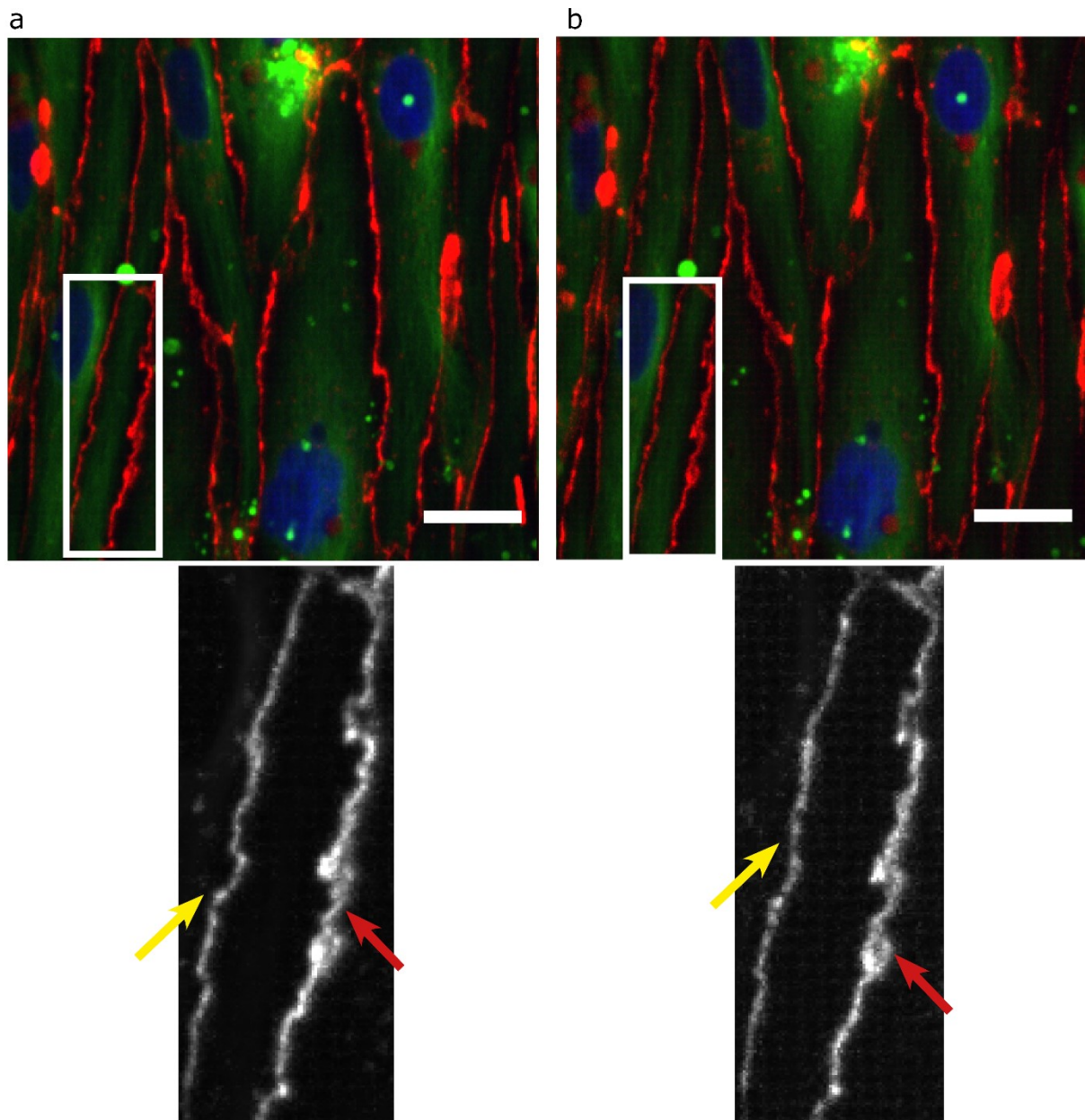
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68 **Fig. s7** Quantification of the tortuosity index of adherens junctions (a)
 69 Cell junctions visualized using VE-cadherin marker (b) Threshold image of
 70 VE-cadherin (c) Skeletonized image of VE-cadherin (d) tortuosity index is
 71 calculated by dividing the length of branch (Lb) by the Euclidean distance
 72 of that branch(Le). Quantification based on one sequence, one point is
 73 one cell junction* indicates P<0.001

74

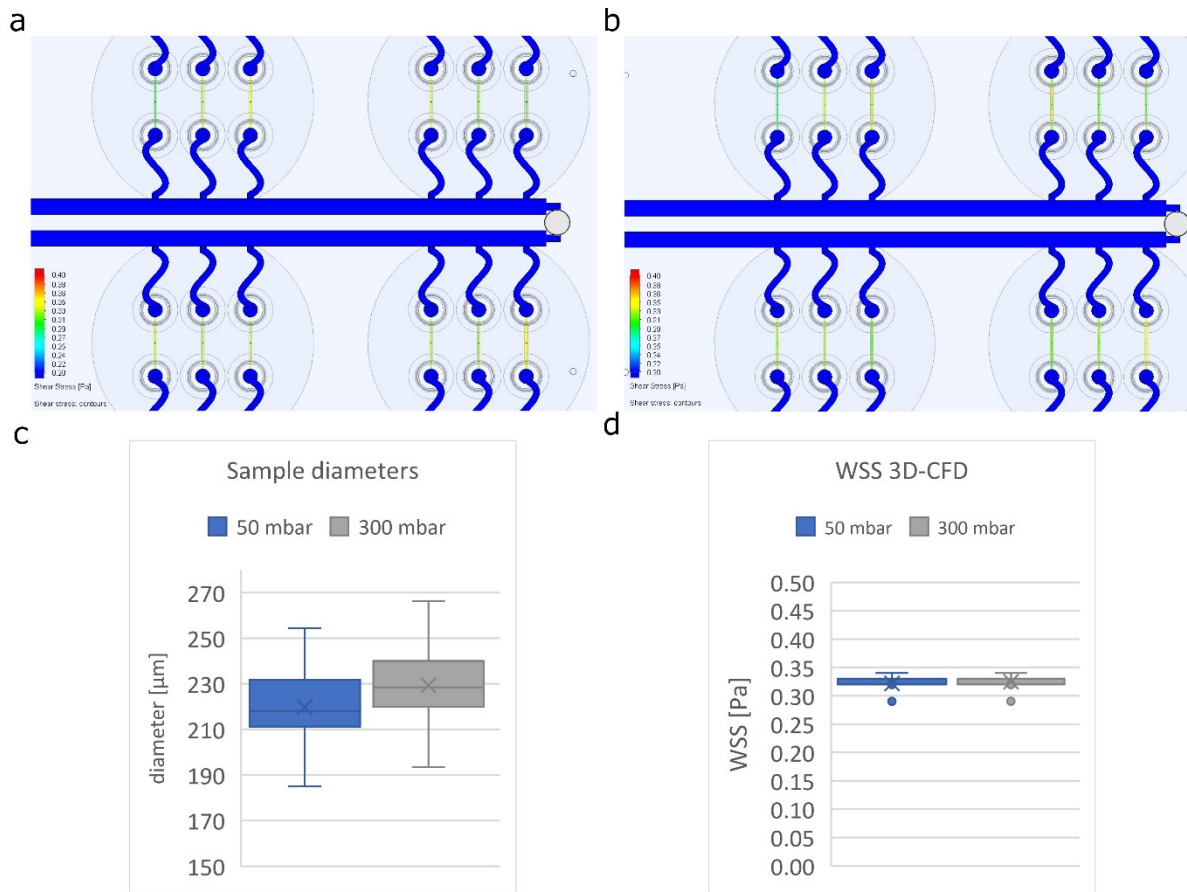
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78 **Fig. s8** Confocal reconstruction of live TUBA1B-eGFP-ECs (green) co-
 79 stained for adherens junctional marker (VE-cadherin, in red) and nuclei
 80 (Hoechst, in blue) at high pressure (345 mbar) (a) and at low pressure
 81 (0 mbar) (b). Inserts give example of morphological changes in VE-
 82 cadherin cell junctions at high and low pressure. Borders go back to a
 83 straight line (yellow arrows) dislocated junctions remain jagged (red
 84 arrows). Scale bar 20 μ m.



85

86 **Fig. s9** CFD model of perfusion experiment (a) with an internal pressure
 87 of 50 mbar of internal pressure (b) with 300 mbar of internal pressure (c)
 88 Boxplot of all sample diameters at specified internal pressure (d) Boxplot
 89 of resulting WSS at specified internal pressure.

90 **Supplementary Videos**

91 **Video 1** Animation of 3D-CFD model showing the velocity stream lines.

92 **Video 2** Brightfield scaffold only. Pressure was manually applied using a
93 syringe up to 1 bar.

94 **Video 3** 2p-SHG sequence of scaffold only of pressure ramp. Frame 1, P
95 = 0 mbar; frame 2, P = 345 mbar.

96 **Video 4** 3D-Confocal sequence of the TUB1a-mGFP-hiPSC-ECs pressure
97 ramp. Frame 1, P = 0 mbar; frame 2, P = 345 mbar.

98 **Video 5** Brightfield pressure ramp of the TUB1a-mGFP-hiPSC-ECs
99 monolayer. P = 0-345 mbar, 25 mbar pressure increment per frame, last
100 frame returns to P = 0 mbar.

101 **Video 6** Widefield fluorescent signal of the TUB1a-mGFP-hiPSC-ECs
102 monolayer analysed using the VasoTracker software (blue lines).

103 **Video 7** Confocal reconstruction of pressure ramp. P = 0-50-75-100
104 mbar. Green: TUB1a-mGFP-hiPSC-ECs, red: VE-Cadherin, blue: Hoechst.
105 Histograms of the red channel were equalized per frame for the
106 reconstruction. Note: last frame shows that the VE-cadherin signal is
107 completely lost due to photobleaching of the fluorophore.

108 **Video 8** Confocal reconstruction of pressure ramp. Frame 1, P = 0 mbar;
109 frame 2, P = 150 mbar; frame 3, P = 345 mbar, frame 4, P = 325 mbar
110 with 1 Pa of WSS. Green: TUB1a-mGFP-hiPSC-ECs, red: VE-Cadherin,
111 blue: Hoechst.

112 **Deriving the equation of optimum resistance of the branch**
 113 **channels to minimize wall shear stress**

114 Hagen–Poiseuille’s law for pressure driven flow:

$$\Delta P = R_h Q$$

115 Eq. s1

116 Pressure difference for a serial connected resistance:

$$\Delta P = Q (R_h^{vessel} + R_h^{\tau EQ})$$

118 Eq. s2

119 WSS for circular lumen with given diameter and flowrate

$$\tau = \frac{32 \mu Q}{\pi d^3}$$

120 Eq. s3

121 Rewrite to flowrate for given diameter and WSS

$$Q = \frac{\tau \pi d^3}{32 \mu}$$

122 Eq. s4

123 Combine Eq. s4 in Eq. s2 with R_h for a circular 3D-VoC assuming uniform
 124 diameter of the sample, negligible interstitial flow

$$\Delta P = \left(\frac{\tau \pi d^3}{32 \mu} \right) \left(128 \mu \frac{l_{vessel}}{\pi d^4} + R_h^{\tau EQ} \right)$$

125 Eq. s5

126 Set WSS d_{min} equal to WSS d_{max} given equal dP (Eq. s6)

$$\left(\frac{\tau \pi d_{min}^3}{32 \mu} \right) \left(128 \mu \frac{l_{min}}{\pi d_{min}^4} + R_h^{\tau EQ} \right) = \left(\frac{\tau \pi d_{max}^3}{32 \mu} \right) \left(128 \mu \frac{l_{max}}{\pi d_{max}^4} + R_h^{\tau EQ} \right)$$

127

128 Eq. s6 can be reduced to Eq. s7

$$\frac{4 l_{min}}{d_{min}} + \left(\frac{\pi d_{min}^3}{32 \mu} \right) R_h^{\tau EQ} = \frac{4 l_{max}}{d_{max}} + \left(\frac{\pi d_{max}^3}{32 \mu} \right) R_h^{\tau EQ}$$

129

130 Optimal τEQ resistance can then be expressed in terms of sample
 131 diameters

$$R_h^{\tau EQ} = \frac{128 \mu \left(\frac{l_{min}}{d_{min}} - \frac{l_{max}}{d_{max}} \right)}{\dots}$$

132 Eq. s8

133 τ EQ resistor dimensions of a rectangular channel:

$$134 \quad \frac{l_{resistor}}{h} = \frac{32 \left(\frac{l_{min}}{d_{min}} - \frac{l_{max}}{d_{max}} \right)}{3\pi(d_{min}^3 - d_{max}^3)} \quad \text{Eq.s9}$$

135 τ EQ resistor dimensions of a circular tube:

$$136 \quad \frac{l_{res}}{d} = \frac{\left(\frac{l_{min}}{d_{min}} - \frac{l_{max}}{d_{max}} \right)}{3\pi(d_{min}^3 - d_{max}^3)} \quad \text{Eq.s10}$$

137 **Deriving equation: Required ΔP for given WSS**

138 Serie circuit of sample and τ EQ resistor combined with Eq. s4

$$139 \quad \Delta P = \left(\frac{\tau \pi d^3}{32\mu} \right) \left(128 \mu \frac{L_{vessel}}{\pi d^4} + 12\mu \frac{L}{8wh^3(1-0.63\frac{h}{w})} \right) \quad \text{Eq. s5}$$

$$140 \quad \Delta P = \left(\frac{\tau 4L_{vessel}}{d} + \frac{\tau 12 \pi d^3 L}{8wh^3(1-0.63\frac{h}{w})} \right)$$

$$141 \quad \Delta P = \tau \left(4 \frac{L_v}{d} + \frac{3 \pi d^3 L_{res}}{8wh^3(1-0.63\frac{h}{w})} \right) \quad \text{Eq. 1}$$

142

143 **Equations wall shear stress used for Fig. 2c**

144 **Fixed Q red plot:**

$$145 \quad \tau = \frac{32 \mu Q}{\pi d^3} \quad \text{Eq.s3}$$

146 τ : WSS

147 Q: flowrate = 90 $\frac{\mu l}{min}$

148 μ : viscosity= 0.79 Pa s

149 d: diameter range= 180-300 μm

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153 **Fixed P (green plot):**

$$\tau = \frac{\Delta P d}{4 l_{vessel}}$$

154

Eq. s11

155 ΔP : Fixed pressure difference= 237 [Pa]

156 d: Diameter range= 180-300 μm

157 l:length =1.43 cm

158 **τ EQ + Fixed ΔP blue plot:**

$$\tau = \frac{\Delta P}{\left(4 \frac{l_{vessel}}{d} + \frac{3\pi d^3 L_{res}}{8wh^3(1 - 0.63 \frac{h}{w})}\right)}$$

159

Eq. s12

160 Fixed ΔP : 333 [Pa]

161 d:diameter range= 180-300 μm

162 l=1.43 cm

163 L_{res}, w, h = dimensions of resistor listed in table s1 [m]

164 **Table s1 channel dimensions FCB**

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				Viscosity [Pa s]	7.90E-04
FCB dimensions	Length [m]	Width [m]	Height [m]	R_h [Pa s m ⁻³]	
Feeder channel	0.2	0.0025	0.002	1.90E+08	
Feeder loop	0.01	0.0012	0.002	4.40E+07	
			Total	2.34E+08	
Waste channel	0.2	0.0025	0.002	1.90E+08	
Waste loop	0.082	0.0035	0.002	4.33E+07	
			Total	2.34E+08	
τ EQ-Resistors	0.0171	0.001	0.0002	2.32E+10	
3D-VoC	length [m]	d [μm]	R_h including chip resistance		
Small	0.0143	180	4.38E+11		
Medium	0.0143	240	1.39E+11		
Large	0.0143	300	5.68E+10		

176 **Table s2 Dimensions lumen expansion**

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	Scaffold-only		EC-monolayer	
	p0	p345	p0	p345
Pressure [mbar]				
Lumen width [μm]	200	220	196	206
Lumen height [μm]	195	215	197	208
Ratio (w/h)	1.03	1.02	0.99	0.99